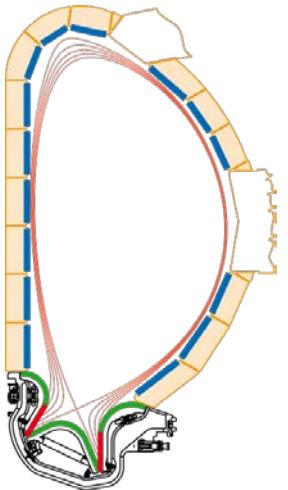


# Fundamental aspects of beryllium compound formation and erosion and hydrogen retention in beryllium

Christian Linsmeier

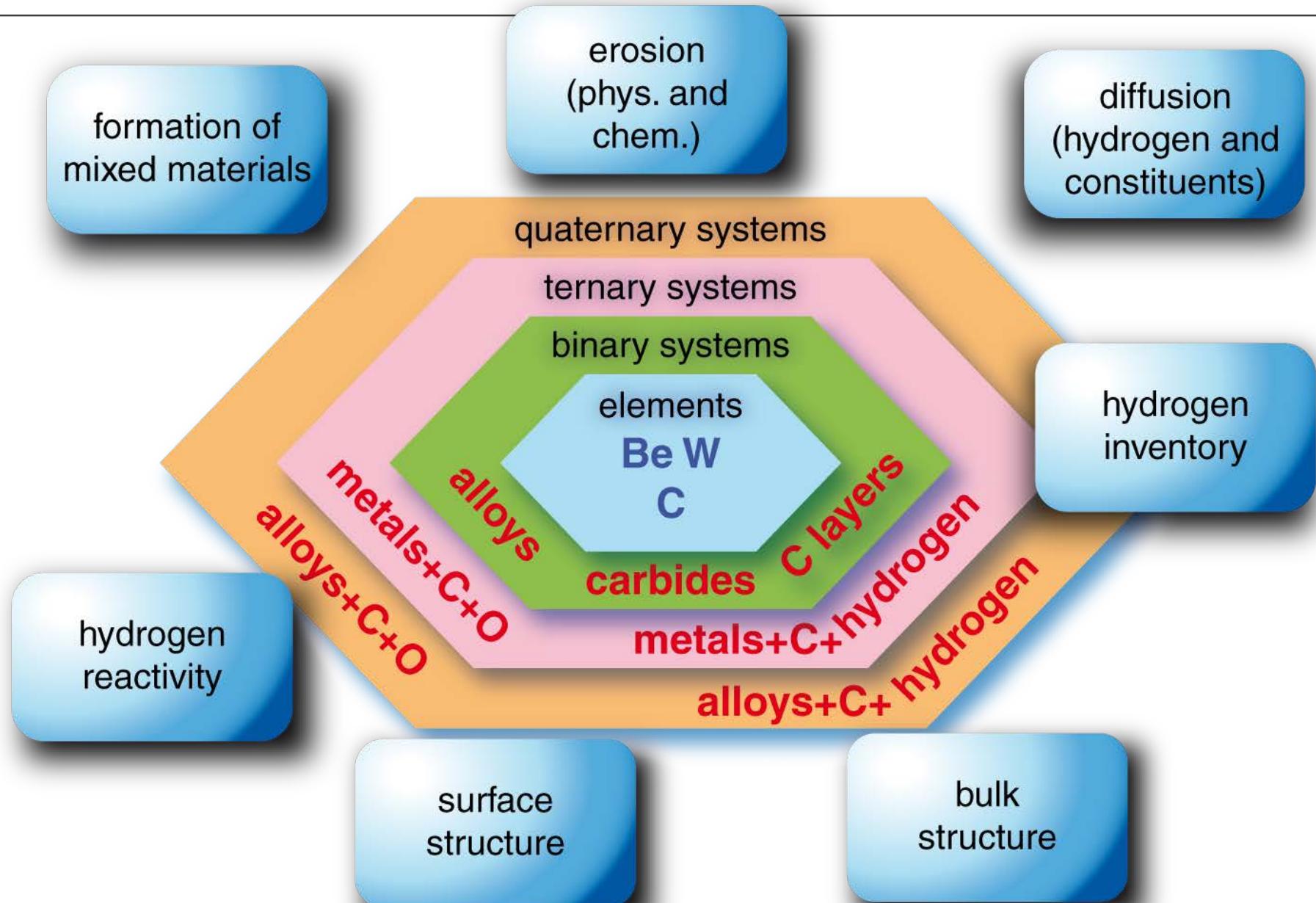
P. Goldstraß, A. Wiltner, F. Kost, M. Reinelt, M. Oberkofler,  
M. Köppen, R. Piechoczek  
A. Allouche, Y. Ferro (*Aix-Marseille Université*)

- 1. Processes at the ITER first wall**
- 2. Investigated Be-based systems**
- 3. Thermally induced reactions (examples)**
  - C/Be, Be/C
  - W/Be, Be/W
- 4. Ion-induced reactions (examples)**
  - $\text{C}^+ \rightarrow \text{Be}$ ,  $\text{CO}^+ \rightarrow \text{Be}$
  - $\text{N}^+ \rightarrow \text{Be}$
  - $\text{O}^+ \rightarrow \text{Be}_2\text{W}/\text{W}$
- 5. Modeling of surface reactions**
- 6. Hydrogen isotope retention and release**
- 7. Surrogates for Be? (separate presentation)**
- 8. Outlook**

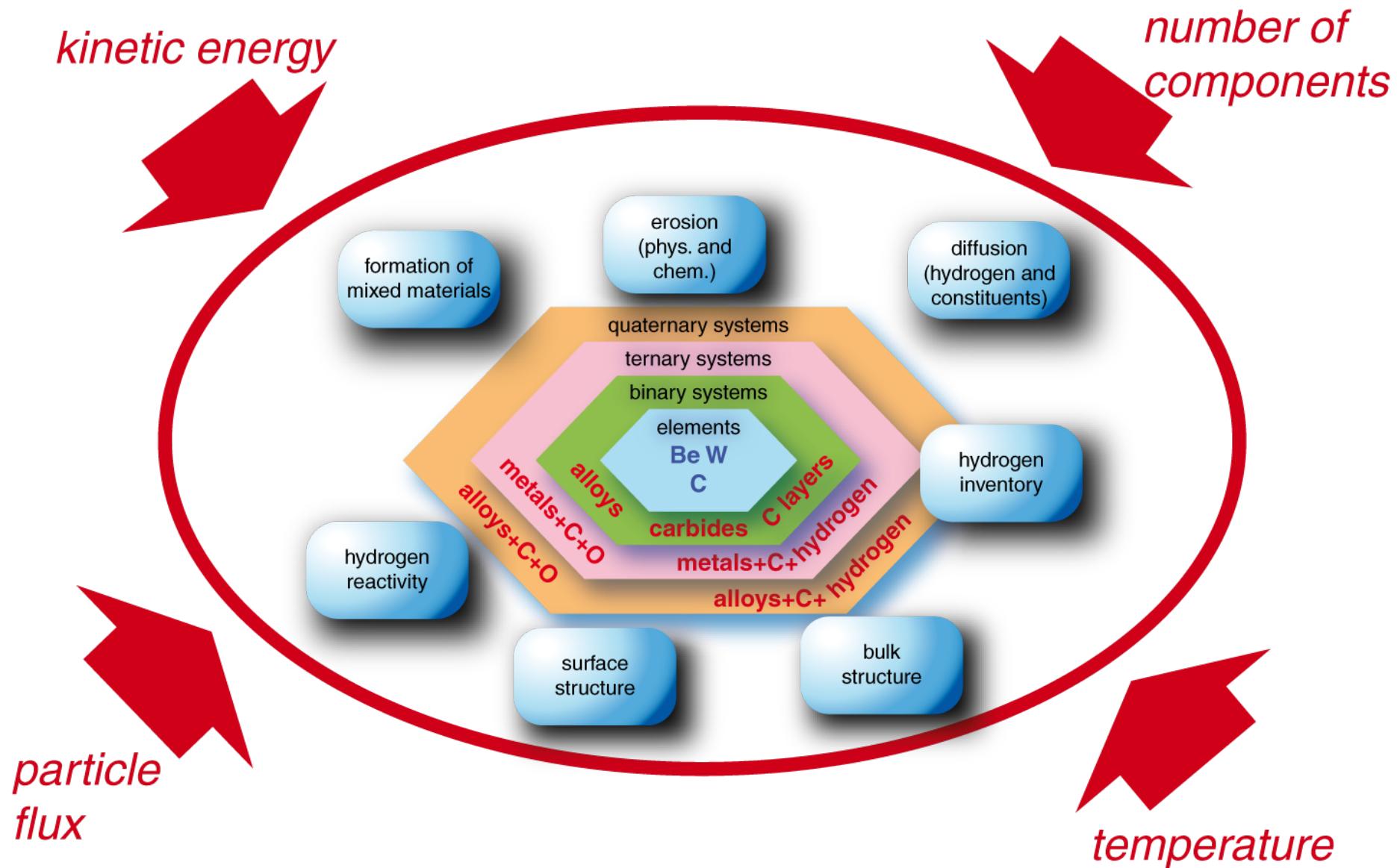


- First wall on ITER
    - carbon 55 m<sup>2</sup>
    - tungsten 140 m<sup>2</sup>
    - beryllium 690 m<sup>2</sup>
  - Variable local conditions (temperature, fluence, species...)
  - Erosion and redeposition, impurities:
    - mixed phases (e.g. carbides, oxides, nitrides, alloys)
  - Layers on metals influence hydrogen (isotope) inventory:
    - reaction, diffusion, desorption
  - Goal: qualitative and quantitative description of fundamental processes
    - formation and erosion of multi-component layers
    - influence of layers on hydrogen inventory
- **Include surface reactions in global integrated PWI model**

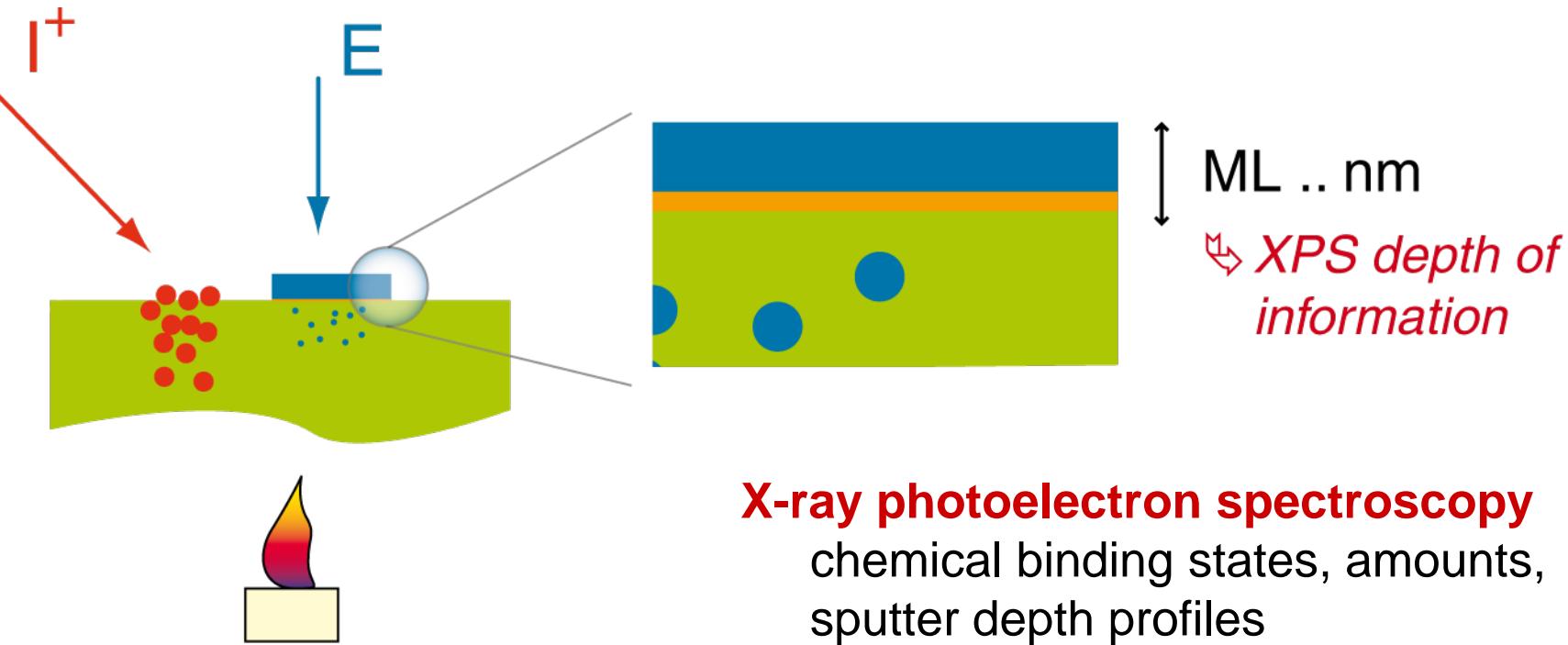
# Components and processes



# Components, processes and parameters



# Experimental approach



## Preparation and treatment conditions

base pressure  $\geq 2 \times 10^{-9}$  Pa

**X-ray photoelectron spectroscopy**  
chemical binding states, amounts,  
sputter depth profiles  
synchrotron: chemical depth profiles

## Accelerator-based techniques

amounts, depth profiles  
hydrogen isotope analysis (amounts,  
profiles)

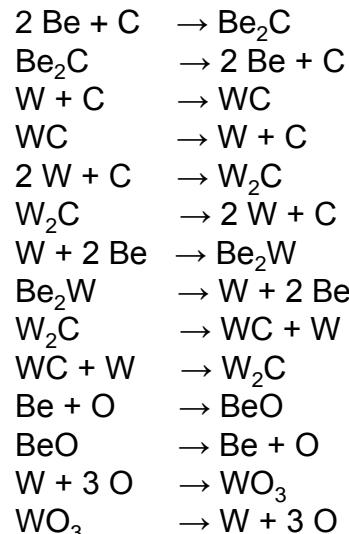
# Modeling approach: Description of chemistry

## 1. Define all substances

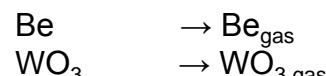
Be  
W  
C  
Be<sub>2</sub>C  
W<sub>2</sub>C  
WC  
Be<sub>2</sub>W  
Be<sub>12</sub>W  
Be<sub>gas</sub>  
BeO  
O<sub>ads</sub>  
WO<sub>3</sub>  
WO<sub>3,gas</sub>

+ Initial areal densities [#/m<sup>2</sup>]

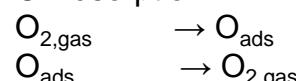
## 2. Elementary reactions



Sublimation:



O-Adsorption:



## 3. Define equations for reaction fluxes

$$\begin{aligned}
 \Gamma_1 \left[ \frac{1}{m^2 s} \right] &= [Be]^2 [C] k_1 \exp \frac{-\Delta E_1}{kT} & \text{with } k_1 \left[ \frac{m^4}{s} \right] \\
 \Gamma_2 \left[ \frac{1}{m^2 s} \right] &= [Be_2C] k_2 \exp \frac{-\Delta E_2}{kT} & \text{with } k_2 \left[ \frac{1}{s} \right]
 \end{aligned}$$

## 4. Define balances

Change of areal density of substance =  
 + all formation reaction fluxes  
 - all destruction reaction fluxes  
 ± all "non-chemical" fluxes

$$\frac{d[Be]}{dt} = -2\Gamma_1 + 2\Gamma_2 + \dots \quad \frac{d[Be_2C]}{dt} = +\Gamma_1 - \Gamma_2 + \dots$$

→ Set of ordinary differential equations

$$y'(t) = f(t, y(t)), \quad \text{with initial value } y(t_0) = y_0$$

## 1. Binary Be-based systems

- C/Be, Be/C lab., DFT
- C<sup>+</sup> → Be lab.
- Be/W, W/Be lab., DFT
- N<sup>+</sup> → Be lab., DFT
- O<sub>at</sub>, O<sub>2</sub> → Be lab.

## 3. Ternary Be-based systems

- CO<sup>+</sup> → Be lab.
- O<sup>+</sup> → Be<sub>2</sub>W/W synchr.
- C/BeO/W synchr.
- Be/C/W, C or Be excess lab.
- C/Be/W, C or Be excess lab.
- Be/WO<sub>2</sub>, Be/WO<sub>3</sub> lab.
- C/W/Be synchr.
- WO<sub>x</sub>/Be synchr.

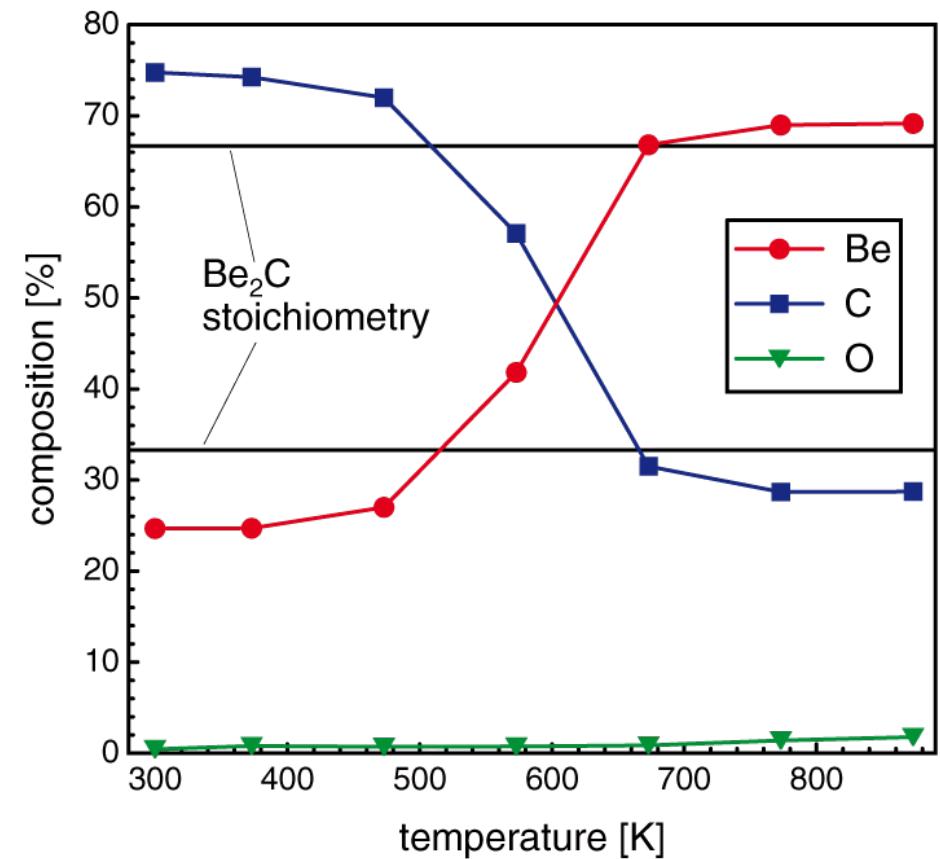
## 2. Hydrogen isotope retention and release

- D<sup>+</sup> → Be<sub>poly</sub>, Be(0001), Be(1 1 -2 0) lab., DFT
- D<sup>+</sup> → O/Be, BeO lab., DFT

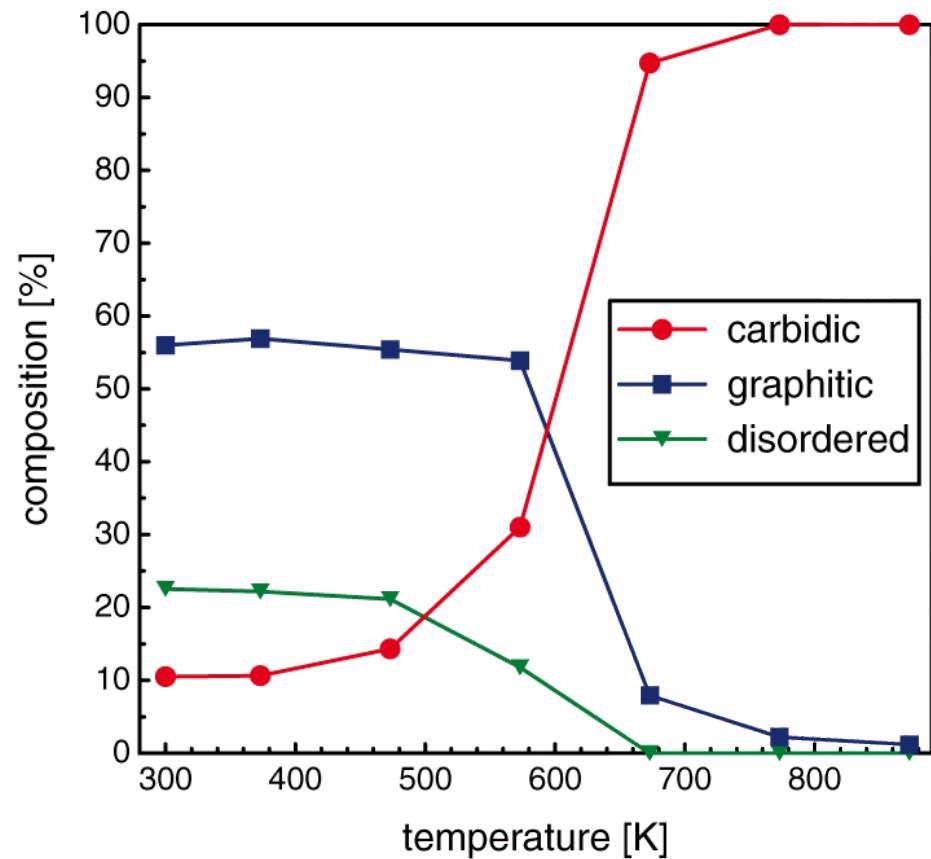
# Be—C thermally induced reactions

C amount:  $4.86 \times 10^{16} \text{ cm}^{-2}$  ( $\approx 5.3 \text{ nm}$ )

