

Design Concept of Korean Fusion Demonstration Reactor (K-DEMO)

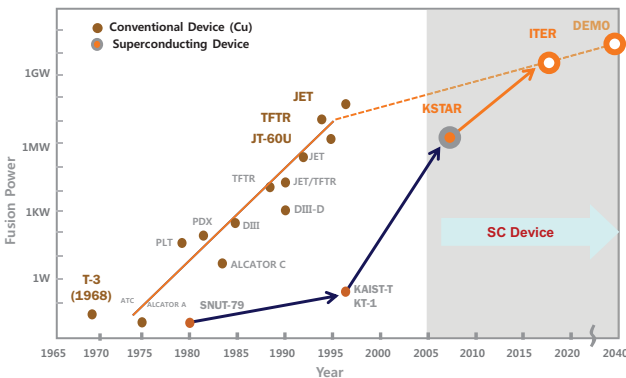
Decennial IAEA Technical Meeting
on Atomic, Molecular and Plasma-Material Interaction
Data for Fusion Science and Technology

December 15th, 2014

National Fusion Research Institute

kkeeman@nfri.re.kr

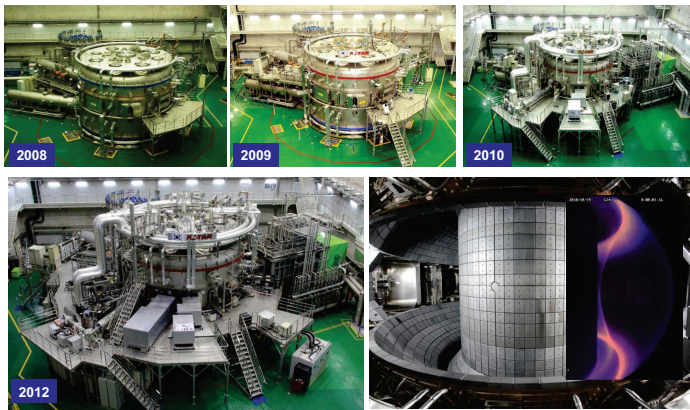
Mid-Entry Strategy in 1995



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KSTAR Superconducting Tokamak



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Fusion Energy Development Promotion Law (FEDPL)

- To establish a long-term and sustainable legal framework for fusion energy development phases.
- To promote industries and institutes which participating the fusion energy development by supports and benefit.
- The first country in the world prepared a legal foundation in fusion energy development.

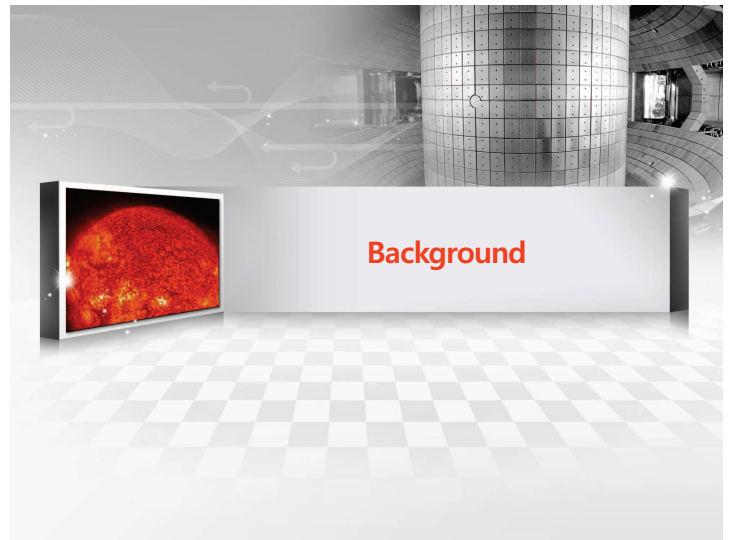
History of the FEDPL

- 1995. 12 : National Fusion R&D Master Plan
- 2005. 12 : National Fusion Energy Development Plan
- 2007. 3 : Fusion Energy Development Promotion Law
- 2007. 4 : Ratification of ITER Implementation Agreement
- 2007. 8 : Framework Plan of Fusion Energy Development (The first 5-Year Plan)
- 2012. 1 : The 2nd 5-year plan has begun



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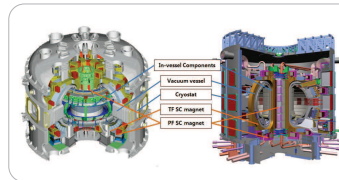


Background

KSTAR Mission and Parameters

KSTAR Mission

- To achieve the superconducting tokamak construction and operation experiences, and
- To develop high performance steady-state operation physics and technologies that are essential for ITER and fusion reactor development



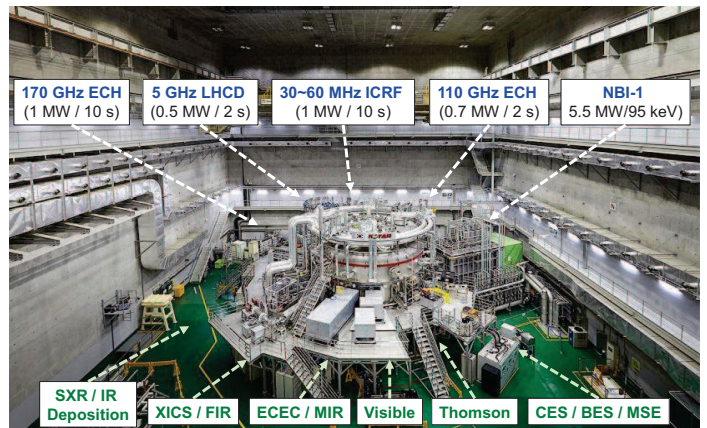
KSTAR Parameters

PARAMETERS	Designed	Achieved
Major radius, R_0	1.8 m	1.8 m
Minor radius, a	0.5 m	0.5 m
Elongation, κ	2.0	2.0
Triangularity, δ	0.8	0.8
Plasma volume	17.8 m ³	17.8 m ³
Bootstrap Current, f_{bs}	> 0.7	-
PFC Materials	C, CFC (W)	C
Plasma shape	DN, SN	DN
Plasma current, I_p	2.0 MA	1.0 MA
Toroidal field, B_0	3.5 T	3.6 T
Pulse length	300 s	10 s
β_N	5.0	> 1.5
Plasma fuel	H, D	H, D, He
Superconductor	Nb ₃ Sn, NbTi	Nb ₃ Sn, NbTi
Auxiliary Heating / CD	~ 28 MW	~ 6 MW
Cryogenic	9 kW @4.5K	5 kW @4.5 K

