



TRILATERAL  
EUREGIO CLUSTER



# **Behavior of tungsten under thermal and plasma exposure and development of advanced tungsten materials**

M. Wirtz, M. Berger, L. Buzi, J. Coenen, A. Huber, A. Kreter, N. Lemahieu, B. Jaspers, J. Linke, A. Litnovsky, D. Matveev, G. Pintsuk, M. Rasinski, M. Reinhart, G. Sergienko, I. Steudel, T. Wegener, B. Unterberg

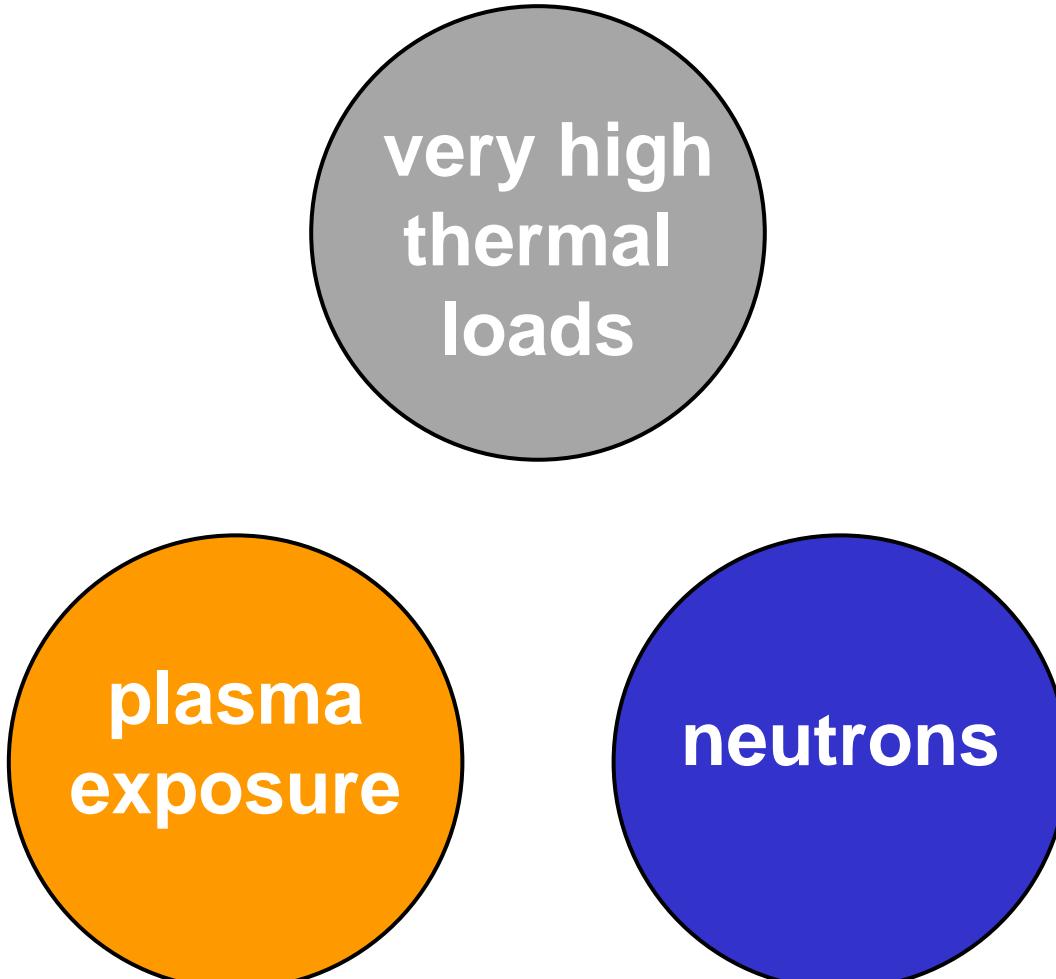
Forschungszentrum Jülich GmbH, Institute of Energy and Climate Research, 52425 Jülich, Germany

# Outline of FZJ contributions

- Thermal shock behavior of irradiated and un-irradiated W grades
- Change of W micro- structure under simultaneous heat and particle loads and impact on W erosion and fuel retention in W
- Development of advanced tungsten materials with improved micro-structure
- Characterization of commercially available tungsten grades

# A

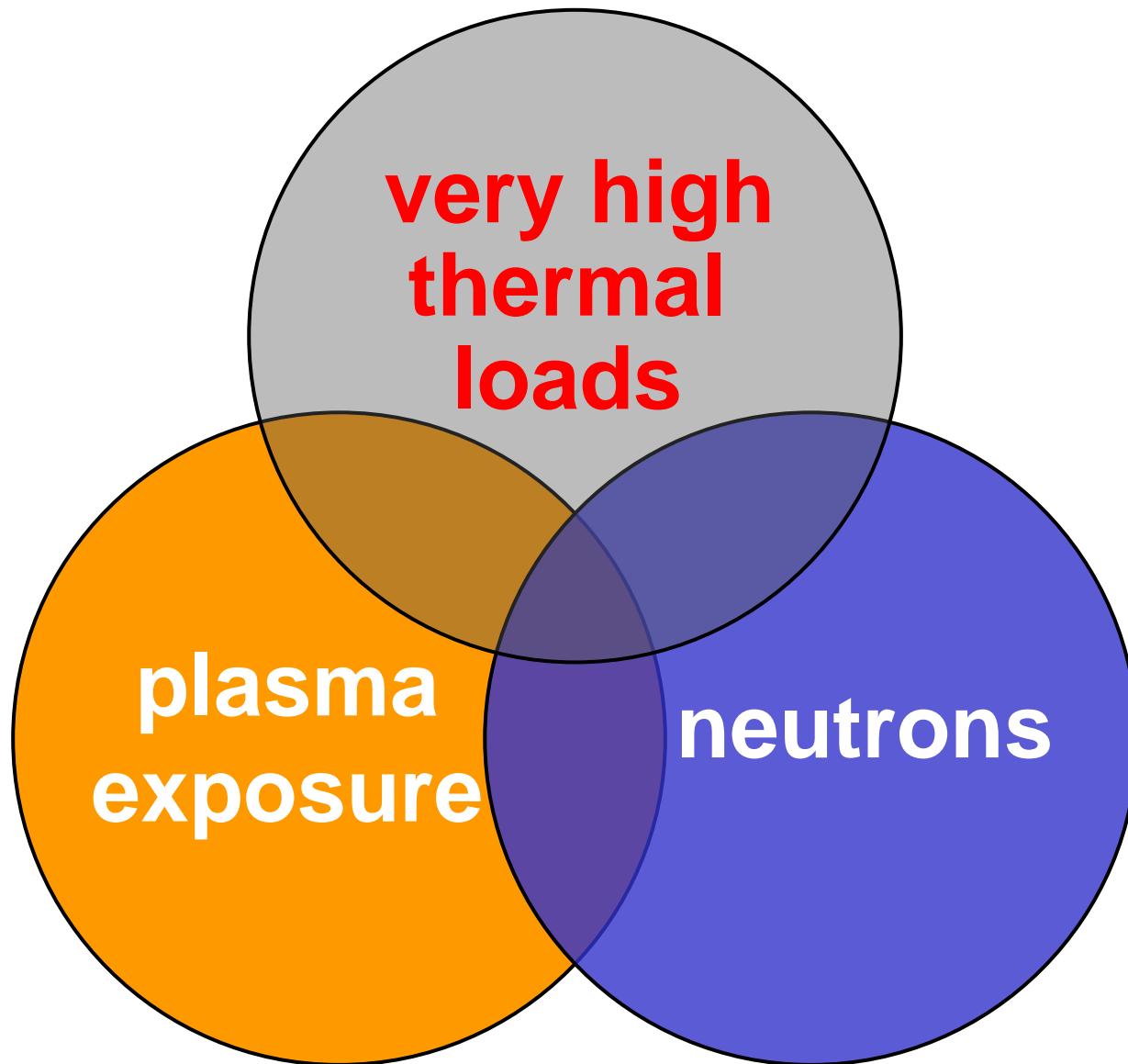
## Environmental conditions - test facilities



very high  
thermal  
loads

plasma  
exposure

neutrons



## Steady state heat loads:

up to  $20 \text{ MWm}^{-2}$  in ITER  
(lower loads in DEMO)

- recrystallization
- failure of joints

## Transient thermal loads:

up to  $60 \text{ MJm}^{-2}$   
(disrupt., ELMs, VDEs)

- crackings
- melting
- dust formation

**very high  
thermal  
loads**

**plasma  
exposure**

**neutrons**

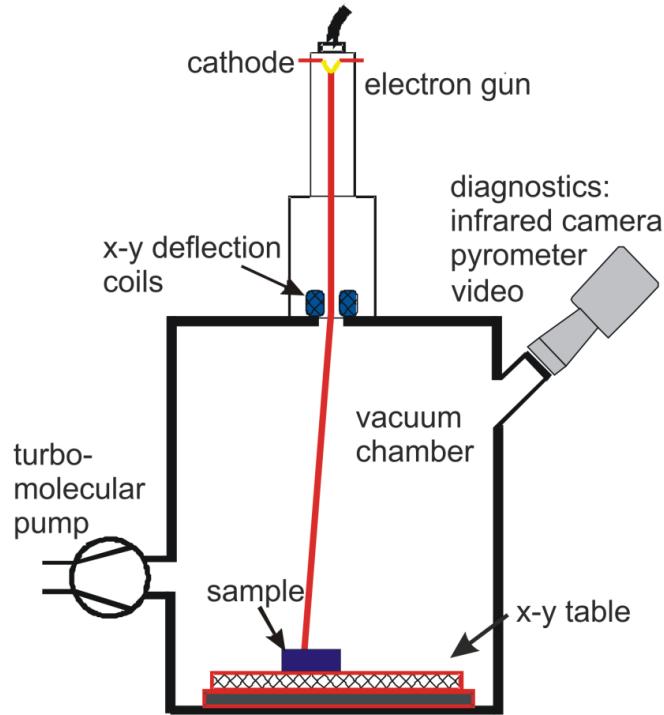
## Plasma loads:

- sputtering
- hydrogen
- helium

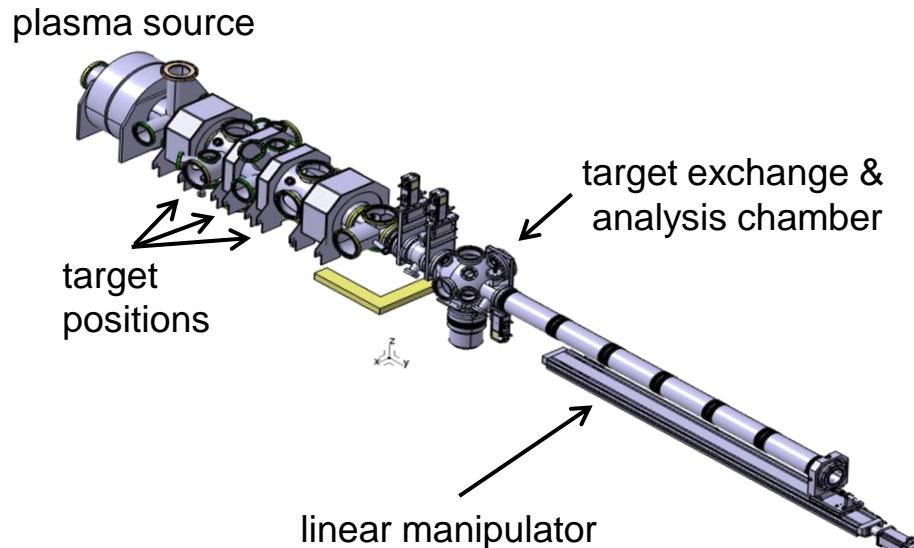
## Neutrons:

- up to 14 MeV
- defects
- transmutation

## Electron beam facility JUDITH 1



## Linear plasma device PSI-2



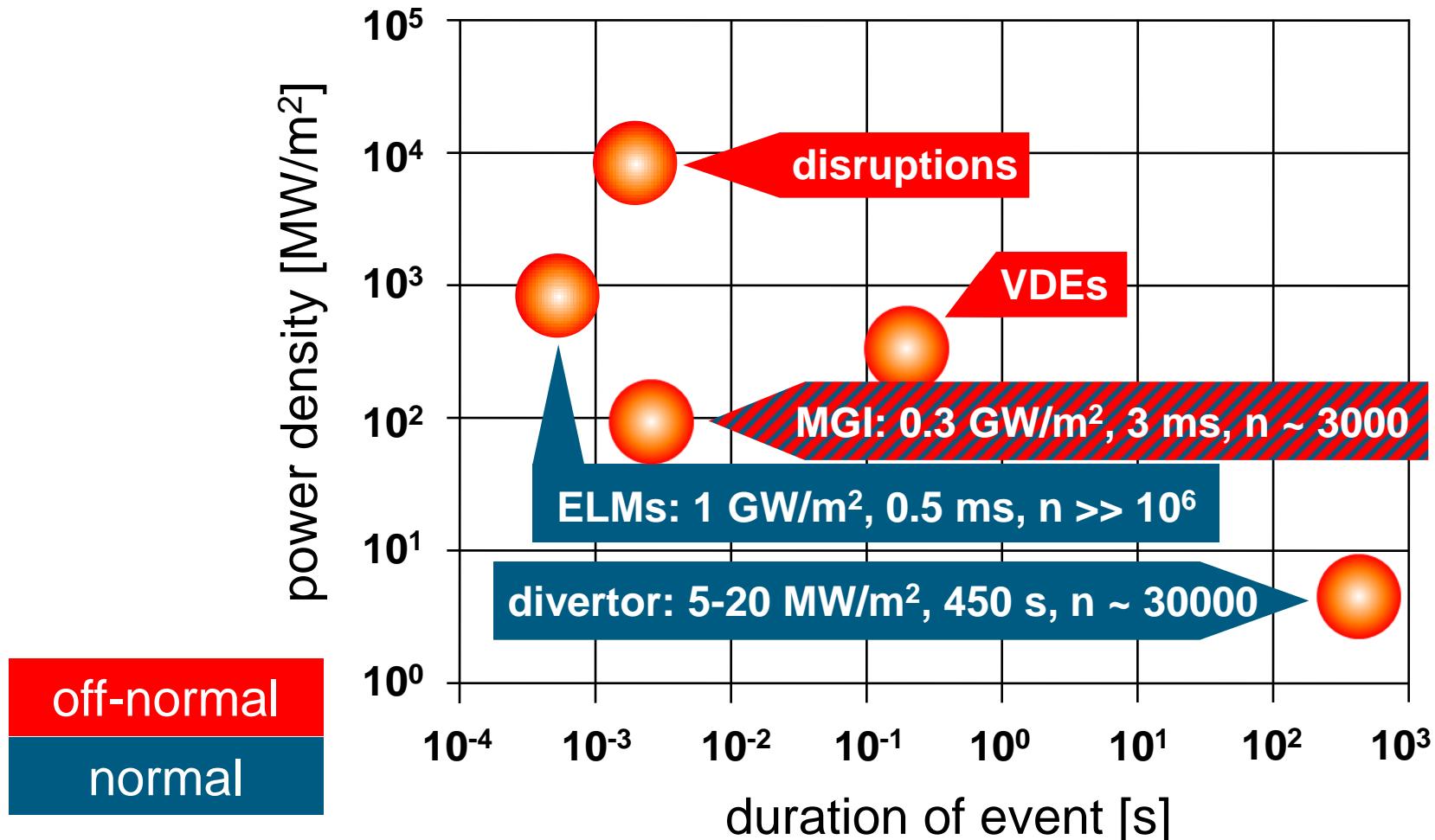
- max. power 60 kW
- acceleration voltage < 150 kV
- EB diameter ~1 mm (FWHM)