elemental composition

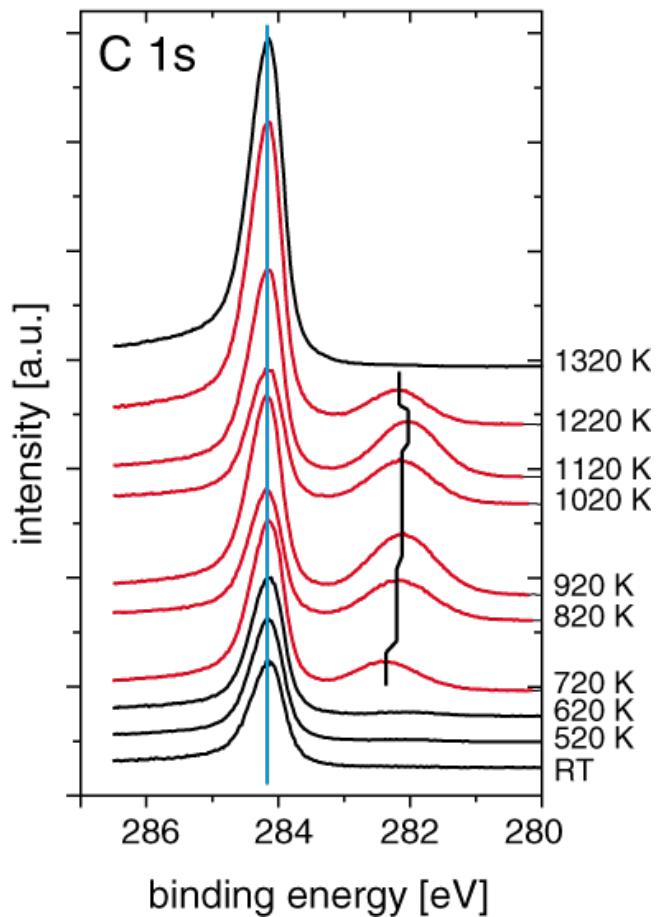


C 1s composition

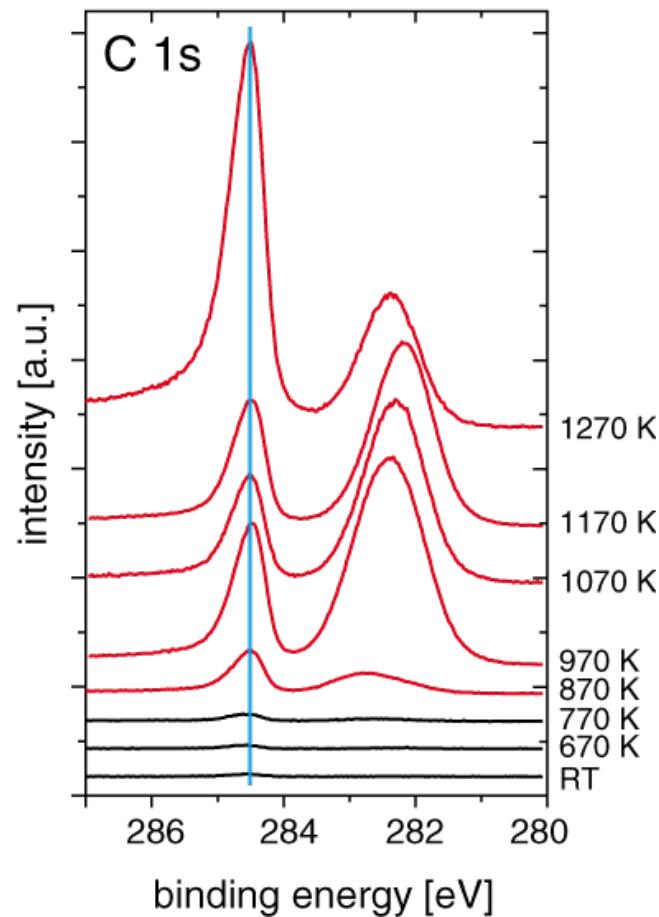


# Phases during annealing

1.35 nm Be on PG



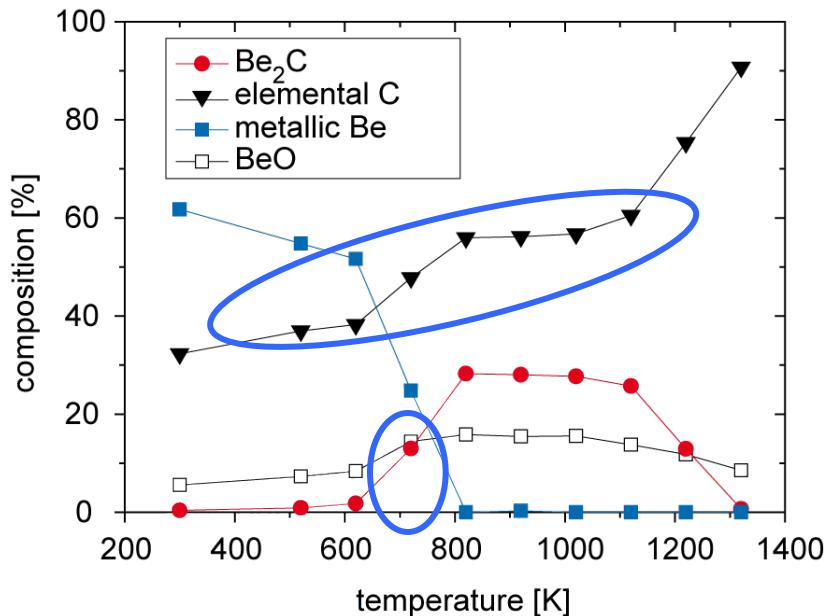
4.6 nm Be HOPG



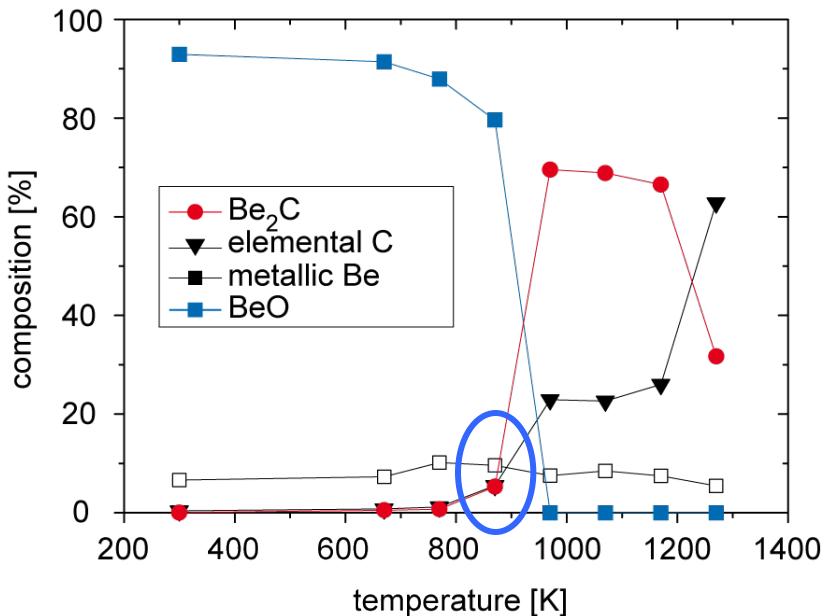
- PG: carbide formation at lower temp.
- Be<sub>2</sub>C peak position: shift due to island size

# Phases during annealing

1.35 nm Be on PG



4.6 nm Be HOPG



- Additional  $\text{Be}_2\text{C}$ : >720 K
- $\text{Be}_2\text{C}$  loss starts at 1170 K, no carbide above 1330 K
- Island growth

- Additional  $\text{Be}_2\text{C}$ : >870 K
- $\text{Be}_2\text{C}$  loss starts at 1270

# Carbide formation kinetics: Be on PG

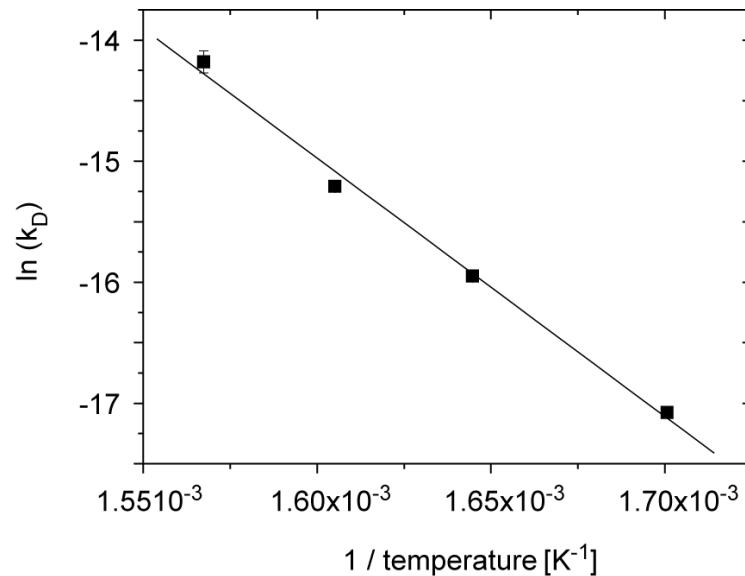
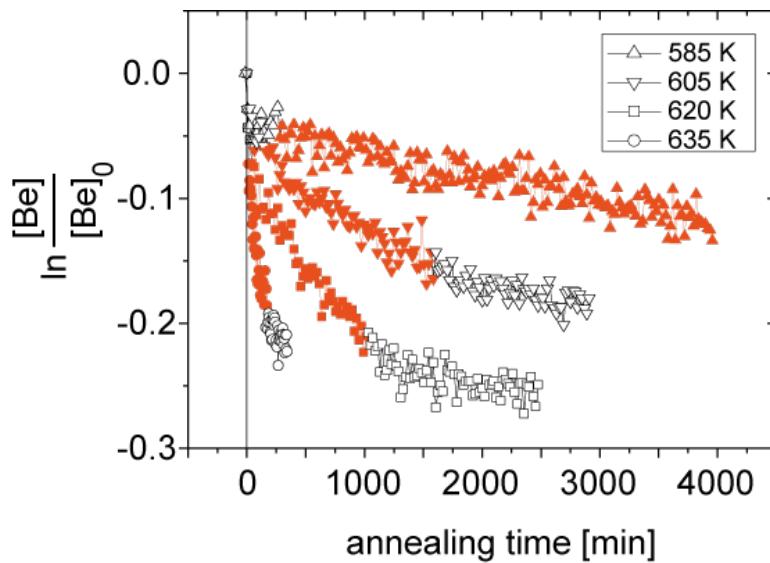
1st order reaction:

$$\ln \frac{[Be]}{[Be]_0} = -k_D(T) \cdot t$$

Activation energy:

$$\ln k_D(T) = -\frac{E_{act}}{k_B \cdot T} + \ln k_0$$

~1.9 nm Be on PG:

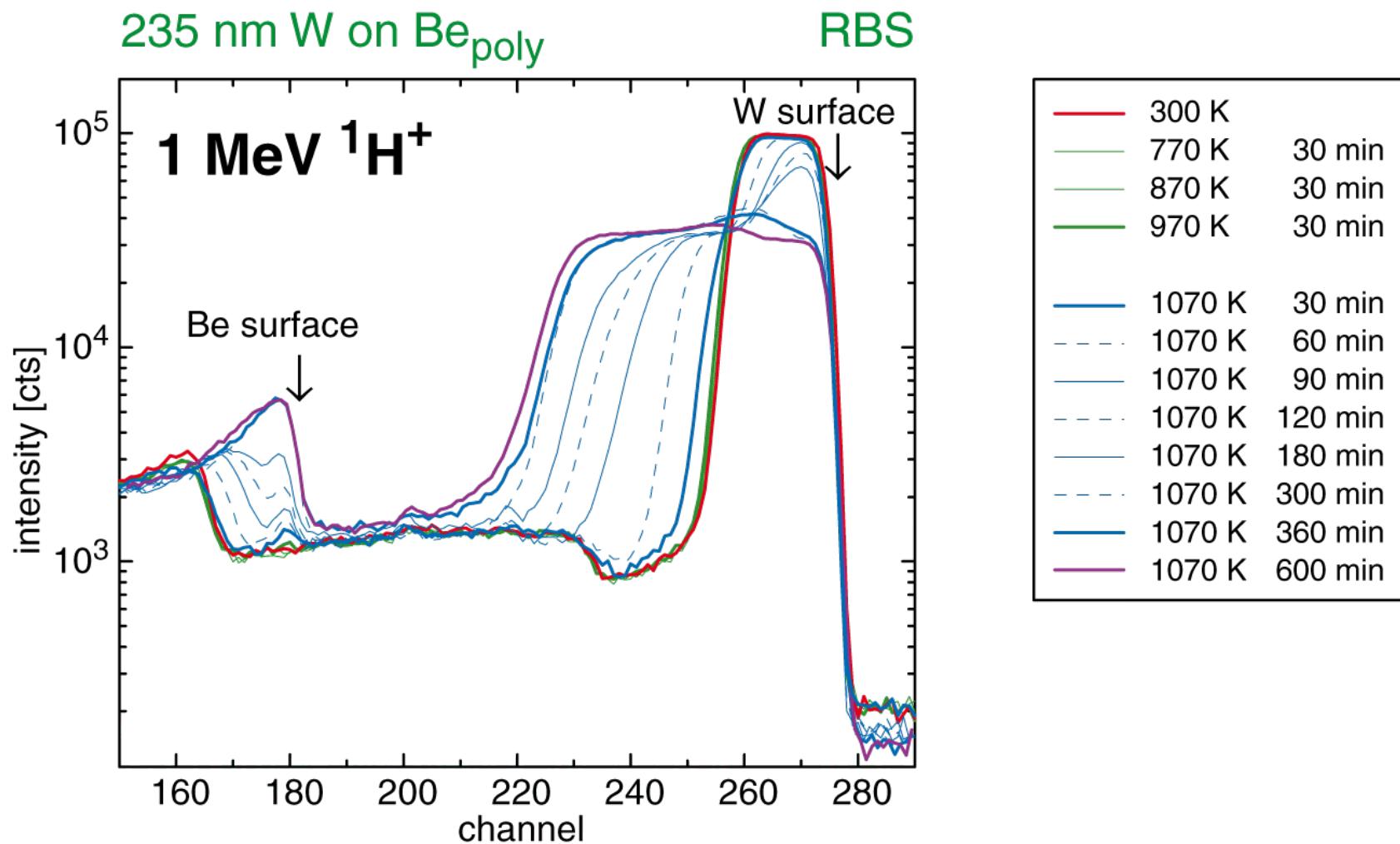


- Activation energy for pyrolytic graphite:  $1.8 \pm 0.1$  eV

# Summary: C—Be binary systems

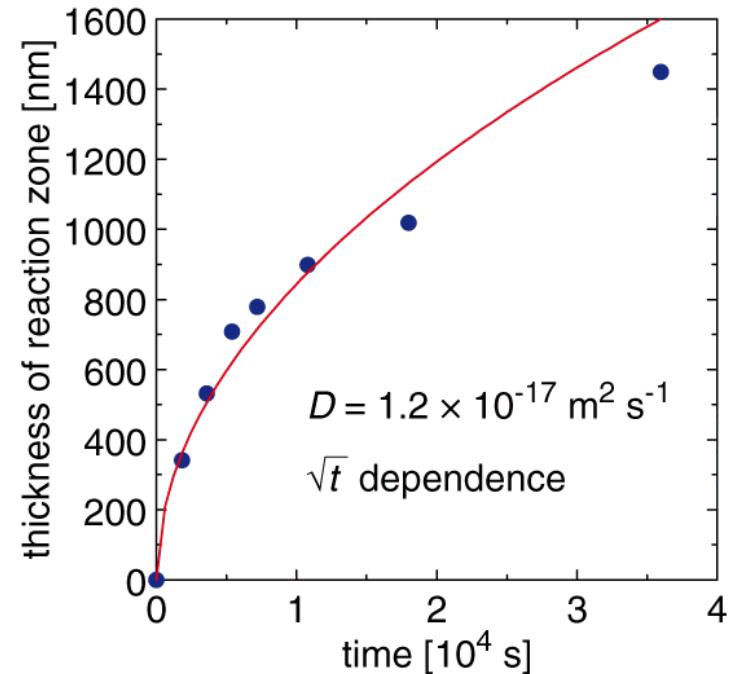
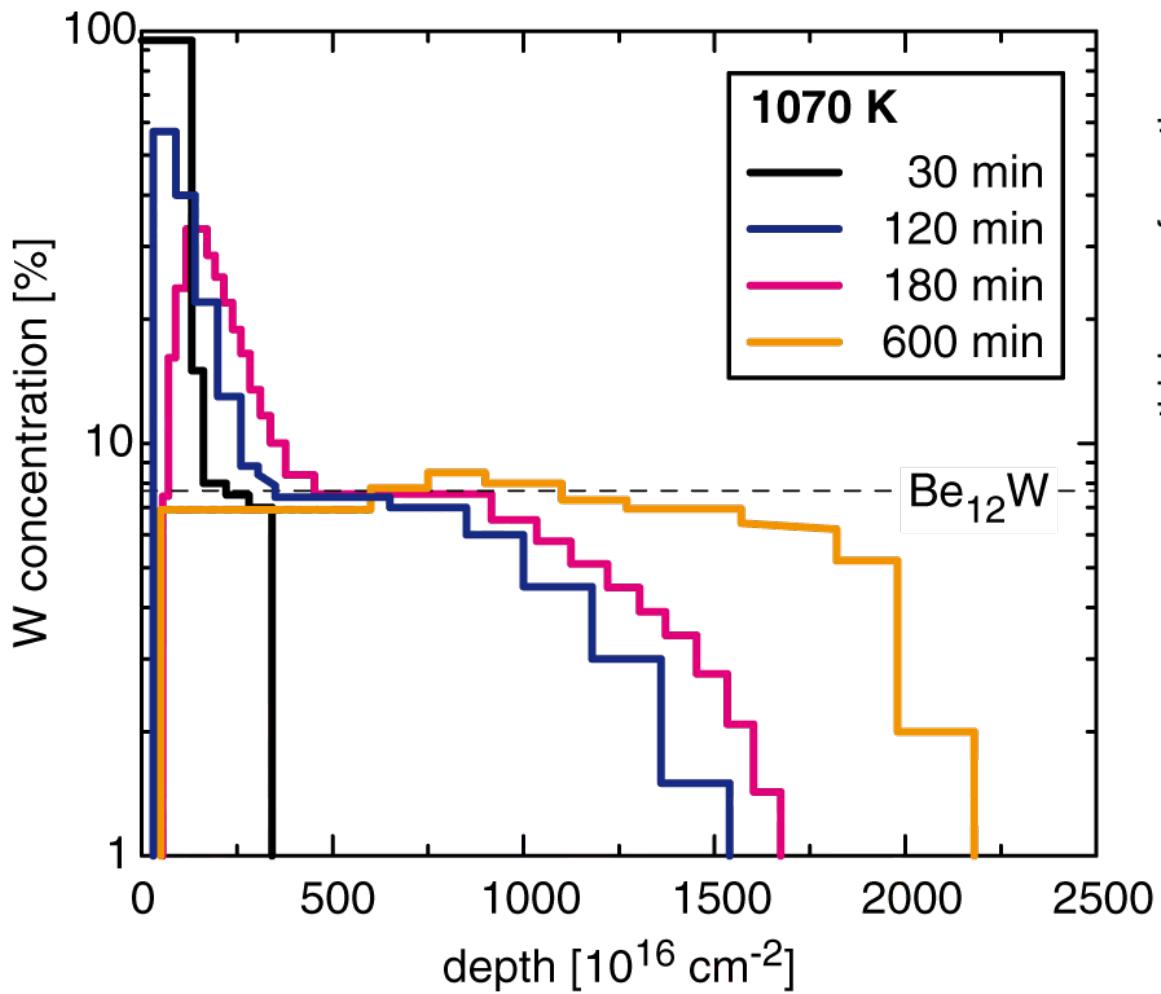
- Be<sub>2</sub>C at interface at 300 K deposition
- Be/graphite: Initially, island growth mode for Be on PG, above 0.6 nm layer growth
- <0.7 nm: carbide formation >570 K (surface diffusion)
- additional Be<sub>2</sub>C:
  - C/Be: >570 K
  - Be/PG: >720 K HOPG: >870 K
- loss of Be (Be<sub>2</sub>C decomp.):
  - both: >1330 K
- Activation energy for Be<sub>2</sub>C formation due to diffusion:
  - PG: 1.8 eV
  - HOPG: 2.1 eV
  - (structural change?)

# Be—W alloy formation



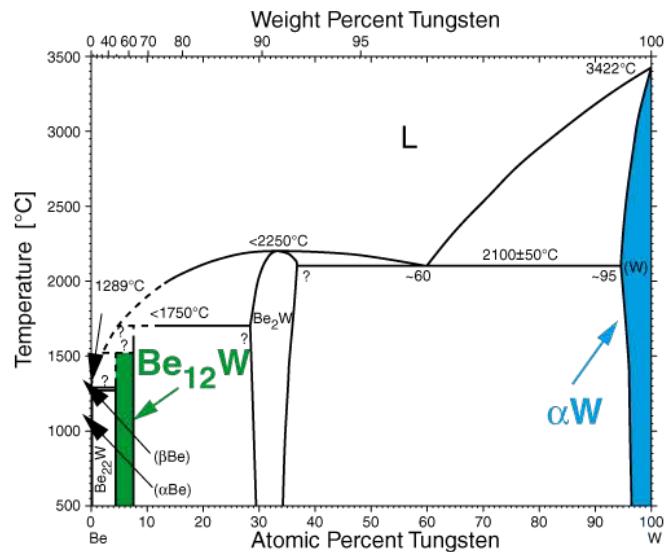
- no visible reaction up to 970 K
- alloy formation starts at 1070 K
- 600 min at 1070 K:  
constant Be/W phase

235 nm W on Be<sub>poly</sub>

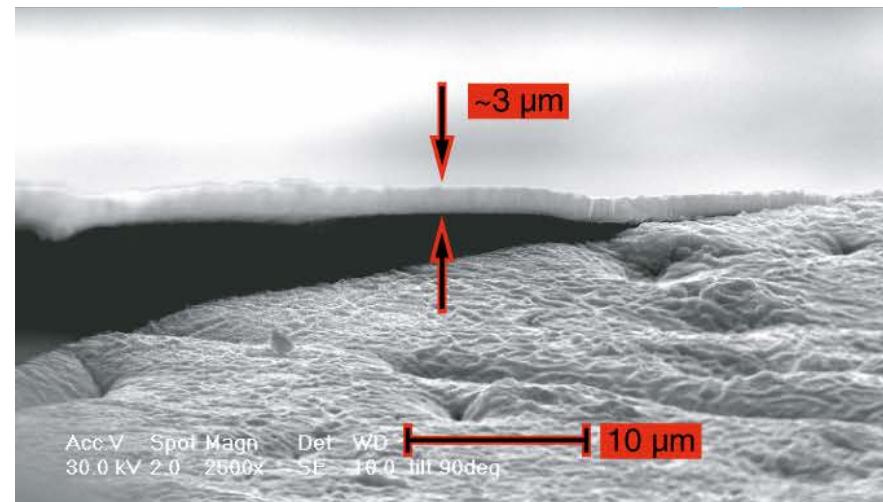


- Be<sub>12</sub>W final phase with  $T_m = <2020 \text{ K}$
- Be diffusion through W and Be-W alloy
- interaction is diffusion-controlled