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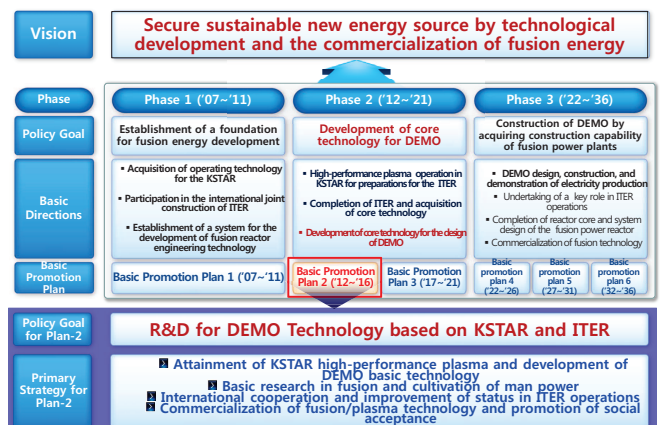
KSTAR 2014 Campaign (H-mode > 30 sec)



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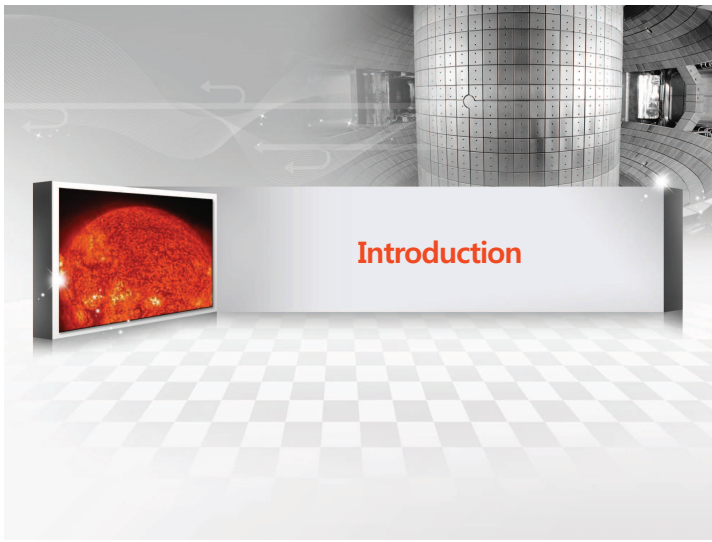
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Vision and Goal of Fusion Energy Development Policy



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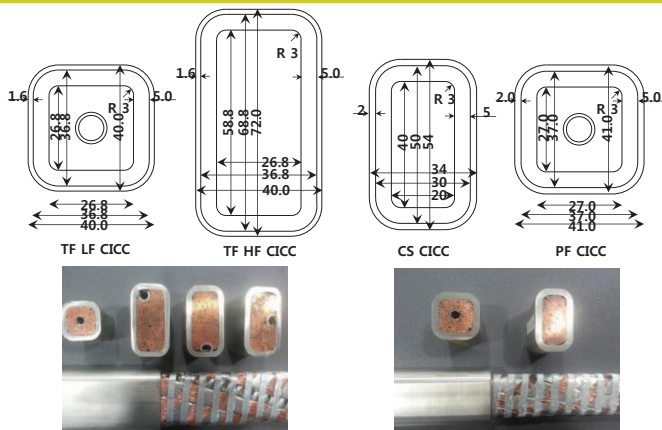


Key Idea of K-DEMO Design

- Current Drive and Magnetic Field
 - Considering the size, a steady state Tokamak is selected as a K-DEMO.
 - Because of high neutron irradiation on ion sources, NBI is not practical for the main off-axis current drive of K-DEMO.
 - Because of high density of K-DEMO plasma, high frequency ECCD systems (> 240 GHz) are required in order to minimize the deflection of wave.
 - In order to match with the high frequency ECCD, a high toroidal magnetic field Tokamak is required and the magnetic field at plasma center requires > 6.5 T.
 - Also, $I_{p,limit} \propto B$, $n_{e,limit} \propto B$, and $Power \propto R^3 B^4$ [Reactor Cost $\propto R^3 B^2$]
- Choice of Coolant and Blanket System
 - Helium is not considered as a coolant of K-DEMO because of its low heat capacity and a required high pumping power.
 - Supercritical water is not considered as a coolant of K-DEMO because of its serious corrosion problem.
 - Pressurized water (superheated water) is considered as a main coolant of K-DEMO considering BOP(Balance of Plant).
 - Both of ceramic and liquid metal blanket system is considered at this stage. But even in the liquid blanket system, the liquid metal will not be used as a main coolant and a water cooling system will be installed inside the liquid metal blanket.