- plasma diameter 60 mm
- particle flux  $\leq 10^{23} \text{ m}^{-2}\text{s}^{-1}$
- incident ion energy (bias) 10 – 300 eV
- Nd:YAG laser 1064 nm
- laser energy 32 J

# B

## Low and high pulse number test

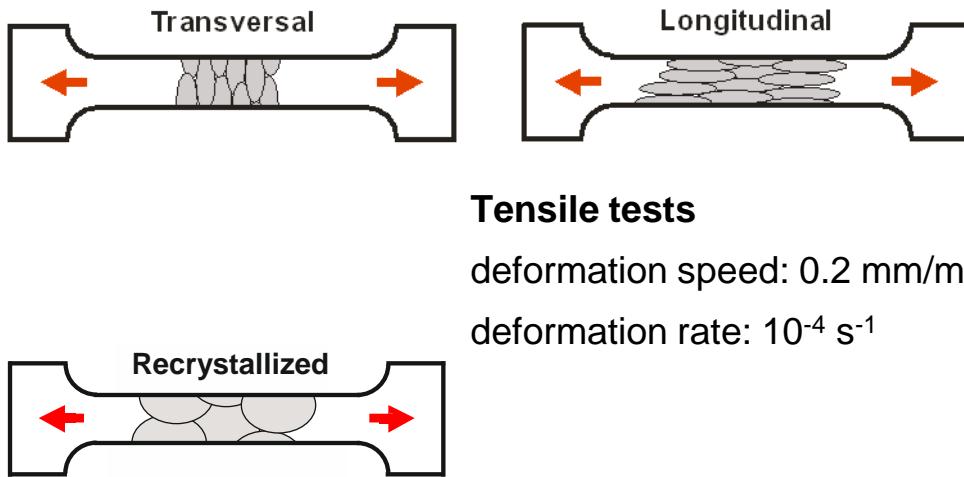
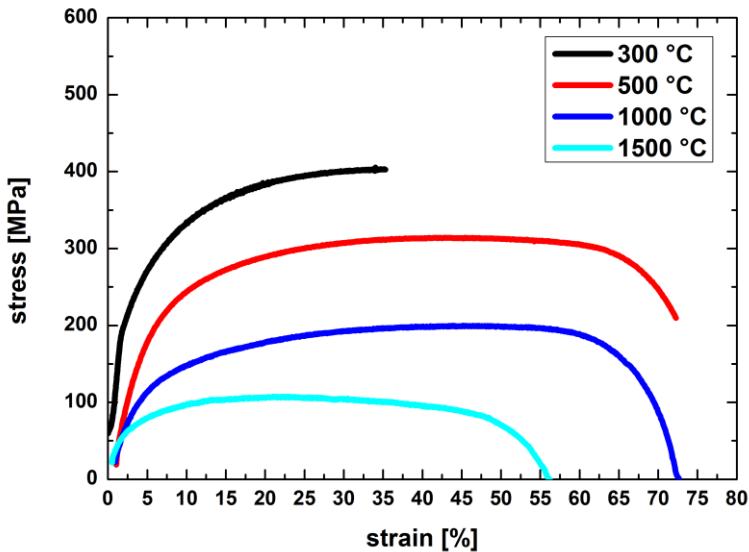
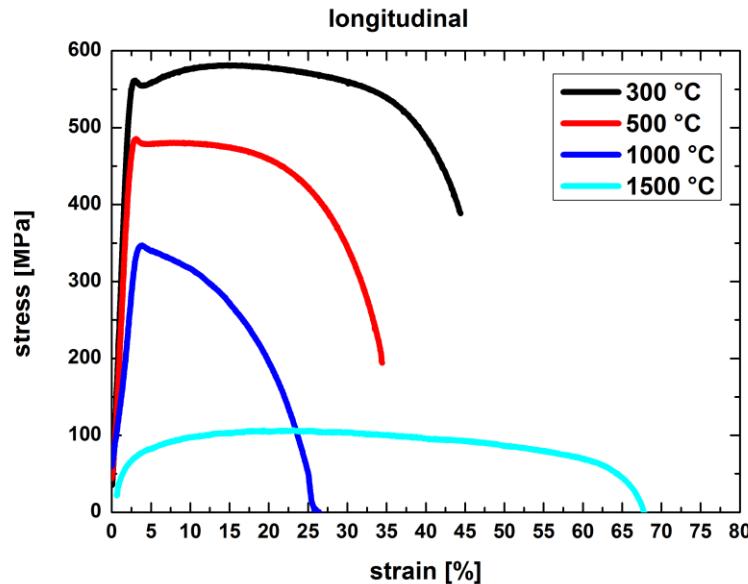
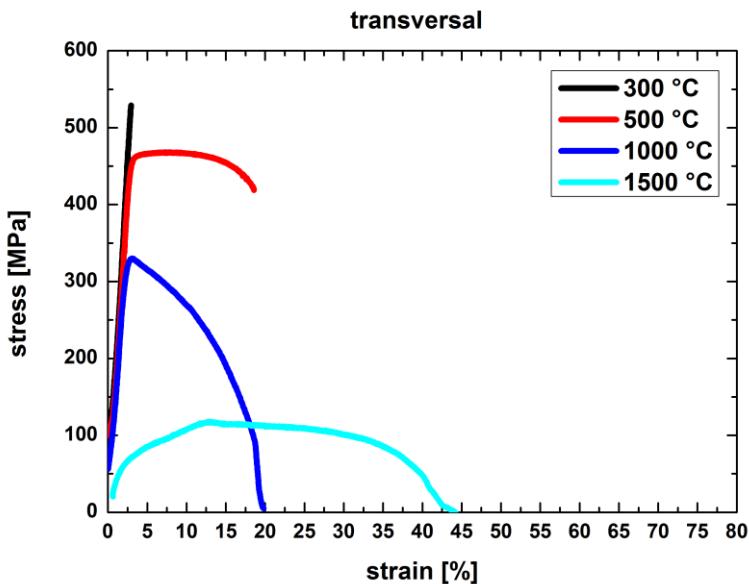
Expected heat loads in ITER divertor:



R. A. Pitts, et al., Journal of Nuclear Materials 438 (2013) S48-S56

J. Linke, Transactions of fusion science and technology 49 (2006) 455-464

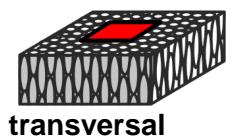
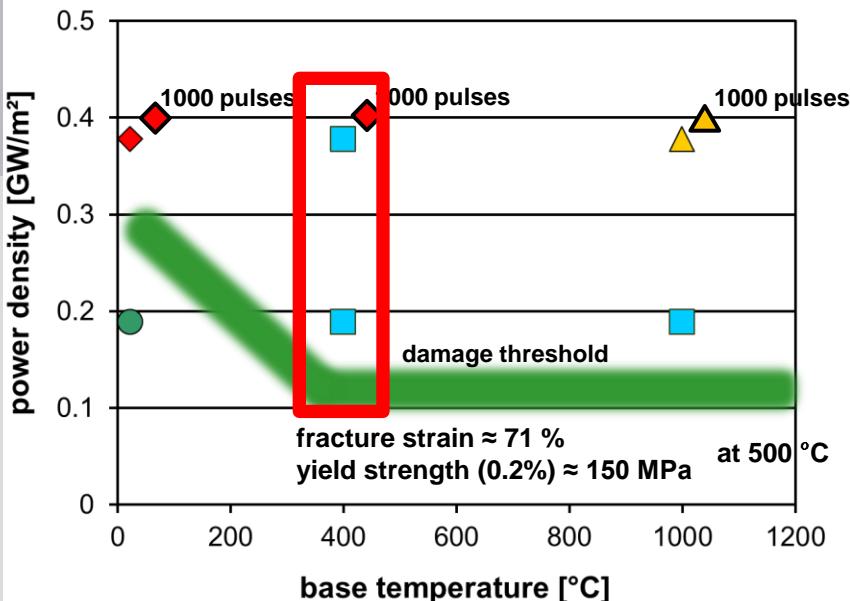
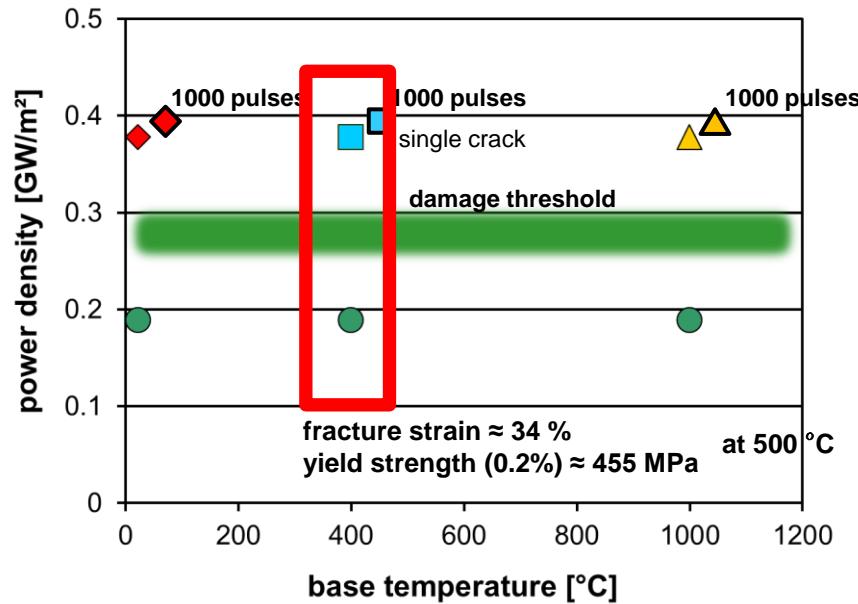
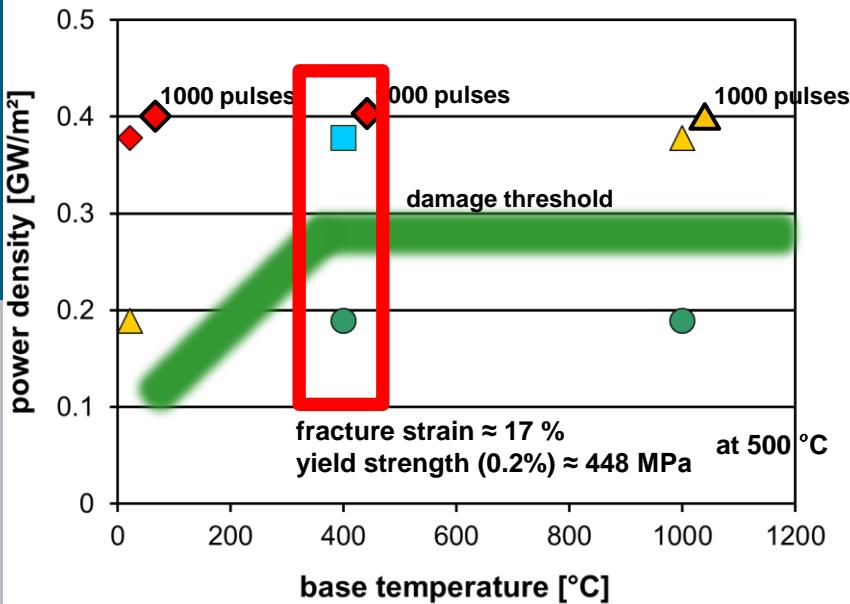
A. Loarte et al., Plasma Physics and Controlled Fusion 45 (2003) 1549-1569



## Tensile tests

deformation speed: 0.2 mm/min

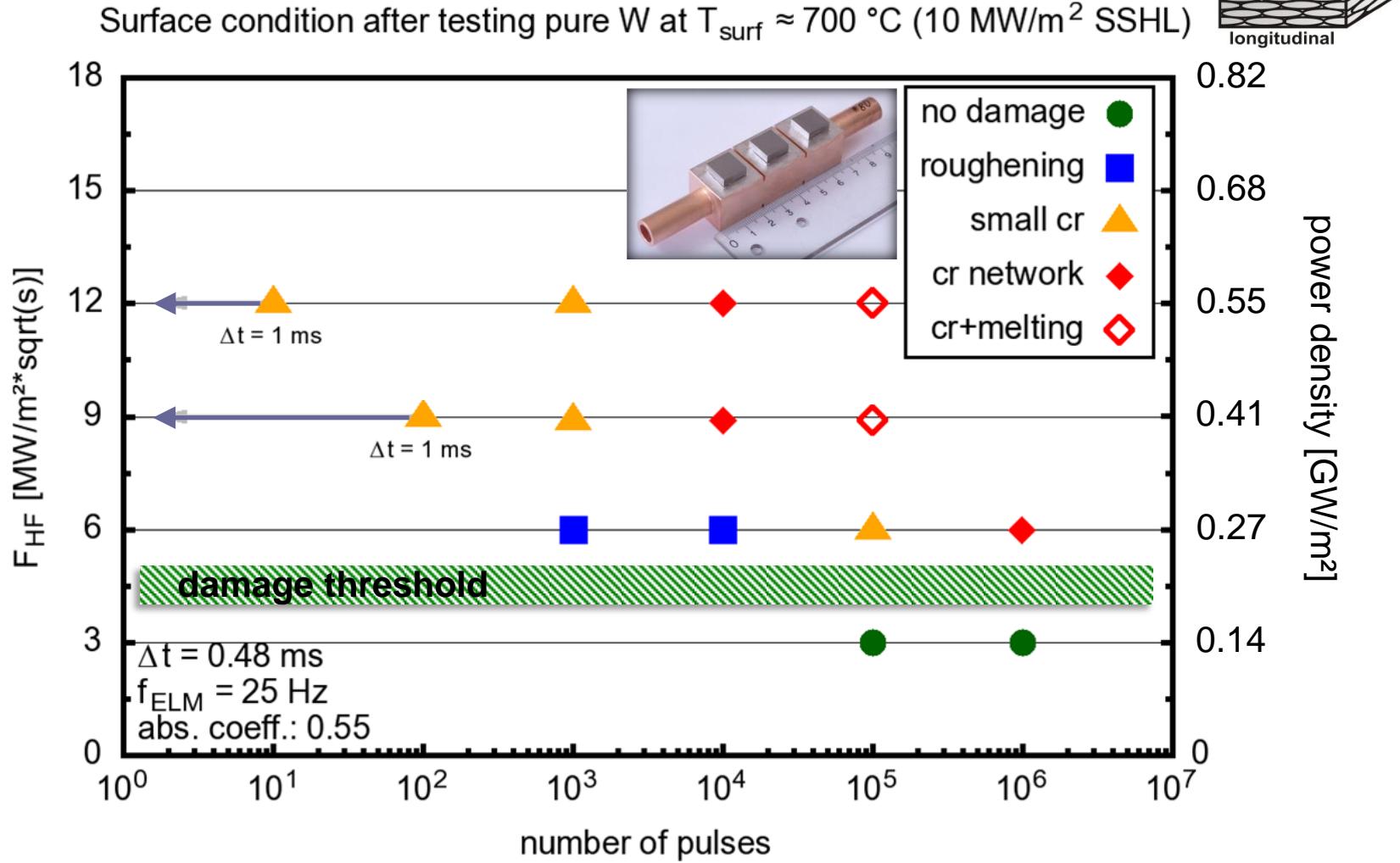
deformation rate:  $10^{-4} \text{ s}^{-1}$