# W / Be: Be<sub>12</sub>W phase

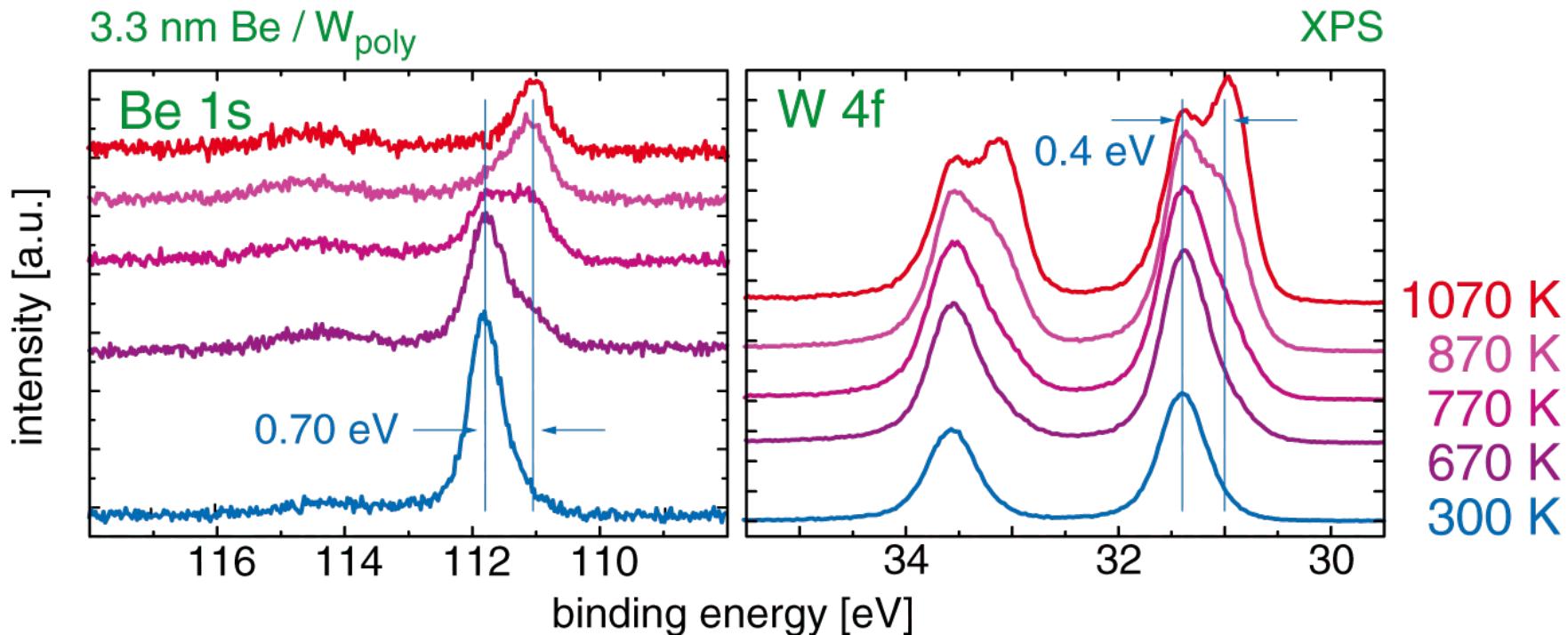


- formation of stable Be<sub>12</sub>W alloy phase above 1000 K
- W layer not dissolved in Be bulk
- Be<sub>12</sub>W melting point <2000 K

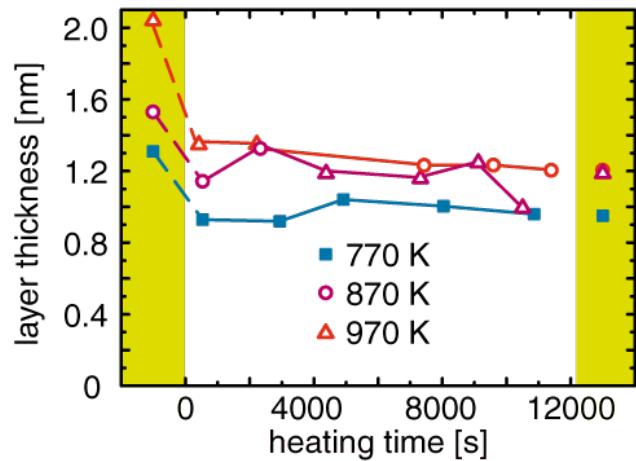


- at 1170 K a ~3 μm Be<sub>12</sub>W layer detaches from bulk Be
- risk of large impurity influx!

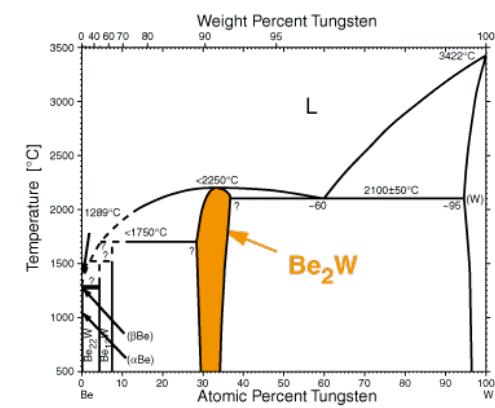
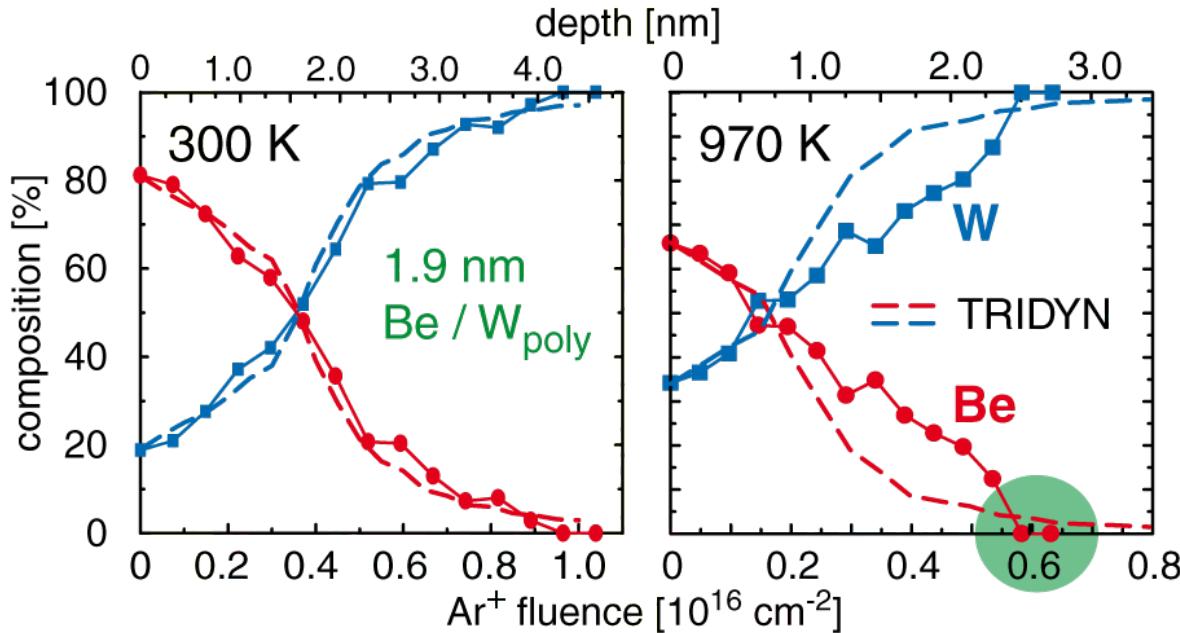
# Be / W: $\text{Be}_2\text{W}$ phase formation



- above 770 K: alloy dominates
- alloy peaks in core levels (Be 1s, W 4f) and valence band
- above 970 K:  $\text{Be}_2\text{W}$  stoichiometry
- Be intensity loss > 570 K

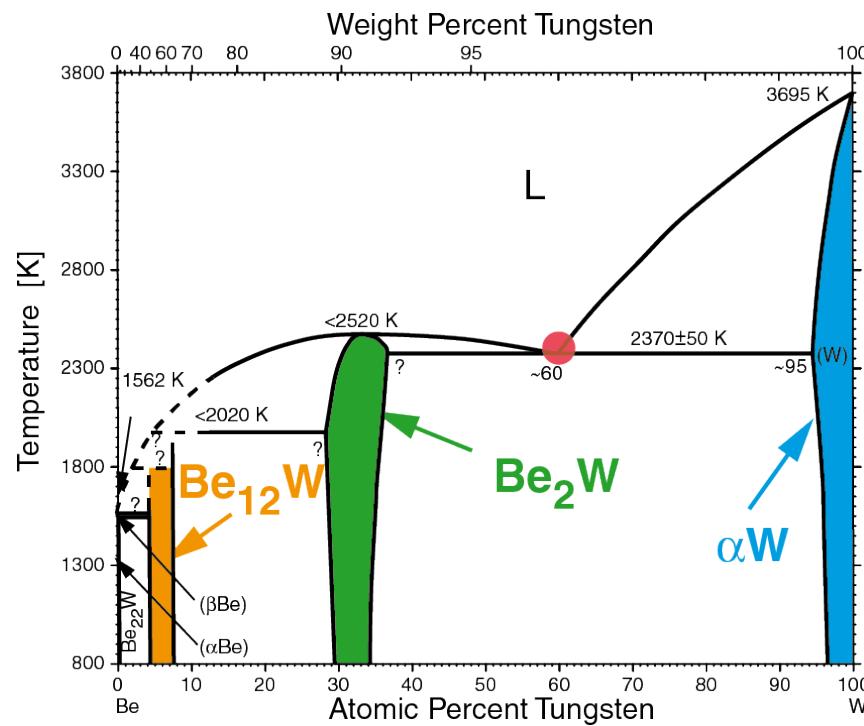


- alloy limited to 1-2 nm (independent of initial Be thickness)
- excess Be: NO dissolution in bulk, evaporation
- sublimation faster than diffusion



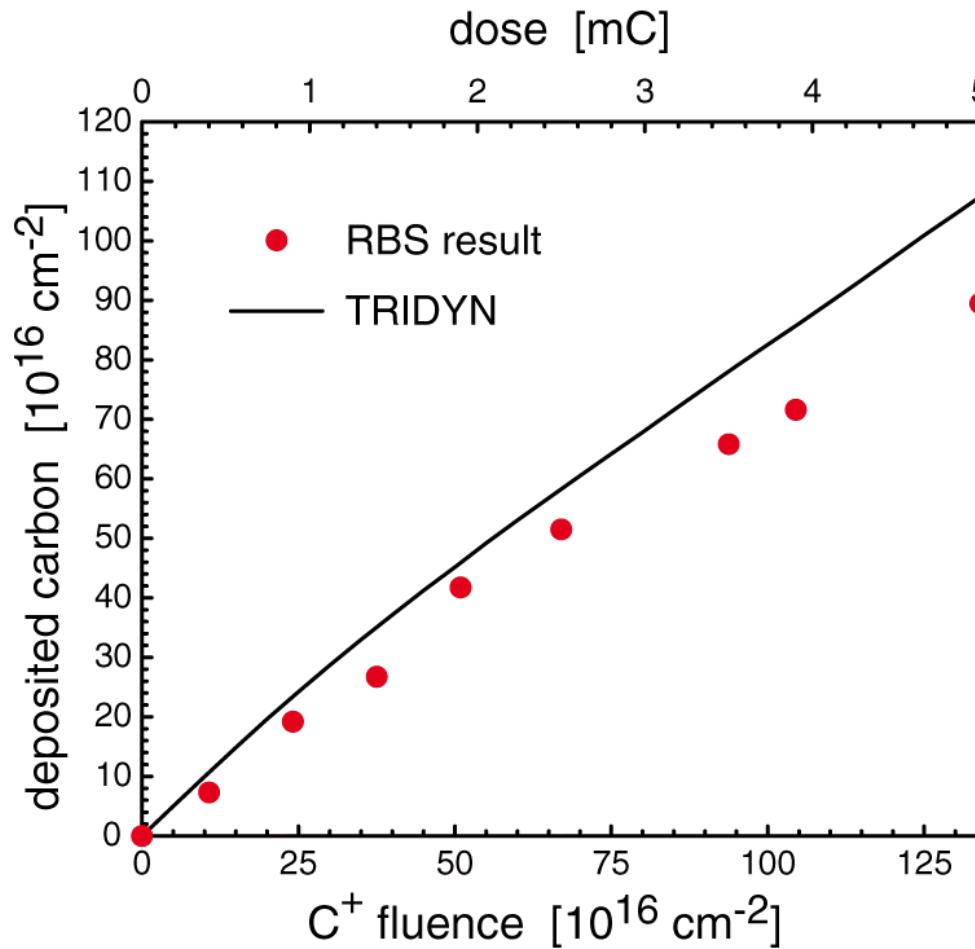
## Alloy formation depends on:

- Temperature
- Deposited amounts and sequence
- Flux balance: deposition, sublimation, erosion fluxes

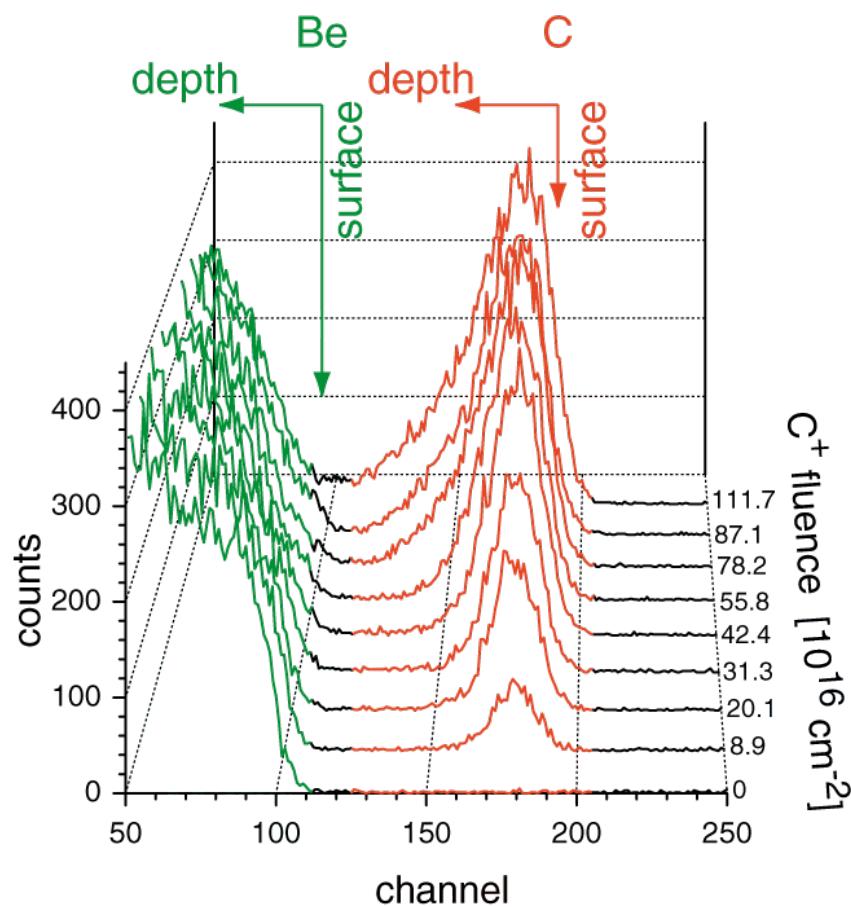


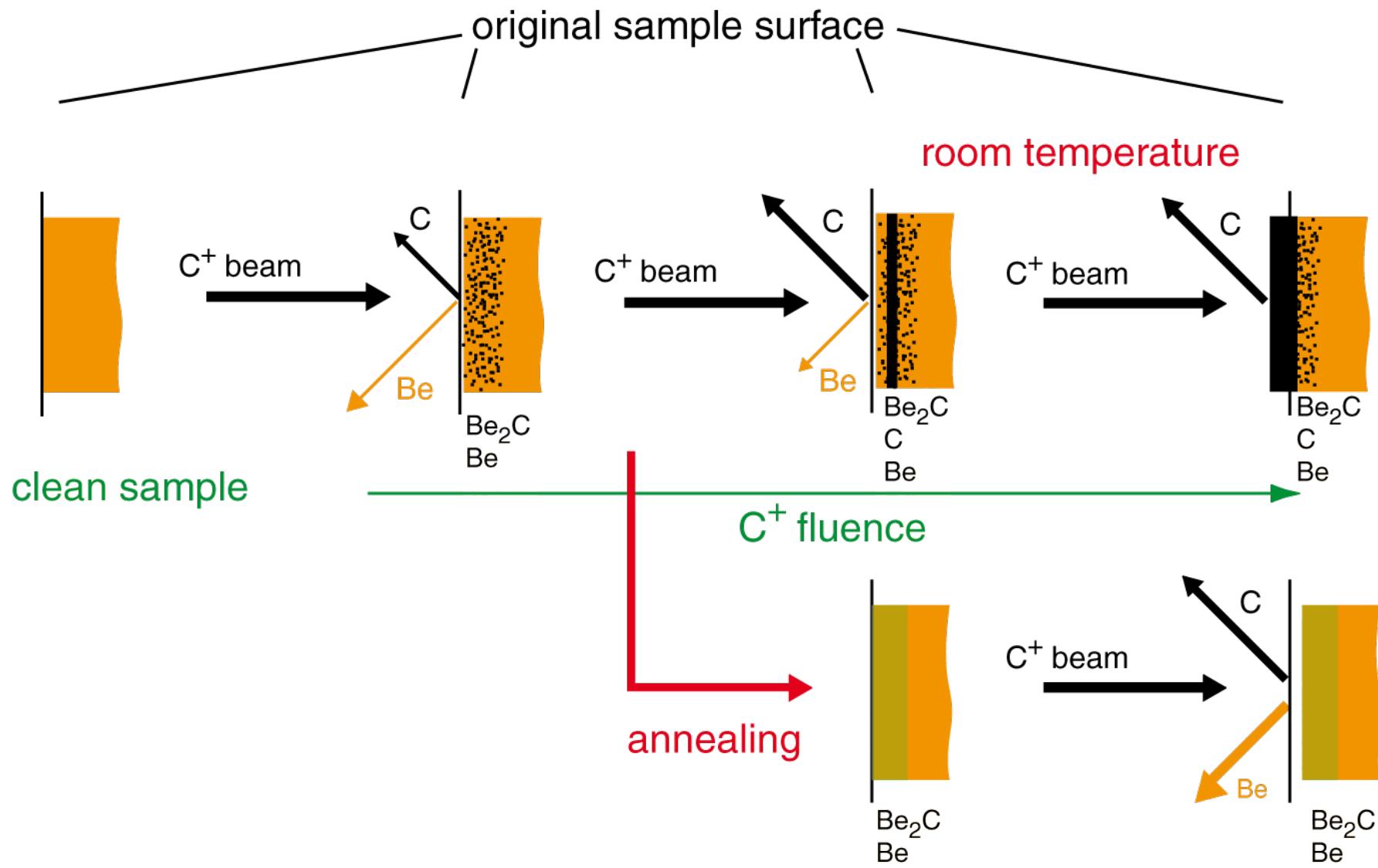
# $C^+ \rightarrow Be$ , $CO^+ \rightarrow Be$ ion-induced processes

5 keV  $C^+$ ,  $I \leq 50$  nA

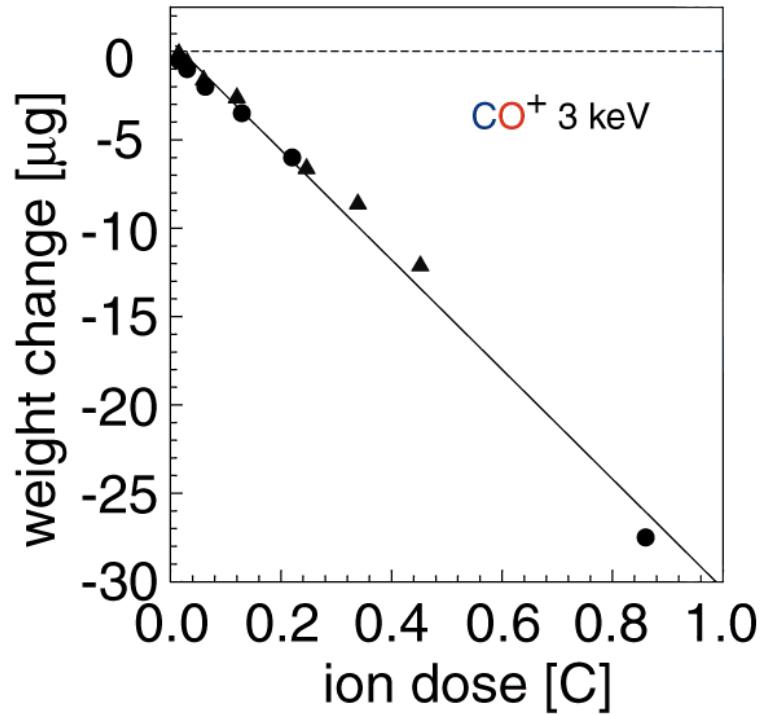
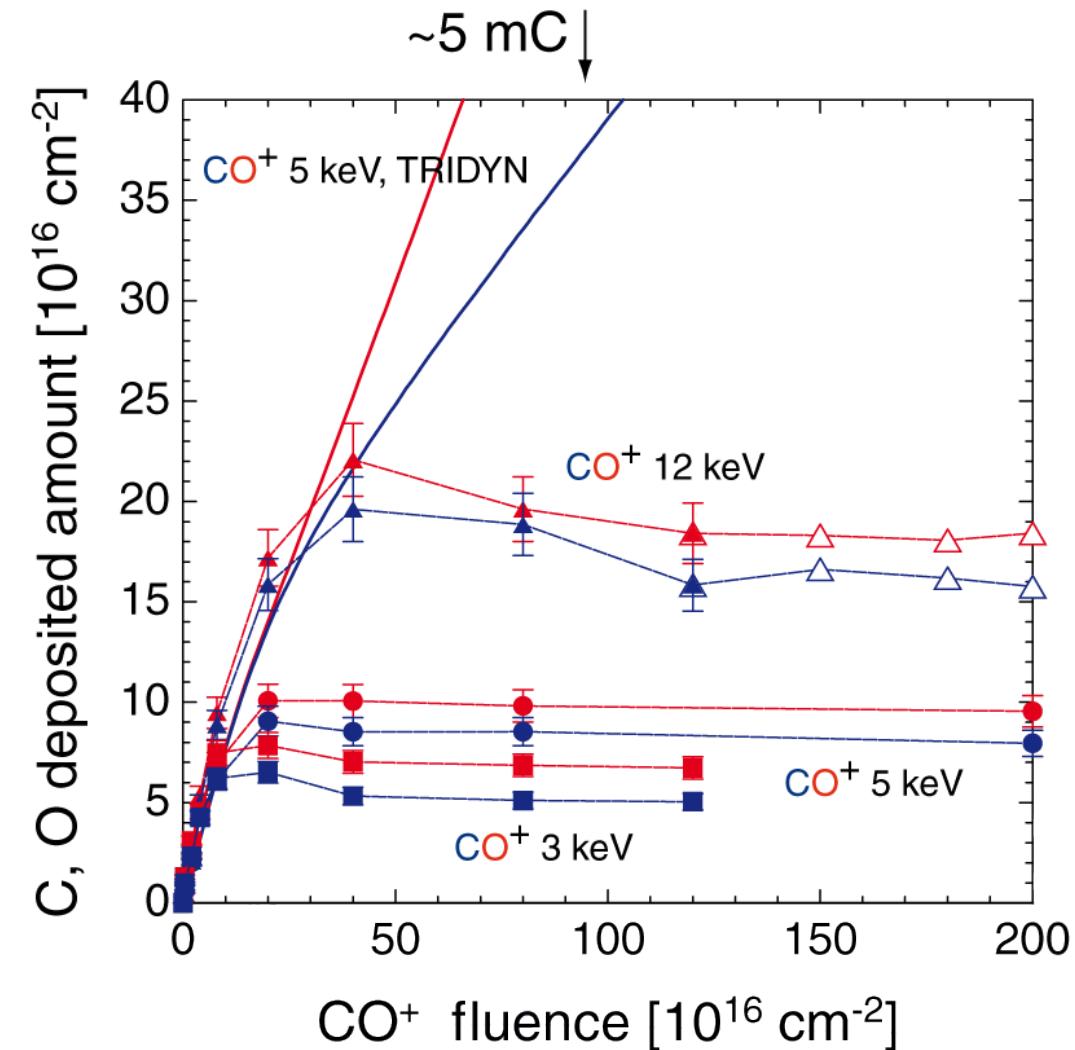


