

The first wall of fusion reactors: a challenge for material research

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From ITER to DEMO

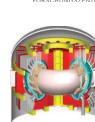
ITER



- operational flexibility (experimental device)
- transient heat flux events
- T-codeposition on „cold“ surfaces
- no energy conversion (80°C water coolant)
- low duty cycle
- low neutron dose (wall: ~1 dpa)

Need to apply available materials and technology

DEMO

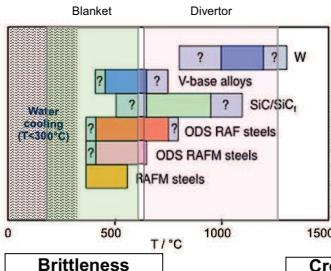


- lifetime (erosion, ageing)
- very limited transient heat flux events
- energy conversion (coolant: $\geq 300^{\circ}\text{C}$ water, $\geq 400^{\circ}\text{C}$ He)
- high duty cycle
- high neutron dose (wall: 80...150 dpa)
- low activation materials

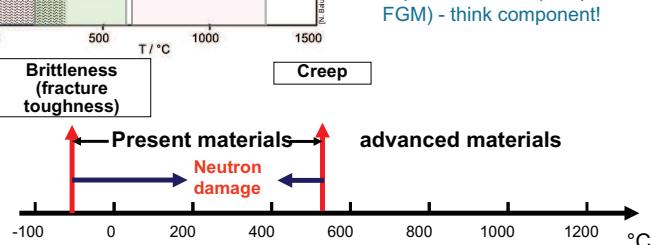
Need for innovation in non-activating materials and technology

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New material approaches needed



- Conventional materials are limited mostly by their parameters in addition to engineering approaches
- New materials should consider limits and mechanisms to improve on limits (composites, FGM) - think component!



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Effects of neutron irradiation

Defect production and migration Transmutation, He production	Hardening and deformations Fracture and embrittlement Creep, swelling surface modifications Precipitation and segregation He embrittlement	Crack formation/ enhanced erosion, melting Brittle destruction / Dust formation Fuel retention	Reduced life time of plasma facing components Issues for operational safety
Radiation damage event Damage cascade Defect formation and diffusion Void and bubble formation	Physical and mechanical effects of radiation damage	Enhancement of PWI processes / material damage under heat and plasma loads	Relevance for nuclear fusion reactors

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Overview

Introduction: the material challenge

Neutron damaged materials

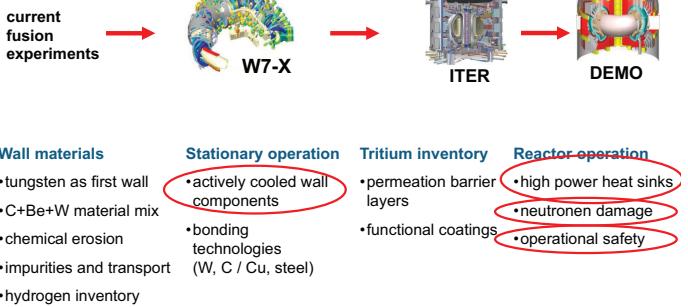
Research tailored towards fusion reactor materials

- Extrinsic toughening: composite materials
- Intrinsic safety: smart alloys

Summary and outlook

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PMI and material aspects in fusion research



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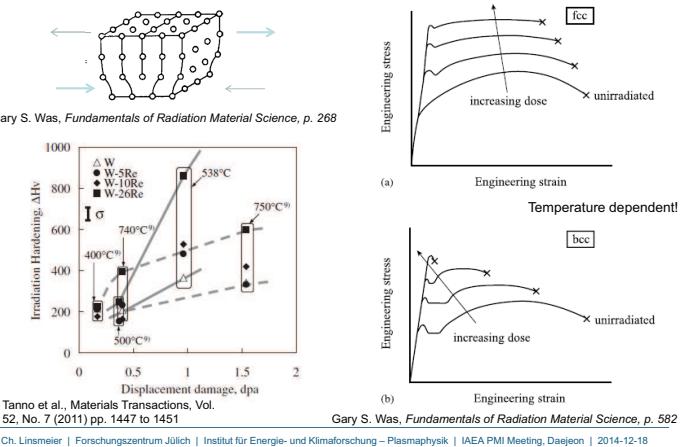
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Irradiation hardening