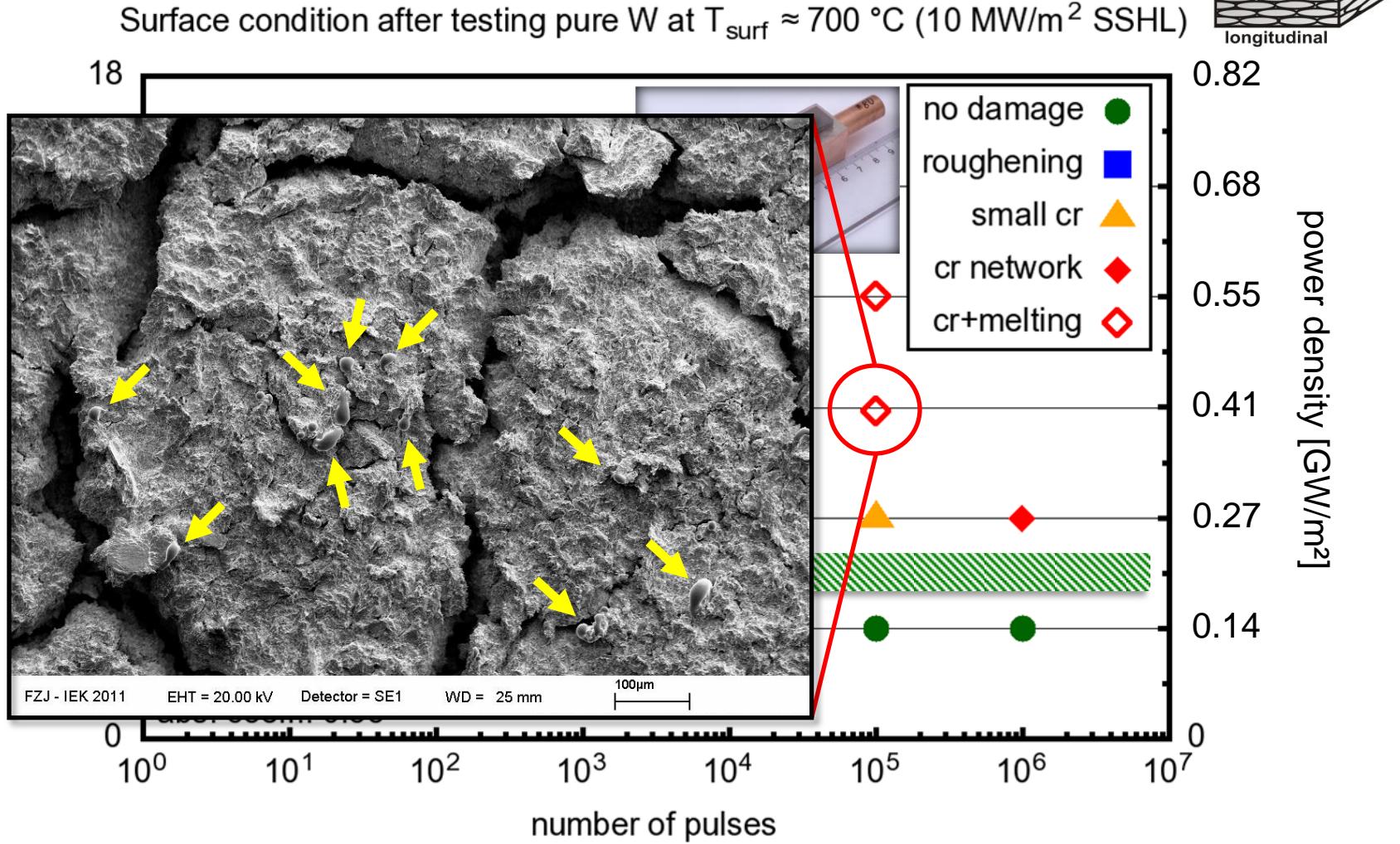
- no damage
- surface modification
- ▲ small cracks
- ◆ crack network

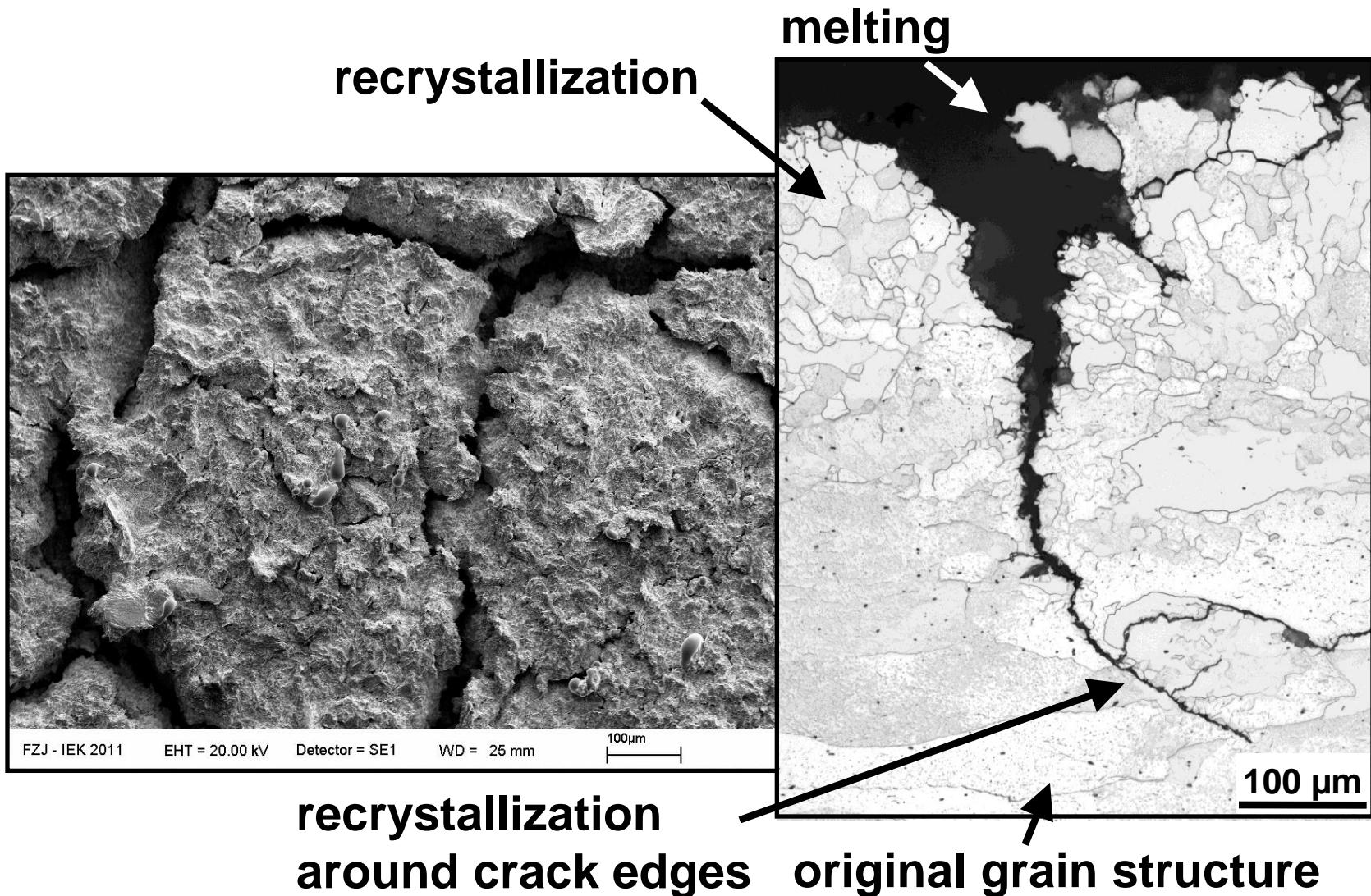
pulse duration 1 ms  
100/1000 pulses  
absorption coefficient: 0.55

## Tungsten at high pulse numbers

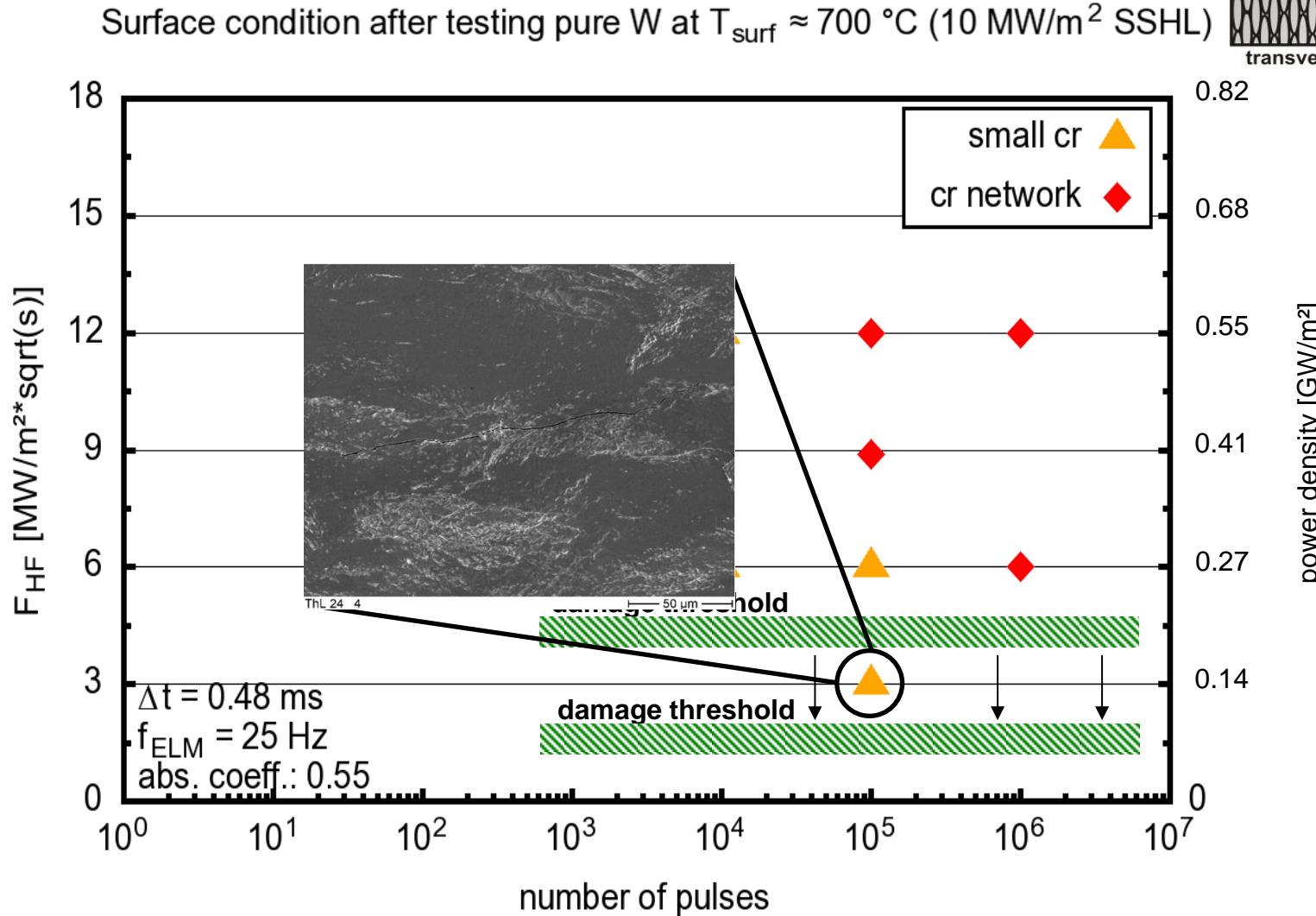


## Tungsten at high pulse numbers

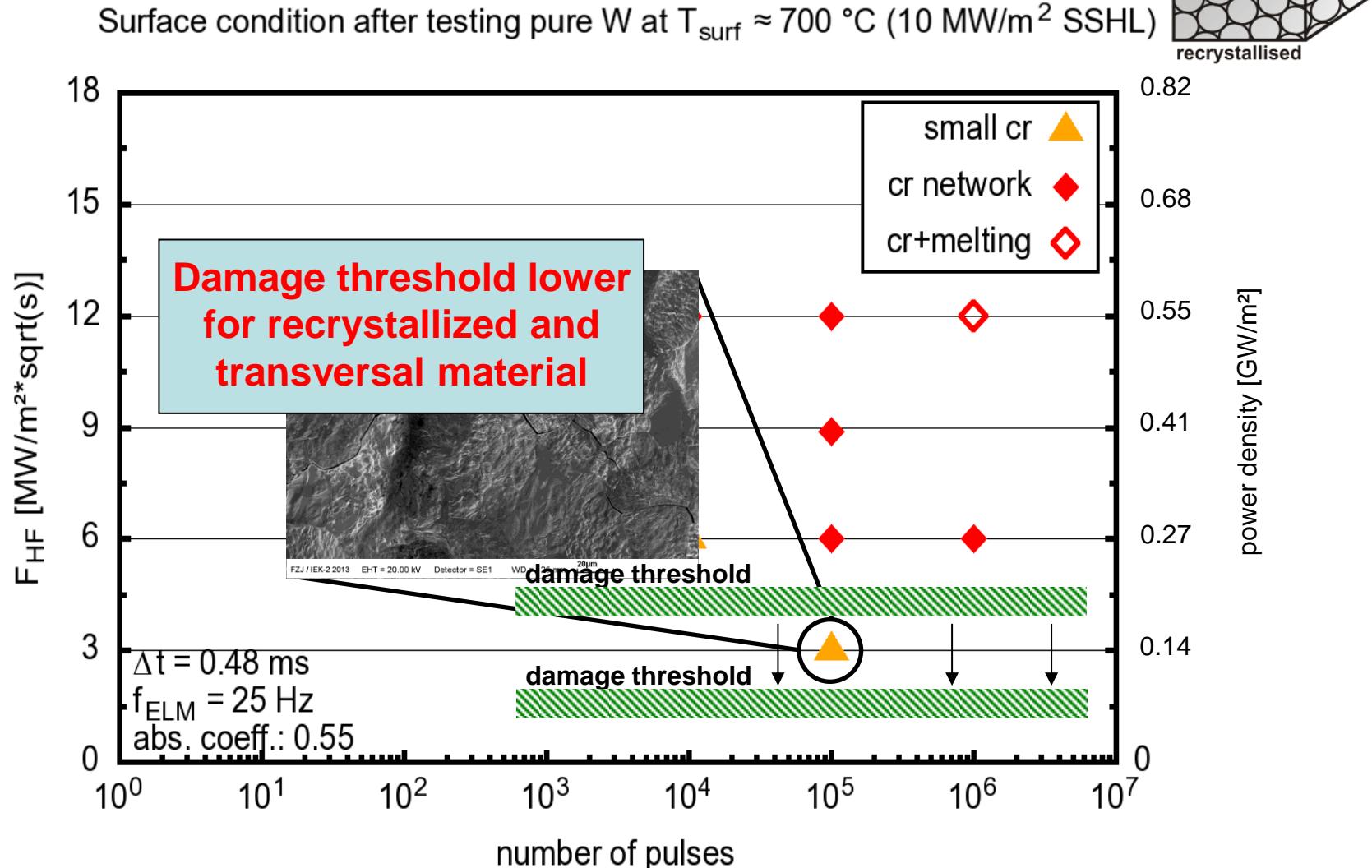




## Tungsten at high pulse numbers



## Tungsten at high pulse numbers

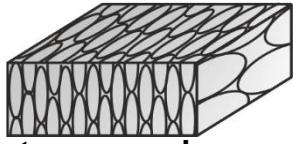
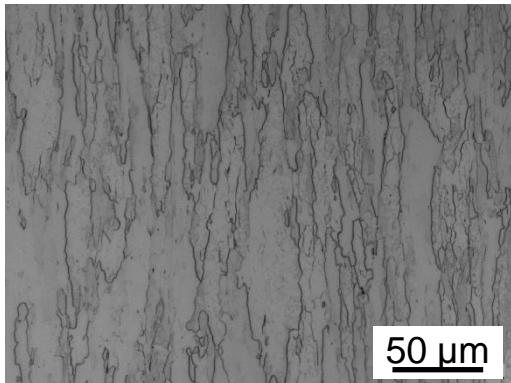