RBS spectra



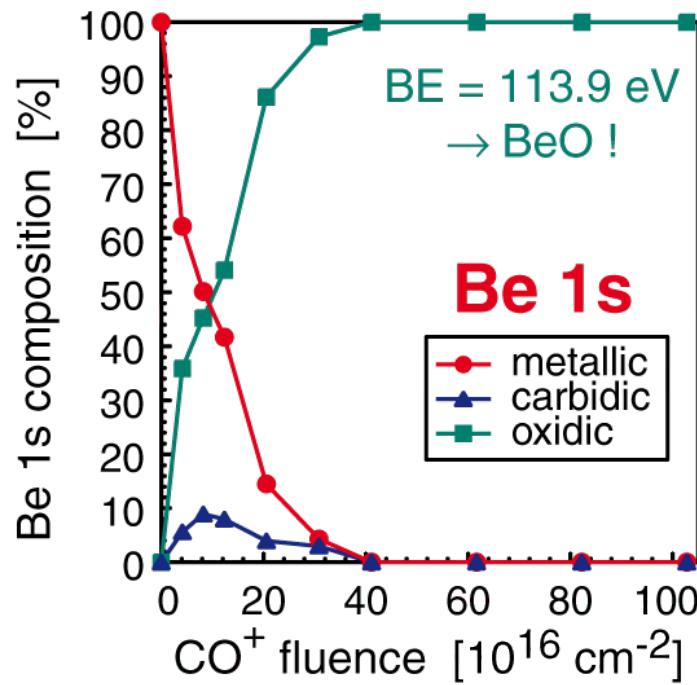
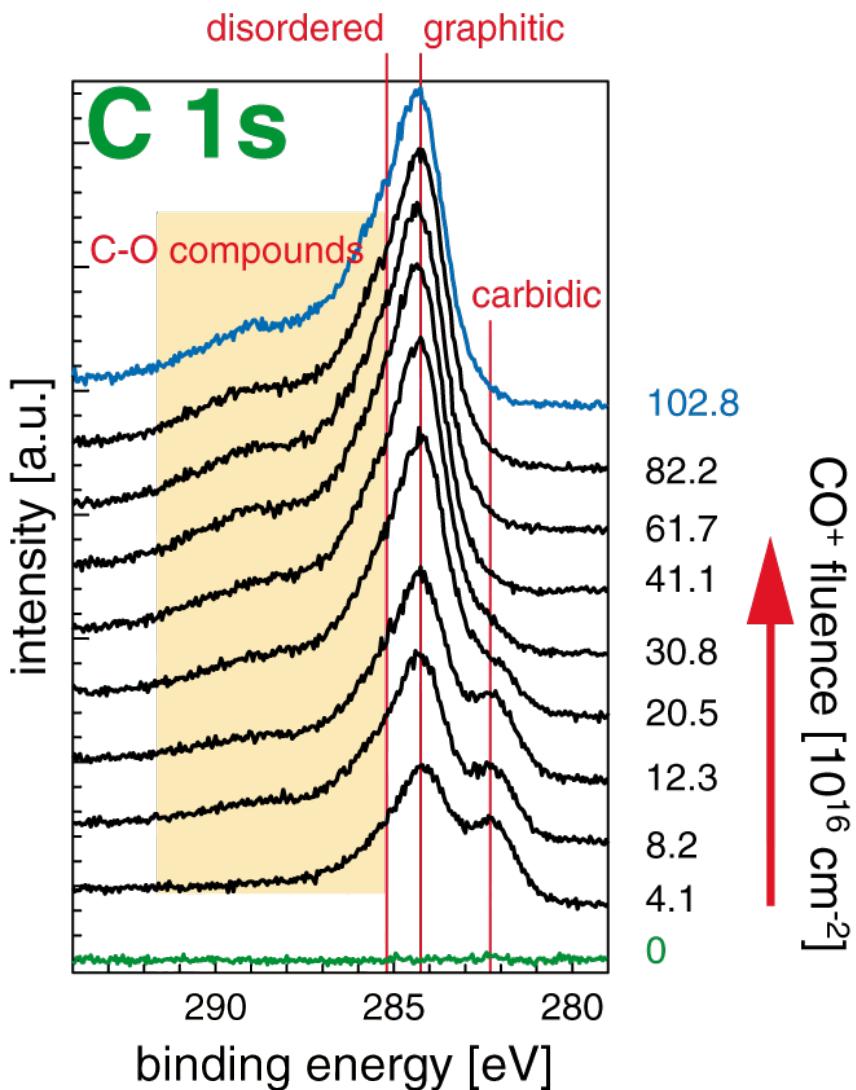


# $\text{CO}^+ \rightarrow \text{Be}$ : deposition / erosion

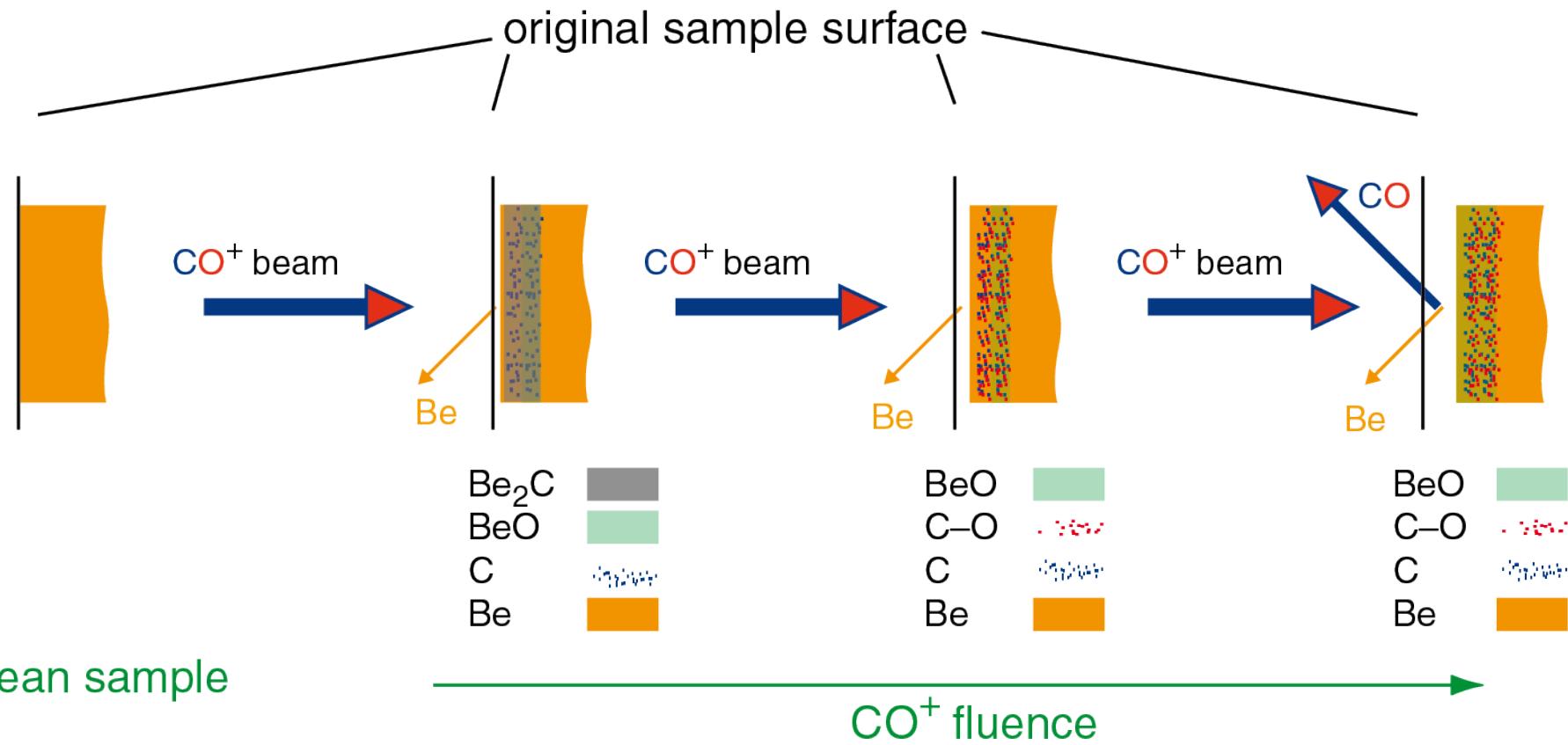


$Y_{\text{Be}} = 0.33$   
continuous erosion

# $\text{CO}^+ \rightarrow \text{Be}$ : chemical species



$$\Delta G_f^0(\text{Be}_2\text{C}) = -115 \text{ kJ/mol}$$
$$\Delta G_f^0(\text{BeO}) = -579 \text{ kJ/mol}$$



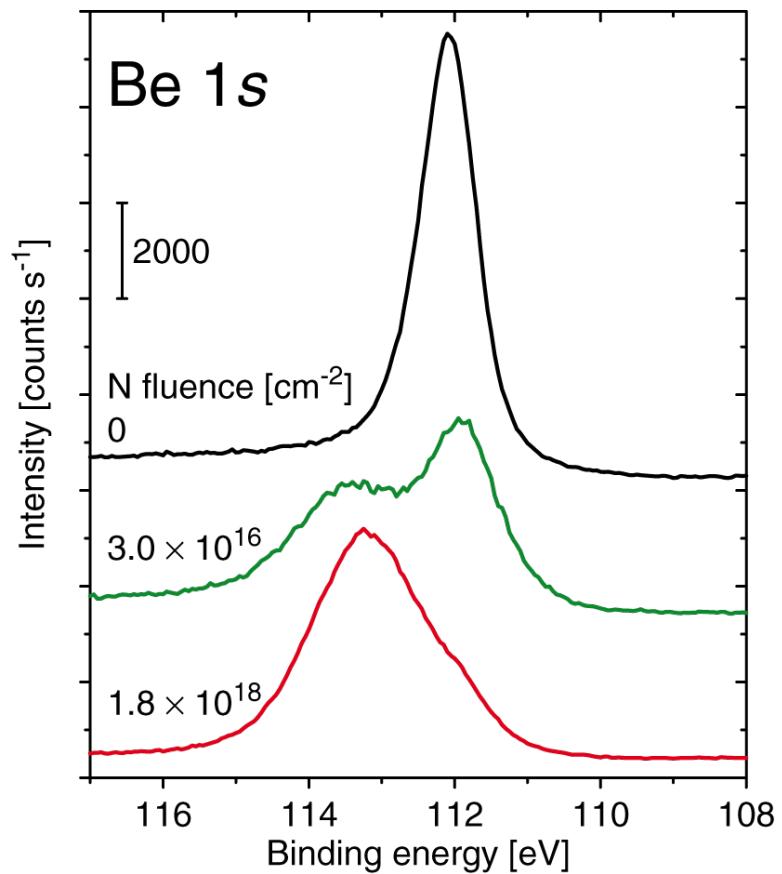
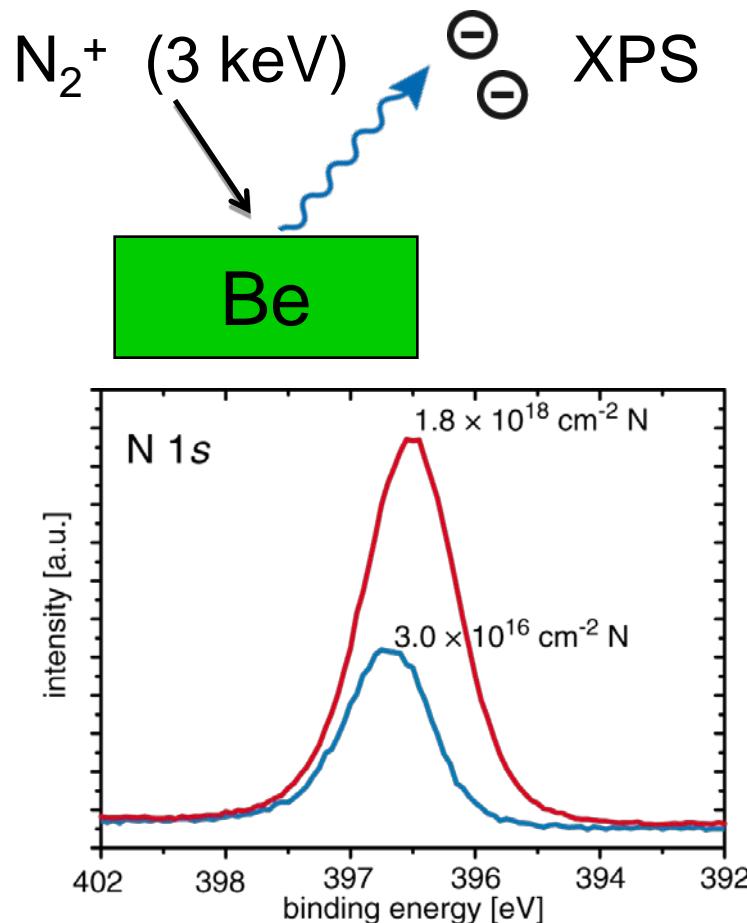
	Be	C	O
$Y_{\text{exp.}}$	0.33	1.00	1.00
$Y_{\text{TRIDYN}}$	0.36	0.24	0.29

## Ternary system opens new reaction pathways

- Binary system: purely kinematic process at 300 K
- Ternary system: chemical reaction path dominates
- Ion energy triggers compounds formation at 300 K
- Deposition-dominated situation can turn into erosion-dominated process

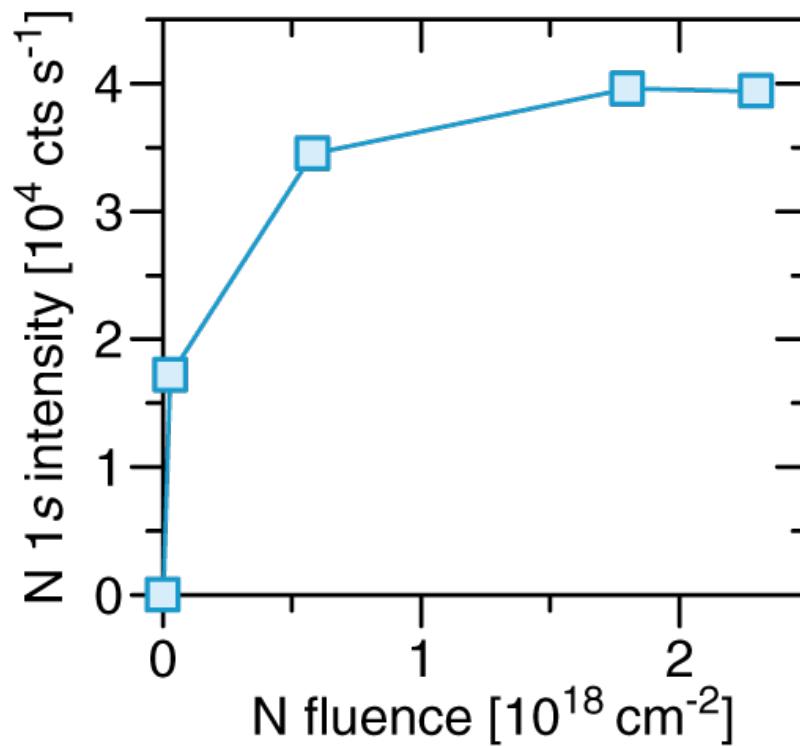
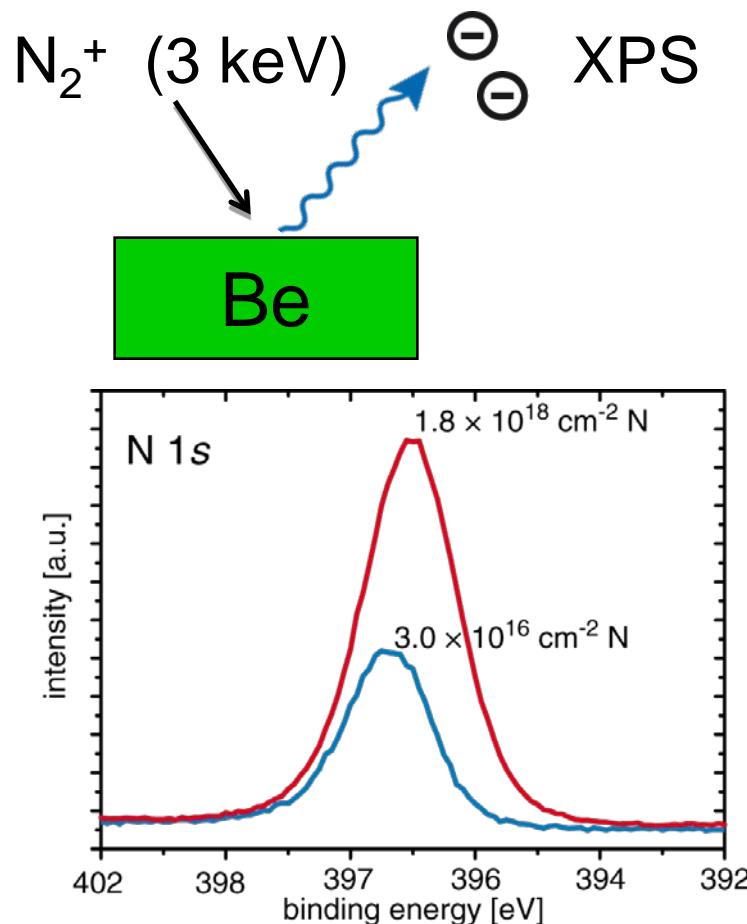


# Be—N phase formation



- nitride formation during N ion implantation
- shift of both Be 1s and N 1s peaks

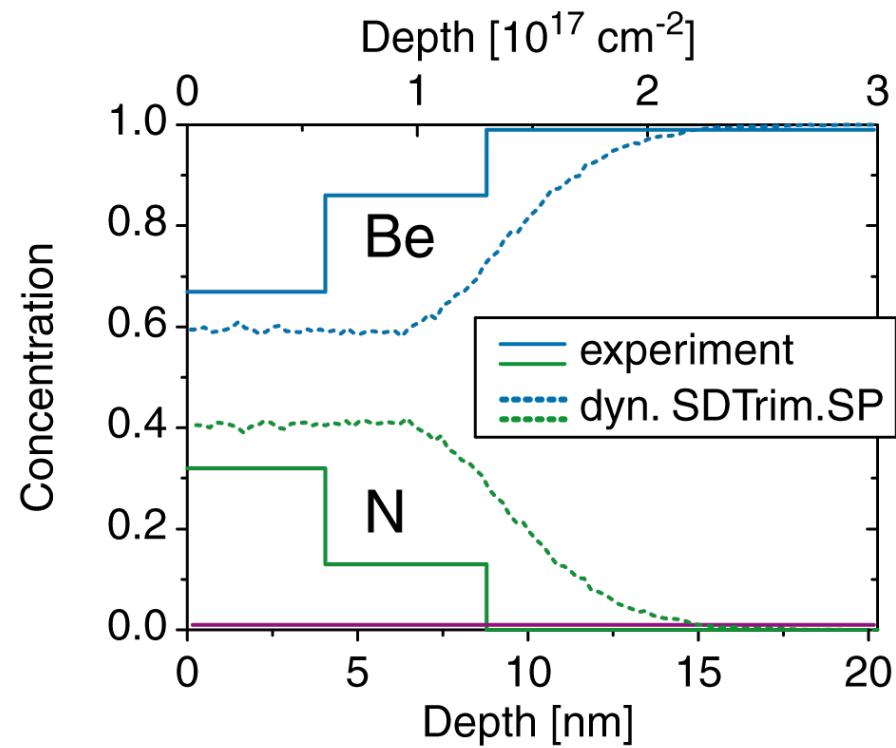
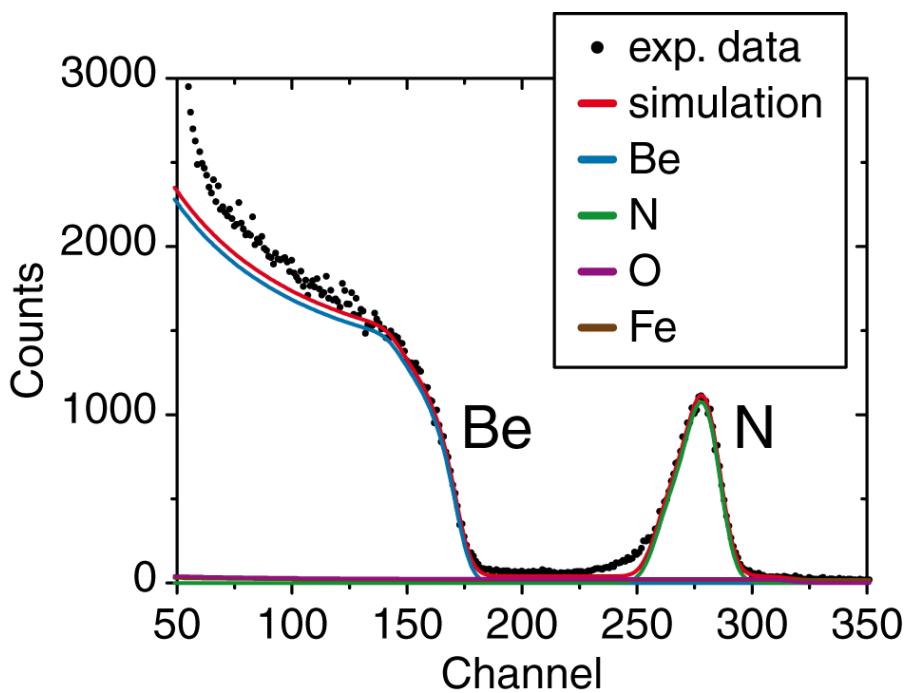
# Be—N phase formation and saturation



- nitride formation during N ion implantation
- shift of both Be 1s and N 1s peaks
- N saturates within implantation range (XPS and RBS)

