

ORNL-6551/V3

Spectroscopic Data for Titanium, Chromium, and Nickel

Volume 3. Nickel

W. L. Wiese and A. Musgrove, Editors



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ATOMIC DATA FOR FUSION - VOLUME VI

SPECTROSCOPIC DATA FOR TITANIUM, CHROMIUM, AND NICKEL Volume 3. Nickel

W. L. Wiese and A. Musgrove National Institute for Standards and Technology

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Date:	10-24-2019



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Series Preface

The primary objective of the Controlled Fusion Atomic Data Center at Oak Ridge National Laboratory is to publish handbooks containing numerical and graphical cross sections and other physical data relevant to fusion energy research. In 1977, a two-volume compilation was published as ORNL reports ORNL-5206 and ORNL-5207. Since that time, a large volume of pertinent data has become available, necessitating an update of the previous compilation. Plans are to include both cross sections and rate coefficients for collisional processes, and to publish the revised series in handbook form. The specific volumes which are in preparation are listed below, with their expected completion dates.

- Vol. 1, "Collisions of H, H₂, He, and Li Atoms and Ions with Atoms and Molecules," C. F. Barnett, ORNL (December 1989).
- Vol. 2, "Collisions of Electrons with Atoms and Molecules," J. W. Gallagher, National Institute of Standards and Technology; and D. C. Gregory, ORNL (December 1990).
- Vol. 3, "Particle Interactions with Surfaces," E. W. Thomas, Georgia Institute of Technology (January 1985).
- Vol. 4, "Spectroscopic Data for Iron," W. L. Wiese, National Bureau of Standards (March 1985).
- Vol. 5, "Collisions of Carbon and Oxygen Ions with Electrons, H, H₂, and He,"
 R. A. Phaneuf, ORNL; R. K. Janev, Institute of Physics, Yugoslavia; and
 M. S. Pindzola, Auburn University (January 1987).
- Vol. 6, "Spectroscopic Data for Titanium, Chromium, and Nickel," W. L. Wiese and A. Musgrove, National Institute for Standards and Technology (September 1989).

C. F. Barnett D. C. Gregory H. T. Hunter M. I. Kirkpatrick R. A. Phaneuf

Abstract

Comprehensive spectroscopic data tables are presented for all ionization stages of titanium, chromium, and nickel. Tables of ionization potentials, spectral lines, energy levels, and transition probabilities are presented. These tables contain data which have been excerpted from general critical compilations prepared under the sponsorship of the National Standard Reference Data System (NSRDS).

Spectroscopic Data for Titanium, Chromium, and Nickel – Volume 3. Nickel

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W. L. Wiese and A. Musgrove, Editors

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	[J. R. Fuhr, G. A. Martin, and W. L. Wiese]	F-1

General Introduction

This compendium contains a collection of recent spectroscopic data tables for titanium, chromium, and nickel. The tables are issued in three separate volumes, each containing one element. The individual volumes are identified as Oak Ridge National Laboratory ORNL 6551/V1 (titanium); ORNL 6551/V2 (chromium); and ORNL 6551/V3 (nickel). These chemical elements, together with the earlier tabulated¹ element iron, are the principal heavy metals which are widely used as firstwall materials (including limiters, armor plates, etc.) of magnetic fusion research machines, particularly tokamaks. Spectral radiation data for both high and low stages of ionization for Ti, Cr and Ni have thus become important for the assessment and modeling of the effects of impurities on plasma properties and power balance, for the study of plasma-wall interactions as well as for the application of plasma diagnostic techniques.

Numerical data are tabulated for those spectroscopic quantities which are of principal importance for such plasma studies and for plasma diagnostics. The specific spectroscopic quantities are ionization energies, wavelengths of allowed and forbidden lines, atomic energy levels, and atomic transition probabilities. Most of the critical evaluation and compilation work for these data has been done at the National Institute of Standards and Technology, formerly the National Bureau of Standards. The tables are usually parts of larger tabulations²⁻⁷ containing many other chemical elements besides Ti, Cr, and Ni. Excerpting the data from these larger compilations required some modifications in the reprinted material, especially the modification of the introductory remarks with comments and explanations that specifically refer to the Ti, Cr, and Ni spectra. All of the material is quite recent, and is under the sponsorship of the National Standard Reference Data System (NSRDS). Since the various data tables have been completed at different times, there may be occasional slight inconsistencies between overlapping material when the data are based on different sources. Also, sometimes there may be different judgments of independent evaluators on the quality of the source material. For example, wavelengths which are derived from atomic energy levels may be sometimes slightly different from the observed data in the wavelength tables. There also may be slight inconsistencies between the energy level data contained in the wavelength and transition probability tables when compared to the data in the energy level table itself. But any such differences are so small that they do not matter for any plasma applications, and therefore the use of any of the recent tabulations is appropriate. But we generally recommend to use the *primary* tables to obtain data on a specific atomic quantity.

Each of the three volumes of this compendium is divided into six sections which cover:

> Ionization energies, General spectral line lists, Vacuum ultraviolet lines, Magnetic dipole lines, Atomic energy levels, and Atomic transition probabilities.

The editors gratefully acknowledge the cooperation of the data compilers. We also thank NSRDS, the American Institute of Physics, and American Chemical Society for permission to reprint excerpts of these tables.