# C

**Combined particle and heat flux exposure of tungsten**

- commercially available sintered tungsten product
- representative example:

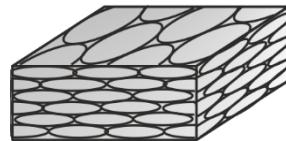
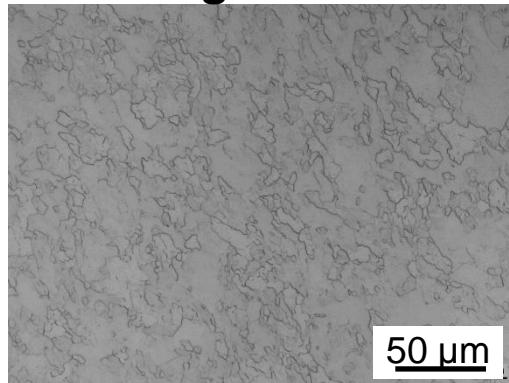
Transversal



transversal

at 1000 °C  
fracture strain ≈ 22 %  
yield strength (0.2%) ≈ 370 MPa

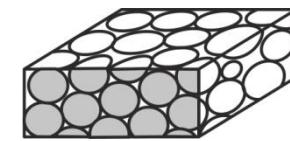
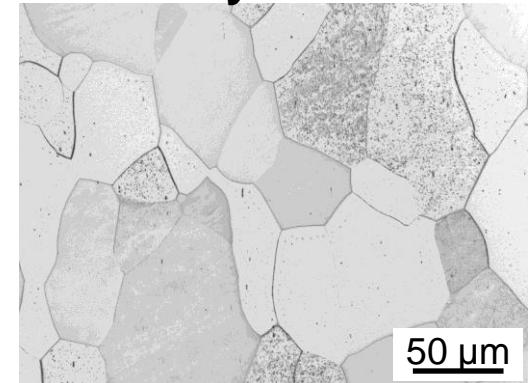
Longitudinal



longitudinal

at 1000 °C  
fracture strain ≈ 17 %  
yield strength (0.2%) ≈ 340 MPa

Recrystallized



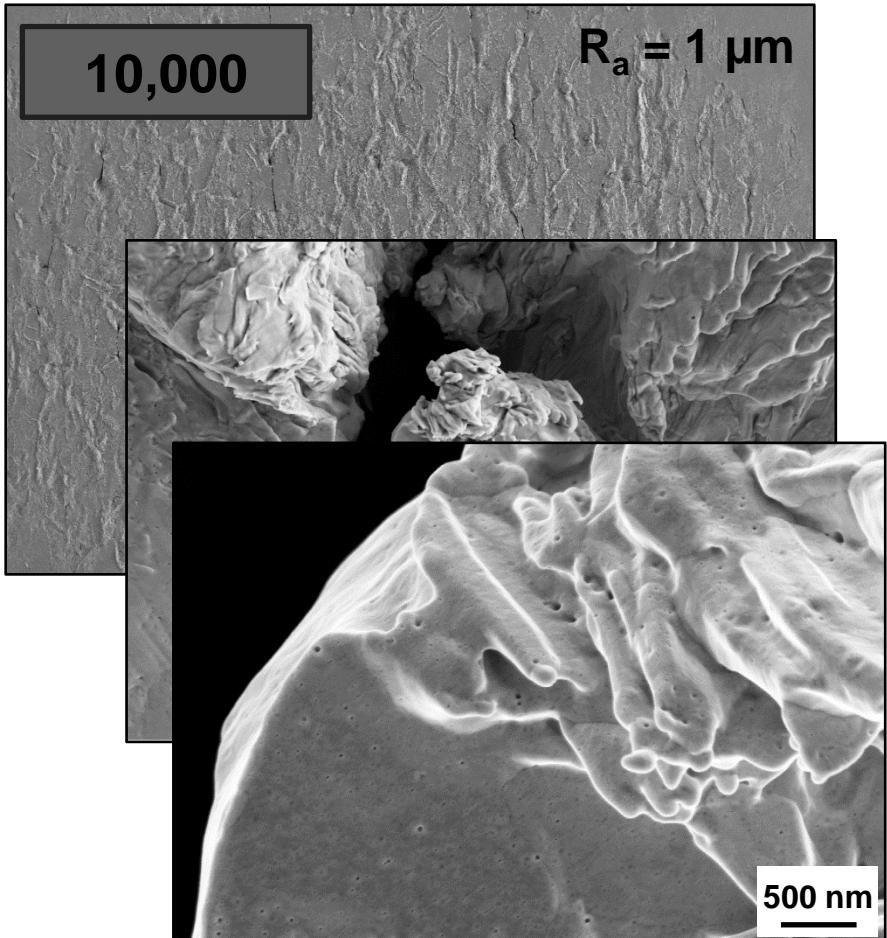
recrystallized 1600 °C, 1 h

at 1000 °C  
fracture strain ≈ 68 %  
yield strength (0.2%) ≈ 100 MPa

- characterization of the high pulse number thermal shock performance (fatigue) with steady state particle background

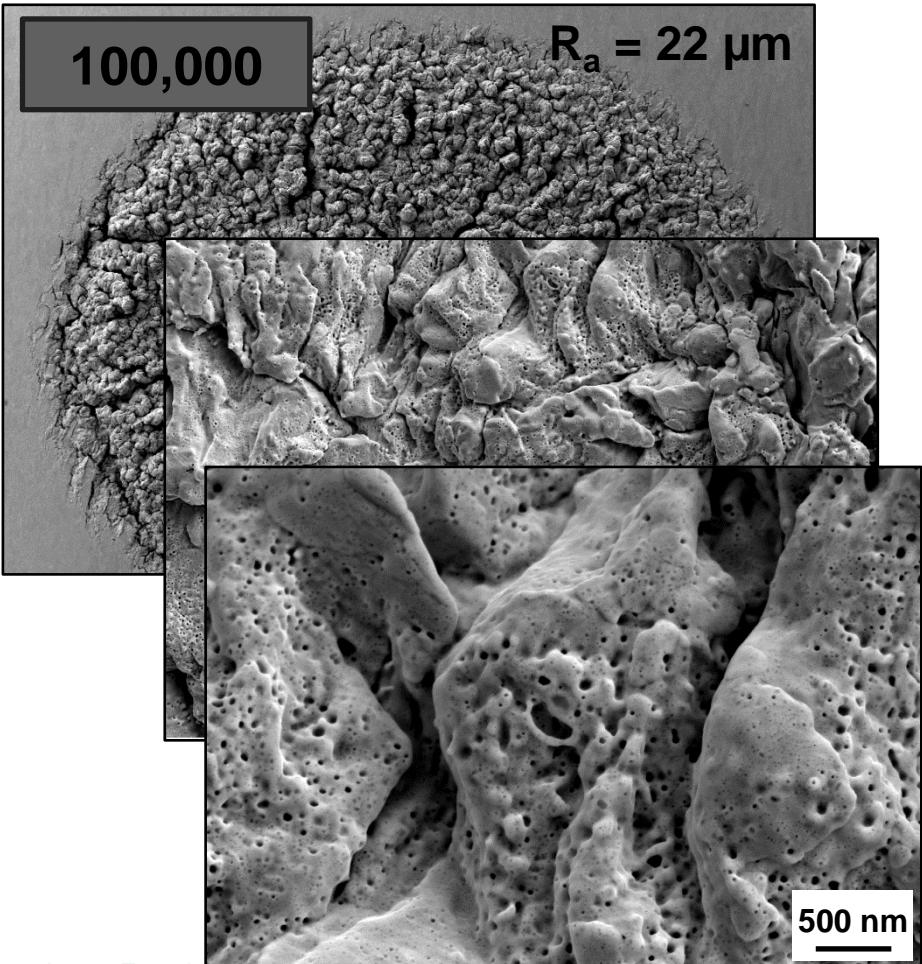
## Laser beam

ELM-like heat loads at 730 °C  
absorbed power density: 0.38 GW/m<sup>2</sup>  
pulse duration: 0.5 ms (f = 10 Hz)

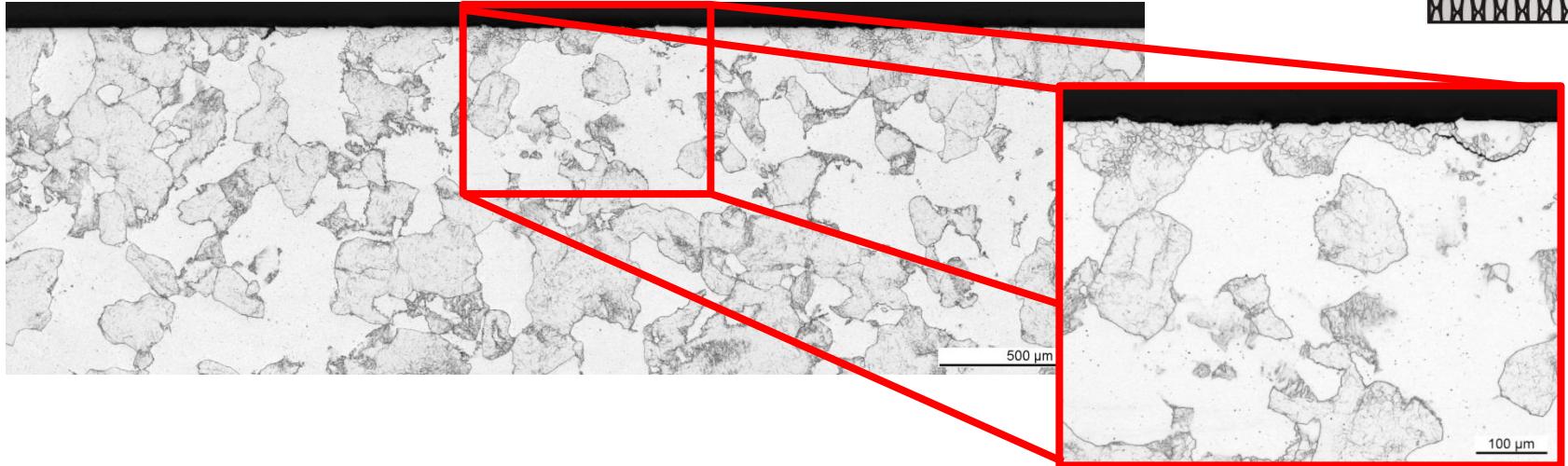


## H/He (6 %) - Plasma

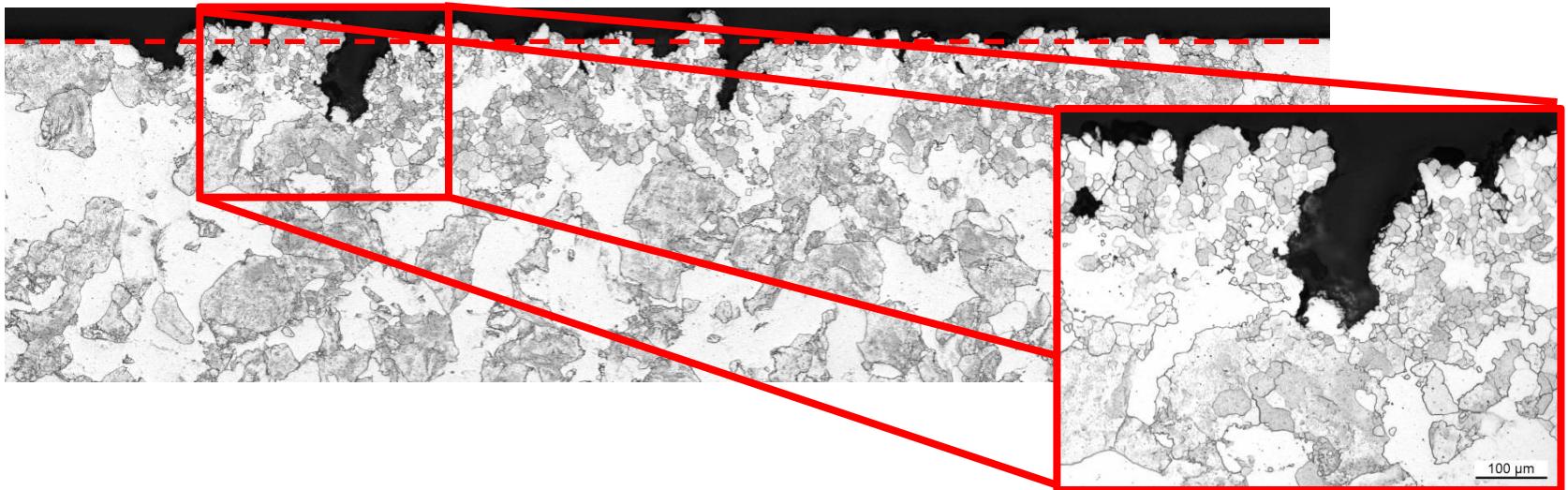
particle energy ≈ 35 eV  
plasma flux ≈  $6.0 \times 10^{21} \text{ m}^{-2}\text{s}^{-1}$   
fluence ≈  $9.0 \times 10^{24} \text{ m}^{-2}$  /  $6.0 \times 10^{25} \text{ m}^{-2}$

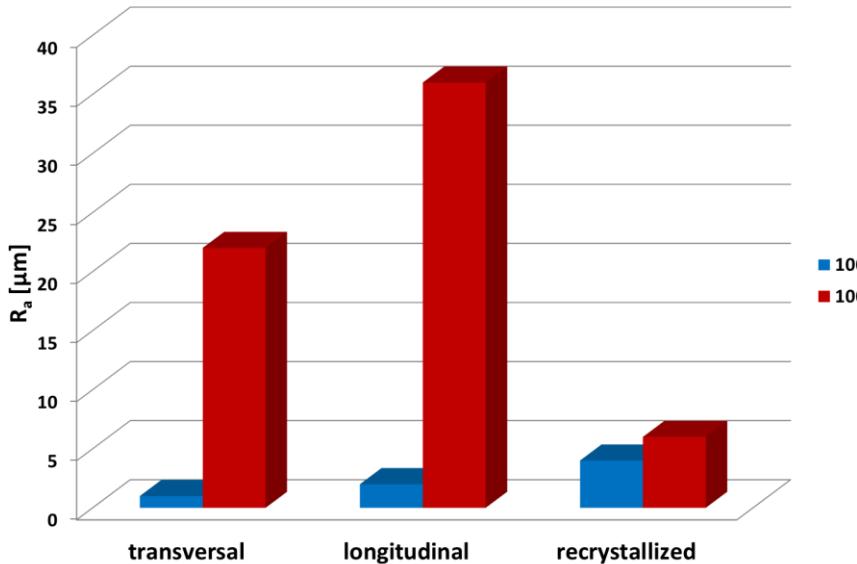


10,000 pulses



100,000 pulses



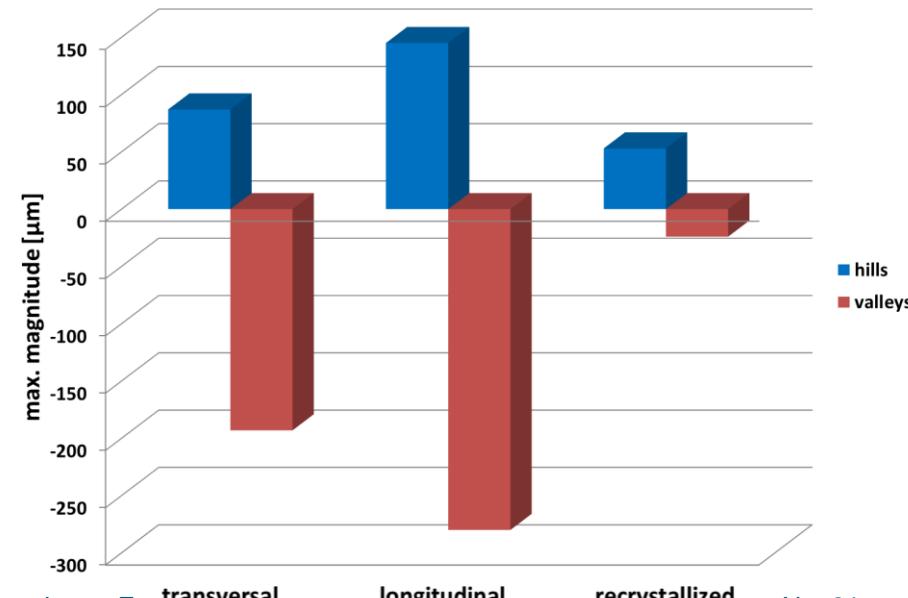


## Arithmetic mean roughness ( $R_a$ )

- significant increase for higher number of pulses (accumulation of plastic deformation)
- high strength/low ductility of the transversal and longitudinal grain orientation leads to severe damage
- lower strength/higher ductility of the recrystallized materials leads to a faster damage evolution but lower  $R_a$  values after high pulse numbers