# N depth distribution

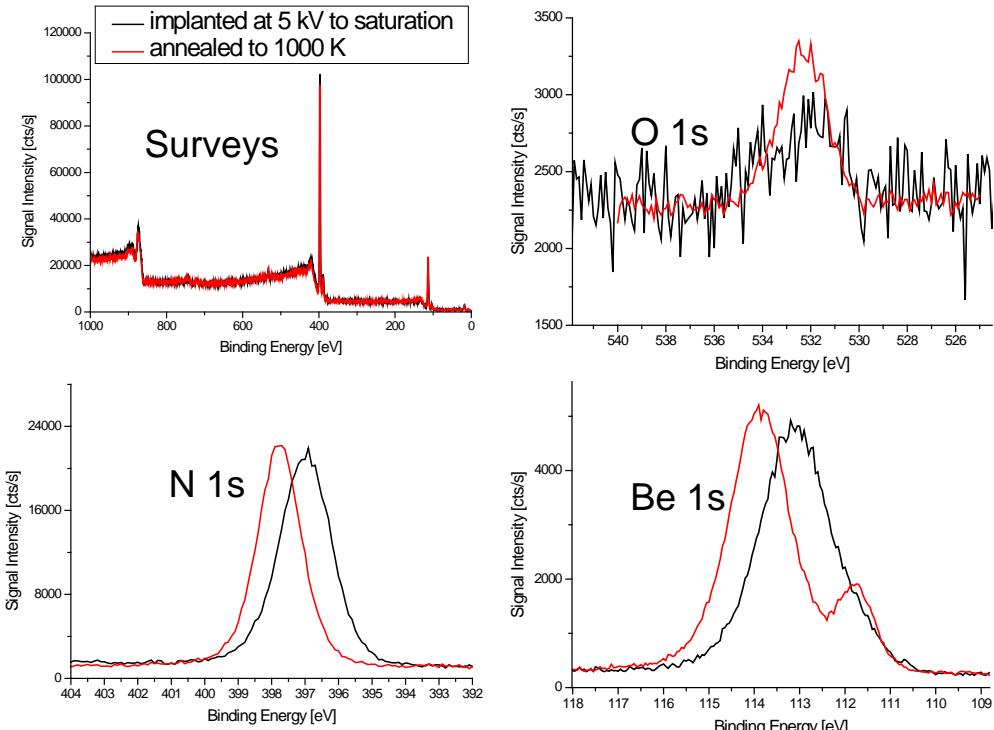
RBS 800 keV  ${}^4\text{He}$ ,  $\theta=105^\circ$



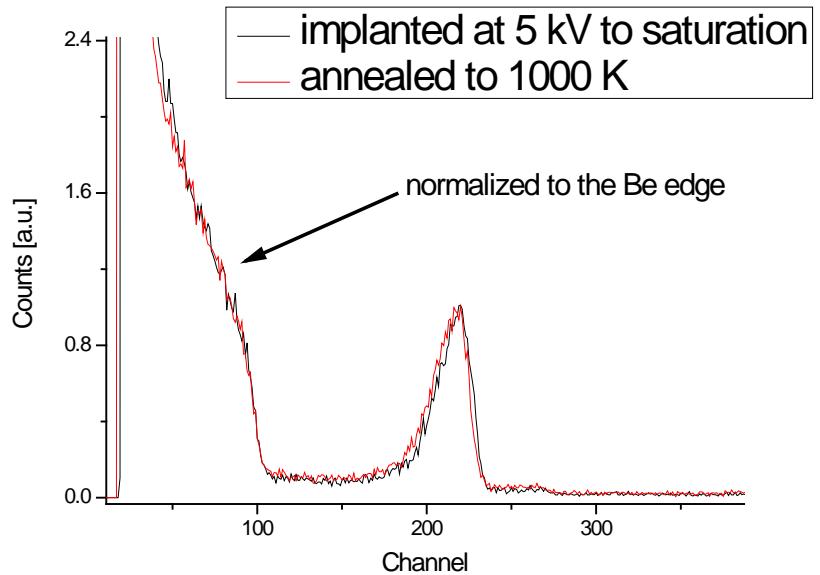
- $\text{N}_2^+$  assumed for simulation → reasonable agreement
- $\text{Be}_3\text{N}_2$  layer: 9 nm (> 1% N), density  $3 \times 10^{22} \text{ cm}^{-3}$  from literature
- implantation range  $\propto$  energy → JET (300 eV ions) < 1 nm nitride  
→ no degradation in electrical conductivity (cmp. to BeO)

# Thermal stability of Be—N phases

## XPS



## RBS



- annealing to 1000 K causes chemical shifts
- no significant reduction in the N content

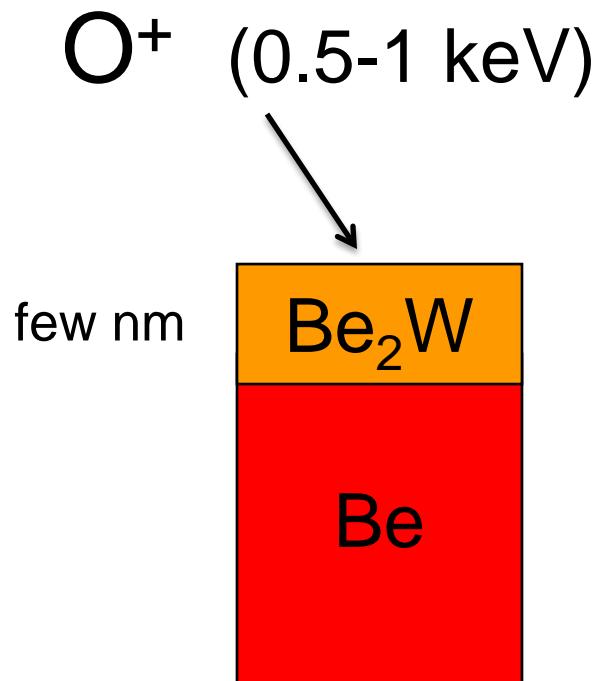
Literature:  $\text{Be}_3\text{N}_2$  very stable, solid  $\beta$  phase  
 $>1700$  K, melting point 2500 K

- N amount and depth profile after implantation and after annealing to 1000 K identical
- no decomposition of nitride
- no diffusion into the bulk

## Consequences of N<sub>2</sub> seeding in ITER

- Nitride formation within ion range
- No chemical erosion
- No volatile species, sudden gas release
- No increased hydrogen retention

$O^+ \rightarrow Be_2W/W$   
chemically resolved depth profiling

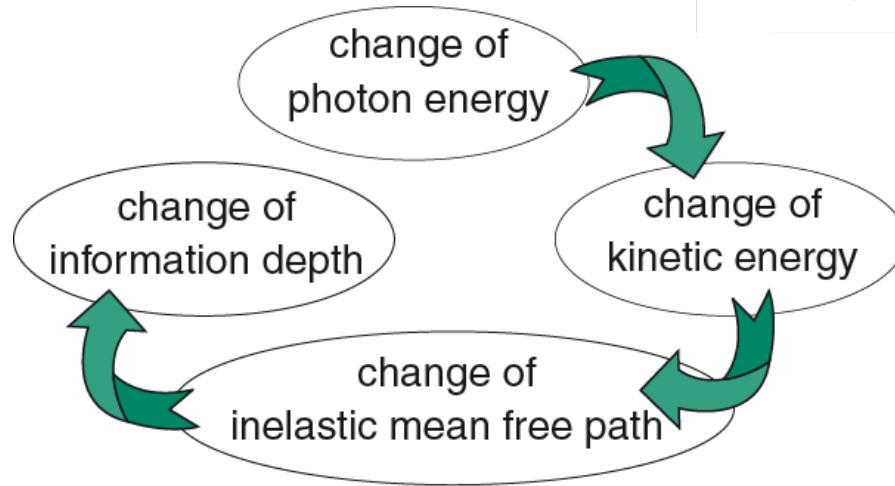
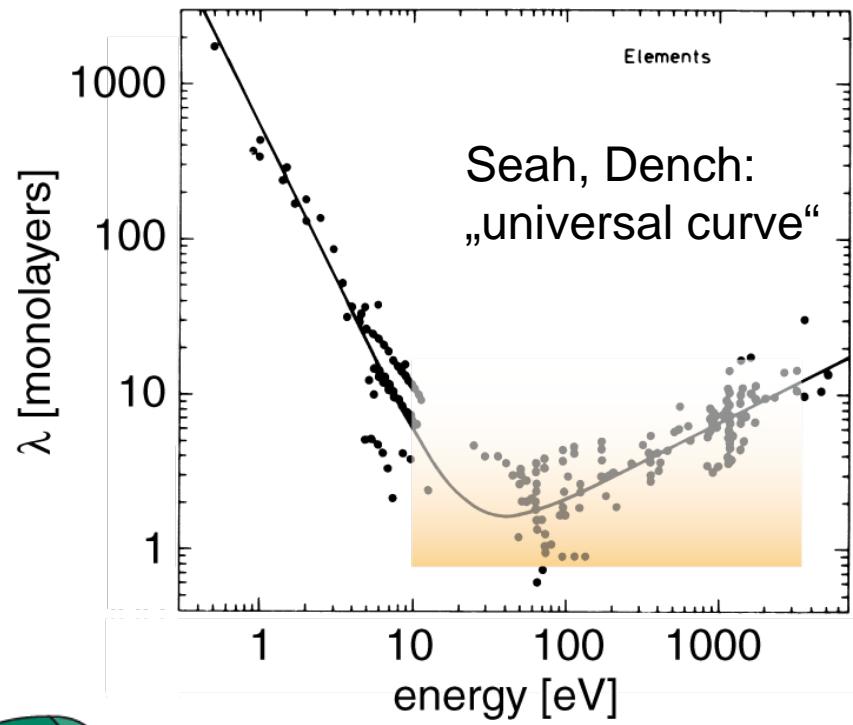


1.  $Be_2W$  preparation (W deposition on Be, 900 K annealing)
2. Implantation of O ions at 1 kV
3. Annealing at 600 K
4. O ion implantation at 500 V

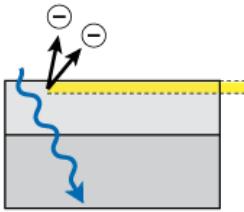
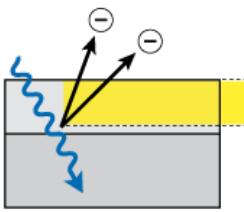
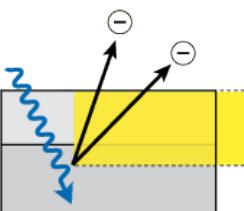
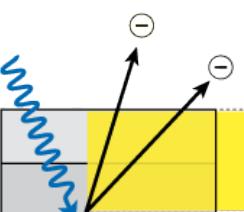
XPS analysis at BESSY II (6 depths, Be 1s, W 4f, O 1s, Au 4f)

# Depth-resolved XPS chemical analysis

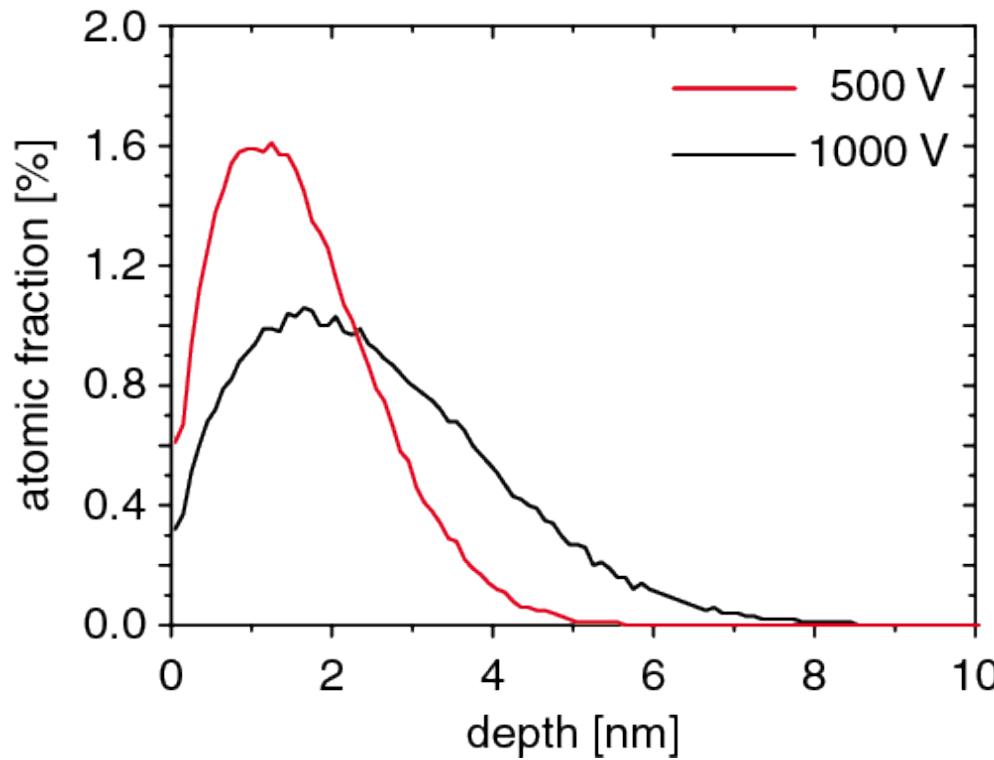
$$E_{\text{kin}} = h\nu - E_B + \phi$$



# Depth-resolved XPS

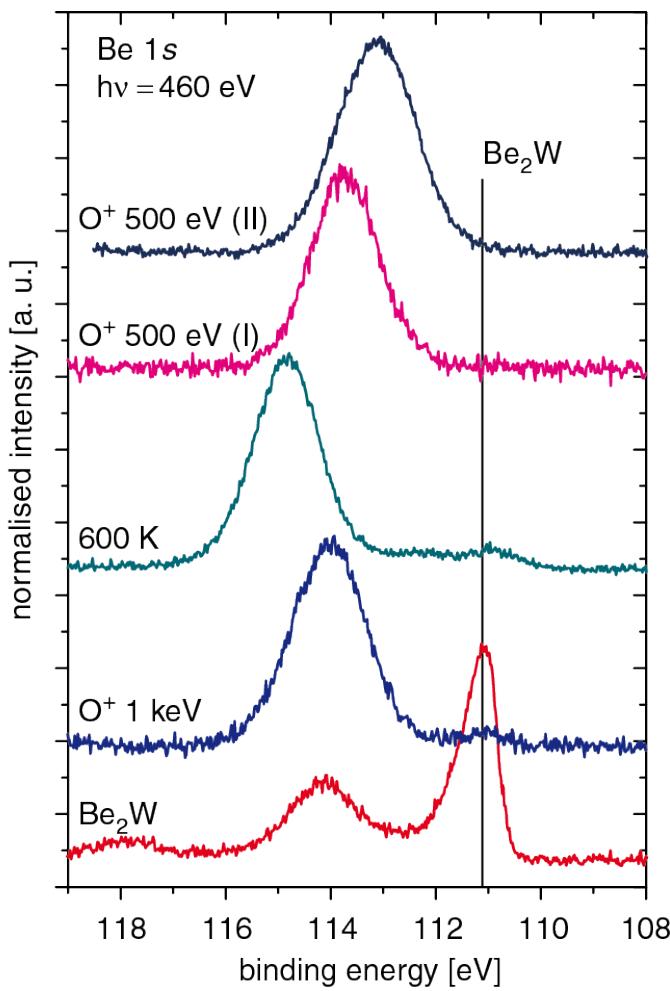
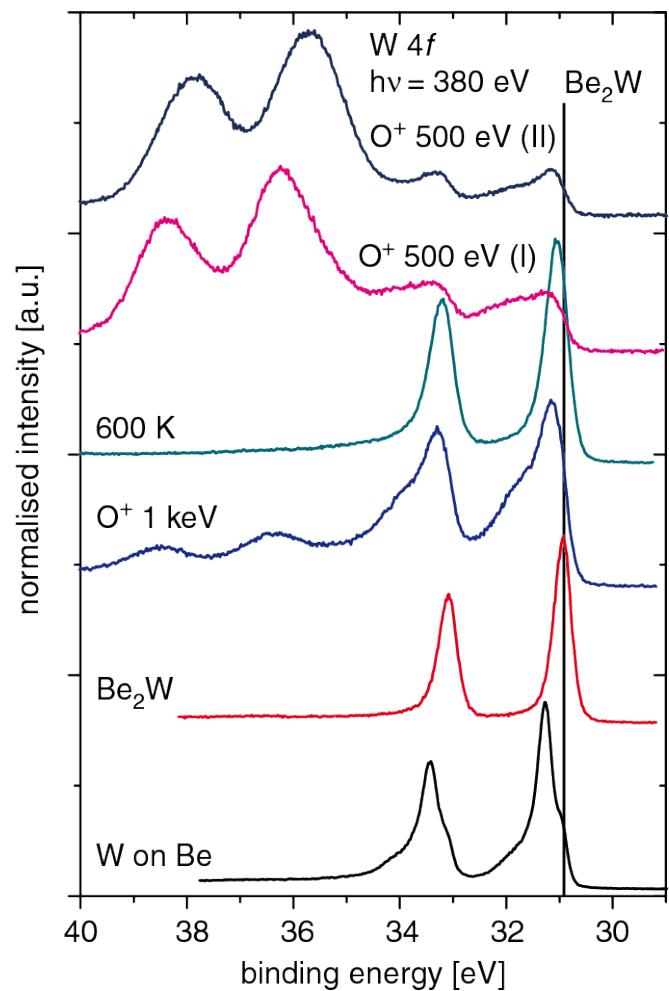
excitation energy	kinetic energy	mean free path
W 4f $h\nu = 90 \text{ eV}$	Be 1s $h\nu = 170 \text{ eV}$	C 1s $h\nu = 340 \text{ eV}$
		
$h\nu = 330 \text{ eV}$	$h\nu = 410 \text{ eV}$	$h\nu = 580 \text{ eV}$
		
$h\nu = 510 \text{ eV}$	$h\nu = 590 \text{ eV}$	$h\nu = 760 \text{ eV}$
		
$h\nu = 730 \text{ eV}$	$h\nu = 810 \text{ eV}$	$h\nu = 980 \text{ eV}$
		
	$\text{depth } d1$ $E_{\text{kin}} = 60 \text{ eV}$	$\lambda \approx 0.31 \text{ nm}$
	$\text{depth } d2$ $E_{\text{kin}} = 300 \text{ eV}$	$\lambda \approx 0.64 \text{ nm}$
	$\text{depth } d3$ $E_{\text{kin}} = 480 \text{ eV}$	$\lambda \approx 0.80 \text{ nm}$
	$\text{depth } d4$ $E_{\text{kin}} = 700 \text{ eV}$	$\lambda \approx 0.97 \text{ nm}$

# SDTrim.SP: O ion implantation profiles in Be<sub>2</sub>W

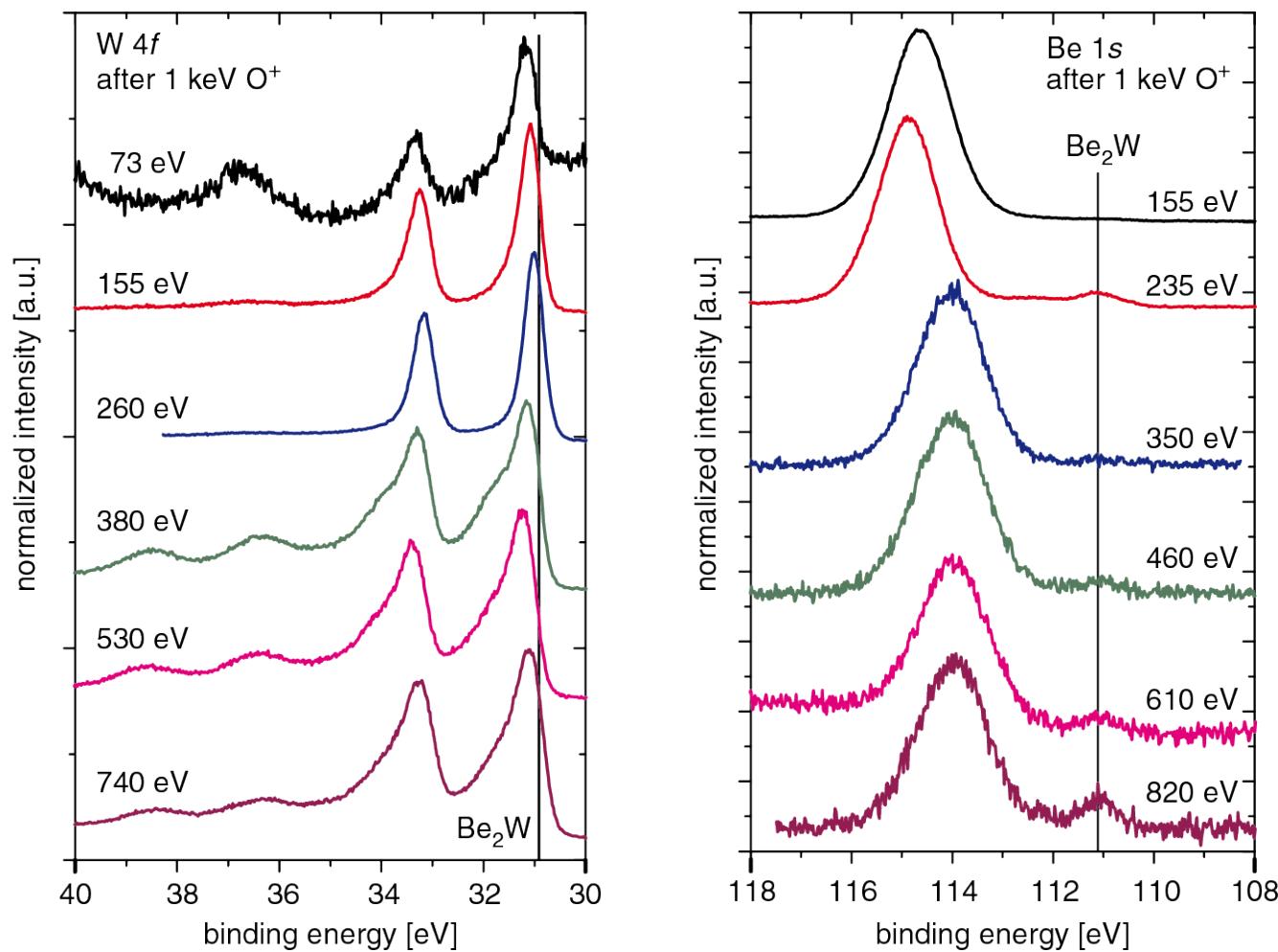


- Assumption: 82% O<sub>2</sub><sup>+</sup> and 18% O<sup>+</sup>
- Fluence:  $5 \times 10^{14} \text{ cm}^{-2}$
- Implantation maxima around 1 and 2 nm