CICC Dimensions and Trial Fabrication

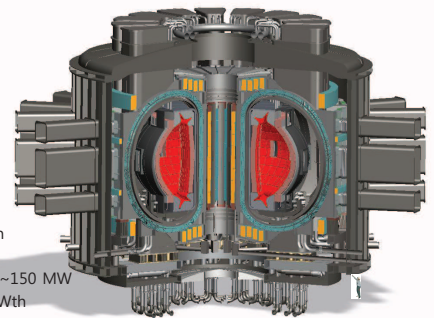


Two Stage Operation

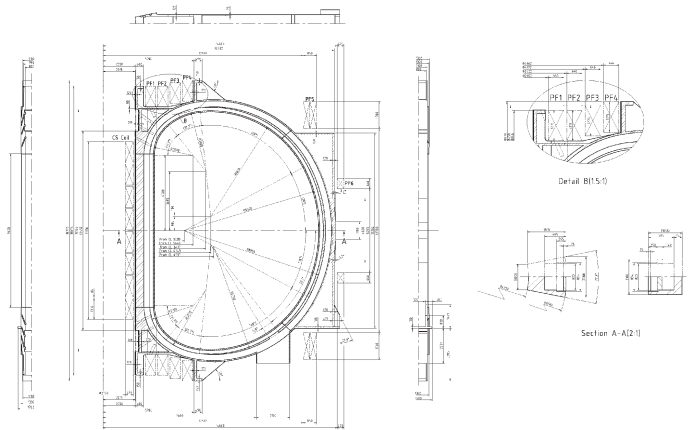
- The operation stage I K-DEMO is not considered as the final DEMO. It is a kind of test facility for a commercial reactor.
- But the operation stage II K-DEMO will require a major up-grade by replacing the blanket & diverter system and others if required.
- The operation stage I K-DEMO
 - At initial stage, many of ports will be used for diagnostics for the operation and burning plasma physics study, but many of them will be transformed to the CTF (Component Test Facility).
 - At least more than one port will be designated for the CTF including blanket test facility.
 - It should demonstrate the net electricity generation ($Q_{eng} > 1$) and the self-sufficient Tritium cycle ($TBR > 1.05$).
- The operation stage II K-DEMO
 - Though there will be a major upgrade of In-Vessel-Components, at least one port will be designated for CTF for future studies.
 - It is expected to demonstrate the net electricity generation larger than 450 MWe and the self-sufficient Tritium cycle.
 - Overall all plant availability > 70%.
 - Need to demonstrate the competitiveness in COE.

K-DEMO Parameters

- Main Parameters
 - $R = 6.8$ m
 - $a = 2.1$ m
 - B-center = 7.0~7.4 T
 - B-peak = 16 T
 - $\kappa_{95} = 1.8$
 - $\delta = 0.625$
 - Plasma Current > 12 MA
 - $T_e > 20$ keV
- Other Feature
 - Double Null Configuration
 - Vertical Maintenance
 - Total H&CD Power = 110~150 MW
 - P-fusion = 2200~3000 MWth
 - P-net > 400 MWe at Stage II
 - Number of Coils : 16 TF, 8 CS, 12 PF



2D Drawing of Magnet System

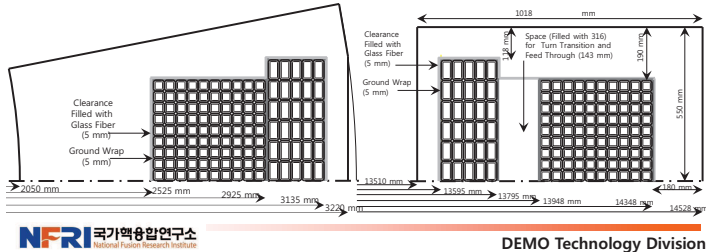


CICC Parameter

Parameter	TF HF	TF LF	CS	PF1-4	PF5-6
■ Cable pattern	(3SC)4x5x6x5 + Helical Spiral	((25C+2Cu)x5)x6+7 Cu)x6 + Central Spiral	(25C+1Cu)x3x4x4x6 No Cooling Spiral	(25C+1Cu)x3x4x4x5+Central Spiral	
No. of SC strands	1800	360	576	480	
No. of Copper strands	-	432	288	240	
Spiral Dimension (mm)	ID 7 / OD 12	ID 7 / OD 9	-	ID 7 / OD 9	
■ Void Fraction (%)	27.1	26.0	36.6	32.5	
■ Strand Type	High Jc (> 2600 A/mm ²) Nb ₃ Sn Strand 0.82 mm diameter (~450 ton + ~280 ton)	ITER type (Jc ~ 1000 A/mm ²) Nb ₃ Sn Strand 0.82 mm diameter (~102 ton + ~90 ton)			NbTi Strand 0.82 mm diameter (~90 ton)
■ Cu/non-Cu of Strand			1.0		
■ Insulation	1.6 mm (including Voltage Tap) (0.1 mm Kapton 400% + 0.3 mm S glass 400%)		2.0 mm (including Voltage Tap) (0.1 mm Kapton 400% + 0.4 mm S glass 400%)		
■ Jacket Thickness			5.0 mm		
■ Twist Pitch (mm)					
1st stage	80 ± 5	80 ± 5	27 ± 5	35 ± 5	
2nd stage	140 ± 10	140 ± 10	45 ± 10	75 ± 10	
3rd stage	190 ± 10	190 ± 10	85 ± 10	135 ± 10	
4th stage	245 ± 15	300 ± 15	150 ± 15	285 ± 15	
5th stage	415 ± 20	-	385 ± 20	410 ± 20	
■ Wrapping Tape					
Sub-cable wrap thickness			0.08 mm, 40% coverage		
Sub-cable wrap width			15 mm		
Cable wrap thickness			0.4 mm, 60% coverage		
Final wrap width			7 mm		