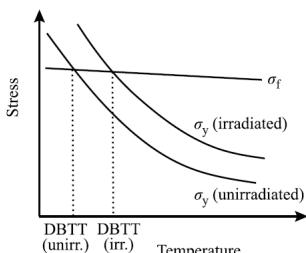
Increase in stress required to start a dislocation moving on its glide plane



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Embrittlement

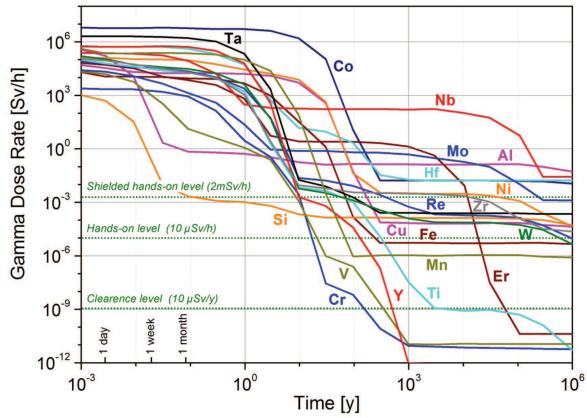
- Ductile-to-brittle transition temperature (DBTT): yield stress σ_y equals fracture strength σ_f
- Irradiation causes DBTT to increase: different sensitivities of yield stress and fracture strength to neutron damage



Gary S. Was, *Fundamentals of Radiation Material Science*, p. 661

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Transmutation: Decay times after n-irradiation

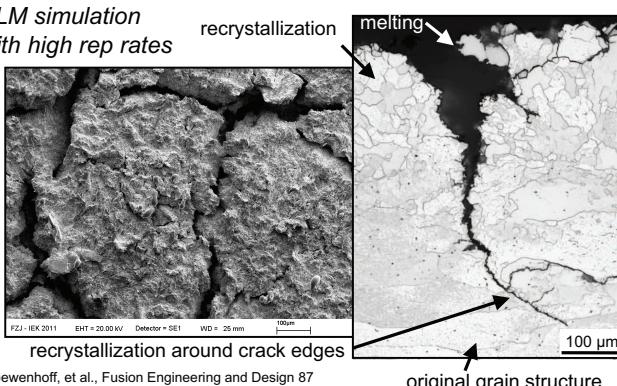


Source: R.A. Forrest et al., *Handbook of Activation Data*, 2009

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Enhanced erosion of irradiated tungsten in synergistic loading conditions

ELM simulation with high rep rates



Th. Loewenhoff, et al., *Fusion Engineering and Design* 87 (2012) 1201-1205

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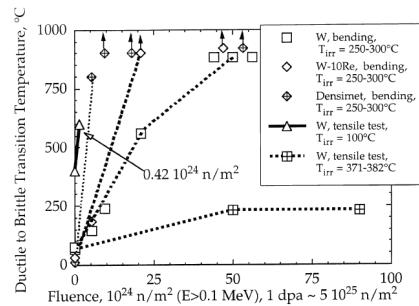
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Embrittlement of tungsten

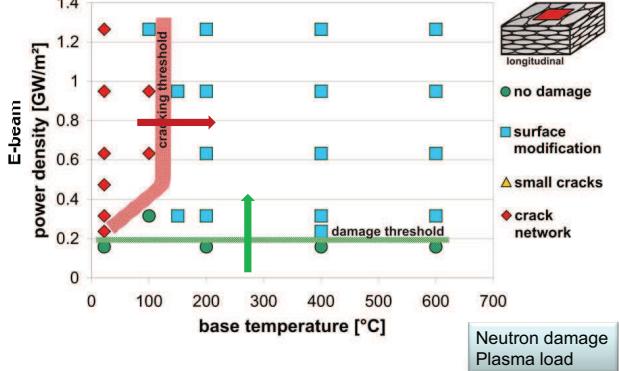


V. Barabash et al. / *Journal of Nuclear Materials* 283-287 (2000) 138-146

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Impact of synergistic loads on crack formation

M. Wirtz et al., *Phys. Scr.* T145 (2011) 014058



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Change of material composition

Radiation (plasma) induced:

- RIS: spatial redistribution of solute and impurity elements in a metal
→ enrichment or depletion of alloying elements near surfaces
- Reason: different coupling of solutes to defects
- Phase instabilities
- Issue for functional surface coatings (e.g. passivating layers or permeation barriers)
- Impact on surface composition as determined by preferential sputtering (e.g. EUROFER)
- Cr enriches in F-M alloys, leading to grain boundary embrittlement [Gupta et al., *J. Nucl. Mater.* 351 (1-3) (2006), 162.]