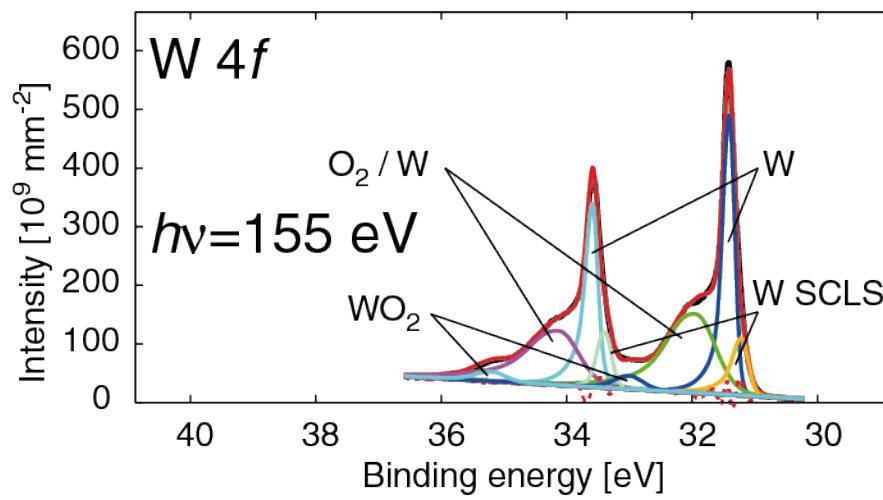
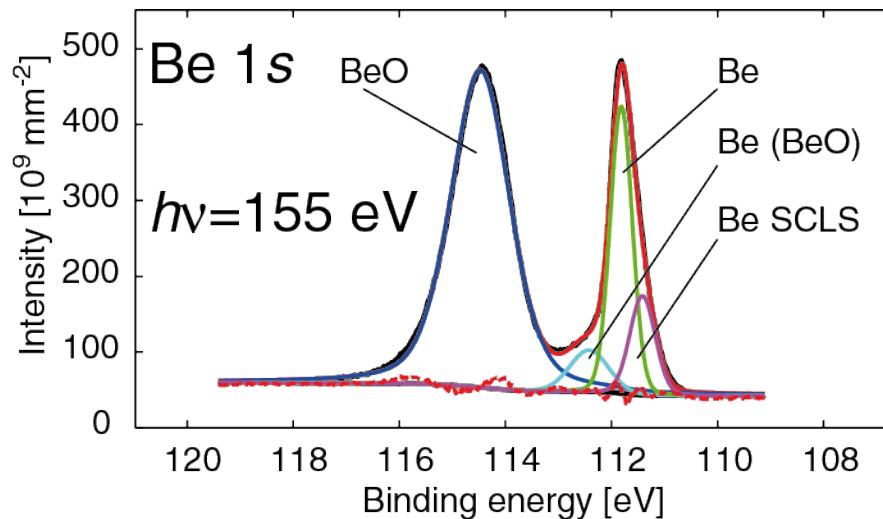
# Overview: chemical changes during implantation / annealing



# Depth-resolved chemical analysis



# Chemical species: Peak fitting



# Real situation: elements distributed over analysis depth

$$I_{x,hv}^{norm} = \sum_{i=1}^n \rho_{x,i} \lambda_{i,E_{kin}} \cos \alpha \left( 1 - \exp \left[ -\frac{d}{\lambda_{i,E_{kin}} \cos \alpha} \right] \right) \exp \left[ \sum_{j=1}^{n-1} -\frac{d}{\lambda_{j,E_{kin}} \cos \alpha} \right]$$

$I_{x,hv}^{norm}$ : norm. intensity

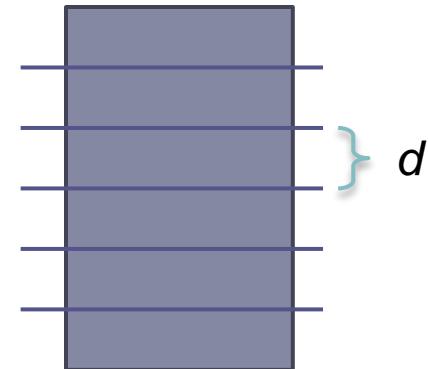
$\rho_{x,z}$ : density

$z$ : depth

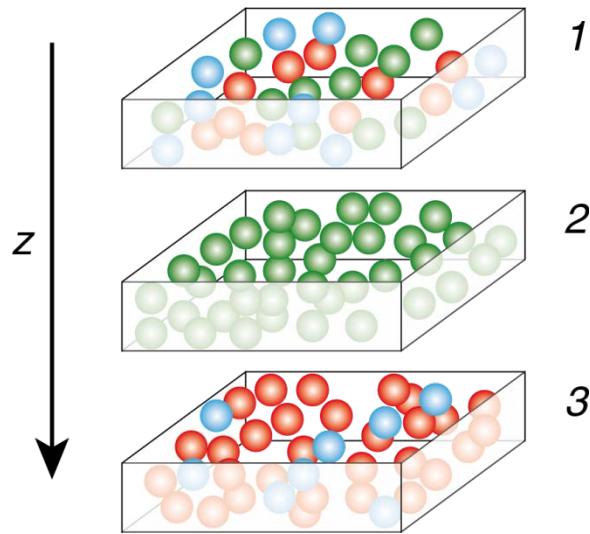
$\lambda_{k,E_{kin}}$ : IMFPs: Gries (1996): mixtures and compounds

$\alpha$ : exit angle

$d$ : layer thickness

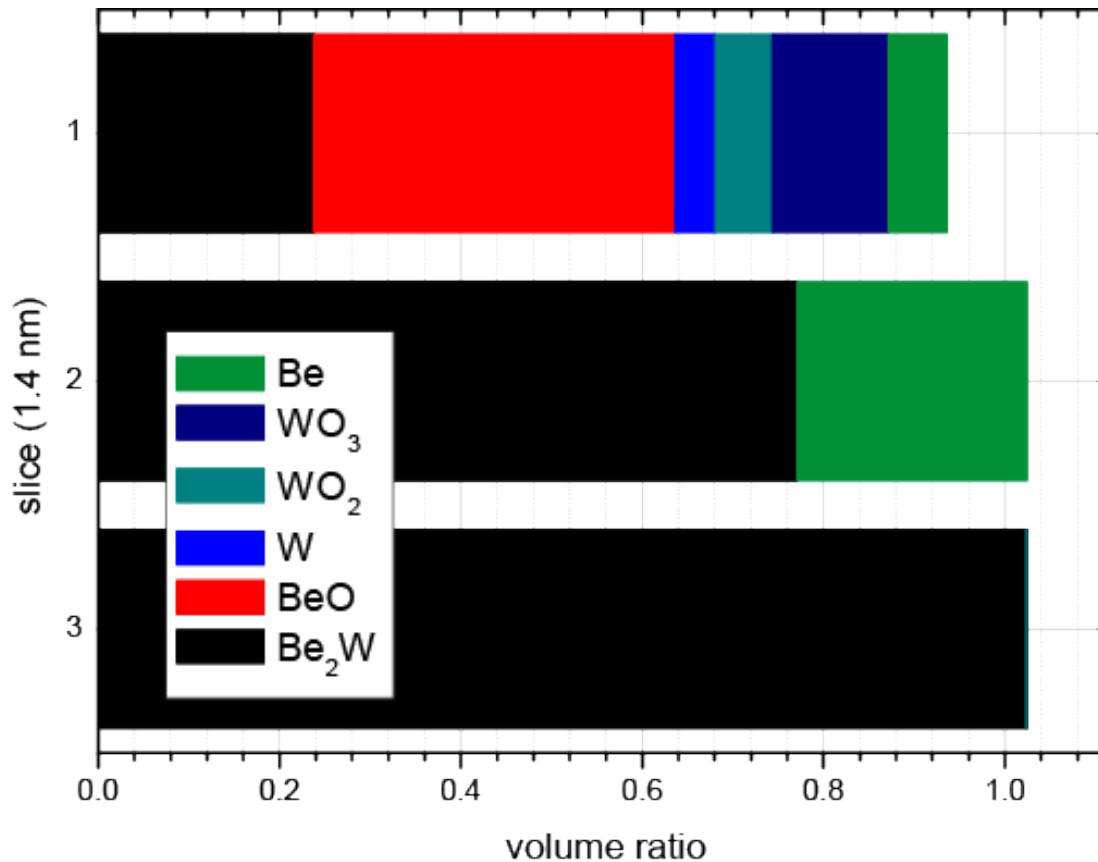


- Element distribution  $\rho_{x,i}$  is the result we are looking for!
- But:  $\rho_{x,i}$  necessary to calculate the IMFPs → nonlinear problem!
- Set of equations can only be solved numerically  
(*Mathematica, interior point method*)

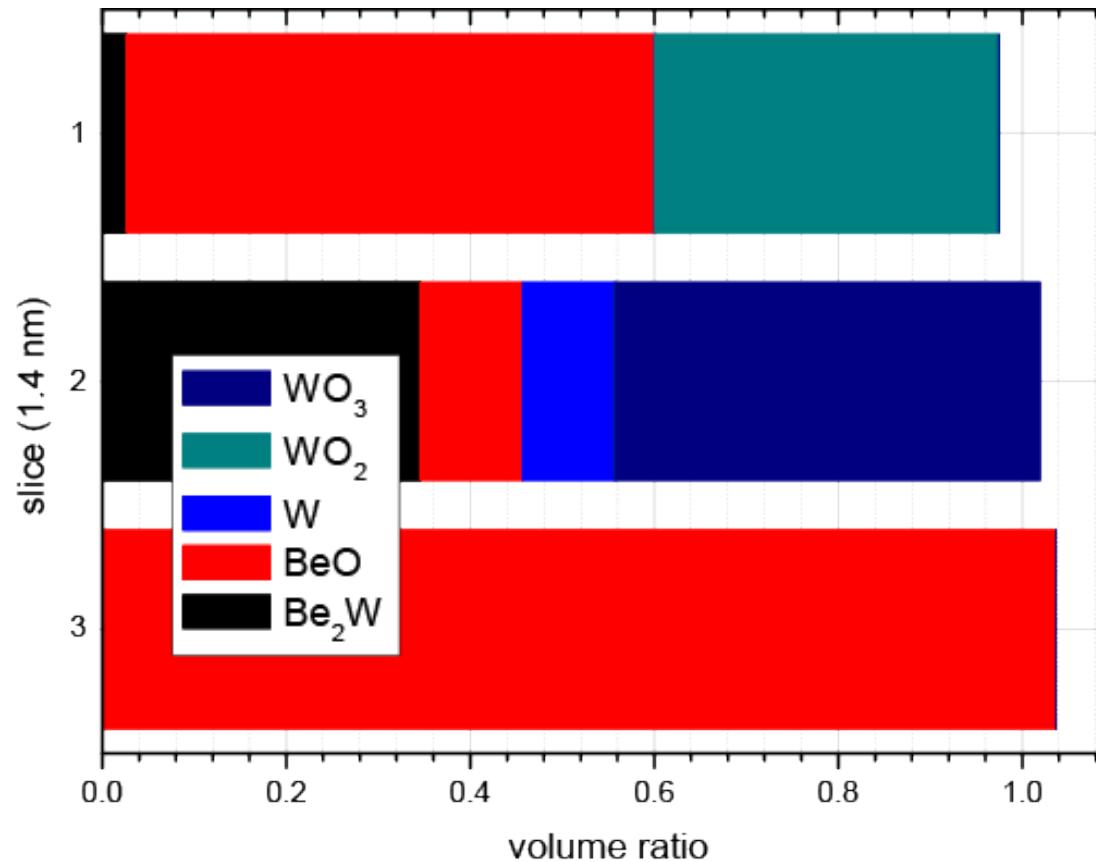


- Fill slices with elements and compounds detected by XPS
- Respect boundary conditions:
  - realistic volume density of each layer
  - fixed stoichiometries for compounds
- Calculate XPS intensities according to element distribution, attenuation by overlayers
- Fit particle densities to reproduce experimental intensities for all photon energies

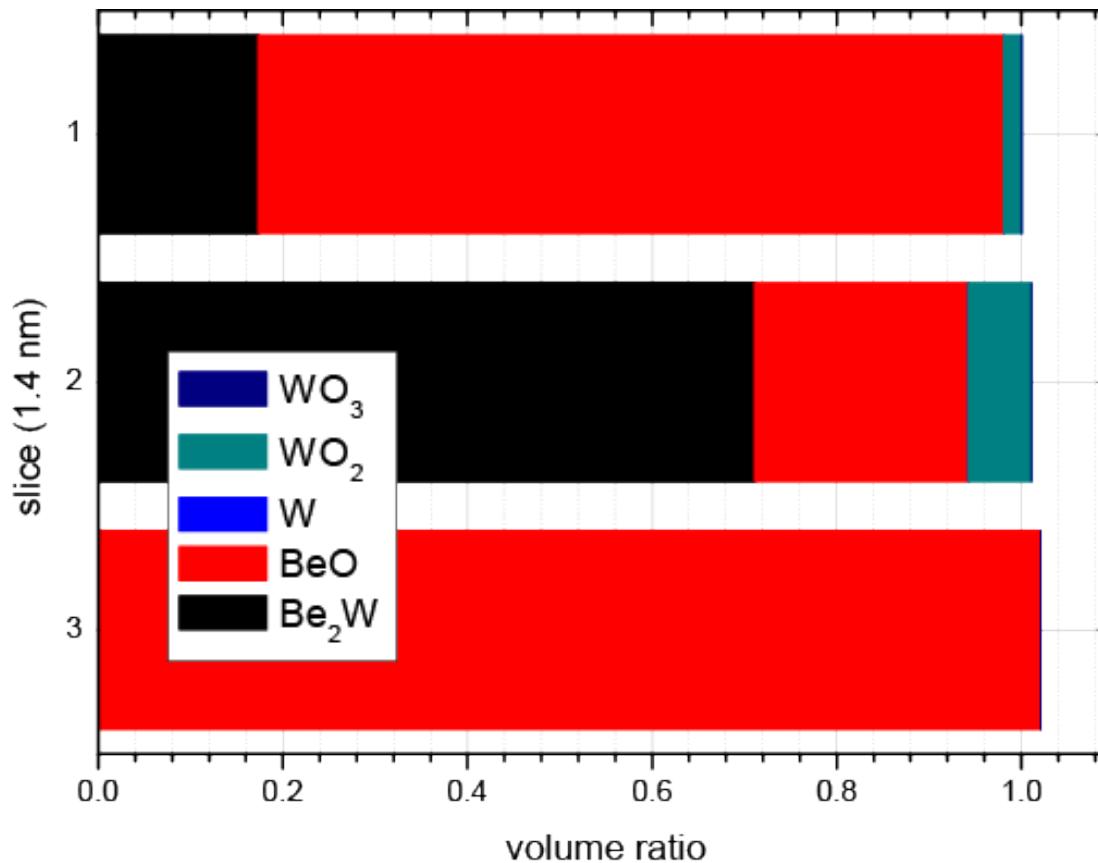
# Profile: Be<sub>2</sub>W formation



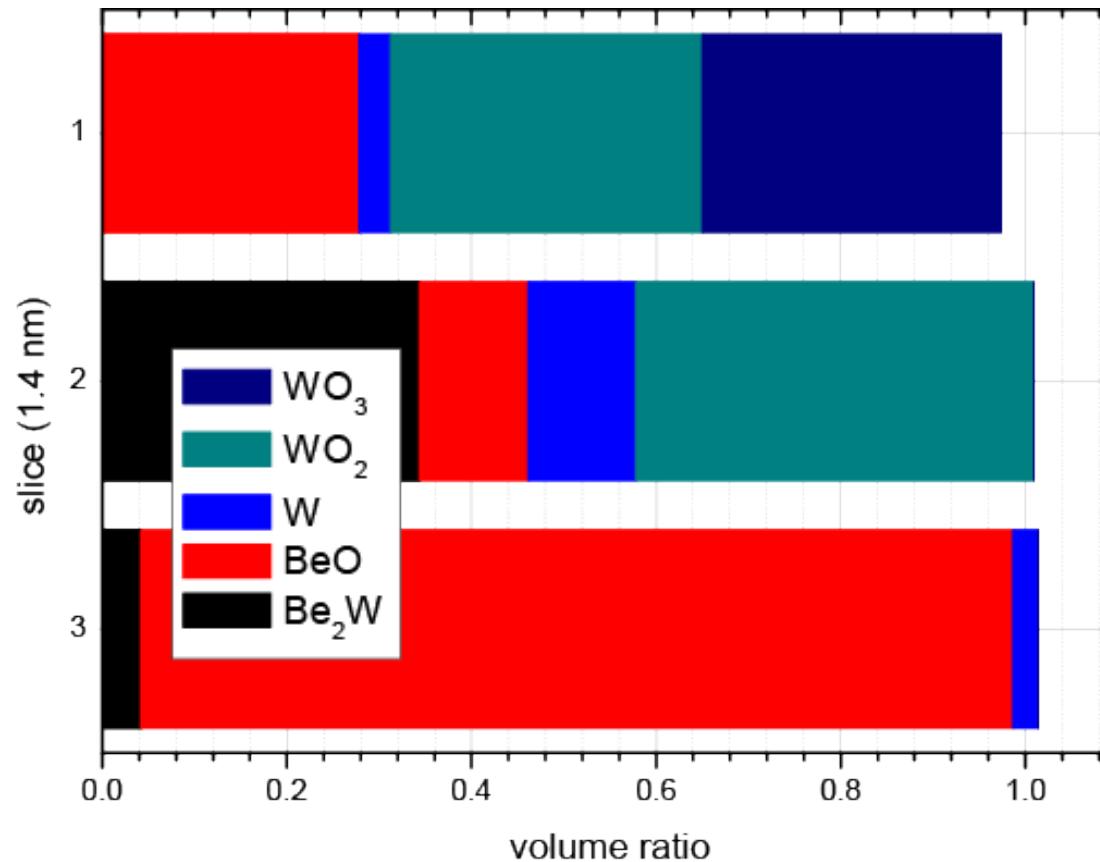
- Be<sub>2</sub>W dominates
- surface oxidation (residual gas)



- O<sup>+</sup> implantation profile: maximum ~2 nm
- Be<sub>2</sub>W is oxidized in slice 3
- available W (from Be<sub>2</sub>W) oxidized



- BeO most stable compound: all O bound to Be
- available W (from  $\text{WO}_x$ ) forms  $\text{Be}_2\text{W}$



- $\text{WO}_x$  formed: strong volume increase (large specific volume)
- remaining BeO in deeper layers not within analysis range
- surface BeO sputtered?

## Depth-resolved chemical analysis

- Synchrotron XPS allows access to identical depth intervals for different elements
- Careful data normalization required
- Qualitative analysis identifies depth-resolved reaction zones

## Quantitative analysis

- Sample discretized in homogeneous slices
- Numerical (non-linear) fit procedure required (multi-parameter fit)
- Reactions during implantation and annealing compatible with implantation profile

## Challenges

- Elaborate measurements at synchotron required
- More efforts needed to assess statistical confidence

# Modeling of surface reactions

Aim: Integration of **surface evolution** in **global modeling** of PWI processes

**Surface composition** determines:

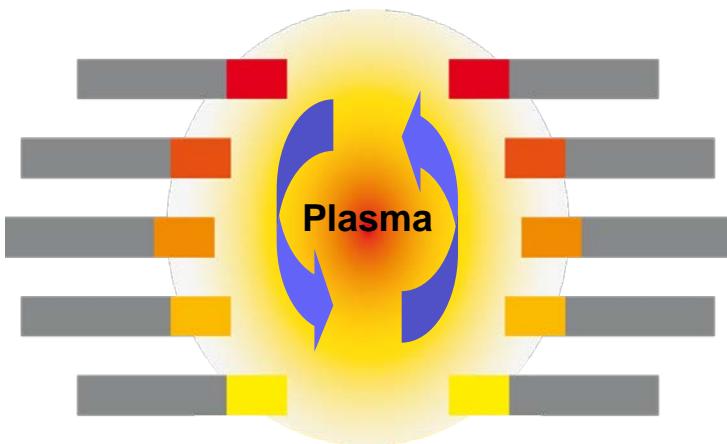
- erosion (phys., chem.)
- hydrogen inventory
- thermomech. properties (melting, sublimation, ...)