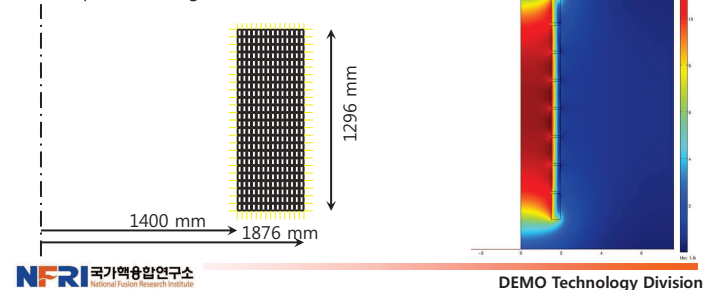
Overview of TF Coil

- Selected for Detailed Study (Maintenance Space = 2.5 m)
- Considering Vertical Maintenance Scheme
- $R = 6.8$ m, $a = 2.1$ m
- Small CICC Coil : 18 x 10 turns Large CICC Coil : 12 x 5 turns (Total : 240 turns)
- Magnetic Field at Plasma Center : ~7.4 Tesla (Bpeak ~ 16 Tesla, T-margin > 1 K)
- Nominal Current : 65.52 kA
- Conductor Length :
 - LQP = ~900 m (Quadruple Pancake) (Total : ~450 ton)
 - SDP = ~930 m (Double Pancake) (Total : ~280 ton)



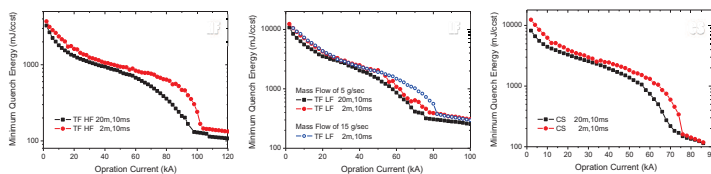
Overview of CS Coils

- Number of Turns : 14 (Total SC strand weight : ~102 tons)
- Number of Layers : CS1, CS2, CS3 & CS4 : 24 layers
- Magnetic Field at Center : ~11.8 T (Bpeak < 12.194 T, Half Flux Swing ~ 85 Wb)
- Conductor Unit Length : 885 m (CS1, CS2, CS3 & CS4 : UL x 4)
- Gap Between Coils : 104 mm
- Magnet Center Position : (1638, 700), (1638, 2100), (1638, 3500), (1638, 4900)
- Nominal Current : 42 kA (Current can be increased)
- Temperature Margin ~ 1.3 K



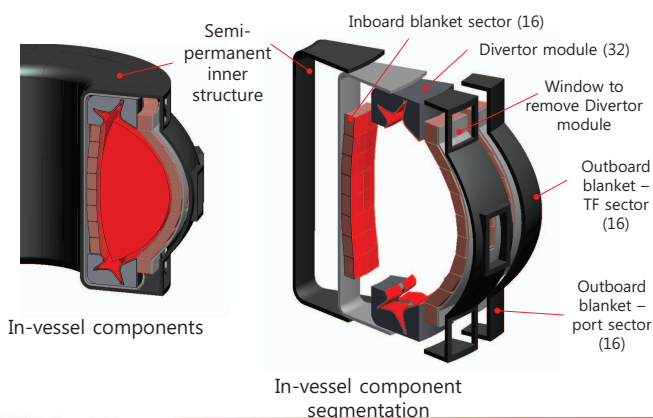
Stability Analysis of TF and CS CICC

- Gandalf Code has been used for the estimation.
- Assumption & Result
 - Gaussian shape DC heat pulse was applied for 10 ms at the center of the CICC's.
 - The nominal strain of -0.5% was assumed for the superconducting wires.
 - The field, temperature and strain dependence of the critical current density was estimated by the scaling law based on strong-coupling theory.
 - The percentage perforation of the separation perimeter between the bundle and hole He channels was set to 0.5 and the inlet pressure of 0.5 MPa case was studied.
 - For the HF CICC, the energy margin at an operation current of 65.52 kA is well above 500 mJ/ccst whether the heating zone is 2 or 20 m, even for the stagnant flow condition.
 - But for the LF conductor, the energy margin at the operation current is above 500 mJ/ccst, when there is a He mass flow of 5 g/sec at the flow path inlet. The energy margin was increased almost twice as the He mass flow increased to 15 g/sec.

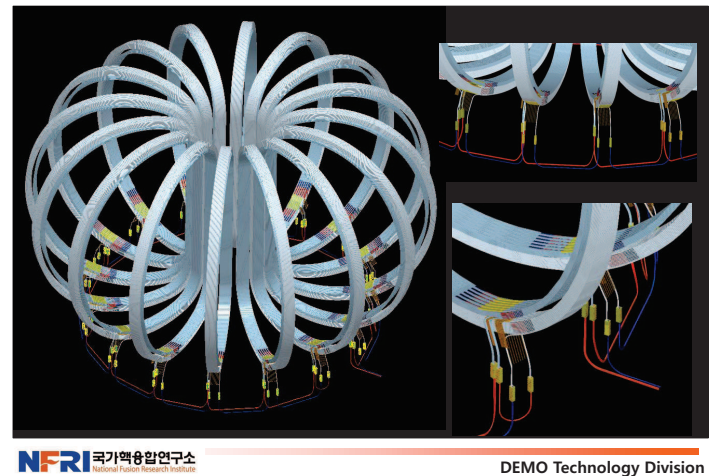


In-Vessel Components

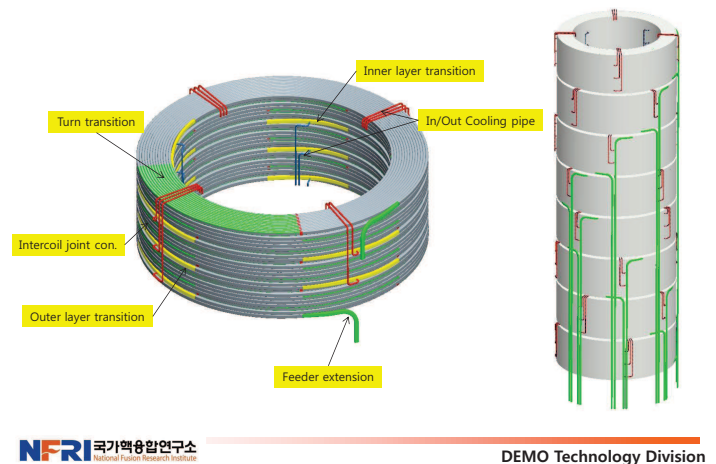
- In-Vessel Component Segmentation 22.5°