## Hill and valley structure after 100,000 pulses

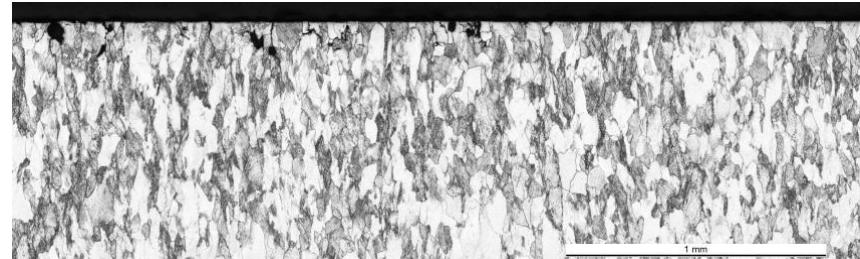
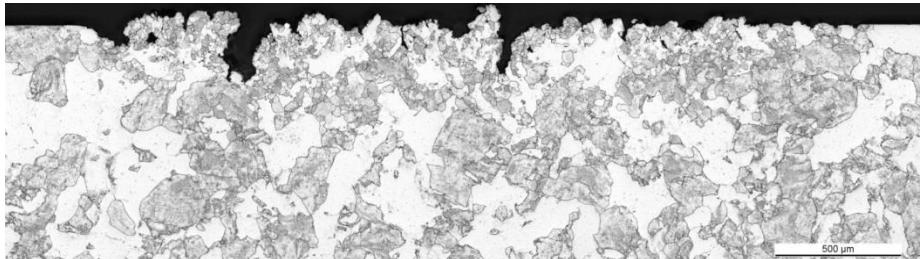
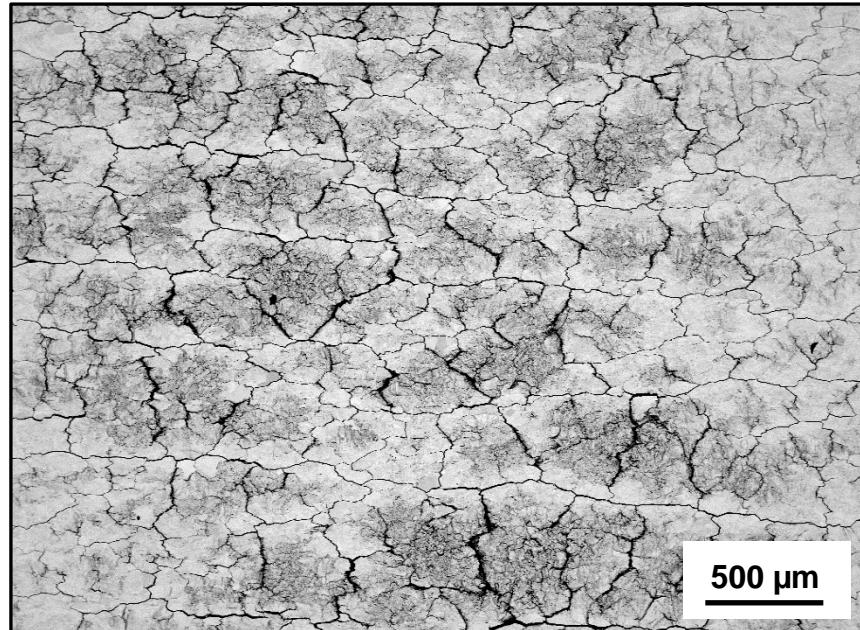
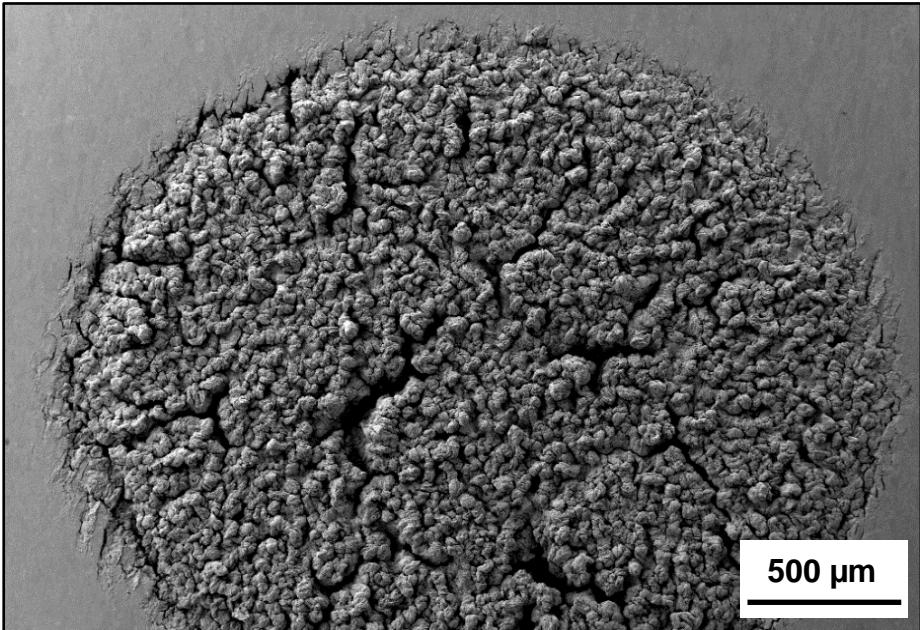
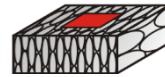
- severe hill and valley structure
- height differences up to 425 μm
- could be an indication for erosion of large parts of the surface (dust formation, plasma contamination)
- enhanced risk of overheating/melting, especially for low angle of incident

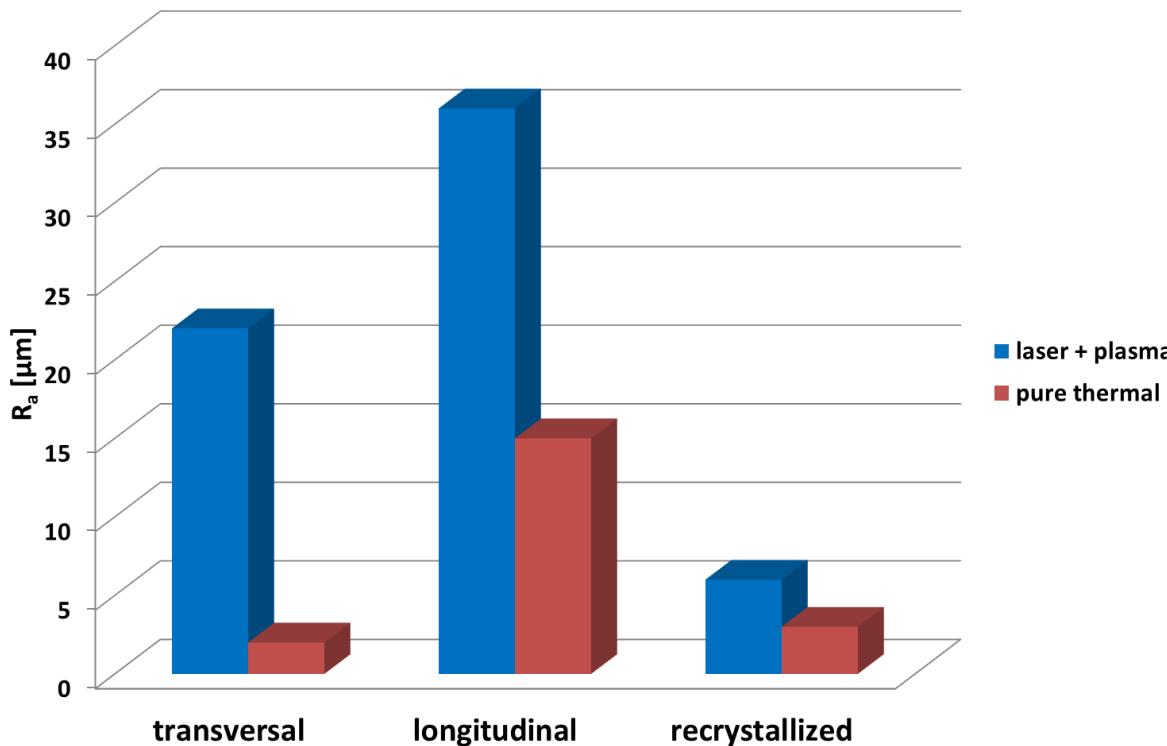


PSI-2 (laser + plasma)

100,000 pulses

JUDITH 2 (pure thermal)



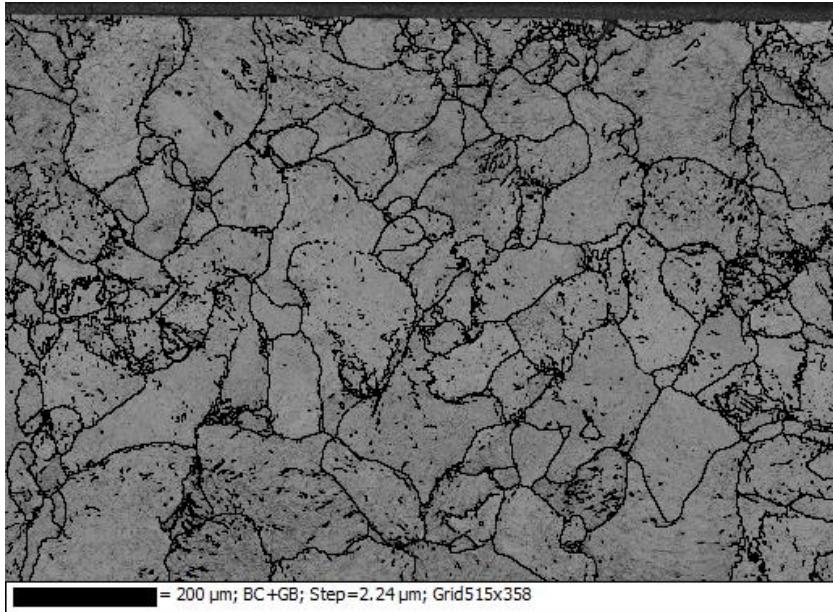


## Comparison PSI-2 (laser + plasma) and JUDITH 2 (pure thermal)

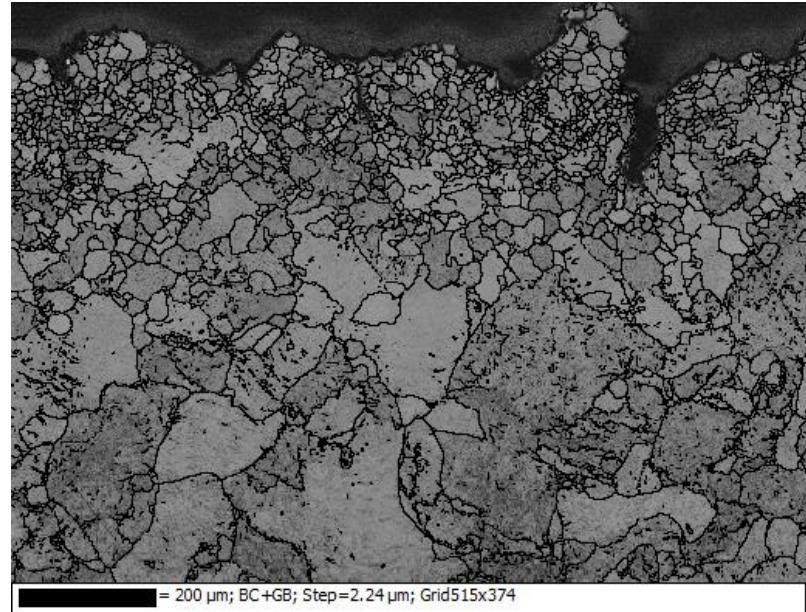
- combination of steady state particle background with transient thermal loads leads to a much faster damage evolution (fatigue) compared to pure thermal ( $\Rightarrow$  H/He embrittlement, degradation of mechanical strength)
- effect of lower strength/higher ductility of the recrystallized materials also reflected in the pure thermal results

Th. Loewenhoff et al., Fusion Engineering and Design 87 (2012), 1201-1205

10,000 pulses



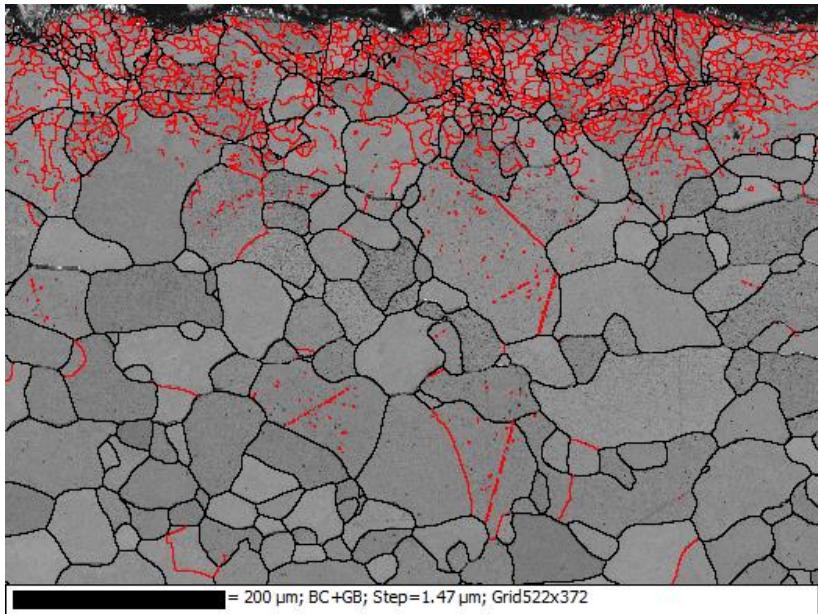
100,000 pulses



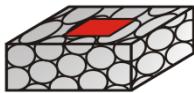
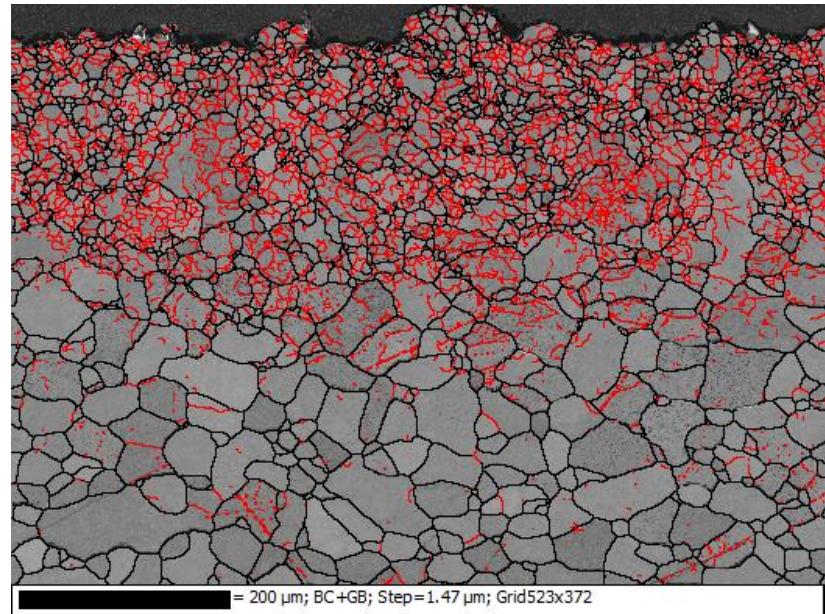
EBSD Band Contrast Image + Grain Boundaries ( $\geq 5^\circ$ )