References

- W. L. Wiese, Editor, Spectroscopic Data for Iron, ORNL-6089 [1985], Fourth Volume of Oak Ridge Natl. Lab. Series 6086.
- Reader, C. H. Corliss, W. L. Wiese, and G. A. Martin, Wavelengths and Transition Probabilities for Atoms and Atomic Ions, Natl. Stand. Ref. Data Ser., Natl. Bur. Stand. (U.S.), 68, 415 pgs. [1980].
- R. L. Kelly, Atomic and Ionic Spectral Lines Below 2000 Å (H through Kr), J. Phys. Chem. Ref. Data 16, Suppl. 1 (1987).
- J. Sugar and C. Corliss, Atomic Energy Levels of the Iron-Period Elements: Potassium through Nickel, J. Phys. Chem. Ref. Data 14, Suppl. 2 [1985].
- V. Kaufman and J. Sugar, Forbidden Lines in ns²np^k Ground Configurations and nsnp Excitation Configurations of Be through Mo Atoms and Ions, J. Phys. Chem. Ref. Data 15, 321-416 [1986].
- G. A. Martin, J. R. Fuhr, and W. L. Wiese, Atomic Transition Probabilities-Scandium through Manganese, J. Phys. Chem. Ref. Data 17, Suppl. 3 [1988].
- J. R. Fuhr, G. A. Martin, and W. L. Wiese, Atomic Transition Probabilities-Iron through Nickel, J. Phys. Chem. Ref. Data 17, Suppl. 4 [1988].

A. Ionization Energies of Nickel Ions

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A. Ionization Energies of Nickel Ions

Spectrum	Ground State Configuration	Ground Level	Ionization Energy (eV)
Ni 1	1s ² 2s ² 2p ⁶ 3s ² 3p ⁶ 3d ⁸ 4s ²	³ F ₄	7.6375
Ni 11	$1s^2 2s^2 2p^6 3s^2 3p^6 3d^9$	$^{2}D_{5/2}$	18.16898
Ni III	$1s^22s^22p^63s^23p^63d^8$	³ F ₄	35.19
Ni IV	$1s^2 2s^2 2p^6 3s^2 3p^6 3d^7$	⁴ F _{9/2}	54.9
Ni v	$1s^2 2s^2 2p^6 3s^2 3p^6 3d^6$	${}^{5}D_{4}$	76.06
Ni vi	$1s^2 2s^2 2p^6 3s^2 3p^6 3d^5$	⁶ S _{5/2}	108
Ni VII	$1s^2 2s^2 2p^6 3s^2 3p^6 3d^4$	⁵ D ₀	133
Ni viii	$1s^{2}2s^{2}2p^{6}3s^{2}3p^{6}3d^{3}$	${}^{4}F_{3/2}$	162
Ni IX	$1s^2 2s^2 2p^6 3s^2 3p^6 3d^2$	${}^{3}\mathbf{F}_{2}$	193
Ni x	$1s^{2}2s^{2}2p^{6}3s^{2}3p^{6}3d$	$^{2}D_{3/2}$	224.6
Ni XI	$1s^2 2s^2 2p^6 3s^2 3p^6$	${}^{1}S_{0}$	321.0
Ni XII	$1s^2 2s^2 2p^6 3s^2 3p^5$	${}^{2}P_{3/2}^{\circ}$	352
Ni XIII	$1s^2 2s^2 2p^6 3s^2 3p^4$	${}^{3}P_{2}$	384
Ni xiv	$1s^2 2s^2 2p^6 3s^2 3p^3$	⁴ S _{3/2}	430
Ni xv	$1s^2 2s^2 2p^6 3s^2 3p^2$	${}^{3}P_{0}$	464
Ni xvi	$1s^2 2s^2 2p^6 3s^2 3p$	${}^{2}\mathbf{P}_{1/2}^{\circ}$	499
Ni xvii	$1s^2 2s^2 2p^6 3s^2$	${}^{1}S_{0}$	571.08
Ni xviii	$1s^{2}2s^{2}2p^{6}3s$	${}^{2}S_{1/2}$	607.06
Ni xix	$1s^2 2s^2 2p^6$	${}^{1}S_{0}$	1541
Ni xx	$1s^2 2s^2 2p^5$	${}^{2}P_{3/2}^{\circ}$	1648
Ni xxi	$1s^2 2s^2 2p^4$	${}^{3}P_{2}$	1756
Ni xxII	$1s^2 2s^2 2p^3$	⁴ S _{3/2}	1894
Ni XXIII	$1s^2 2s^2 2p^2$	${}^{3}P_{0}$	2011
Ni xxiv	$1s^2 2s^2 2p$	${}^{2}\mathbf{P_{1/2}^{o}}$	2131
Ni xxv	$1s^{2}2s^{2}$	${}^{1}S_{0}$	2295
Ni xxvi	$1s^{2}2s$	${}^{2}S_{1/2}$	2399.2
Ni xxvii	$1s^2$	$^{1}S_{0}$	10 288.8
Ni xxviii	15	${}^{2}S_{1/2}$	10 775.48

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. Mariji [Excerpted from: J. Sugar and C. Corliss, J. Phys. Chem. Ref. Data 14, Suppl. 2 (1985)]

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B. Prominent Spectral Lines for Ni 1 to Ni v

(Vacuum Ultraviolet to Near Infrared Regions)

[Excerpted from: J. Reader, C. H. Corliss, W. L. Wiese, and G. A. Martin, Natl. Stand. Ref. Data Ser., Natl. Bur. Stand. (U.S.) 68, 415 pgs. (1980); and J. Reader and C. H. Corliss, in *Handbook of Chemistry and Physics*, 70th Edition (1989)]

These lists were recently prepared under the auspices of the Committee of Line Spectra of the Elements of the National Academy of Sciences—National Research Council as part of a general wavelength table^{1,2}. The tables contain the outstanding spectral lines, — from the far ultraviolet to the far infrared, — of neutral (I), singly ionized (II), doubly ionized (III), triply ionized (IV), and quadruply ionized (V) nickel atoms. The lines are selected from larger lists (see references) in such a way as to include the stronger observed lines in each spectral region.