3D Modeling of TF Assembly

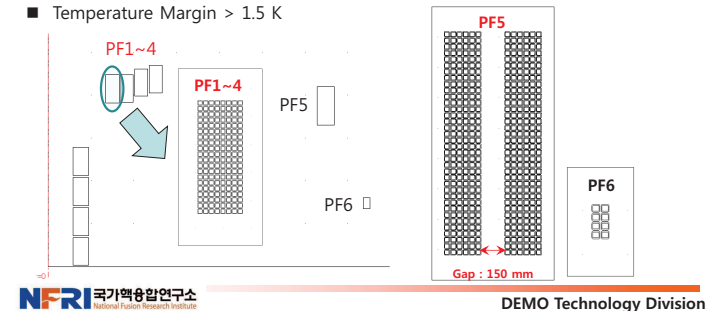


3D Modeling of CS Coils



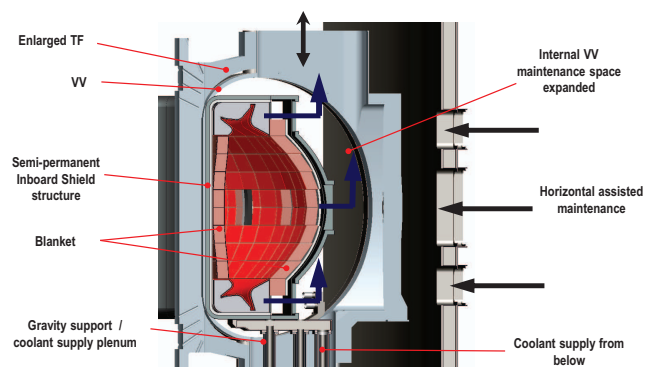
Overview of PF Coils

- Number of Turns : 8 turns for PF1~4, 12 for PF5, and 2 for PF6
- Number of Layers : 20 layers for PF1~4, 36 for PF5 and 4 for PF6
- Nominal Current : 36, 50, 50, 44, 37, 28 kA for PF1 to 6, respectively.
- Conductor Unit Length : 620, 755, 890 and 1030 m for PF1~4, 980 & 1010 m for PF5 and 770 m for PF6
- Coil Center Position : (2980, 8310), (3660, 8310), (4340, 8590) – PF1~3, (5020, 8750), (12762 & 13158, 7500), (14880, 2950) – PF4~6
- Temperature Margin > 1.5 K

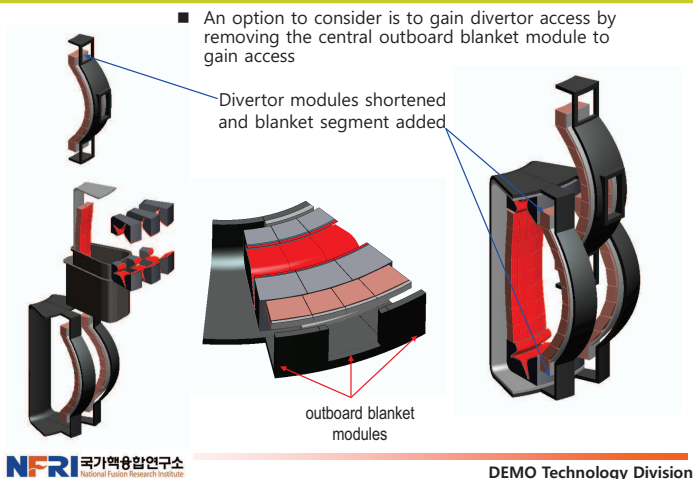


Concept of Vertical Maintenance [I]

- Vertical maintenance of all in-vessel components



Concept of Vertical Maintenance [II]

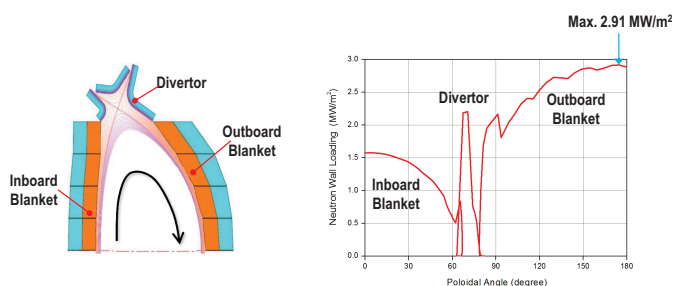


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Neutron Wall Loading Distribution

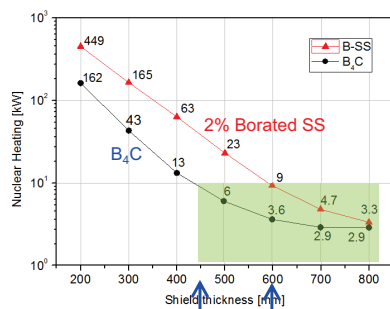
- Fusion power = 2200 MW



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Nuclear Heating in TF Coils



- 450 mm thick B₄C or 600 mm thick 2% Borated SS could reduce the nuclear heating in 16 TF coils below 10 kW.