- near surface microstructural changes occur already after 10,000 pulses
- region increases for higher pulse numbers
- sub-grains/grain nucleation can be observed

10,000 pulses

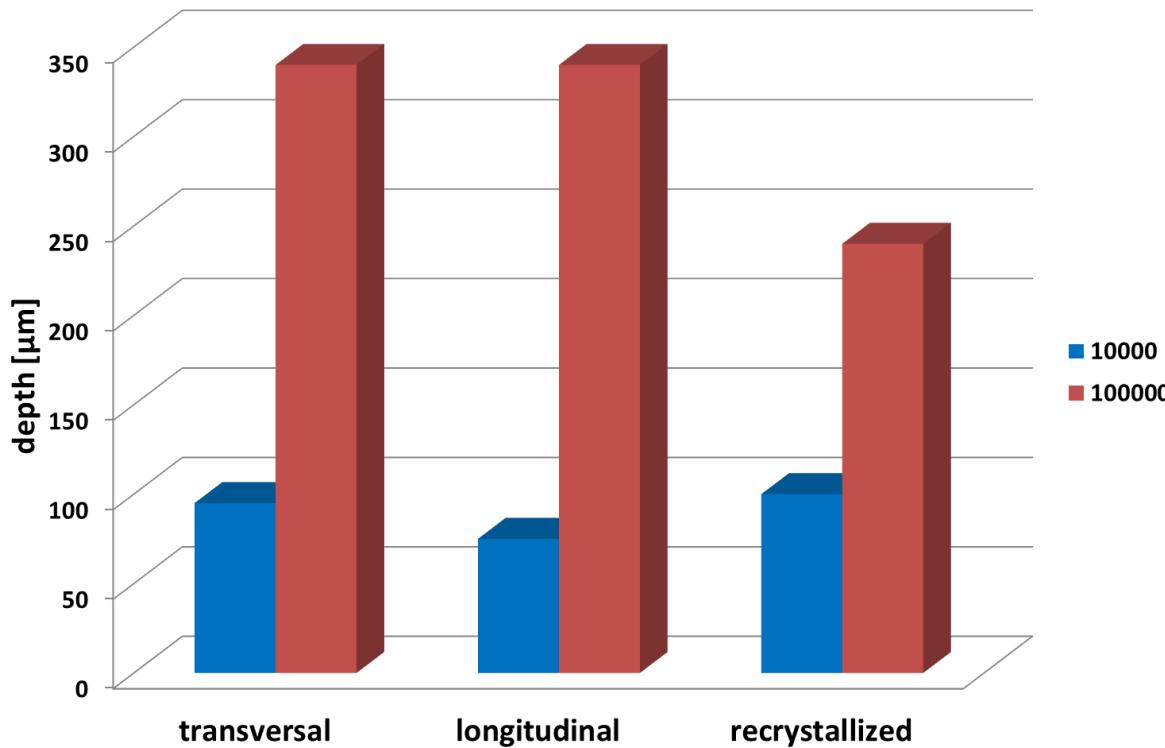


100,000 pulses



EBSD Band Contrast Image + Grain Boundaries (red: 3.5° up to 10°, black: > 10°)

- microstructural changes also visible for recrystallized material (1600 °C, 1 h)
- formation of small angle grain boundaries, grain refinement, dynamic recrystallization
- increase of the effected zone with higher number of pulses

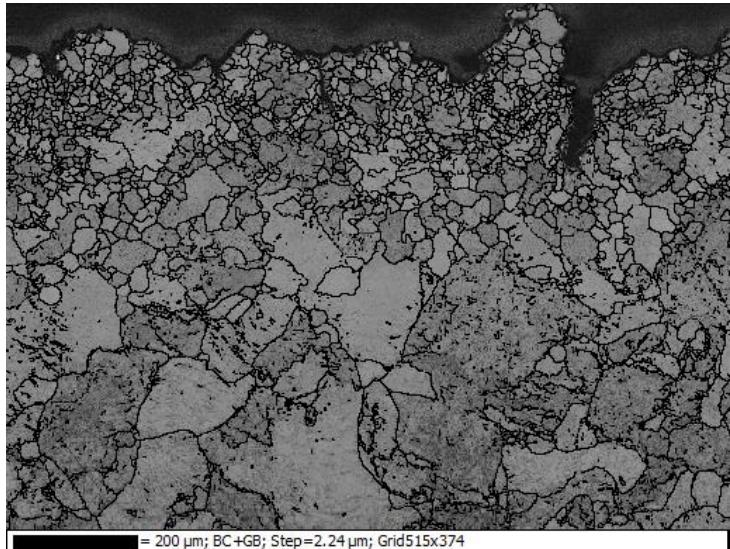


- significant increase of the depth from 10,000 to 100,000 pulses
- depth of the zone depends on the time (number of pulses) and temperature gradient ⇒ saturation for higher number of pulses?
- change of the mechanical properties in a near surface region ⇒ reduced strength/higher ductility like for the recrystallized material?
- impact on the diffusion/retention of H/He not clear ⇒ possibly higher retention as reported in: A. Huber et al. Physica Scripta T167, art. no. 014046 (2016)

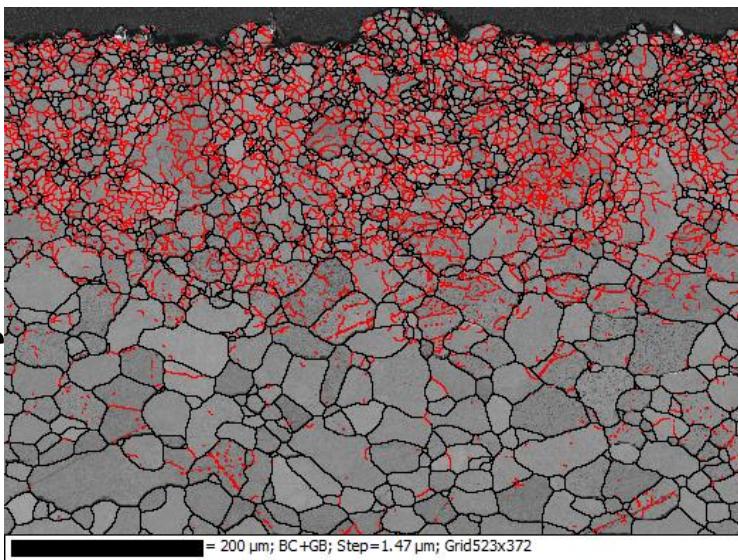
transversal

PSI-2 (laser + plasma)

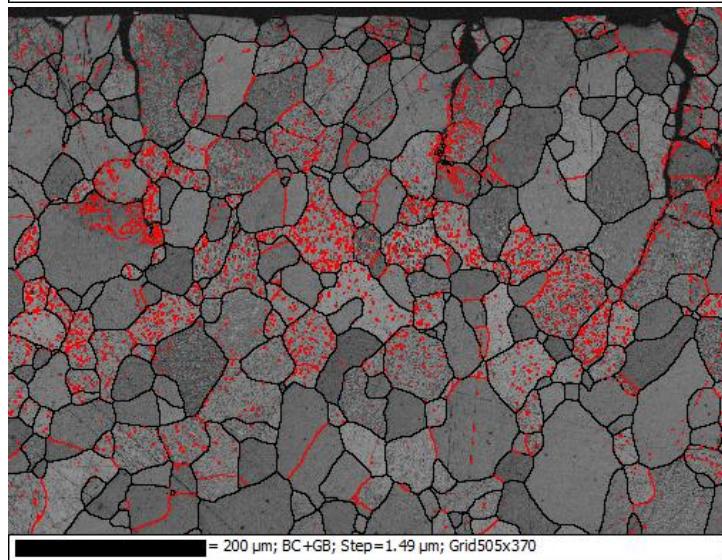
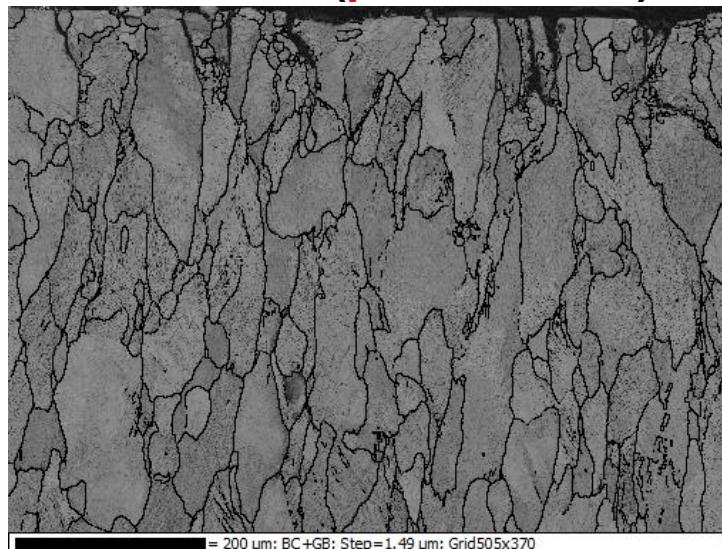
100,000 pulses



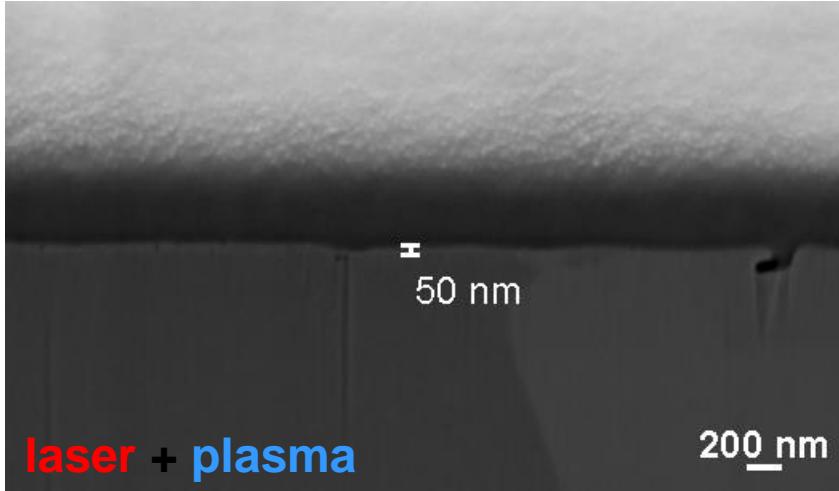
recrystallized



JUDITH 2 (pure thermal)

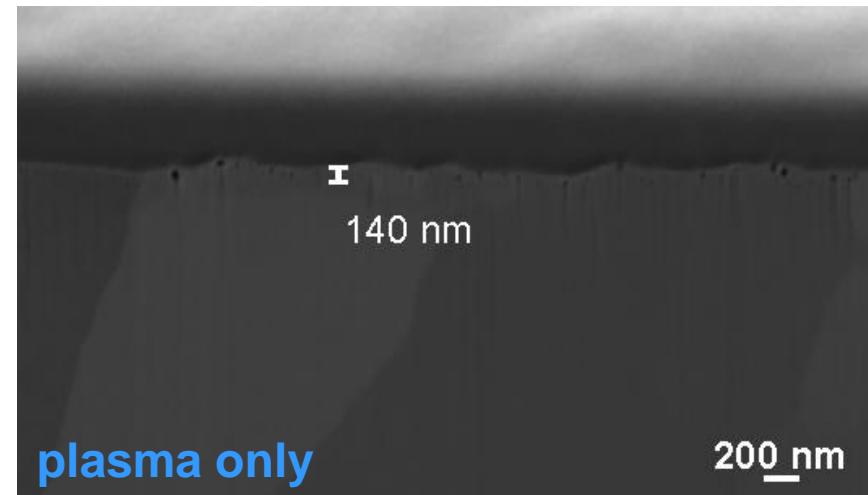
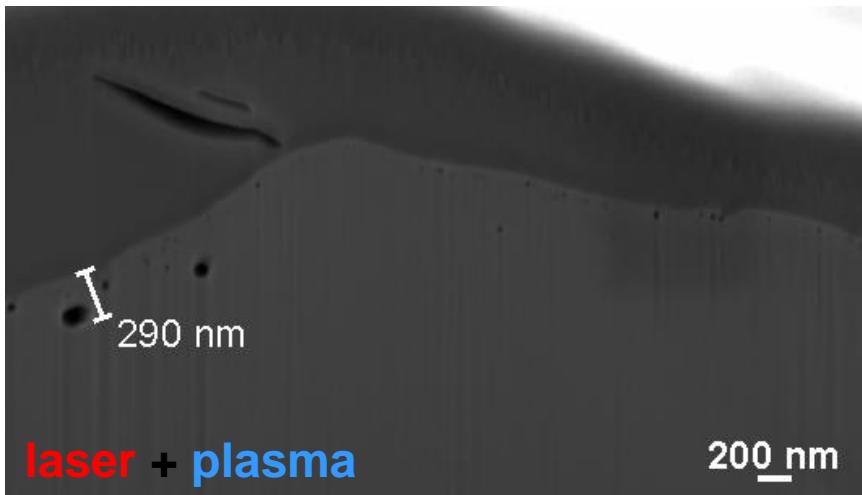