The data were compiled by Charles H. Corliss, NBS (Ni I – Ni V). For Ni I and II, the following literature references were used as the principal sources of data:

- W. F. Meggers, C. H. Corliss, and B. F. Scribner, Nat. Bur. Stand. (U.S.), Monogr. 145, Washington, D.C. (1975).
- A. G. Shenstone, J. Res. Nat. Bur. Stand. (U.S.) 74A, 801 (1970).

For Ni III, IV and V, the following references were used:

- A. G. Shenstone, J. Opt. Soc. Am. 44, 749 (1954).
- R. Poppe, Physica (Utrecht) 81C, 351 (1976).
- A. J. J. Raassen, T. A. M. van Kleef, B. C. Metsch, Physica (Utrecht) 84C, 133 (1976).

All wavelengths are given in Angstrom units (Å). Below 2000 Å, the wavelengths are in vacuum; above 2000 Å, the wavelengths are in air. Wavelengths given to three decimal places have an uncertainty of less than 0.001 Å and are, therefore, suitable for the calibration of most spectrometers. The line intensities are normally estimates of the relative strengths of lines which are not greatly separated in wavelength. However, because different sources are involved, based on different scales for the intensity estimates, these intensities are only useful as a rough indication of the appearances of the spectra. Furthermore, in the tables of first and second spectra the intensities of the lines of the singly ionized atoms relative to those of the neutral atom should be used with caution, inasmuch as the concentration of the ions in the light source depends greatly on the excitation conditions.

The descriptive symbols used in the tables have the following meaning:

- H hazy
- D line consists of two unresolved lines
- W wide

References

- J. Reader, C. H. Corliss, W. L. Wiese, and G. A. Martin, Wavelengths and Transition Probabilities for Atoms and Atomic Ions, Natl. Stand. Ref. Data Ser., Natl. Bur. Stand. (U.S.), 68, 415 ppg. (1980).
- J. Reader and C. H. Corliss, in Handbook of Chemistry and Physics, 70th Edition (R. C. Weast, Ed.), CRC Press, Inc., Boca Raton, FL (1989).

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Nickel (Ni)

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Intensity	Wavelength (Å)	Spectrum	Intensity	Wavelength (Å)	Spectrum
	Ni t and t		1400	0010.00	
	INI I and II		1400	2313.98	I
	Vacuum		1000	2316.04	п
			1400	2317.10	I
500	1317.22	II	500	2319.75	II
400	1335.20	II	2600	2320.03	I
500	1370.14	II	1900	2321.38	I
1000	1741.55	II	240	2322.68	I
500	1748.28	II	1400	2325.79	I
	Air		940	2329.96	I
1000			500	2334.58	II
1000	2165.55	II	460	2337.49	I
2000	2169.10	II	160	2337.82	I
2000	2174.67	II	500	2341.20	II
1500	2175.15	II	1200	2345.54	I
500	2177.09	II	190	2346.63	I
400	2177.36	II	400	2347.52	I
400	2179.35	II	160	2360.63	I
800	2180.47	II	200	2362.06	I
800	2184.60	II	1000	2375.42	II
2500	2185.50	II	240	2386.58	I
3000	2192.09	II	1000	2394.52	II
600	2201.41	II	2000	2416.13	I
5000	2205.55	II	240	2419.31	I
4000	2206.72	II	85	2421.23	I
6000	2216.48	II	70	2423.33	I
800	2220.40	п	70	2423.66	I
500	2221.06	II	70	2424.03	I
900	2222.96	II	500	2437.89	II
500	2242.68	п	85	2453.99	I
500	2253.85	II	160	2472.06	I
1000	2264.46	II	85	2476.87	I
2000	2270.21	II	500	2510.87	II
800	2277.28	11	500	2565.92	II
400	2278.32	II	500	2606.26	11
800	2278.77	II	500	2609.94	II
500	2287.65	II	500	2615.06	11
1600	2289.98	I	45	2696.49	I
400	2296.55	II	150	2798.65	I
400	2297.14	II	250	2821.29	I
630	2300.78	I	500	2864.02	II
1000	2303.00	п	50	2865.50	I
2000	2310.96	I	60	2907.46	I
1700	2312.34	I	25	2914.01	J
1400	2313.66	I	500	2943.91	I