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Research tailored towards fusion reactors

Research focus:

- material development
 - definition
 - preparation and characterization
 - optimization
- PWI issues
 - erosion
 - retention
 - lifetime

Materials tests:

- neutron damage (simulation AND “real” neutrons)
- plasma exposure
- ELM (off-normal events) simulation

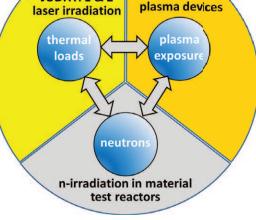
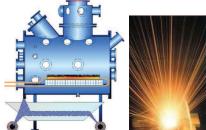
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Material testing at FZJ

- **Integrated** characterization of thermo-mechanical and physical-chemical properties of **neutron irradiated and toxic plasma-facing materials** under high heat loads and plasma exposure
- **Selection of plasma-facing materials** tested under n-irradiation and optimized for PMI processes (tritium retention, embrittlement, erosion)

JUDITH 1 and JUDITH 2
e-beam facilities



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Tungsten: Brittleness problem

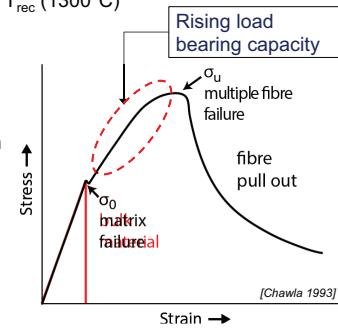
Limitations of operation temperatures for tungsten:

Lower limit: ductile-brittle-transition temp. T_{DBT} (260-650°C)

Upper limit: recrystallization temp. T_{rec} (1300°C)

plus: neutron embrittlement

- scattering in strength (small Weibull modulus)
 - no damage tolerance
 - uncertainty in lifetime prediction
- Solution: extrinsic toughening (ductilization) mechanisms**



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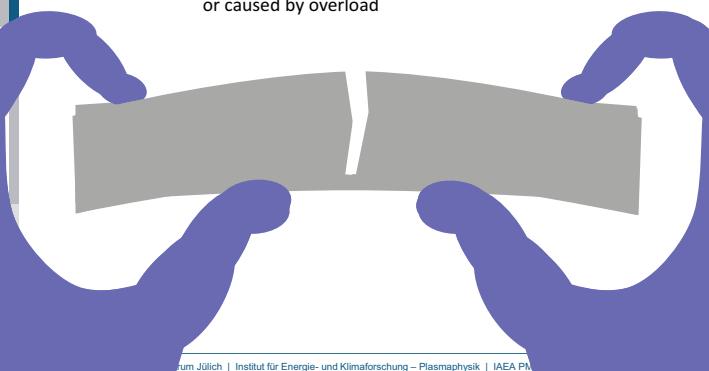
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Solution: extrinsic toughening (ductilization) mechanisms

- ⇒ local energy dissipation
 - crack bridging
 - fiber pull-out
 - crack deflection
- Main advantages for fusion**
- damage tolerance
 - mechanical effect
 - ⇒ less susceptible to operational embrittlement

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catastrophic failure by brittle fracture
after a random number of cycles
or caused by overload



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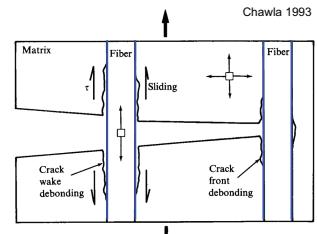
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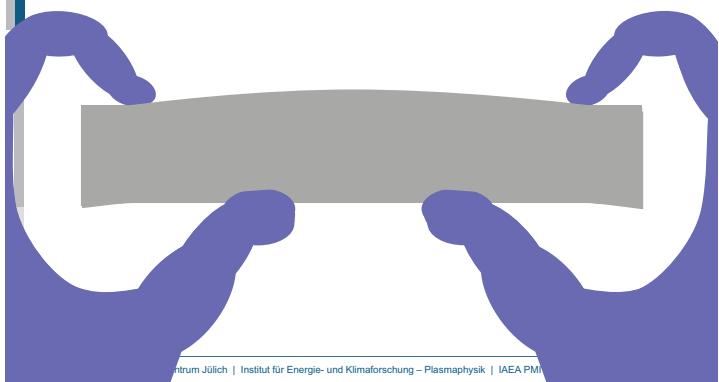
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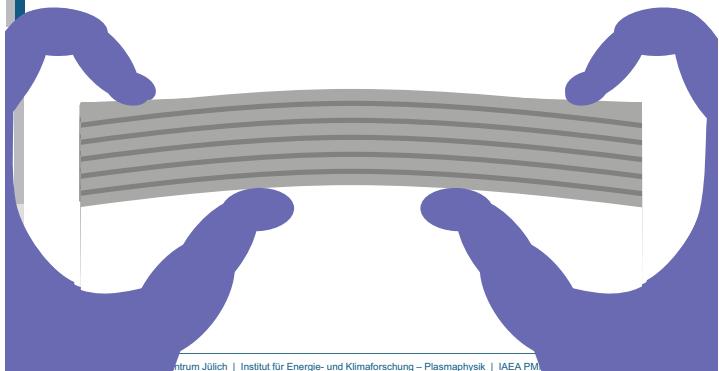
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e.g. full tungsten tile under cyclic loading