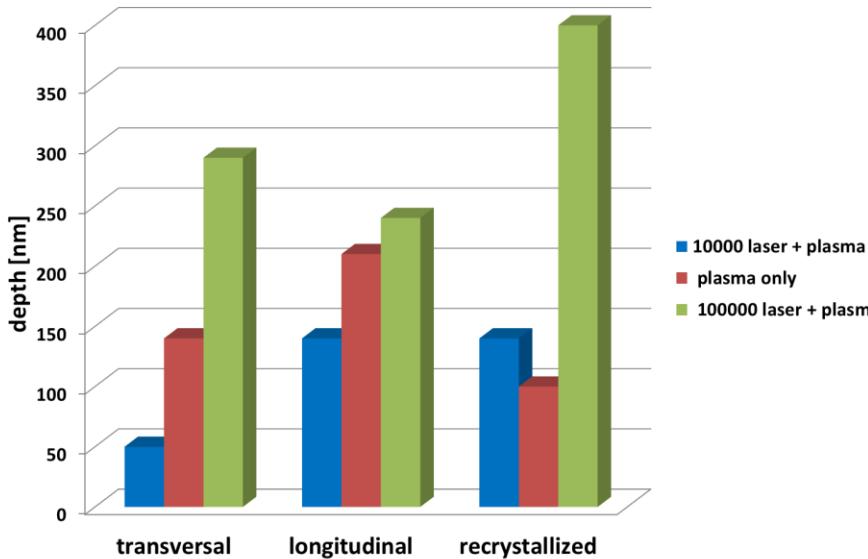
10,000 pulses



- He bubbles/layer only visible (in SEM) in the **laser + plasma** exposed area after 10,000 pulses
- He bubbles/layer become visible (in SEM) in the **laser + plasma** and **only plasma** exposed area after 100,000 pulses

100,000 pulses



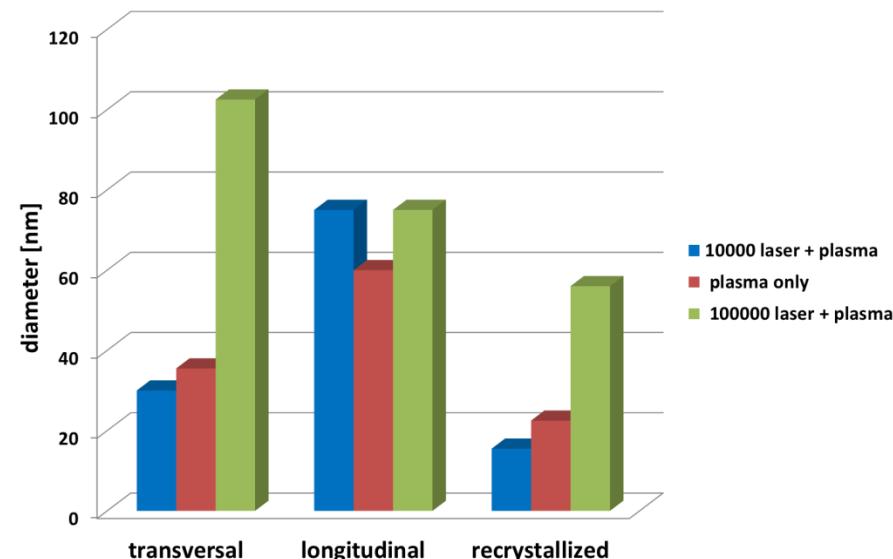


## Size of the He effected layer

- depth of the He affected layer increases with number of pulses/fluence
- additional transient heat loads result in an extension of the He affected layer
- higher thermal gradients could lead to a deeper diffusion into the bulk material

## Size of the visible He bubbles

- size of the visible bubbles increases for higher number of pulses/fluence
- additional transient heat loads accelerate this effect
- impact on the He bubble density not clear

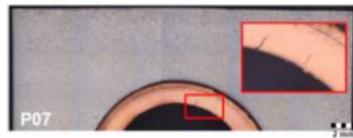
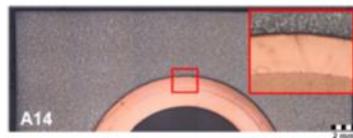


# D

## Tungsten characterization

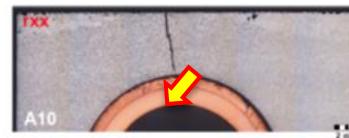
## SMALL SCALE MOCK-UPS

A) 1000 cycles at 10 MW/m<sup>2</sup>



- no visible defects in tungsten
- small cracks in copper

C) 1000 cycles at 10 MW/m<sup>2</sup> +  
500 cycles at 20 MW/m<sup>2</sup>



- recrystallization → enhanced for HRP ( $\leq 2$  mm)
- surface roughening / erosion → enhanced for HIP
- cracking → enhanced for W-sheet / HRP

D) 1000 cycles at 10 MW/m<sup>2</sup> +  
1000 cycles at 20 MW/m<sup>2</sup>



- recrystallization → HRP (2-4 mm)
- surface roughening / melting → peak/valley of  $\leq 500$   $\mu\text{m}$

## VERTICAL TARGET PROTOTYPICAL COMPONENTS (VTPCs)

A) 1000 cycles at 10 MW/m<sup>2</sup>



- cracking → W-sheet / HRP® (initially existing damage?)

B) 1000 cycles at 10 MW/m<sup>2</sup> +  
1000 cycles at 15 MW/m<sup>2</sup>



- cracking → W-rod / HIP®

E) 1000 cycles at 10 MW/m<sup>2</sup> +  
1000 cycles at 15 MW/m<sup>2</sup> +  
300 cycles at 20 MW/m<sup>2</sup>



- recrystallization (2-4 mm)
- surface roughening / erosion → enhanced for W-rod / HIP®
- cracking

**W Plate: 1/10 self-castellation**  
**W bar: 8/14 self-castellation**

G. Pintsuk, et al. "Qualification and post-mortem characterization of tungsten mock-ups exposed to cyclic high heat flux loading", SOFT2012 Liege BE

## □ Observation

- Self-castellation often appeared in W monoblocks used by EU industry

## □ Conformity of W material with ITER material specification

- Chemical composition: similar

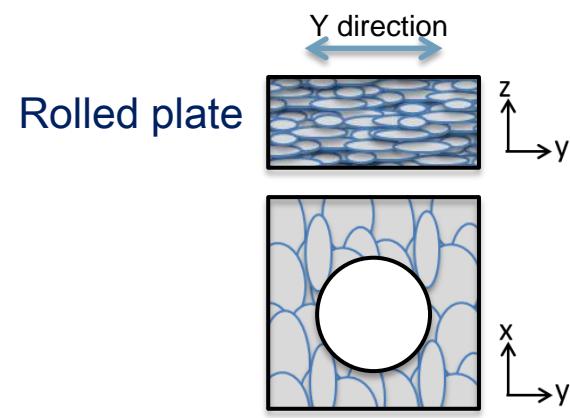
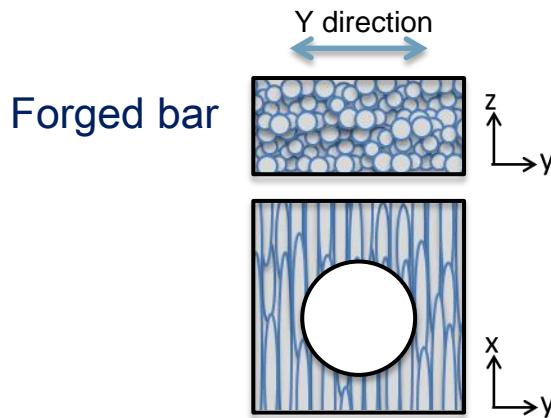
- Hardness: similar

- Density: similar

	W-Plansee	W-Polema	W-ALMT	W-AT&M
HV30	441	443	461	448
density [g/cm <sup>3</sup> ]	19.25	19.12	19.17	19.25

- Microstructure: different

N.B. production routes are different (e.g. forged bar vs rolled plates)

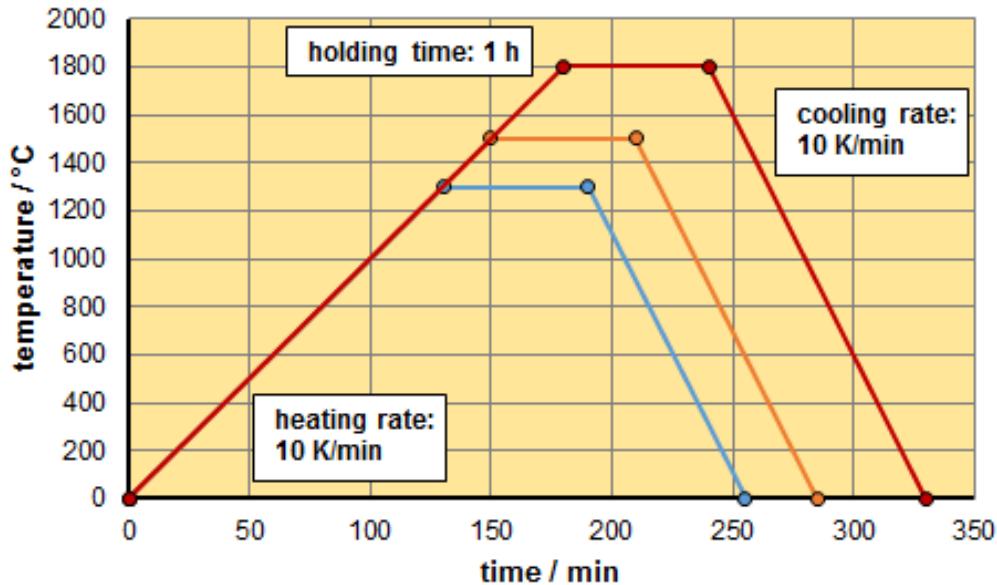


Strength in y-direction would be different

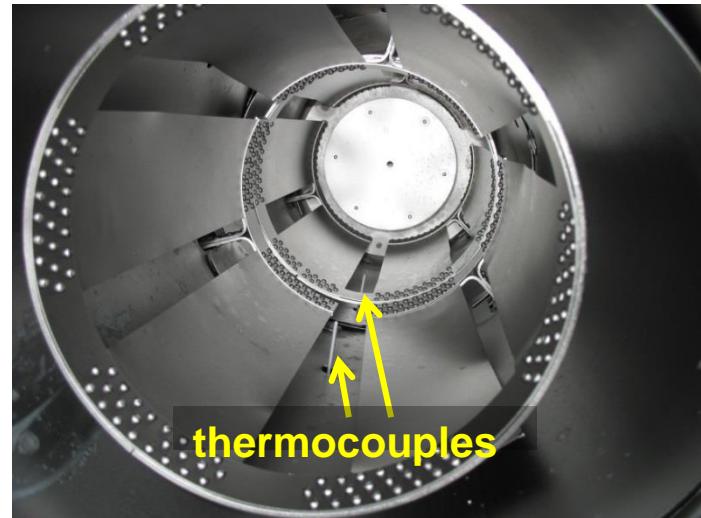
See supporting data in M. Wirtz, et al. presented at SOFT2012  
<http://dx.doi.org/10.1016/j.fusengdes.2013.05.07>

## □ Recrystallization Sensitivity Tests

- Heat treatment at 1300 °C, 1500 °C, 1800 °C for 1 hour in vacuum
- Test surface yz-plane
- Vickers hardness HV30, microstructure and grain size



Temperature profiles up to 1300, 1500 and 1800 °C for the annealing treatment of the tungsten products



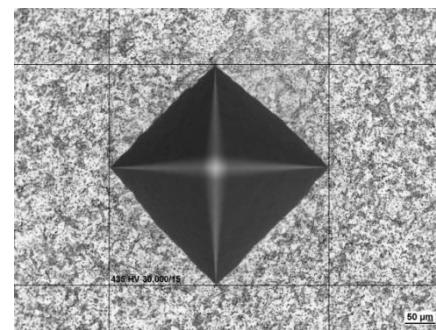
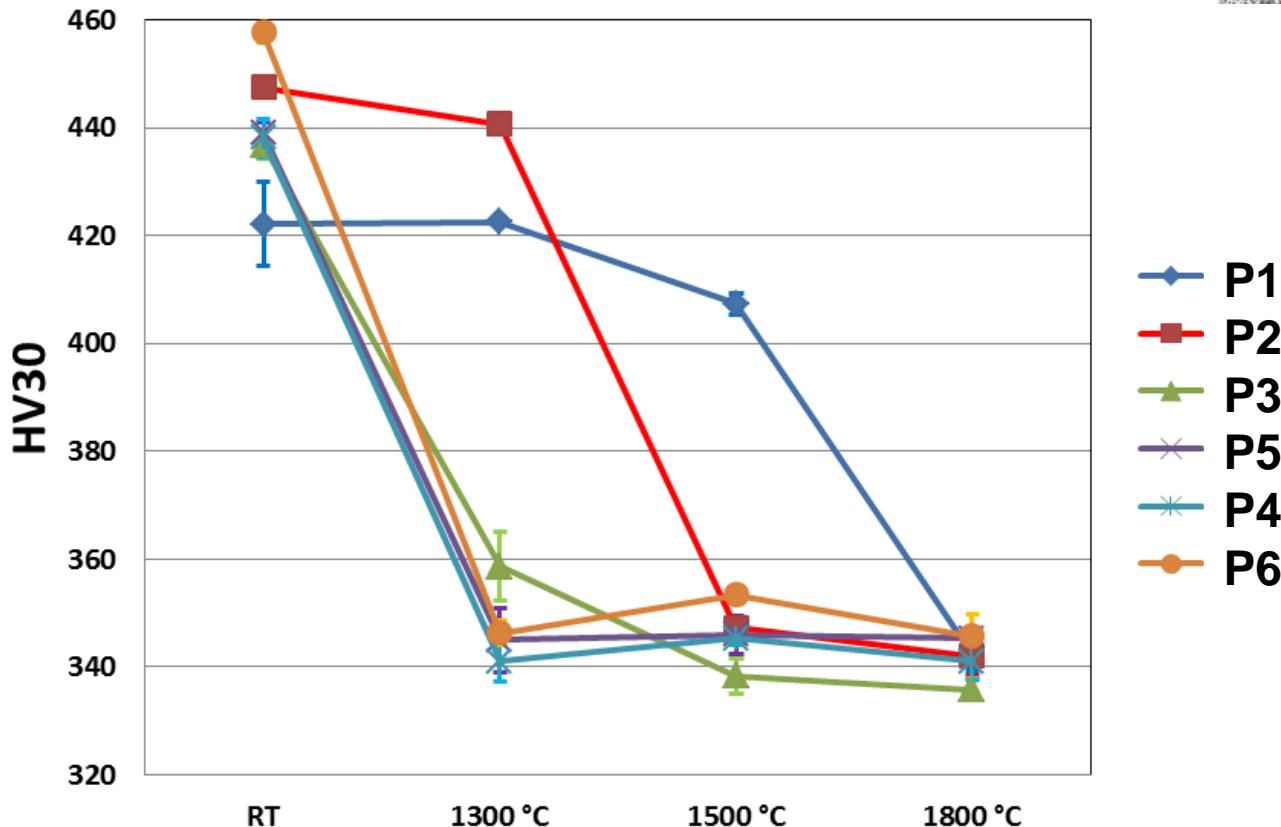
High temperature furnace with the position of the thermocouples.