Intensity	Wavelength (Å)	Spectrum	Intensity	Wavelength (Å)	Spectrum
570	2981.65	I	400	3335.64	Ш
250	2984.13	I	500	3338.09	п
500	2992.60	I	500	3348.84	II
1000	2994.46	I	500	3349.24	II
4000	3002.49	I	600	3358.68	II
2200	3003.63	I	330	3361.56	I
3700	3012.00	I	500	3363.45	п
350	3019.14	I	330	3365.77	I
120	3031.87	I	330	3366.17	I
1700	3037.94	I	65	3366.81	I
150	3045.01	T	65	3367.89	I
3500	3050.82	I	2900	3369.57	I
1500	3054.32	I	400	3371.99	I
1900	3057.64	I	260	3374.22	I
500	3064 62	I	130	3374 64	I
420	3080 76	I	500	3378 97	п
260	3097 12	T	3300	3380.57	I
200	3099.12	I I	240	3380.85	г Т
2600	3101 55	I T	1300	3391.05	T
1300	3101.55	T	3300	3392.99	T
220	3105.47	I I	500	3401.05	п
220	3105.47	1	130	3409 58	1
200	3134.12	I T	330	3413 48	T
2900	3134.11	I	330	3413.04	I
55	2191 74	I	8200	3414 76	1
100	2194 27	1	1600	2422 71	I
100	3104.37	I	2600	3423.71	I
150	2107 11	1	2000	2427.28	I
150	2202.14	1	4800	2446.26	I T
190	3202.14	1	1200	2452.80	I T
180	3214.00	1	5000	2452.07	I
100	3217.83	1	5000	2461 65	I
100	3221.27	1	3000	2467 50	I
150	3221.03	1	200	3407.30	I
210	3223.02	1	1600	2407.47	I
1100	3232.90	1	1000	34/2.34	I
290	3234.03	1	120	3403.//	I
6 00	3243.00	1	130	3483.89	I
100	3248.40	1	5500	3492.90	1
120	3250.74	1	65	3500.85	1
100	32/1.12	1	65	3502.00	I
120	3282.70	1	2600	3510 24	1
400	3272.81	11	2000	3510.34	1
500	327/.00	11	200	3515.93	1
400	3303./1	11	660	3515.05	1
000	3313.00	1	8200	3519.77	1
330	3320.20	I	8200	3324.34	1
310	3322.31	1	110	3521.90	1
2000	3331.88	п	330	3348.18	1

1 M

Intensity	Wavelength (Å)	Spectrum	Intensity	Wavelength (Å)	Spectrum
55	3551.53	I	40	4904.41	т
65	3561.75	I	22	4918.36	ī
5000	3566.37	ī	16	4935.83	T
990	3571.87	I	45	4980 16	I I
130	3587.93	ī	45	4984 13	1
1300	3597.70	T	500	4992 02	
1300	3610.46	T	16	H 5000 34	11
530	3612.74	T	18	5012.46	1
6600	3619.39	I	50	5017 59	1
130	3624 73	T	100	5035 37	1
200	3664 10	T	16	5049.95	1
130	3669.24	I I	100	5090 57	1
180	3670 43	1	65	5080.52	1
260	3674.15	I T	05	JU01.11	1
160	3688 13	1	20	E 2084.08	I
80	3603 03	1	10	5099.32	I
120	2722 49	1	20	H 5099.95	I
150	3726.91	1	21	5115.40	I
60	3730.81	1	18	H 5129.38	I
600	3739.23	1	23	5137.08	I
700	3//3.3/	I	23	H 5142.77	I
700	3783.33	I	40	H 5146.48	I
110	3807.14	I	40	H 5155.76	I
1200	3831.09	I	16	5168.66	I
1200	3858.30	I	13	5176.56	I
30	3889.67	I	8	5435.87	I
35	3972.17	I	180	5476.91	I
110	39/3.56	I	6	5510.00	I
110	4401.55	I	6	5578.73	I
85	4459.04	I	9	5587.86	I
18	4462.46	I	13	5592.28	I
55	4470.48	I	9	5614.79	I
35	4592.53	1	5	H 5625.33	I
18	4600.37	I	4	5649.70	I
65	4605.00	I	5	5664.02	I
18	4606.23	I	12	5682.20	I
75	4648.66	I	8	5695.00	I
23	4686.22	I	23	5709.56	I
110	4714.42	I	10	5711.90	I
22	4715.78	I	10	5715.09	I
30	4756.52	I	16	5754.68	I
15	4763.95	I	8	5760.85	I
45	4786.54	I	10	5857.76	I
22	4807.00	I	10	5892.88	I
22	H 4829.03	I	10	6108.12	I
19	4831.18	I	10	6176.81	I
45	4855.41	I	10	6191.18	I
30	4866.27	I	13	6256.36	I
17	4873 44		10	(214.66	-

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Intensity	Wavelength (Å)	Spectrum	Intensity	Wavelength (Å)	Spectrum
16	6643.64	I	300	722.09	III
22	6767.77	I	250	725.20	111
9	6772.32	I	500	729.82	111
10	6914.56	-	250	730.11	111
5	7110.90	ī	400	731 70	111
26	7122.20	I	300	732.16	111
6	7182.00	I	200	738.26	111
5	7197.02	I	300	747 99	111
5	7261.93	I	200	749.68	111
5	7291.45	I	300	750.05	111
4	7385.24	I	200	752.02	111
16	7393.60	T	300	757.80	111
16	7409.35	I	250	758 73	111
5	7414 51	I	250	758.75	111
23	7422.28	T	400	770.27	111
13	7522.20	T	200	772 04	111
9	7525.10	I	500	772.04	111
19	7525.12	I	200 F	785.02	111
8	7574.05	I	300	788.04	111
23	7617.00	I	200	788 30	111
25 Q	7619.21	T	200	805.01	111
16	7714 32	I	500	811 57	111
- 10 5 H	7715.52	T	500	826.14	111
19	7727 61	1	200	826.14	111
19	7748 80	1	500	842 14	111
10	7788 04	1	400	845.24	111
10	7707 50	I	200	947.42	111
15	7017 44	I	300	04/.43 957 00	111
1000	8006 75	1	200	857.09	111
500	8114 21	11	300	000.04	111
700	8121 AP	11	300	002.00	111
100	8800 42	11	300	003.22 967 51	111
2	0007.42	1	300	860 70	111
500 W	0002.33	1	200	809.70	111
500 ₩	3300.92	11	200	072 70	
	Ni III		300	973.79	111
	Vacuum		200	1120 07	111
100	675 68		200	1420.07	111
500	630 71	111	200	1454.51	111
200	637 54	111	300	1604 54	111
200	662 37	111	300	1652 97	111
150	663 57	111	200	1653 12	111
500	676 94	111	250	1656 13	111
200	700 17	111	200	1661 70	111
300	713 33	111	400	1687 90	111
300	713 38	111	1000	1692 51	111
500	718 48	111	200	1707 35	111
200	721 26	111	200	1707 43	111
200	121.20	111	1 200	1/0/.43	111