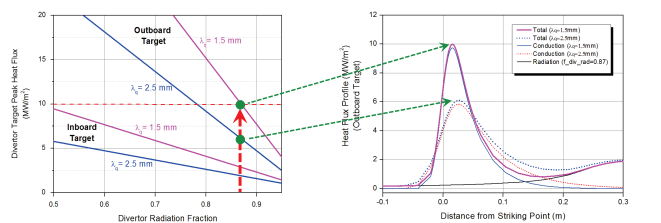
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Divertor Peak Heat Flux & Distribution

- Convection + radiation heat load (for 2.2 GW of fusion power)
 - Core radiation fraction = 40%
 - $\lambda q = 1.5 \sim 2.5$ mm
 - flux expansion = 4.3

- Divertor Radiation ~87% is required to meet Peak Heat flux = 10 MW/m² ($\lambda q = 1.5$ mm)



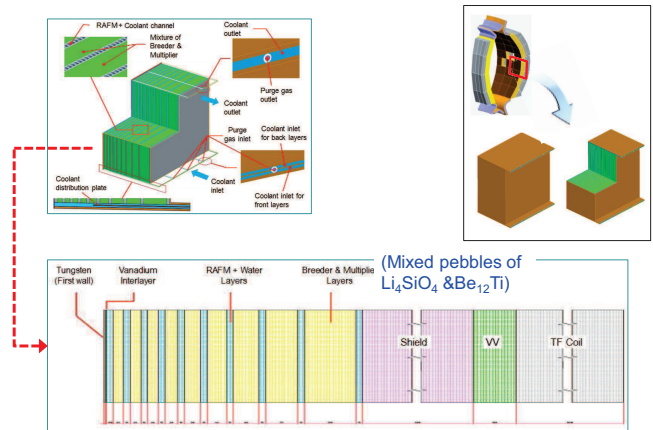
Peak Heat Flux vs. Divertor Radiation Fraction

Heat Flux Distribution at Outboard Divertor Target ($f_{rad,div} = 0.87$)

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Blanket Module Configuration (water cooling)

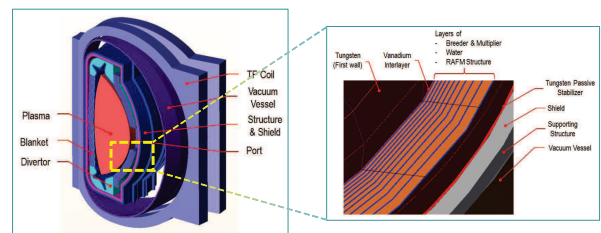


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3D Global TBR (Tritium Breeding Ratio)

- MCNP model – tokamak 45° sector



- MCNP Calculation with the help of MCAM developed by Chinese FDS team

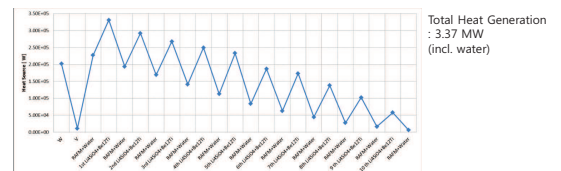
Breeder Pebble	Multiplier Pebble	Global TBR
Li ₄ SiO ₄	Be	> 1.20
Li ₄ SiO ₄	Be ₁₂ Ti	< 1.00 (so far)
Li ₄ SiO ₄ + Be ₁₂ Ti (Mixed pebbles)		~ 1.00 (so far)

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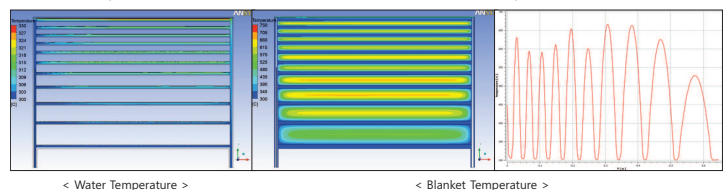
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Thermo-hydraulic Analysis on Blanket Module

- Heat generation vs. Pebble Layers (10 layers)



- Temperature distribution of blanket module (coolant speed = 10 m/s)



< Water Temperature >

< Blanket Temperature >

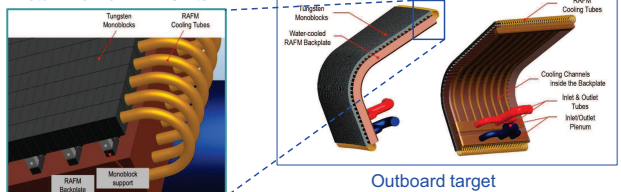
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Concept of Divertor

- Each divertor module is consisted of a central part, an inboard target, and an outboard target.
- High Heat Flux (HHF) unit:
 - Tungsten mono-blocks
 - RAFM cooling tube
 - Vanadium interlayer

Detail View of HHF Units

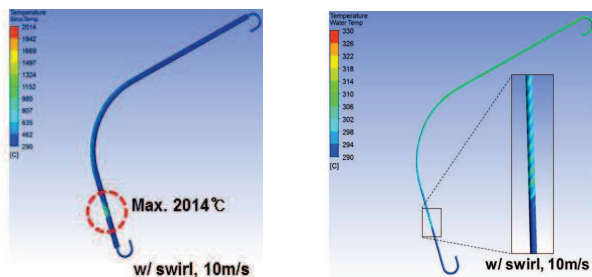


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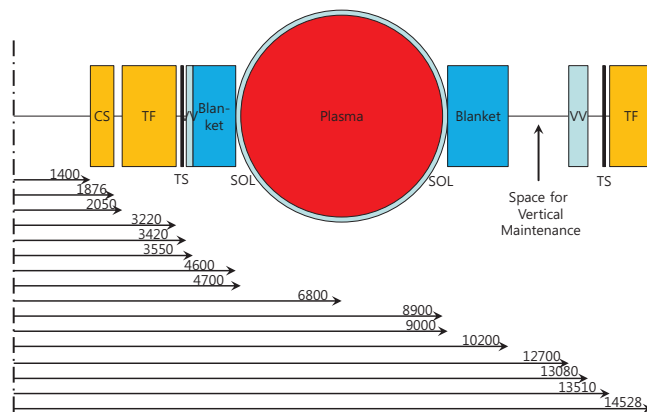
Preliminary Thermo-hydraulic Analyses

Thermo-hydraulic Analyses for the HHF unit



- Peak temperature of tungsten ~ 2000 °C
- Coolant temperature: 290~315 °C (15 MPa)
→ meet a PWR-like coolant conditions

Radial Build of K-DEMO [unit : mm]