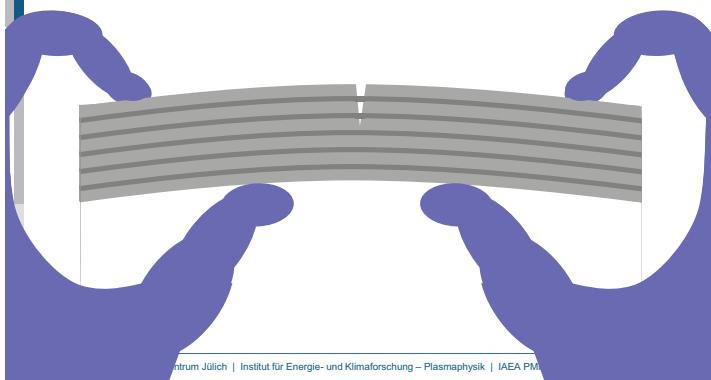
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W_f/W under cyclic loading



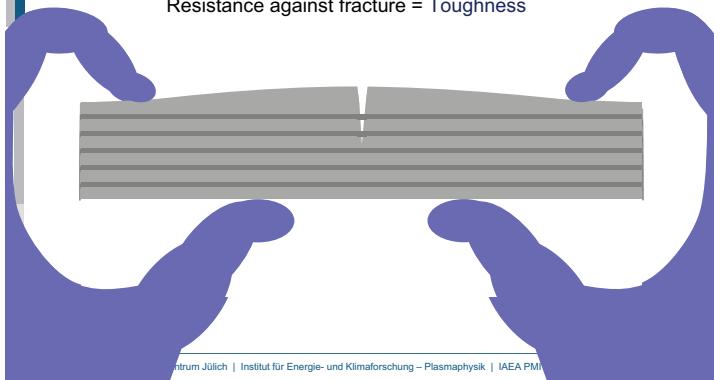
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Crack is bridged by fibres



Further loading still possible

Resistance against fracture = Toughness



Architecture of W_f/W

• Fibre

Drawn tungsten wire ($d = 150 \mu\text{m}$):
high strength + some ductility

• Interface

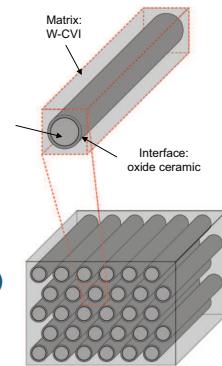
PVD coating:
Optimised adhesion + stability

• Matrix

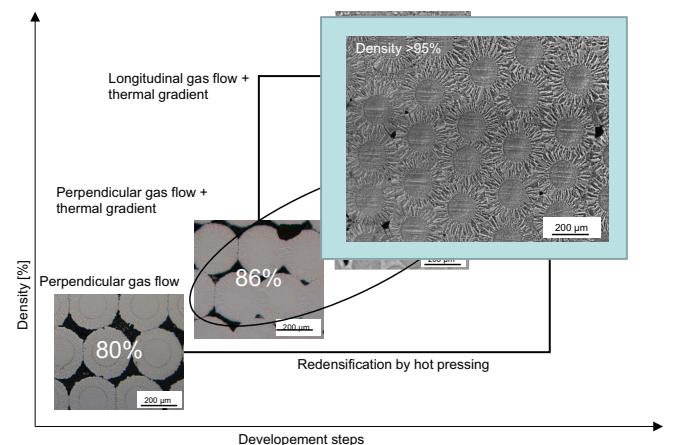
Interface integrity + high density

Develop **chemical vapour infiltration (CVI)**
technique for W/W

- No mechanical impact
- Low process temperature



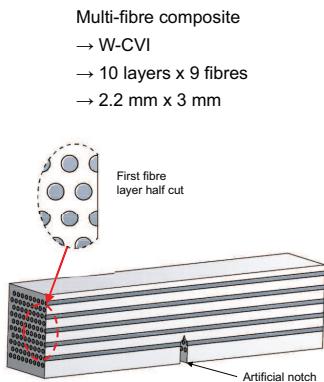
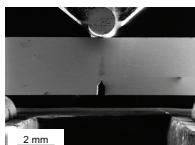
Development of CVI-tungsten