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Intensity	Wavelength (Å)	Spectrum	Intensity	Wavelength (Å)	Spectrun
800	1709.90	III	69	1419.58	IV
650	1715.30	III	74	1421.22	IV
500	1719.46	III	70	1427.45	IV
200	1721.26	III	67	1428.93	IV
400	1722.28	III	67	1435.24	IV
250	1733.13	III	70	1438.82	īv
500	1738.25	Ш	73	1449.01	IV
300	1739.78	III	76	1452.22	IV
300	1741.96	ш	70	1455.42	IV
550	1747.01	III	69	1472.63	IV
300	1752.43	ш	68	1476.82	īV
400	1753.01	III	73	1482.25	IV
800	1764.69	TII	67	1489.53	IV
500	1767.94	III	72	1489.83	IV
2000	1769.64	III	69	1493.01	īv
400	1776.07	111	74	1493.67	īv
200	1788.30	111	68	1498 71	īv
250	1790.40	111	71	1498 77	īv
200	1790.93	 III	72	1498 90	íV
200	1791.64	III	67	1499.97	īv
200	1794.90	III	70	1512 74	īv
300	1807.24	111	70	1516.66	IV
200	1811.69	111	73	1520.63	IV IV
300	1819.28	111	75	1525.31	IV IV
800	1823.06	111	74	1527.68	IV
400	1830.01	111	74	1527.80	ĩV
200	1830.08	111	76	1534.71	IV IV
650	1847.28	111	73	1537.25	IV IV
800	1854.15	111	69	1538.03	IV
300	1858.75		75	1543 41	IV
200	1930.43	111	74	1546.23	IV
200	1952.54	111	68	1548.04	IV
	Ni		69	1557.28	IV
	IN1 IV		67	1560.18	IV
2.2	Vacuum			Ni v	
00 20	392.08	IV		Vacuum	
52 40	393.24	IV			
49	424.40	IV	29	304.02	v
51	444.ZI	IV	55	315.24	v
65	409.07	IV	56	315.71	v
65	4(1.24 105 19	IV	03	330.79	V
03 66	400.42 526 00	IV	08	343.93	v
00 67	550.28 597.06	IV	78	347.34	v
0/	537.90	IV	70	347.46	v
58	1345.72	IV	67	347.72	v
69 7 -	1357.07	IV	71	348.10	v
76	1398.19	IV	69	350.77	v
74	1411.45	IV	69	353.59	v

Intensity	Wavelength (Å)	Spectrum	Intensity	Wavelength (Å)	Spectrum
72	354.18	v	70	370.62	v
76	354.42	v	67	371.31	v
68	354.49	v	68	371.76	v
68	355.61	v	67	373.60	v
70	355.78	v	72	377.68	v
65	357.37	v	70	393.91	v
69	358.57	v	66	394.31	v
68	358.58	v	66	395.24	v
66	359.47	v	41	400.59	v
69	365.62	v			

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C. Vacuum Ultraviolet Lines for Ni I through Ni XXVIII (Wavelengths and Classifications)

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C. Vacuum Ultraviolet Lines for Ni I through Ni XXVIII

[Excerpted from: R. L. Kelly, J. Phys. Chem. Ref. Data 16, Supplement 1 (1987)]

The following tables, including the introductory comments, are excerpted from a new tabulation by R. L. Kelly,¹ which supersedes and revises his previous tables published with Palumbo in 1973.²

The listed wavelength data are generally from observations, with lines of the helium-like and hydrogen-like ions (Ni XXVII and Ni XXVIII) as notable exceptions. But also in some cases where lines have been observed, wavelengths given here are those resulting from a comprehensive analysis of the spectrum rather than the measured values. A few lines have been predicted from unpublished extrapolations along isoelectronic sequences, and some unobserved weak lines in multiplets have been included for completeness. Such predicted values of wavelength are marked by the symbol P in the column labeled "Notes".

The lines are arranged in order of increasing wavelength within each spectrum, and the vacuum wavelengths are given as they are reported in the reference listed first for each line. A complete listing of these references is given at the end of these introductory comments. Where more than one publication reports the wavelength of the line, the decision as to which to retain was based primarily on the present author's judgement of the best value. This judgement was based on consideration of the dates of publication, on probable accuracy from the type of instrumentation used and the wavelength standards employed, on the spectroscopic source used, and on the comparison of the observations with the wavelengths predicted from the best known values of energy levels as described above.

With respect to the accuracy of the wavelength data, it is conservatively estimated that all wavelengths reported should have uncertainties of ten to twenty in the last digit given.

The listed intensities have been normalized to a maximum of 1000 for convenience in comparing the different references. The normalization procedure used was generally a linear or logarithmic transformation of the intensities reported by the original authors, depending on the particular case. Intensities given by different observers have seldom been found compatible, however, and the tabulated intensities should be used only as a rough estimate.