K-DEMO Conceptual Study & CDA Schedule

2012.1~2012.12	2013.1~2013.12	2014.1~2014.12	2015.1~2017.12	2018.1~2021.12
Pre-study				
Memo for Pre-study				
Design Parameter				
		Circulation & Modification		
		Physics & Backup Study – Phase I		
		Physics & Backup Study – Phase II		
		Parameter Study & Conceptual Study Report		
		Improvement of Report		
		CDA & R&D Phase I		
		CDA & R&D Phase II + CDR		

Target Date for K-DEMO Construction : End of 2037

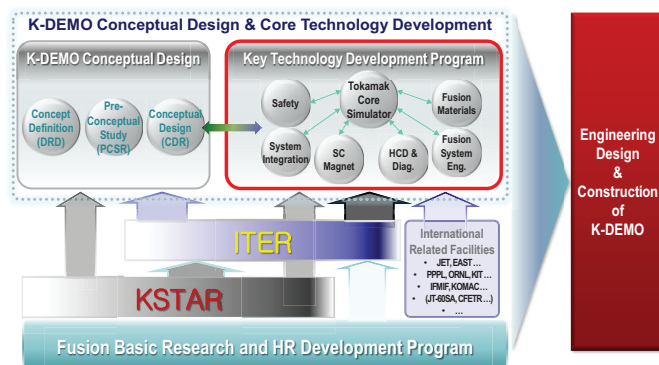
DEMO Core Technology Development Plan

Development of Core Technology

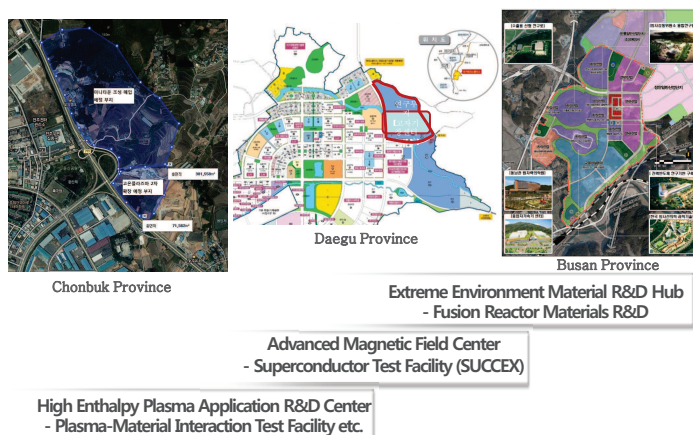
- 3 Major Research Fields, 7 Core Technologies, 18 Detail Technologies and 6 Major Research Facilities
- Through the complete technical planning process with the full participation of experts from all fields covering fusion, fission, physics, computing, mechanics, material, electric, electronics, and so on.

K-DEMO 3 Major Research Fields	K-DEMO 7 Core Technologies	Major Research Facilities
Design Basis Technology	Tokamak Core Plasma Technology	• Extreme Scale Simulation Center
	Reactor System Integration Technology	
	Safety and Licensing Technology	
Material Basis Technology	Fusion Materials Technology	• Fusion Materials Development Center • Fusion Neutron Irradiation Test Facility • SC Conductor Test Facility
	SC Magnet Technology	
	H&CD and Diagnostics Technology	
Machine and System Engineering Basis Technology	Heat Retrieval System Technology	• Blanket Test Facility • PMI Test Facility

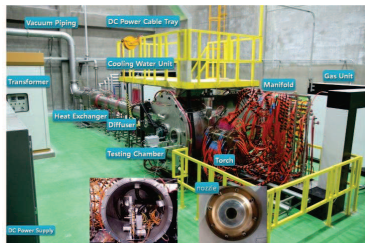
K-DEMO Design & Core Technology Development



Nation-wide DEMO R&D Center Planning

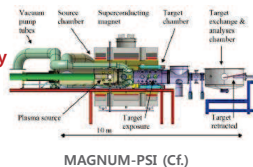


PMI Test Facility (Chonbuk Province)



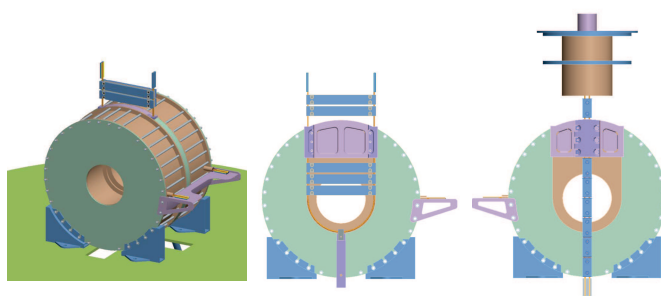
● 400kW High-Temperature Plasma Test Facility

- Upgrade Plasma Facility for PMI Test
- Additional, Blanket Test Facility

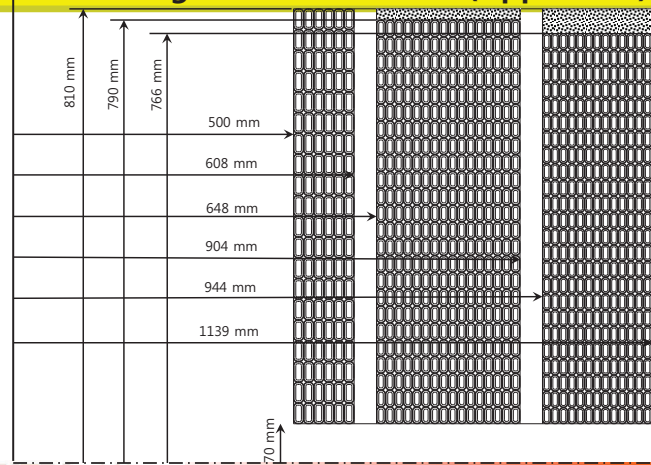


MAGNUM-PSI (CF)