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3-Point bending test (ESI Leoben)

Stepwise 3-point bending

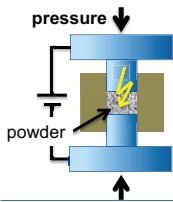
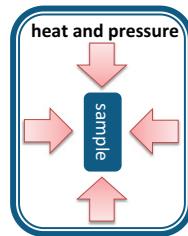


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Alternative production routes

HIP – Hot isostatic pressing

- capsule filled with tungsten powder and fiber inside a pressure vessel
- powder compaction due to high pressure and temperature
- $T_{\max} 2000^\circ\text{C}$
- $p_{\max} 350\text{ MPa}$ (via Ar)

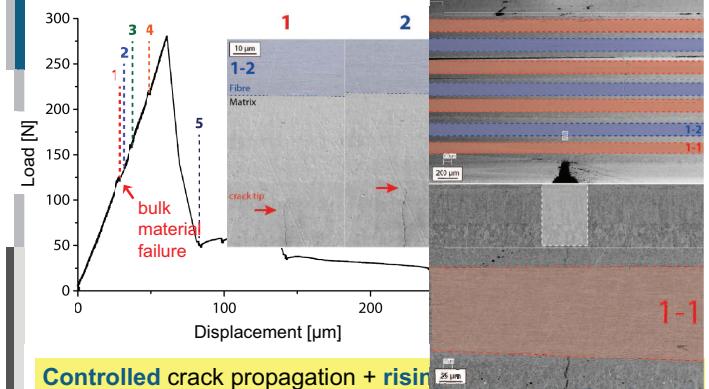


EDS – Electro discharge sintering

- tungsten powder and fiber are put inside an extrusion die
- powder compaction due to ohmic heating by a high current (500kA) + uniaxial pressure ($p_{\max} 350\text{ MPa}$)
- process time <1s, $E_{\max} = 80\text{ kJ}$

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Stable crack propagation

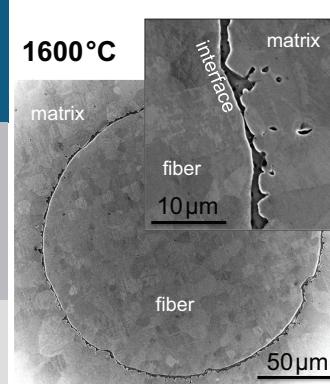


Controlled crack propagation + risir

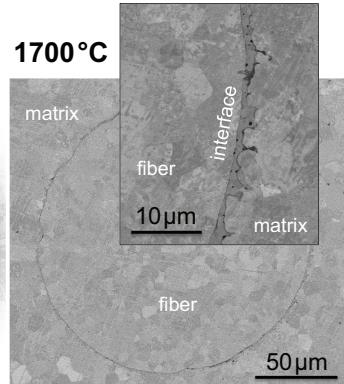
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HIP W_f/W composites

1600 °C



1700 °C



- intact interface after HIPing
- dense matrix achievable

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Requirements for “smart” W alloys

Normal operation conditions

- W-dominated plasma-wall interactions
- Limited and controlled H isotope retention

After LOCA event (loss of coolant accident)

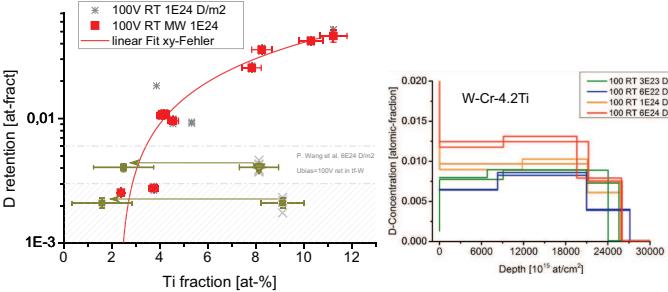
- Strong reduction of oxidation rate
- Stable protective layer