The transitions are shown in standard spectroscopic notation with the lower level given first, and the energy levels, i.e., energies above the ground state, are presented in units of 1000 cm^{-1} , each value being rounded off to conserve space. Additive uncertainties are indicated by B, C, K, etc. which may be thousands of cm⁻¹. The energy level data are taken from the files of the Naval Postgraduate School Spectroscopic Data Center (and thus do not necessarily agree with those tabulated in Section E of this book). The multiplet numbers assigned by C. E. Moore³ are given in a separate column. The classifications of the transitions are given in the accepted form, the primary references being the NBS spectroscopy tables.³⁴ For convenience, separate columns are used for showing the configurations, terms, and *J*-values. In the term column, the symbol g is used to denote the ground term. Otherwise, the term designation follows that of Cowan and Andrew.⁵

The parent terms are given where they are known and where they are not immediately obvious. The older practice of using primes, double primes, etc. to indicate that the parent term of a configuration is an excited state of the next higher ion has been abandoned. But the notation of a, b, c, ... (for even terms) and z, y, x, ... (for odd terms) to indicate the order of appearance of terms of the same multiplicity and same type has been continued.

A few descriptive symbols are used in the "Notes" column which have the following meanings:

- F line is forbidden by electric dipole selection rules
- Q uncertain classification
- P predicted value of wavelength

There are three classes of predicted lines:

- (a) lines that have been observed but for which calculations of wavelengths from energy levels are superior to the observations as in hydrogenic spectra and in other specific transitions.
- (b) lines which have not been observed but for which Ritz calculations between known levels can be made, as in many of the forbidden lines.
- (c) lines for which one or both of the energy levels have been found by Hartree-Fock type calculations, by interpolation, or by extrapolation.

These three classes are not separately distinguished in the "Notes" column.

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NICKEL , Z = 28Unclassified Lines

Multiplet Re	el. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	0	8.516						716
	30	8.549						716
	30	8.605						716
	20	8.649						716
	20	8.694						716
	3	9.135						1089
	10	9.482						1089
	20	10.215						716
	10	10.500						716
	10	10.580						716
	20	10.762						716
	20	10.902						716
	20	11.636						716
	20	12.250						716
	0	12.315						716
	30	12.552						716
	30	12.581						716
	20	12.759						716
	10	13 120						716
	10	13.658						716
	20	139 55					-	256
	20	140.52						256
	30	140.32						256
	50	141.06						256
	60	141.25				İ		256
	20	141.33						250
	50	141.70				1		250
	40	141.87						250
	40	142.22						250
	50	142.42						256
	50	115.00						200
	70	147.00						256
	50	148.62						256
	40	148.83						256
	30	149.21						256
	50	149.47						256
	40	149.97						256
	40	150.56						256
	30	151.70						256
	30	151.85						256
	30	155.62						256
	30	156.30						256
	40	156.68						256
	40	157.24						256
	40	158.00						256
	50	158.54						256
	30	160.38						256
	30	161.94						256
	40	162.16						256
	50	162.90						256
	70	165.43						256
	30	165.69						256
	40	165.81						256
	50	166.08						256
	50	166.29						256

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NI UNCLASSIFIED LINES - Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	50	166.46						256

NICKEL I (Ni ⁰⁺), Z = 28 Ground State $1s^22s^22p^63s^23p^63d^84s^2({}^{3}F_4)$ (28 electrons) Ionization Potential 61 600 cm⁻¹; 7.638 eV

Multiplet	Rel. Int.	$\lambda_{\rm vac}$ (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
47 23 47	50 50 150	1963.85 1968.90 1976.87	0.204786 - 51.1248 0.0 - 50.7895 0.204786 - 50.7895	3d ⁹ (a ² D)4s - 3d ⁸ (a ¹ G)4s4p(³ P [°]) 3d ⁸ 4s ² - 3d ⁸ (a ¹ G)4s4p(³ P [°]) 3d [°] (a ² D)4s - 3d ⁸ (a ¹ G)4s4p(³ P [°])	$a^{3}D - u^{3}F^{\circ}$ g $a^{3}F - u^{3}F^{\circ}$ $a^{3}D - u^{3}F^{\circ}$	3 - 3 4 - 4 3 - 4		602 602 602
47 47	100 200 100	1981.61 1990.25 1994.29	0.879813 - 51.34380 0.879813 - 51.1248 0.0 - 50.1428	$\begin{array}{l} 3d^9(a^2D)4s-3d^8(a^1G)4s4p(^3P^\circ)\\ 3d^9(a^2D)4s-3d^8(a^1G)4s4p(^3P^\circ)\\ 3d^8(a^2D)4s-3d^8(a^1G)4s4p(^3P^\circ)\\ 3d^84s^2-3d^9(a^2D)5p \end{array}$	$a^{3}D - u^{3}F^{\circ}$ $a^{3}D - u^{3}F^{\circ}$ $ga^{3}F - 5^{\circ}$	2 - 2 2 - 3 4 - 3		602 602 602
23	0	1999.53	1.332153 - 51.34380	$3d^{8}4s^{2} - 3d^{8}(a^{1}G)4s4p(^{3}P^{\circ})$	$ga^{3}F - u^{3}F^{\circ}$	3 – 2		602

NICKEL II (Ni ¹⁺), Z = 28 Ground State $1s^22s^22p^63s^23p^63d^9(^{2}D_{5/2})$ (27 electrons) Ionization Potential 146 541.56 cm⁻¹; 18.16898 eV

