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R.Doerner, 1st Steel CRP, IAEA, December, 2015

# The PISCES-B facility at UCSD





# Motivation:



- Explore the possibility to use bare RAFM steel as plasma facing material on the main vessel wall of DEMO
- The limiting factor is the erosion life time of bare steel. Rough erosion estimate (ITER) yields ~5 cm/year at the first wall. Needs reduction by factor 10
- Nuclear steels contain typically 0.5-1 at% W (EUROFER, RUSFER, F82H(Japan))
- Investigate the influence of W on the erosion yield of RAFM steel at energies close to the threshold energy for W sputtering
- Study low energy, high fluence erosion of RAFM steel in PISCES
- Study fundamental aspects of preferential sputtering in the simple Fe-W system on deposited layers on C
- Modelling of tungsten enrichment in EUROFER due to plasma erosion

### Sputtering Yield of Fe and W in the threshold regime



#### D threshold energies: Fe ~45 eV

W~200 eV

The large difference in erosion yield close to the threshold energies may lead to strong modifications of the composition for Fe-W alloys:

- Enrichment of W
- Reduction of erosion yield



	С	Cr	W	Mn	V	Та	N <sub>2</sub>	Р	S	0 <sub>2</sub>
Eurofer 97	0.09- 0.12	8.5- 9.5	1.0- 1.2	0.2- 0.6	0.15- 0.25	0.10- 0.14	0.015- 0.045	0.004- 0.005	0.003- 0.004	0.0013- 0.0018
F82H (Japan)	0.09	7.7	1.94	0.16	0.16	0.02	0.006	0.002	0.002	0.01

#### Composition of RAFM steels (in wt.%) (Fe is base material)

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#### Erosion of the Fe/W layers determined by RBS



Fluence dependence of Fe erosion for different initial W concentrations:

- Already at the lowest fluences, Fe/W layers show lower erosion than pure Fe (8e-3).
  (J. Roth et al. Report IPP 9/26 (1979))
- Strong yield reduction with increasing fluence, more than one order of magnitude
- Fluence dependence of W erosion for different initial W concentrations:
- W erosion about two orders of magnitude smaller than Fe. However, some erosion even at energies below 200V.





• Experimental data from PISCES-A follow the trend indicated by TRIDYN

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- Experimental values represent an average over the total fluence. For comparison with TRIDYN the values need to be recalculated into yield values for each fluence interval.
- "Corrected" values show steady state erosion with a yield 5x10<sup>-4</sup>.



Preliminary data presented at Steel TM was in error. EUROFER samples were not outgassed prior to exposure in PISCES-A.

**Dependence on Temperature:** 

- At 225°C the erosion yield increases to values for pure Fe
- At 500°C measurable sputtering even for 100V
- More data needed to determine transition temperature



**Temperature Dependent Erosion Yield of EUROFER in PISCES-A** 



- Exposure of EUROFER to low-energy (140 eV/D<sup>+</sup>) / high-flux (~10<sup>21</sup> D<sup>+</sup>/m<sup>2</sup>s) plasma at various temperatures (370 - 870 K).
- Sputtering yield varies within a limited range at < ~800 K, while it clearly increases at 870 K.
- No clear temperature dependence of sputtering in the DEMO FW working temperature range (< 800 K)</p>
  - to be carefully compared with low-flux irradiation data (exposure duration may influence the elemental diffusion and the sputtering behaviour).



Sputtering yield of EUROFER steel by 140 eV/D<sup>+</sup> exposure as a function of exposure temperature





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- Exposure of EUROFER to low-energy (100 eV/He<sup>+</sup>) / high-flux (~10<sup>21</sup> He<sup>+</sup>/m<sup>2</sup>s) plasma at various temperatures (370 -870 K).
- □ Lower sputtering yield at < ~ 600 K, while it already increases > 700 K. (Y<sub>He→Fe</sub> (100eV/He) ~ 4.6 x 10<sup>-2</sup>)



Sputtering yield of EUROFER steel by 100 eV/He<sup>+</sup> exposure as a function of exposure temperature

#### 100 eV/He+, (0.4-1.2)E25 He+/m<sup>2</sup>

#### Surface Morphology: PISCES-A He Exposure







Exposed surface turns black after He plasma exposure (under all exposure conditions).



#### EUROFER:

- Sputtering yield of EUROFER is strongly reduced compared to pure iron. The reason for this reduction is thought to be W enrichment at the surface.
- The reduction continues up to ~ 550C. The reason for this transition is thought to be due to Fe diffusion through the layer of W enrichment, but could also be due to surface morphology.
- Strong surface morphology changes are observed with temperature and plasma species.



- Identify readily available material for study
  - Recall in the early days of W investigations, the variety of materials and fabrication techniques made systematic investigations difficult
- Determine temperature threshold for yield reduction/surface enrichment
  - Useful temperature for energy conversion will be relatively high
  - Possible flux dependence
- Expose EUROFER (or similar steel) to mixed D/He plasma
  - Connect to, or take advantage of, work on structural materials and He bubble nucleation
  - Examine the role of He in altering surface morphology
- Influence of other trace materials in steels (i.e. Cr)
- Changing surface morphology will be an issue and how do we deal with that in a database
  - Will morphology be different in a confinement device?





Sputtering yield of EUROFER steel by D ion irradiation with different D energies as a function of D fluence (320 K)

From W. Jacob et al, ICFRM 2015 presentation.

- Fe sputtering can result in W surface enrichment
- Temperature limit for Fe diffusion to surface
- Role of Cr is uncertain
- PISCES-B will provide basic S/XB data for Fe and Cr
- Examine fluence dependence of F82H surface sputtering at various sample temperatures
- Expose samples to mixed D/He plasma

- Pure Fe and Pure Cr samples have been prepared
- F82H samples have been obtained from Japan
- Fe I, Cr I and W I emission lines identified (ADAS calculations exist for Cr I and W I)
- S/XB (ionizations per photon) for both Cr and Fe samples will be measured for a variety of plasma conditions
- Data will be compared to ADAS calculations for Cr (no ADAS calculations for Fe available)







- Fluence dependence of erosion from F82H has been measured at 300°C
- Both Fe and Cr sputtering is reduced in He plasma until a fluence of ~ 3x10<sup>24</sup> m<sup>-2</sup> is reached then erosion is constant
- S/XB will quantify sputtering rate from measured intensity
- Post-exposure surface analysis (AES) will quantify change in surface composition
- Try to separate surface composition from morphology effects on erosion





- Year 1:
  - Under controlled plasma conditions, measure the S/XB for Fe I, vary ne & Te
  - Under controlled plasma conditions, measure the S/XB for Cr I, vary ne & Te
  - Investigate the temperature dependence of W surface segregation

#### • Year 2:

- Investigate the surface loss rates of each of the components of steel in real time using visible spectroscopy (quantify these losses with the S/XB data mentioned above), vary ion energy

- Investigate the impact of mixed D/He plasma on steel and surface segregation, vary plasma composition, surface temperature

#### • Year 3:

- Use LIBS (under development in PISCES) to investigate real-time surface composition as a function of plasma fluence

- Investigate changes to the surface composition after exposure to transients heat pulses using existing laser systems and the aforementioned real-time diagnostic techniques