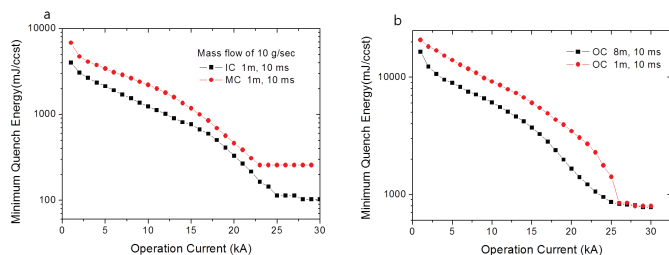
Conceptual View of SUCCEX



SUCCEX Magnet Cross-Section (Upper Coil)



Stability Analysis of SUCCEX Magnets

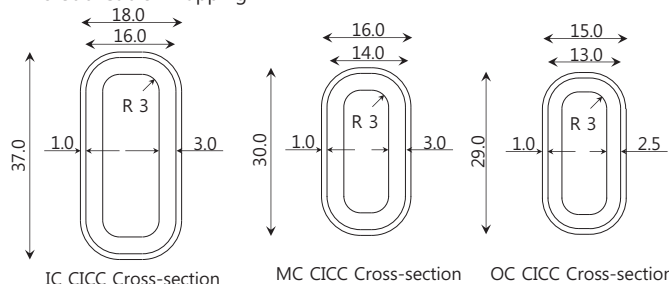


Superconductor Test(SUCCEX) Facility

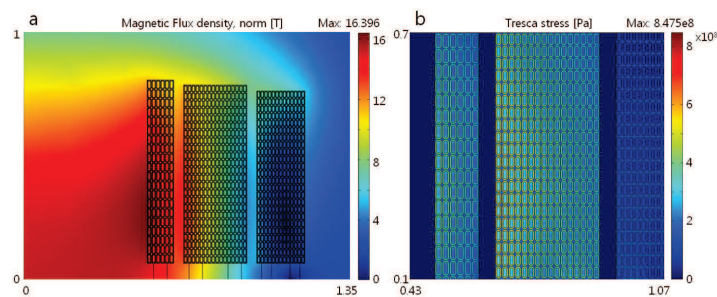
- SUCCEX : **S**uper**C**onducting **C**onductor **E**xperiment
- Split pair solenoid magnet system
- Inner bore size : ~1 m
- $B_{peak} \sim 16.39$ Tesla, $B_{center} \sim 15.33$ Tesla
- Maximum Helium flow channel length : < 100 m
 - One magnet of the split pair consists of three coil (IC, MC, OC) and the maximum of Helium channel length should be maintained below 100 m
 - Every double pancake of each coil will have Helium inlet and outlet
 - Each coil have a number of inter magnet joints because of the maximum fabrication capability in the length of CICC
- Test Mode
 - Semi-circle type conductor sample test mode
 - ✓ U-shape sample with the bottom radius of 0.5 m
 - ✓ DEMO TF conductor will have a rectangular cross-section to reduce the strain effect & will have capability of a minimum bending radius of 0.5 m
 - ✓ No joint : no question regarding voltage arising from the joint
 - ✓ There are enough distance for the voltage relaxation from the sample terminal to voltage taps
 - Sultan like sample test mode
 - ✓ For the case of CS conductor, the size of the is expected to be a range of 50 mm. And it is not easy to make the U-shape sample because of the minimum bending radius
 - ✓ Also the facility could support the joint technology development

Conductor Parameter of SUCCEX Magnets

- IC (Inner Coil) CICC : (3SC)x4x5x6[360 SC strand], VF = 27.62%
- MC (Middle Coil) CICC : (2SC+1Cu)x3x4x6[144 SC strand], VF = 26.96%
- OC (Outer Coil) CICC : (1SC+2Cu)x3x4x6[72 SC strand], VF = 26.96%
- Strand : High J_c (> 2600A/mm²) Nb3Sn (total ~ 6.8 ton)
- Twist Pitch : 50 mm ~ 110 mm ~ 170 mm ~ 290 mm
- No Sub-Cable Wrapping



Magnetic Field & Stress of SUCCEX Magnets

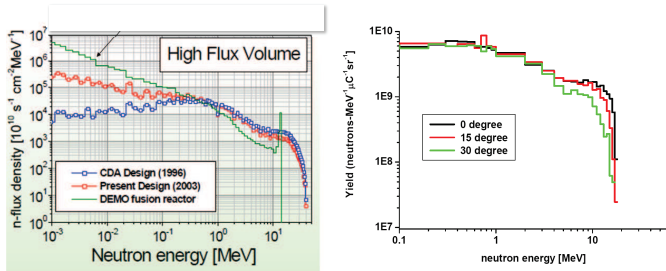


KOMAC Site (Gyeong-ju)



Neutron Energy Spectrum in KOMAC

Fusion Neutron similar Spectrum by Pulse-type Proton beam on Be-target (>1dpa/y)



(Ref) Institute for Materials Research, KIT
I. A. Moslang

Neutron Energy Spectrum in KOMAC

Summary

- The conceptual study on the Korean fusion demonstration reactor (K-DEMO) has been started in 2012, based on the National Fusion Roadmap released in 2005 and Korean Fusion Energy Development Promotion Law (FEDPL) enacted in 2007.
- After the thorough 0-D system analysis, the major radius and minor radius of K-DEMO are chosen to be 6.8 m and 2.1 m, respectively
- For matching the high frequency ECCD, the designed K-DEMO TF magnet system provides the magnetic field at the plasma center above 7 T with a peak field of ~16 T by using high performance Nb₃Sn-based superconducting strand.
- For a high availability operation, K-DEMO incorporates a vertical maintenance design.
- Pressurized water is the most prominent choice for the main coolant of K-DEMO when considering balance of plant development details.
- A global TBR greater than 1 is achieved using a water cooled ceramic breeder blanket system.
- Considering the plasma performance and the peak heat flux in the divertor system, a double-null divertor system becomes the reference choice of K-DEMO.

IFMIF(International Fusion Material Irradiation Facility)