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	2	727.100	0.0 - 137.53596	$3d^9 - 3d^8(a^3F_4)7f$	g ² D - 4[4]°	$\frac{5}{2} - \frac{7}{2}$		835
	5	737.300	0.0 - 135.62940	$3d^9 - 3d^8(a^3F_3)6f$	$g^{2}D - 3[4]^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		835
	2	738.201	0.0 - 135.46486	$3d^{9} - 3d^{8}(a^{3}P)4f$	$g^2D - {}^2G^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		835
	1	738.548	0.0 - 135.40067	$3d^9 - 3d^8(a^3P_2)4f$	$g^2D - 2[4]^\circ$	$\frac{5}{2} - \frac{7}{2}$		835
	2	744.636	0.0 - 134.29499	3d° – 3d ⁸ (a³F₄)6f	g ² D - 4[3]°	$\frac{5}{2} - \frac{5}{2}$		835
	5	744.867	0.0 - 134.25285	3d ⁹ - 3d ⁸ (a ³ F ₄)6f	$g^2D - 4[3]^\circ$	$\frac{5}{2} - \frac{7}{2}$		835
	1	745.640	1.50694 - 135.61991	$3d^9 - 3d^8(a^3F_3)6f$	g ² D - 3[1]°	$\frac{3}{2} - \frac{3}{2}$		835
	5	746.241	1.50694 - 135.51292	$3d^9 - 3d^8(a^3P_2)4f$	g ² D – 2[2]°	$\frac{3}{2} - \frac{5}{2}$		835
	0	746.525	1.50694 - 135.46155	$3d^9 - 3d^8(a^3P_2)4f$	g ² D - 2[3]°	$\frac{3}{2} - \frac{5}{2}$		835
	0	752.403				ĺ		835
	4	752.626	0.0 - 132.86916	$3d^{9} - 3d^{8}(a^{1}D_{2})4f$	g ² D - 2[3]°	$\frac{5}{2} - \frac{7}{2}$		835
	1	767.898	0.0 - 130.22587	$3d^9 - 3d^8(a^3F_3)5f$	g ² D - 3[4]°	$\frac{5}{2} - \frac{7}{2}$		835
	1	771.626	1.50694 - 131.10318	$3d^9 - 3d^8(a^3F_2)5f$	g ² D - 2[2]°	$\frac{3}{2} - \frac{5}{2}$		835
	3	776.000	0.0 - 128.86700	3d ⁹ – 3d ⁸ (a ³ F₄)5f	g²D – 4[4]°	$\frac{5}{2} - \frac{7}{2}$		835
	5	776.078	0.0 - 128.85387	3d° – 3d8(a3F4)5f	g ² D - 4[3]°	$\frac{5}{2} - \frac{5}{2}$		835
	10	795.506	8.39390 - 134.10016	3d ⁸ (a ³ F)4s - 3d ⁷ (a ² F)4s4p(³ P°)	⁴F – v⁴G°	$\frac{9}{2} - \frac{11}{2}$		835
	200	797.074	8.39390 - 133.85304	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	⁴ F − v ⁴ F°	$\frac{9}{2} - \frac{9}{2}$		835
	150	797.088	8.39390 - 133.85083	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	⁴ F - s ⁴ D°	$\frac{9}{2} - \frac{7}{2}$		835
	30	798.518	1.50694 - 126.73882	3d° - 3d7(a4P)4s4p(1P°)	g ² D - x ⁴ S°	$\frac{3}{2} - \frac{3}{2}$		835
	2	799.145	8.39390 - 133.52802	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	⁴ F − v ⁴ F°	$\frac{9}{2} - \frac{7}{2}$		835
	100	802.292	9.33004 133.97333	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{4}F - s^{4}D^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		835
	15	803.064	9.33004 - 133.85304	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{4}\mathbf{F} - \mathbf{v}^{4}\mathbf{F}^{\circ}$	$\frac{7}{2} - \frac{9}{2}$		835
	150	805.168	9.33004 - 133.52802	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{4}F - v^{4}F^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		835
	30	806.188	10.11566 - 134.15628	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	4F - s4D°	$\frac{5}{2} - \frac{3}{2}$		835