General

- Large-scale bulk material production routes
- No formation of brittle phases

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D retention after plasma exposure



- correlation between Ti concentration and D retention
- comparable to PVD tungsten for low Ti fraction
- bulk material: similar after Ti correction for oxide fraction

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Summary

PMI and materials for DEMO / a fusion reactor

- Combination of neutron / thermo-mechanical / particle loading
- No operational window for available materials
- Development and testing for new material (composites) required

W fiber / W matrix composites

- Development of W-CVI and powder metallurgical routes
- Verification of toughening effect: Stable crack propagation + rising load bearing capacity: damage tolerance
- Active toughening mechanism for fully brittle samples: resistance against embrittlement

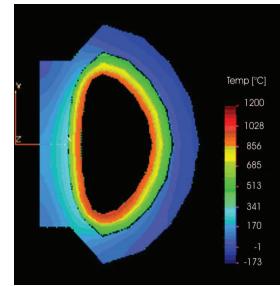
Self-passivating W alloys

- Up to 1/1000 reduction of oxidation rates for ternary alloys
- Transfer from thin films to bulk material successful
- PWI processes: D retention quantified

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Accidental loss of coolant in reactor

Power plant conceptual study



Temperature profile in PPCS Model A,
10 days after accident with a total loss
of all coolant.

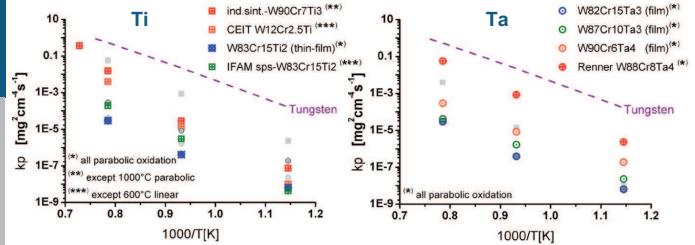
[Final Report of the European Fusion Power
Plant Conceptual Study, 2004]

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- Accidental loss of coolant:
peak temperatures of first wall
up to 1200 °C due to nuclear
afterheat
- Additional air ingress:
formation of highly volatile WO₃
(Re, Os)
- Evaporation rate:
order of 10 - 100 kg/h at
>1000°C in a reactor (1000 m²
surface)
→ large fraction of radioactive
WO₃ may leave hot vessel

Development of self-
passivating tungsten
alloys

Si-free alloys: W-Cr- (Ti / Ta / Y)



Reduction of oxidation rates

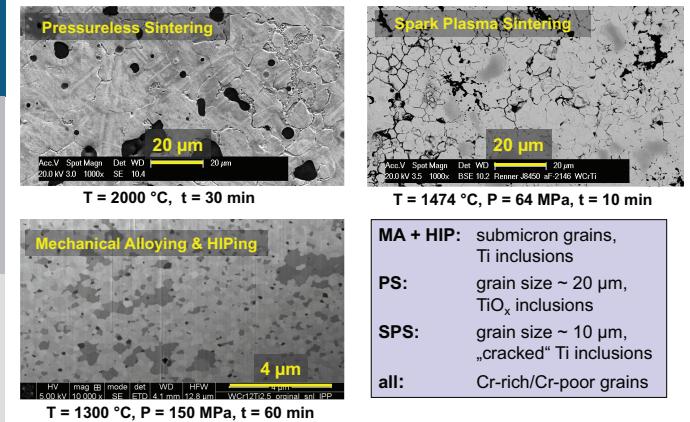
- Model thin films: several orders of magnitude
- Bulk materials: less reduction, different mechanisms?

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Composition

- Both Ti and Ta alloys successful
- Maximise W fraction:
W-Cr6-Y0.04: 82 at% W
Oxidation rate <5x10⁻⁶ mg²cm⁻⁴s⁻¹

W alloy bulk production methods



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Outlook

Multi-component materials

- Combination of materials solutions: brittle alloys with composites
- Hydrogen isotope inventory (PWI processes):
 - Dynamic evolution of composition during operation
 - Composites and alloys: new transport/trapping channels for T
 - n-induced damage: increased T retention?

DEMO: open issues, new ideas

- Steel first wall / breeding blanket: T permeation barriers required
- Thermomechanical properties after 14 MeV neutron irradiation?
- Neutron damage: large T inventory, erosion behavior?
- Transmutations: intrinsic formation of alloys (ref. to all above!)

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