## Vickers Hardness HV30

tested surface xy-plane

temperature treatment for 1 h

xy-plane

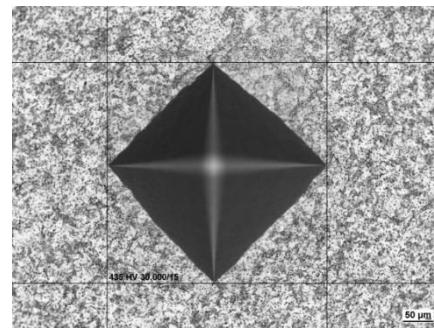
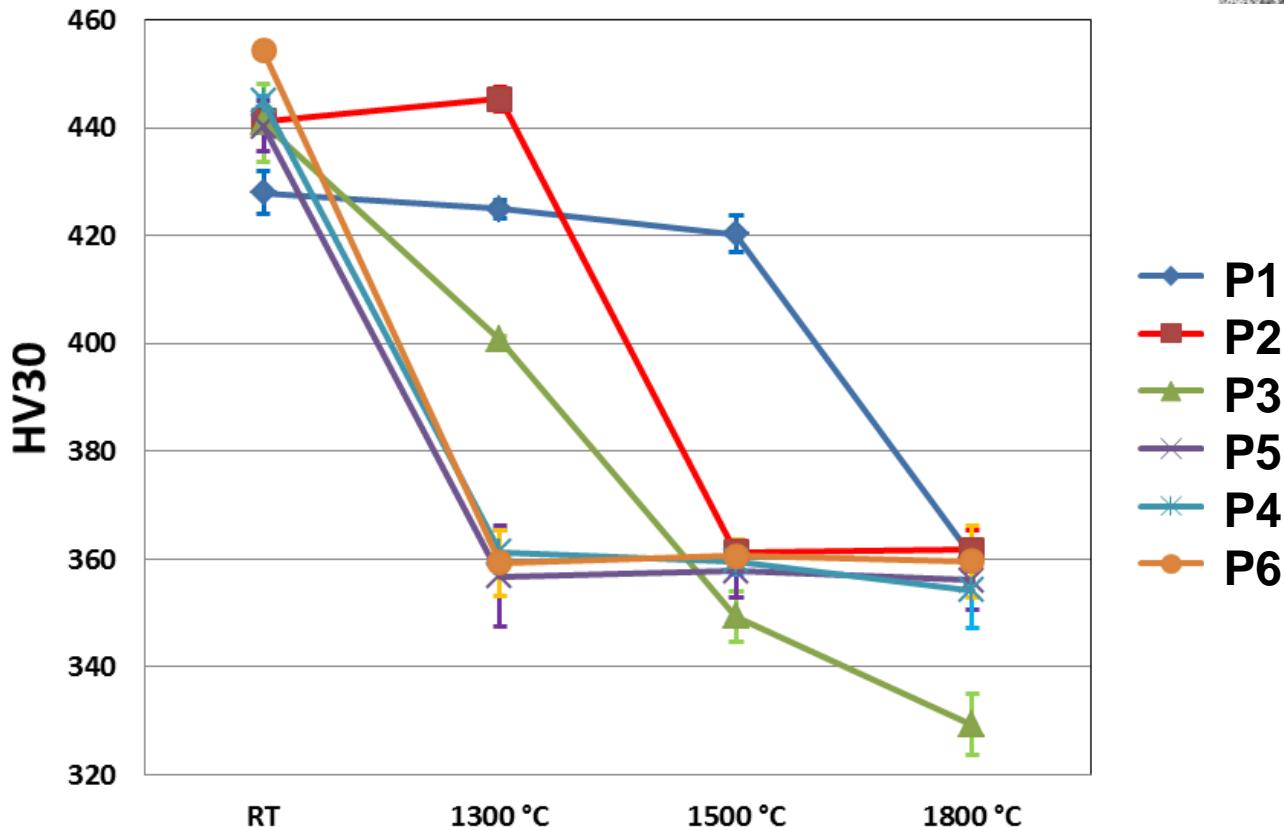


## Vickers Hardness HV30

tested surface yz-plane

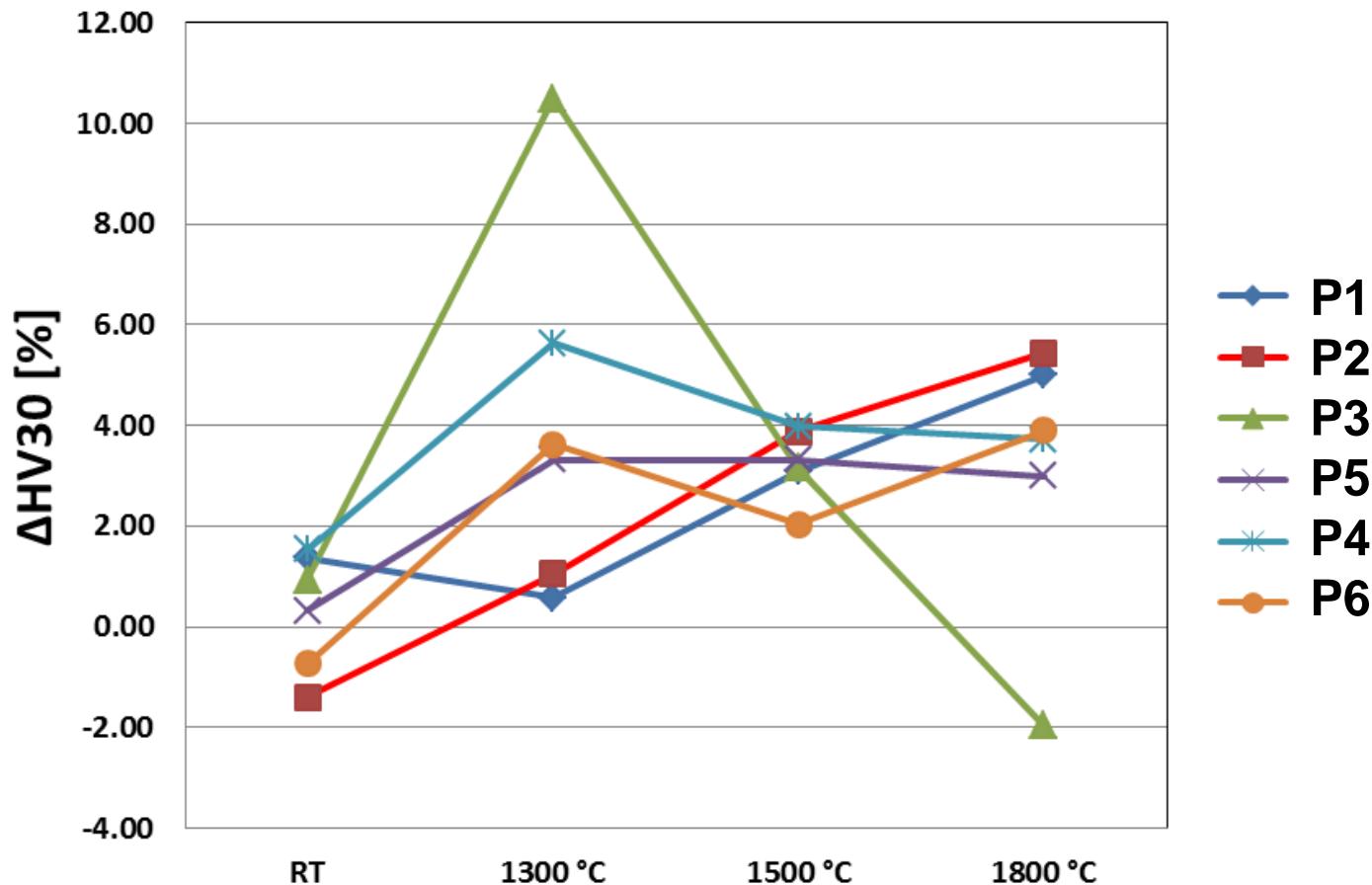
temperature treatment for 1 h

yz-plane

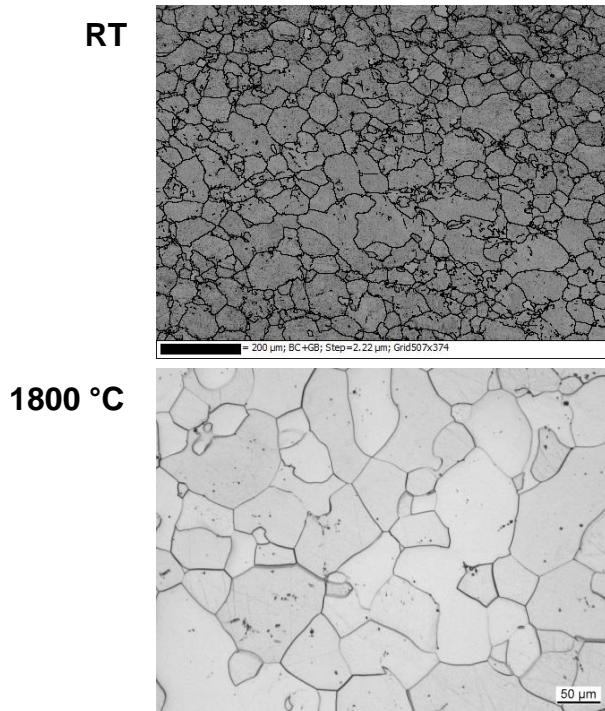


## Hardness difference of the xy and yz-plane temperature treatment for 1 h

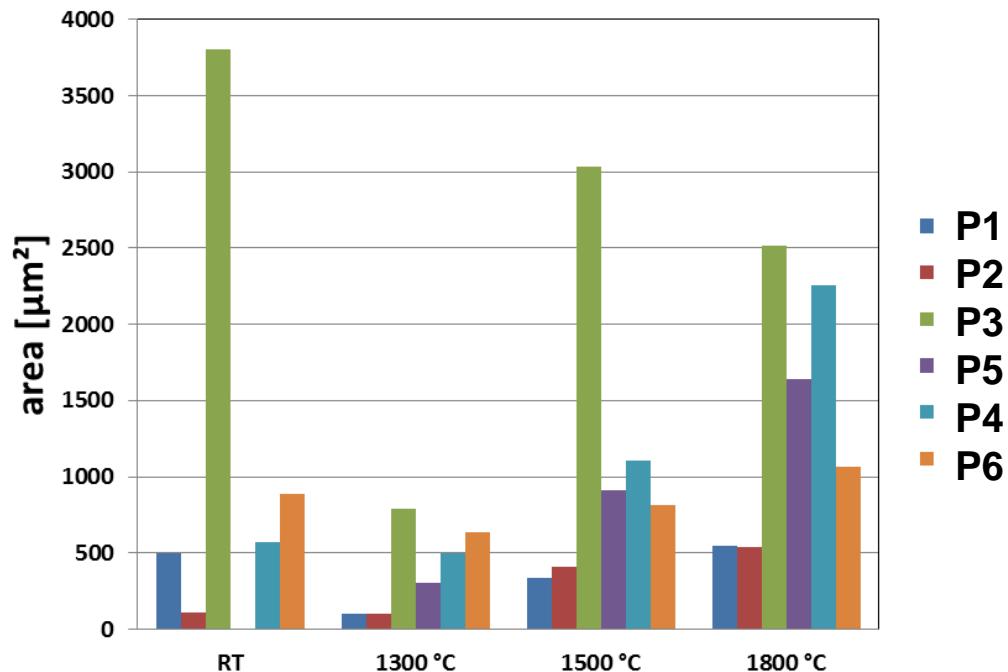
### $\Delta(xy/yz)$ -plane



## Investigated surface xy-plane

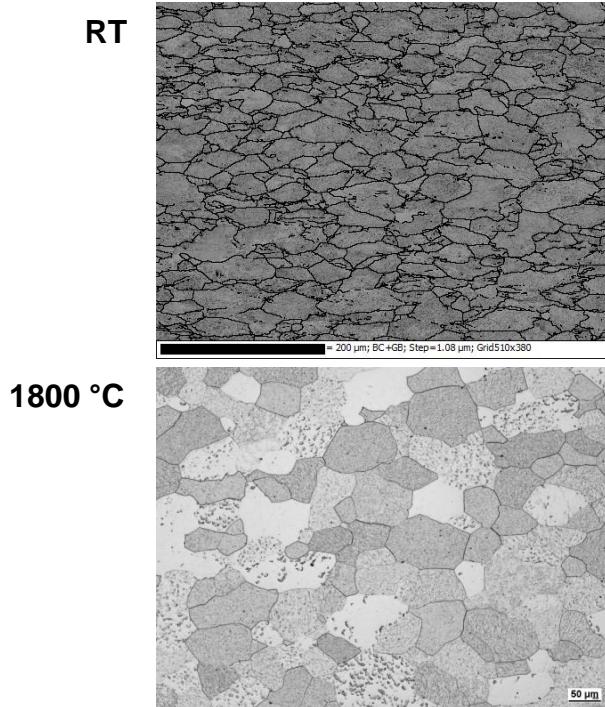


## grain size xy-plane

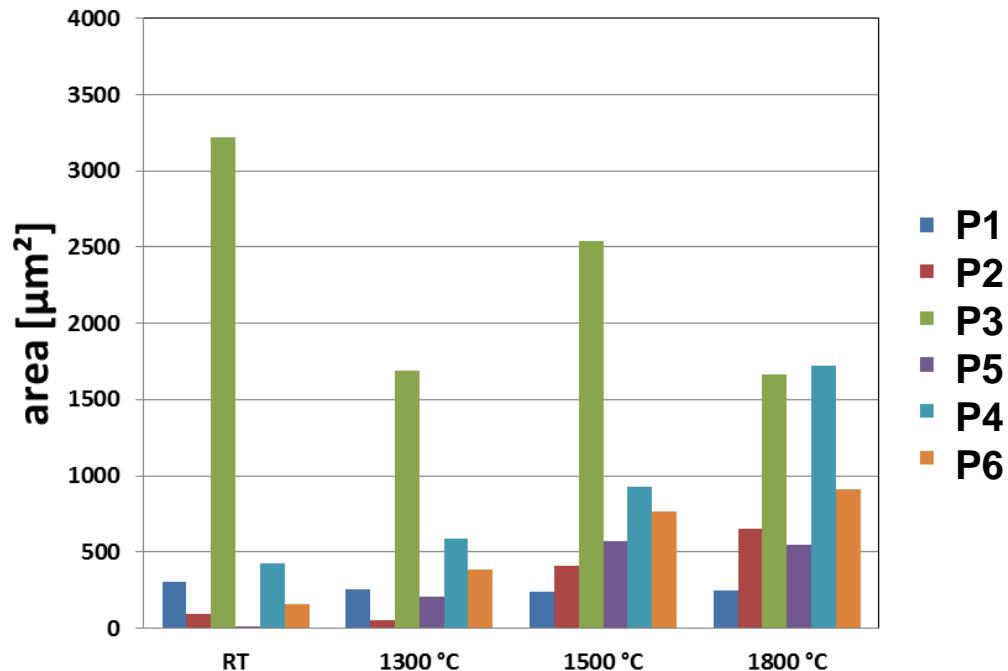


aspect ratio	ALMT	Ansaldo Polema	AT&M	Plansee (M213)	MMC NSMC	STARCK
RT	0.63	0.59	0.61	-	0.62	0.53
1300 °C	0.53	0.53	0.62	0.59	0.59	0.67
1500 °C	0.66	0.61	0.55	0.59	0.63	0.62
1800 °C	0.55	0.66	0.61	0.60	0.63	0.65

## Investigated surface yz-plane



## grain size yz-plane



aspect ratio	ALMT	Ansaldo	AT&M	Plansee (M213)	MMC NSMC	STARCK
RT	0.50	0.47	0.48	0.50	0.36	0.27
1300 °C	0.50	0.43	0.53	0.65	0.49	0.61
1500 °C	0.56	0.69	0.60	0.59	0.57	0.60
1800 °C	0.54	0.70	0.53	0.64	0.64	0.61

## Summary & Outlook

- Extensive characterization of the thermal shock behavior of W (interaction between material properties and damage behavior)
- Synergistic effects of particle and transient heat loads on thermal shock performance of W (H/He embrittlement, microstructural changes)
- Development of advanced tungsten materials with improved micro-structure
- Characterization of commercially available and new developed W grades
  
- Selection of W reference materials/samples for n-irradiation
- Thermal shock exposure of W reference materials after n-irradiation/comparison with un-irradiated damage response
- Thermal shock exposure of new developed W grades (e.g. PIM, Wf/W)
- Synergistic effects of particle and transient heat loads on thermal shock performance of reference W and new developed W grades after n-irradiation
- Characterization of the thermal and mechanical properties after n-irradiation