**Full description of material processes:**

- diffusion of  $i$  components in  $j$  materials ( $D(c, T)$ )
- all reaction rates
- collision-induced reactions

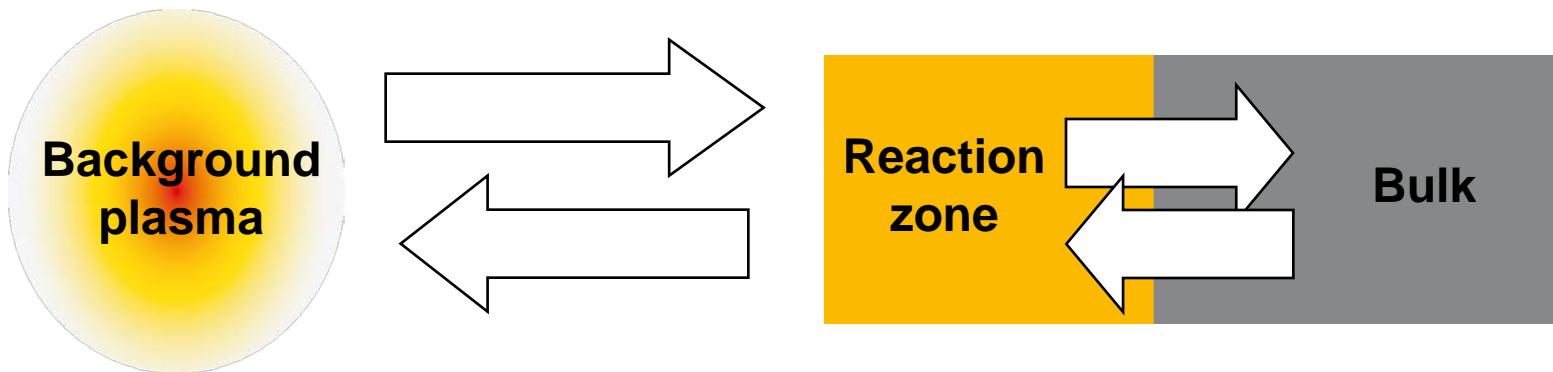
→ much too complicated for integration in **analytical model!**

Treat complex **plasma-wall interactions** and **material evolution** in a simplified way



## Analytical model:

- first wall:  $n$  tiles, different loads
- background plasma (B2 + EIRENE ...)
- redistribution matrix (DIVIMP)
- SDTrim sputter yields
- parametrized surface materials evolution



## Full description of material processes:

- diffusion of  $i$  components in  $j$  materials ( $D(c, T)$ )
- all reaction rates
- collision-induced reactions

## Parametrized material evolution

### 1st approximation: homogeneous layer

- one reactive layer
- homogeneous distribution of elements
- rate equation system

### 2nd approximation: reaction front system

- layered reaction zone
- reaction fronts
- rate equation system

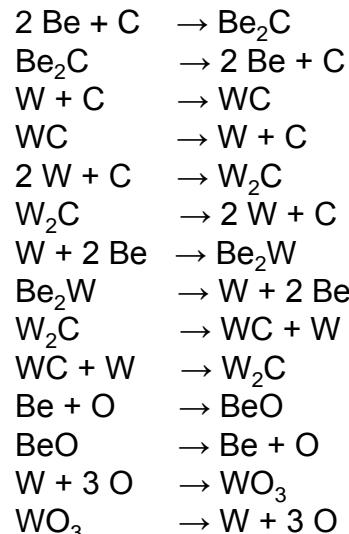
# Modeling approach: Description of chemistry

## 1. Define all substances

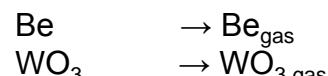
Be  
W  
C  
Be<sub>2</sub>C  
W<sub>2</sub>C  
WC  
Be<sub>2</sub>W  
Be<sub>12</sub>W  
Be<sub>gas</sub>  
BeO  
O<sub>ads</sub>  
WO<sub>3</sub>  
WO<sub>3,gas</sub>

+ Initial areal densities [#/m<sup>2</sup>]

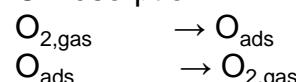
## 2. Elementary reactions



Sublimation:



O-Adsorption:



## 3. Define equations for reaction fluxes

$$\begin{aligned}
 \Gamma_1 \left[ \frac{1}{m^2 s} \right] &= [Be]^2 [C] k_1 \exp \frac{-\Delta E_1}{kT} & \text{with } k_1 \left[ \frac{m^4}{s} \right] \\
 \Gamma_2 \left[ \frac{1}{m^2 s} \right] &= [Be_2C] k_2 \exp \frac{-\Delta E_2}{kT} & \text{with } k_2 \left[ \frac{1}{s} \right]
 \end{aligned}$$

## 4. Define balances

Change of areal density of substance =  
 + all formation reaction fluxes  
 - all destruction reaction fluxes  
 ± all "non-chemical" fluxes

$$\frac{d[Be]}{dt} = -2\Gamma_1 + 2\Gamma_2 + \dots \quad \frac{d[Be_2C]}{dt} = +\Gamma_1 - \Gamma_2 + \dots$$

→ Set of ordinary differential equations

$$y'(t) = f(t, y(t)), \quad \text{with initial value } y(t_0) = y_0$$

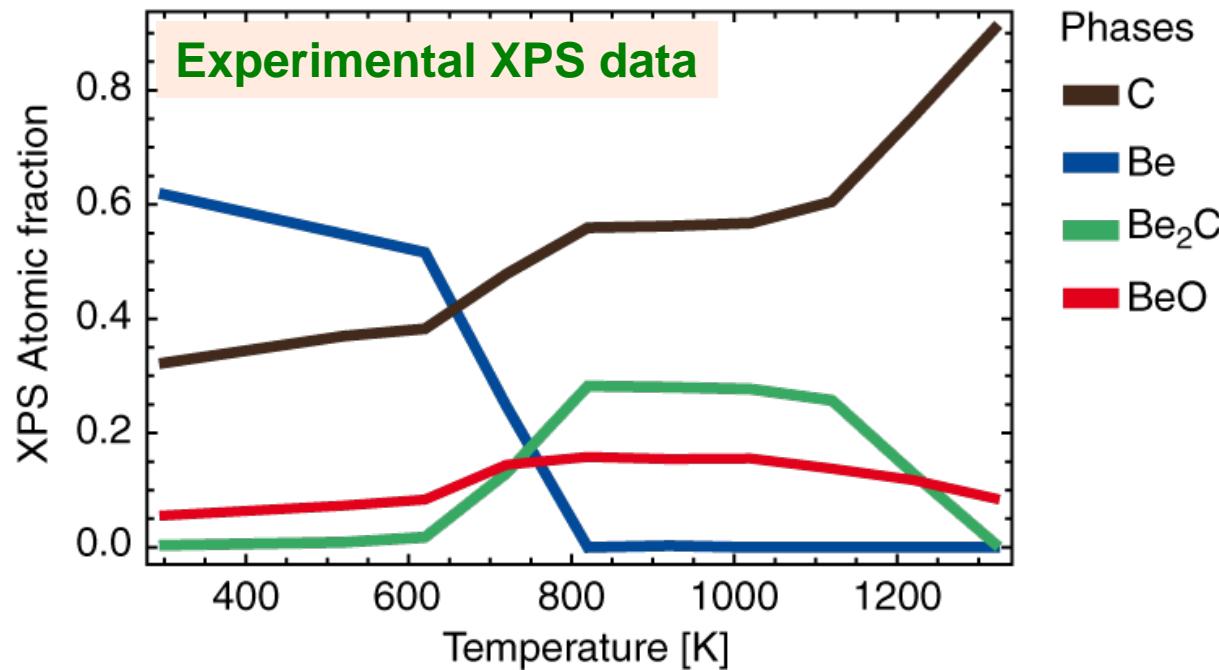
- **Standard literature:** vapor pressures, enthalpies of formation
- **XPS measurements:** investigation of thin layers  
(lab, synchrotron)      → chemical phase information  
                                → determination of reaction enthalpies  
                                → ions: relevant depth information  
                               (binary systems: Be-C, Be-W, W-C, W-O, Be-O,  
                               ternary systems: Be-C-O, Be-W-O, Be-W-C ...)
- **RBS measurements:** e.g. diffusion data

## Binary Be-C system

- Be / C
- homogeneous layer model

## System

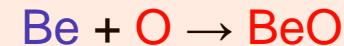
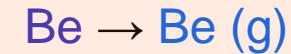
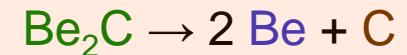
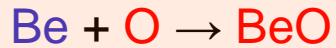
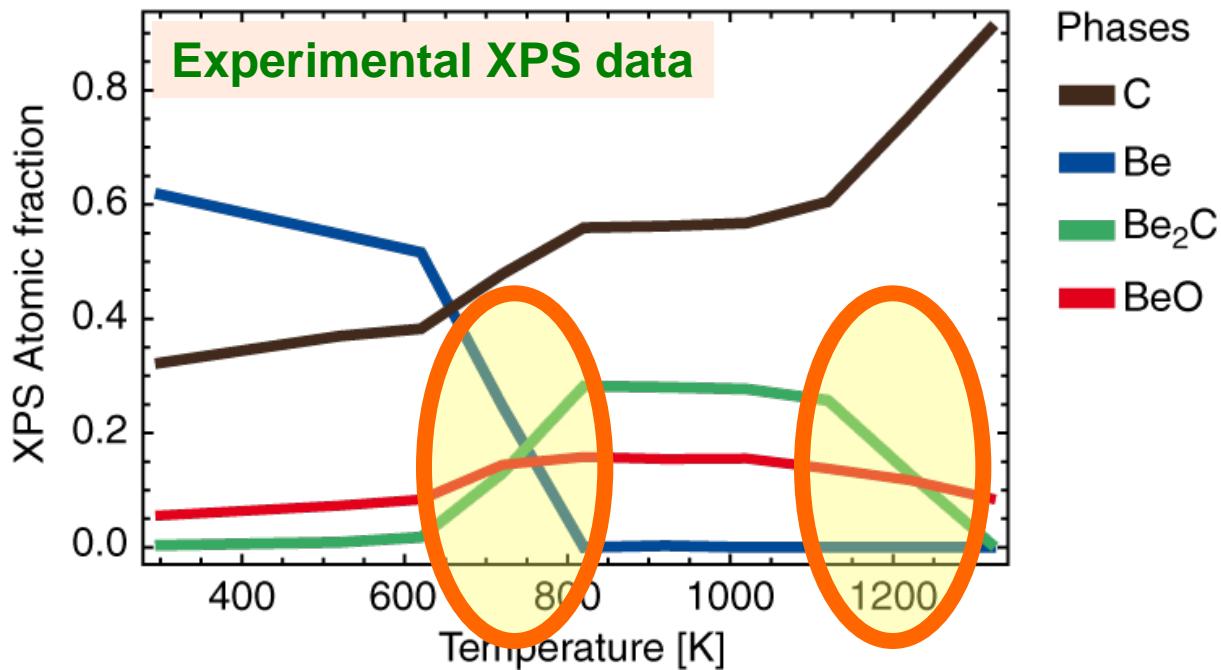
- substrate: pyrol. graphite
- 1.6 nm Be surface layer
- $\sim 10^{-10}$  mbar O<sub>2</sub>
- homogeneous reaction layer



# Benchmarking: Be/C

## System

- substrate: pyrol. graphite
- 1.6 nm Be surface layer
- $\sim 10^{-10}$  mbar O<sub>2</sub>
- homogeneous reaction layer



# Benchmarking: Be/C

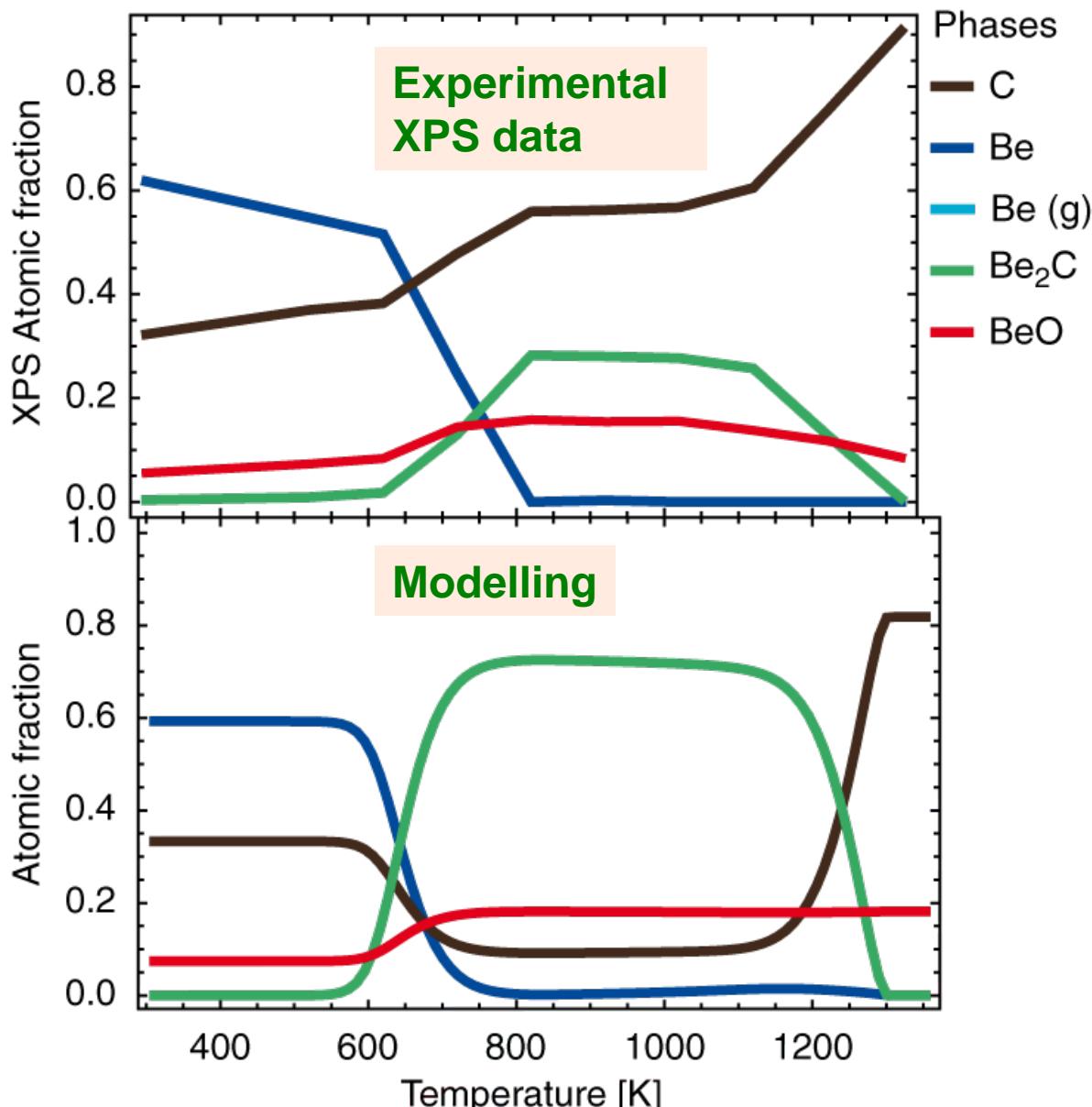
## System

- substrate: pyrol. graphite
- 1.6 nm Be surface layer
- $\sim 10^{-10}$  mbar O<sub>2</sub>
- homogeneous reaction layer

Fully coupled rate equation system

Be<sub>2</sub>C formation:  
 $\Delta E = 1.8 \text{ eV}$  (exp.),  $k_0 = 10^{-29} \text{ m}^4/\text{s}$

Be<sub>2</sub>C dissociation:  
 $\Delta E = 3.0 \text{ eV}$  (from  $\Delta H_f$ ),  $k_0 = 10^{13} \text{ s}^{-1}$



# Benchmarking: Be/C

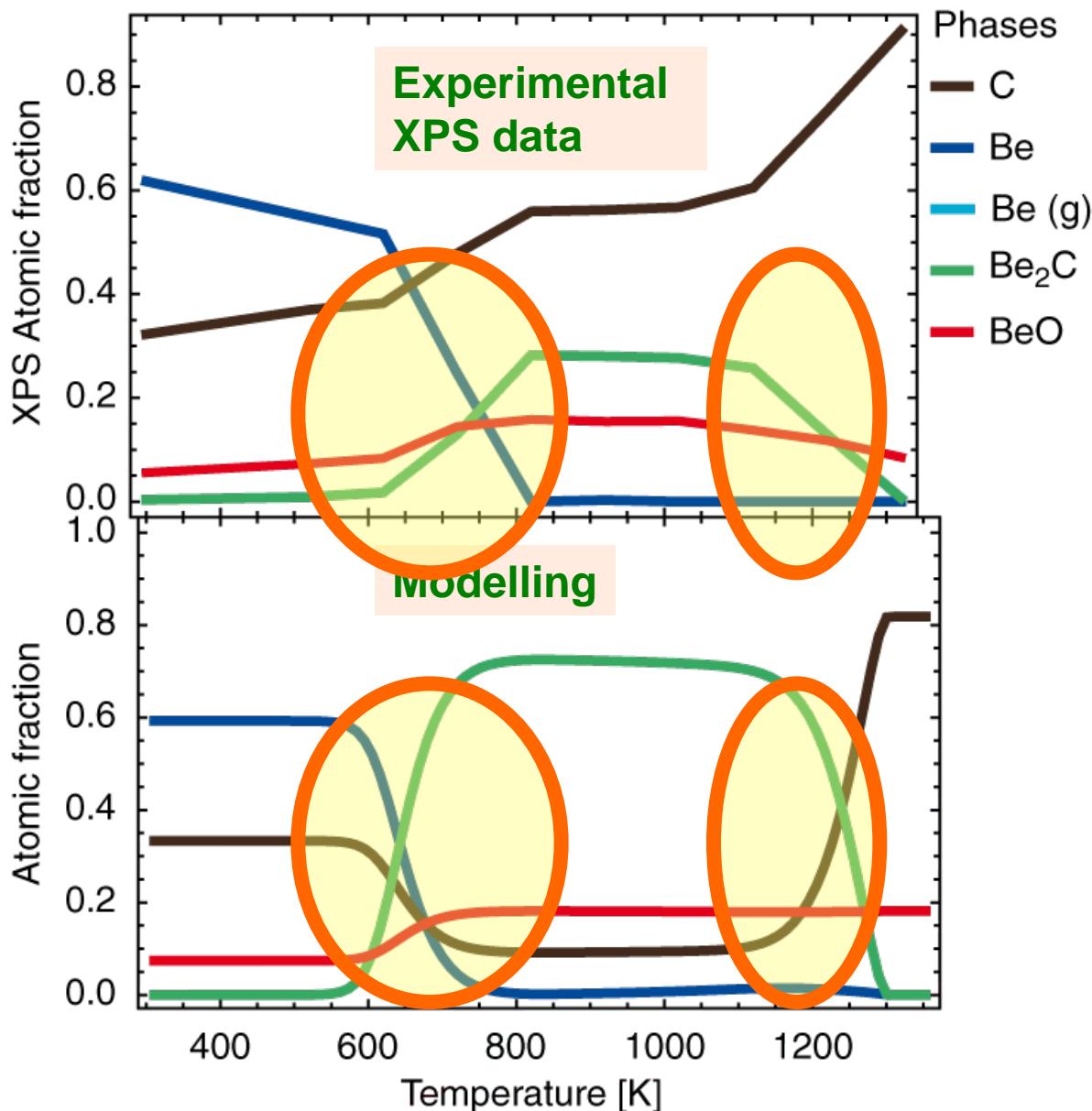
## System

- substrate: pyrol. graphite
- 1.6 nm Be surface layer
- $\sim 10^{-10}$  mbar O<sub>2</sub>
- homogeneous reaction layer

Fully coupled rate equation system

Be<sub>2</sub>C formation:  
 $\Delta E = 1.8 \text{ eV}$  (exp.),  $k_0 = 10^{-29} \text{ m}^4/\text{s}$

Be<sub>2</sub>C dissociation:  
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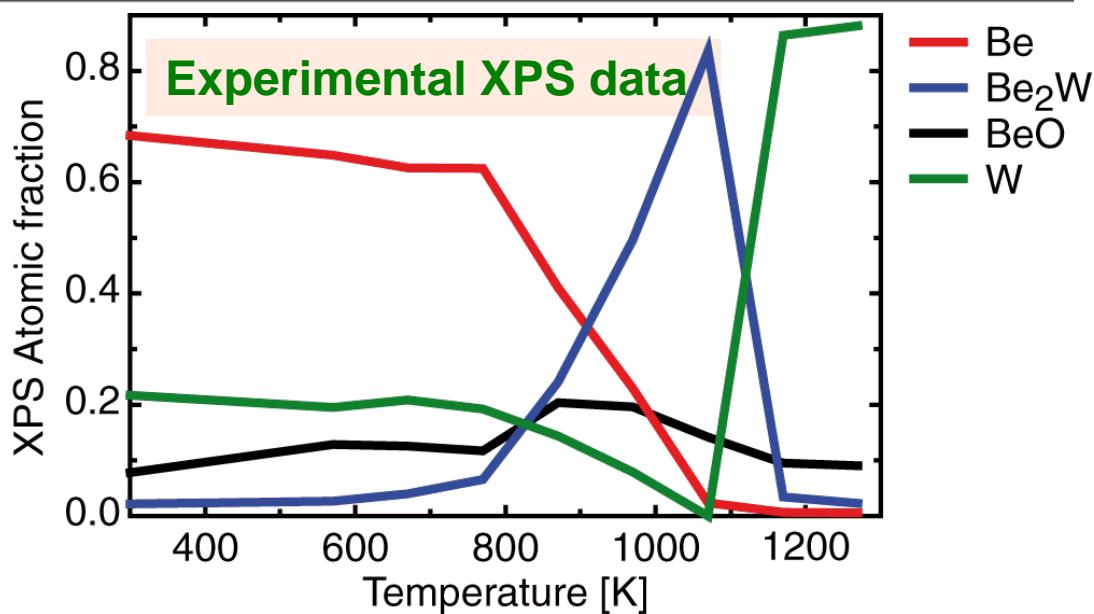
## Binary Be-W system

- Be / W
- reaction front model

# Benchmarking: Be/W

## System

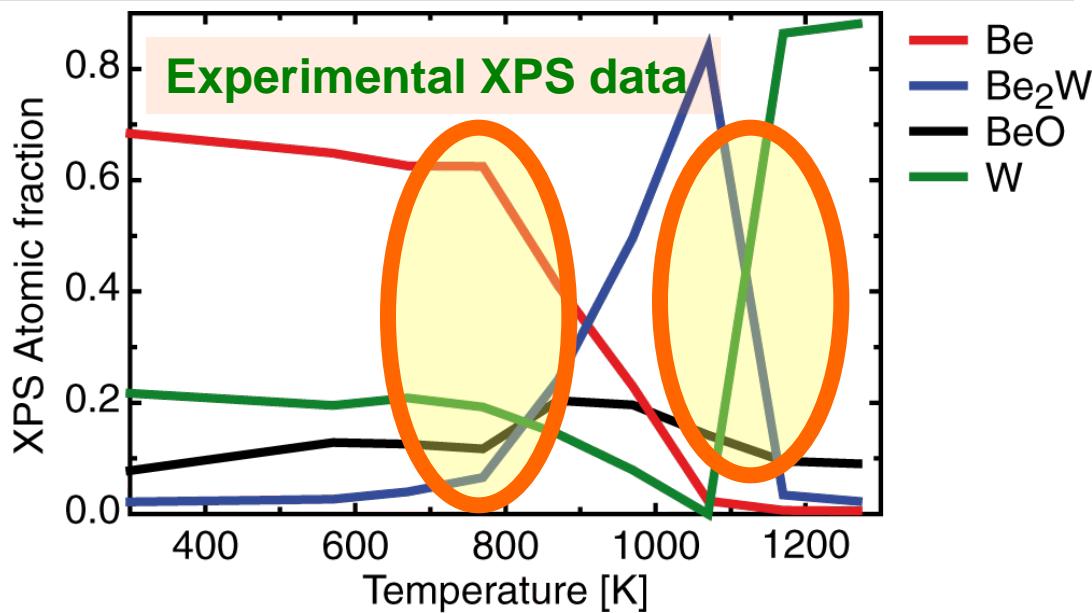
- substrate: W
- 2.1 nm Be surface layer
- layered system with reaction fronts



# Benchmarking: Be/W

## System

- substrate: W
- 2.1 nm Be surface layer
- layered system with reaction fronts



Be diffusion in  $\text{Be}_2\text{W}$

Be diffusion in BeO

$\text{Be}_2\text{W}$  dissociation

BeO dissociation

Be sublimation

# Benchmarking: Be/W

## System

- substrate: W
- 2.1 nm Be surface layer
- layered system with reaction fronts

Fully coupled rate equation system

Diffusion:

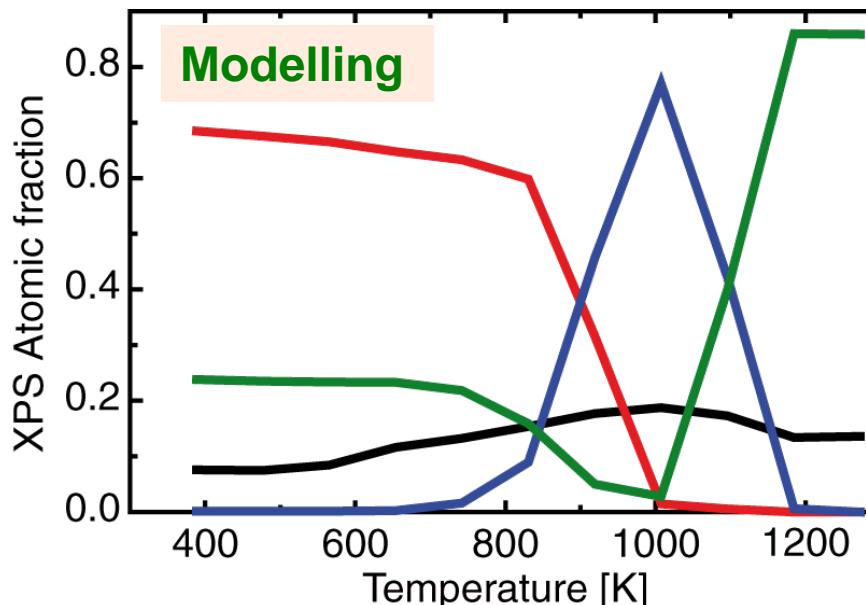
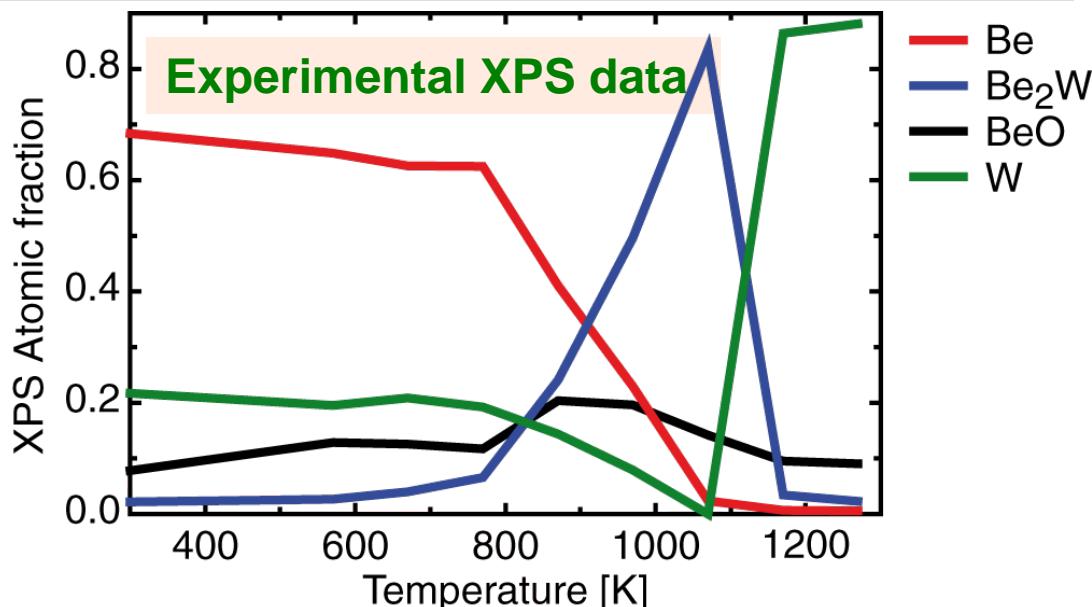
$$E_D(\text{Be in alloy}) = 1.5 \text{ eV}, D_0 = 10^{-12} \text{ m}^2 \text{ s}^{-1}$$
$$E_D(\text{Be in BeO}) = 1.6 \text{ eV}, D_0 = 10^{-6} \text{ m}^2 \text{ s}^{-1}$$

Dissociation:

$$E_A(\text{Be}_2\text{W}) = 3.1 \text{ eV}, k_0 = 10^{13} \text{ s}^{-1}$$
$$E_A(\text{BeO}) = 6.0 \text{ eV}, k_0 = 10^{13} \text{ s}^{-1}$$

Sublimation:

$$E_S(\text{Be}) = 3.2 \text{ eV}, k_0 = 4.3 \times 10^{34} \text{ s}^{-1}$$



# Benchmarking: Be/W

## System

- substrate: W
- 2.1 nm Be surface layer
- layered system with reaction fronts

## Fully coupled rate equation system

### Diffusion:

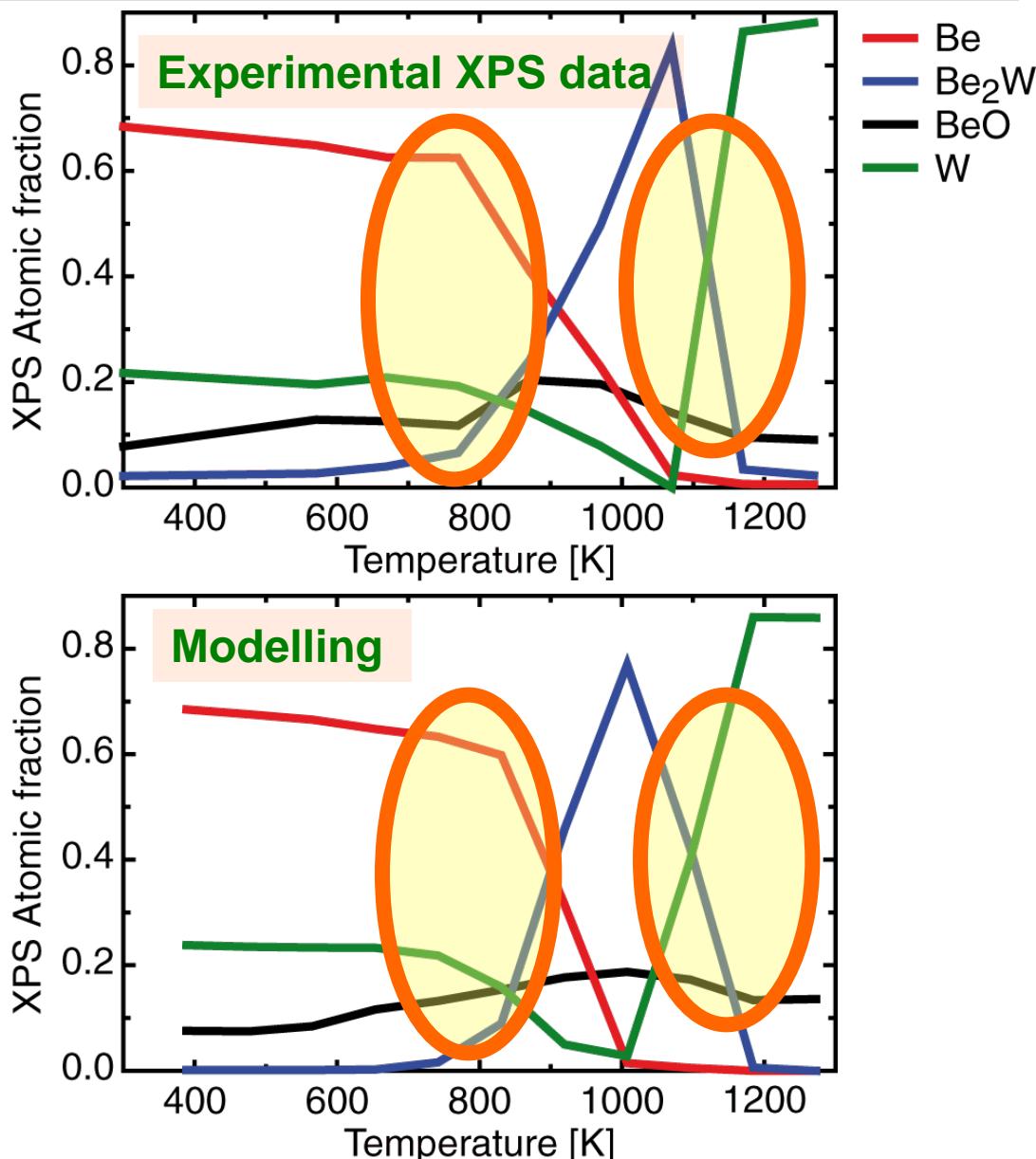
$$E_D(\text{Be in alloy}) = 1.5 \text{ eV}, D_0 = 10^{-12} \text{ m}^2 \text{ s}^{-1}$$
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### Dissociation:

$$E_A(\text{Be}_2\text{W}) = 3.1 \text{ eV}, k_0 = 10^{13} \text{ s}^{-1}$$
$$E_A(\text{BeO}) = 6.0 \text{ eV}, k_0 = 10^{13} \text{ s}^{-1}$$

### Sublimation:

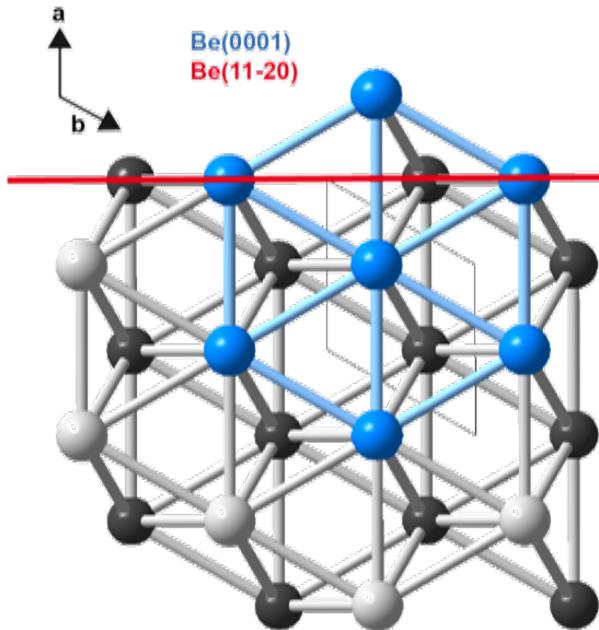
$$E_S(\text{Be}) = 3.2 \text{ eV}, k_0 = 4.3 \times 10^{34} \text{ s}^{-1}$$



- Fundamental reaction parameters from well-defined experiments
- XPS yields chemical data (qualitative and quantitative), complemented with other techniques
- Integration of surface chemistry into a modeling approach for PWI: predictive power for different locations with different loads
- Further identified reactions and processes can easily be integrated in modeling approach
- Tool for wall material compatibility testing: knowledge of material evolution due to PWI allows modification of local parameters (temperature, fluxes, composition)

# Hydrogen isotope retention

# D diffusion in beryllium



Be crystal lattice

Be(0001) plane  $\parallel$  to surface

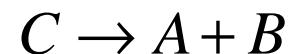
Be(11-20) plane  $\perp$  to surface

- Beryllium has **not** an “ideal” hcp structure. Be-Be distances are closer in  $\langle 0001 \rangle$  than perpendicular to it (e.g.  $\langle 11-20 \rangle$ )
- DFT (Density Functional Theory) calculations show anisotropy in transport processes with respect to Be basal planes

## Strategy

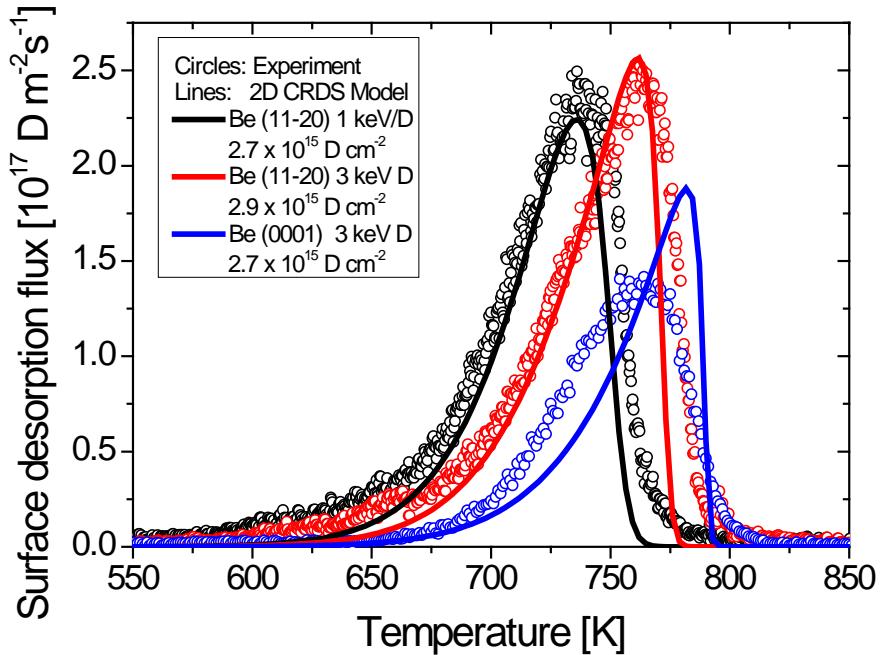
- Solve a coupled reaction diffusion system (CRDS) consisting of an arbitrary number of diffusing species  $i=A,B,C\dots$  in 1, 2 or 3 dimensions
- Solve system of partial differential equations for the time dependent 2D depth profile  $\rho(x,z,t)$  [ $\text{m}^{-3}$ ]

$$\frac{\partial \rho_A(x,z,t)}{\partial t} = \frac{\partial}{\partial x} \left( D_x(T(t)) \frac{\partial \rho_A(x,z,t)}{\partial x} \right) + \frac{\partial}{\partial z} \left( D_z(T(t)) \frac{\partial \rho_A(x,z,t)}{\partial z} \right) + \\ + \sum \Gamma_i^{Form}(\rho_{A,B,C\dots}) - \sum \Gamma_i^{Annihilation}(\rho_{A,B,C\dots}) + \Gamma_i^{Source}(x,z,t)$$



$$\Gamma_1(\rho_A, \rho_B, t) = k_1 \rho_A \rho_B \exp\left(-\frac{\Delta E_1}{k_B T(t)}\right) \quad \Gamma_2(\rho_C, t) = k_1 \rho_C \exp\left(-\frac{\Delta E_2}{k_B T(t)}\right)$$

# TPD of D implanted in Be single crystals

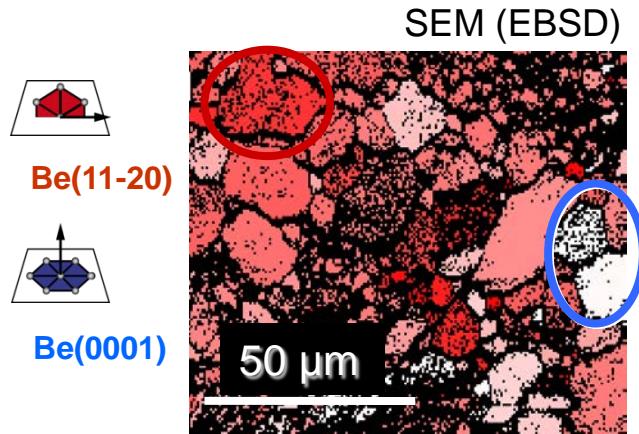


TPD spectra and 2D-CRDS simulations after implantation of D at 1 keV/D and 3 keV/D in Be(0001) and Be(11-20)

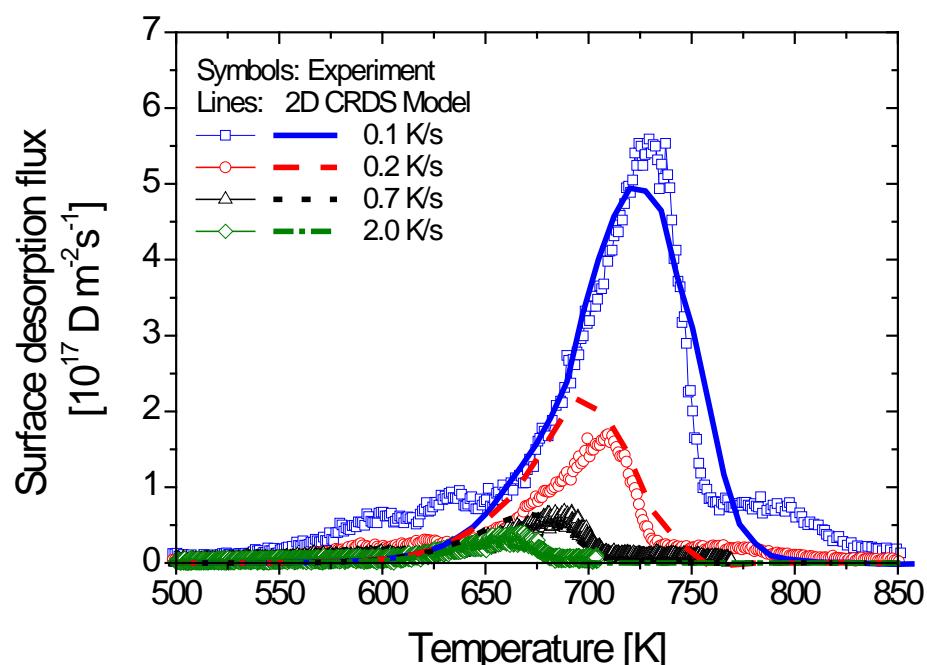
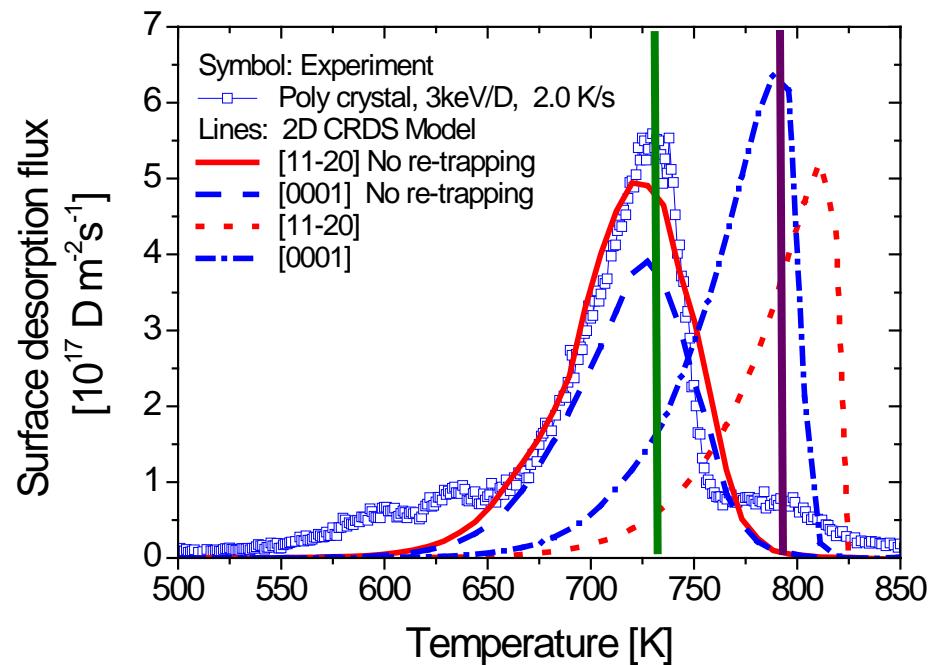
1. Desorption temperature shift for different implantation energies
2. Desorption temperature shift for Be(0001) and Be(11-20)
3. Less D retention in Be(0001) than in Be(11-20)

1. Deeper implantation → longer diffusion path to the surface → higher TPD peak temperature
2. Anisotropy of Be lattice → 2D anisotropic modelling required to implement results from DFT calculations
3. Dynamics during D implantation (MV+SI annihilation and trapping in MV) determines retention

**Identical parameters also applied for polycrystalline Be**



- Shift for Bepoly reproduced with no retrapping: **fast grain boundary diffusion**
- heating ramp variation reproduced: **no (self)trapping during heating**



# Parameters for D release and diffusion

## Experimentally and DFT determined parameters for full description

		v	$\Delta E_{act}$ [eV]	$\Delta E_{act}$ [eV]
		CRDS	CRDS	DFT 1 [1]
Diffusivity    Basal Plane	Mobile Hydrogen $H_{mob}$	3.11E-06	<0.4*	0.2
	Mono vacancy MV	3.11E-06	0.7	0.7
	Self interstitial SI	3.11E-06	0.4	0.4
	Trapped Hydrogen $H_{trap}$	-	-	-
Diffusivity $\perp$ Basal Plane	$H_{mob}$	7.68E-06	<0.4*	0.4
	MV	7.68E-06	0.7	0.7
	SI	7.68E-06	0.004	0.004
	$H_{trap}$	-	-	-
Trapping	$H_{mob} + MV \rightarrow H_{trap}$	1.00E+13	0.4	0.4
Detrapping	$H_{trap} \rightarrow H_{mob} + MV$	1.00E+11*	1.75	1.75
Annihilation	$MV + SI \rightarrow -$	1.00E+13	0.004	0.004
Self trapping	$H_{mob} + 1 H_{trap} \rightarrow 2 H_{trap} + SI$	1.00E+13	0.4	0.4

Anisotropy in diffusion of self-interstitials crucial for modeling!

# Summary: Hydrogen retention modeling

- Fundamental reaction parameters from well-defined experiments
- XPS yields chemical data (qualitative and quantitative), complemented with other techniques
- Integration of surface chemistry into a modeling approach for PWI: predictive power for different locations with different loads
- Further identified reactions and processes can easily be integrated in modeling approach
- Tool for wall material compatibility testing: knowledge of material evolution due to PWI allows modification of local parameters (temperature, fluxes, composition)

## 1. Binary Be-based systems

- C/Be, Be/C lab., DFT
- C<sup>+</sup> → Be lab.
- Be/W, W/Be lab., DFT
- N<sup>+</sup> → Be lab., DFT
- O<sub>at</sub>, O<sub>2</sub> → Be lab.

## 3. Ternary Be-based systems

- CO<sup>+</sup> → Be lab.
- O<sup>+</sup> → Be<sub>2</sub>W/W synchr.
- C/BeO/W synchr.
- Be/C/W, C or Be excess lab.
- C/Be/W, C or Be excess lab.
- Be/WO<sub>2</sub>, Be/WO<sub>3</sub> lab.
- C/W/Be synchr.
- WO<sub>x</sub>/Be synchr.

## 2. Hydrogen isotope retention and release

- D<sup>+</sup> → Be<sub>poly</sub>, Be(0001), Be(1 1 -2 0) lab., DFT
- D<sup>+</sup> → O/Be, BeO lab., DFT

## Open issues and work plan

- Interactions of nitrogen with Be—W alloys, together with presence of other impurities (O, C)  
Here, a large set of DFT calculations, incl. the interaction of hydrogen with N-containing compounds, is available (A. Allouche). These results require experimental verification.
- Erosion studies of Be and Be compounds by N ions  
Experiments are planned in an IPP-TU Wien collaboration, starting this November at IPP (quantitative erosion measurements using quartz crystals microbalances).
- Full exploitation of available depth-resolved XPS measurements of ternary Be compounds (new measurements where required)  
Data from BESSY measurements available, analysis tool available.
- Investigate suitable DFT-determined parameters as input for SDTRIM.SP calculations for compounds  
Replace surface binding energies by DFT-based energies in TRIM calculations. Collaboration IPP—U Aix-Marseille.

## Open issues and work plan

- Investigate influence of intrinsic and ion-induced defects in D retention  
Compare TPD studies from D<sup>+</sup>-implanted Be with atomic D (defects: intrinsic or ion-induced).
- Investigate retention and release mechanisms for Be compounds and compound layers on Be  
Extend studies on metallic Be to compounds and layers.
- Interpretation of H isotope retention by CRDS (coupled reaction diffusion system) modeling  
Extend available model to compounds. Include possible DFT results (Cooperation IPP—U Aix-Marseille).

## Application of fundamental data on Be and Be compounds to simulations for JET and ITER

- Extend and apply existing models (WallDyn) by integrating the determined parameters for various wall processes