NI II - Continued

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ultiplet Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J Notes	Reference
0	807.391	10.11566 - 133.97333	3d8(a3F)4s - 3d7(a2F)4s4p(3P°)	4F - s4D°	$\frac{5}{2} - \frac{5}{2}$	835
5	808.933	10.66389 - 134.28376	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{*})$	⁴ F – s ⁴ D°	$\frac{3}{2} - \frac{1}{2}$	835
0	809.772	10.66389 - 134.15628	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	⁴ F − s ⁴ D°	$\frac{1}{2} - \frac{1}{2}$	835
20	810.292	10.11566 - 133.52802	3d8(a3F)4s - 3d7(a2F)4s4p(3P°)	${}^{4}\mathbf{F} - \mathbf{v}^{4}\mathbf{F}^{\circ}$	$\frac{5}{2} - \frac{7}{2}$	835
2	811.389					835
100	812.388	10.11566 - 133.20930	3d8(a3F)4s - 3d7(a2F)4s4p(3P°)	⁴F - v⁴F°	$\frac{5}{2} - \frac{5}{2}$	835
2	813.602					835
5	814.050	13.55039 - 136.39285	3d ⁸ (a ³ F)4s - 3d ⁸ (¹ D)6p	² F - ² F [•]	$\frac{7}{2} - \frac{7}{2}$	835
5	815.570	10.11566 - 132.72948	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{1}D_{2})4f$	⁴F - 2[3]°	$\frac{5}{2} - \frac{5}{2}$	835
8	816.024	10.66389 - 133.20930	3d8(a3F)4s - 3d7(a2F)4s4p(3P°)	⁴ F − v ⁴ F°	$\frac{3}{2} - \frac{5}{2}$	835
30	816.150	10.66389 - 133.19019	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{4}\mathbf{F} - \mathbf{v}^{4}\mathbf{F}^{\circ}$	$\frac{3}{2} - \frac{3}{2}$	835
150	816.156	13.55039 - 136.07626	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{2}\mathbf{F} - \mathbf{v}^{2}\mathbf{G}^{\circ}$	$\frac{7}{2} - \frac{9}{2}$	835
1	816.864					835
1	817.884	8.39390 - 130.66132	3d ⁸ (a ³ F)4s - 3d ⁸ (a ³ F₄)7p	⁴F - ⁴G°	$\frac{9}{2} - \frac{11}{2}$	835
5	819.090	8.39390 - 130.48055	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{3}F_{4})7p$	⁴F - ⁴D°	$\frac{9}{2} - \frac{7}{2}$	835
1	821.612	13.55039 - 135.26199	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{3}F_{4})8p$	² F − ⁴ G °	$\frac{7}{2} - \frac{9}{2}$	835
20	821.634	13.55039 - 135.25892	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}P)4s4p(^{1}P^{\circ})$	${}^{2}\mathbf{F} - \mathbf{v}^{2}\mathbf{D}^{\circ}$	$\frac{7}{2} - \frac{5}{2}$	835
1	821.875					835
3	823.277	14.99557 - 136.46110	$3d^8(a^3F)4s - 3d^7(a^2P)4s4p(^1P^\circ)$	${}^{2}\mathbf{F} - \mathbf{v}^{2}\mathbf{D}^{\circ}$	$\frac{5}{2} - \frac{3}{2}$	835
2	824.856	13.55039 - 134.78314	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{2}\mathbf{F} - \mathbf{w}^{2}\mathbf{D}^{*}$	$\frac{1}{2} - \frac{5}{2}$	835
10	828.152	14.99557 - 135.74606	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{2}\mathbf{F} - \mathbf{v}^{2}\mathbf{G}^{\circ}$	3-3	835
1	828.786	9.33004 - 129.98805	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}P)4s4p(^{1}P^{\circ})$	${}^{4}\mathbf{F} - \mathbf{t}^{4}\mathbf{D}^{*}$	1 - 2	835
2	830.677	,			2 2	835
2	831.475	0.0 - 120.26881	3d° – 3d8(a3F3)4f	g ² D - 3[4]°	$\frac{5}{2} - \frac{7}{2}$	835
100	834.059	13.55039 - 133.44575	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	${}^{2}F - w^{2}G^{\circ}$	7 - 2	835
0	835.739	1.50694 - 121.16181	$3d^9 - 3d^8(a^3F_2)4f$	$g^2D - 2[2]^\circ$	$\frac{1}{3} - \frac{1}{3}$	835
75	835.983	13.55039 - 133.16992	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	$^{2}\mathbf{F} - \mathbf{w}^{2}\mathbf{F}^{*}$	$\frac{1}{2} - \frac{1}{2}$	835
1	836.954	13.55039 - 133.03100	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{1}D_{2})4f$	${}^{2}F - 2[5]^{\circ}$	$\frac{2}{3} - \frac{2}{3}$	835
50	837.624	14.99557 - 134.38082	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	${}^{2}F - w^{2}G^{\circ}$	<u>5</u> <u>-</u> <u>7</u>	835
10	838.224	14.99557 - 134.29499	3d8(a3F)4s - 3d8(a3F4)6f	² F – 4[3]°	$\frac{5}{2} - \frac{5}{2}$	835
1	838.524	14.99557 - 134.25285	3d ⁸ (a³F)4s – 3d ⁸ (a³F₄)6f	² F - 4[3]°	$\frac{5}{2} - \frac{7}{2}$	835
50	838.834	14.99557 - 134.20830	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	${}^{2}\mathbf{F} - \mathbf{w}^{2}\mathbf{F}^{\circ}$	3-3	835
5	840.878	0.0 - 118.92320	$3d^9 - 3d^8(a^3F_4)4f$	g ² D - 4[4]°	2 - 7	835
10	841.056	0.0 - 118.89794	$3d^9 - 3d^8(a^3F_4)4f$	$g^2D - 4[3]^\circ$	3-5	835
0	841.205	0.0 - 118.87709	$3d^9 - 3d^8(a^3F_4)4f$	$g^2D - 4[2]^\circ$	5_1	835
2	844.748	13.55039 - 131.92877	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{3}F_{3})7p$	$^{2}\mathbf{F} - ^{2}\mathbf{G}^{\circ}$	$\frac{7}{2} - \frac{9}{2}$	835
3	845.033					835
5	849.086					835
5	849.398					835
3	854.604					835
5	855.282	13.55039 - 130.47090	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{3}F_{4})7p$	² F - ⁴ F°	$\frac{7}{2} - \frac{9}{2}$	835
2	858.562					835
0	876.829	8.39390 - 122.44122	3d ⁸ (a ³ F)4s - 3d ⁸ (a ³ F₄)6p	⁴F – ⁴F°	$\frac{9}{2} - \frac{9}{2}$	835
2	881.608	8.39390 - 121.82297	3d8(a3F)4s - 3d8(a3F4)6p	⁴ F − ⁴ D°	$\frac{9}{2} - \frac{7}{2}$	835
1	882.337					835
5	888.818	8.39390 - 120.90320	3d ⁸ (a ³ F)4s - 3d ⁸ (a ³ P)5p	${}^{4}F - {}^{4}D^{\circ}$	$\frac{9}{2} - \frac{7}{2}$	835
3	893.630					835
2	894.004	23.10828 - 134.96478	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}\mathbf{D} - \mathbf{w}^{2}\mathbf{D}^{\circ}$	$\frac{5}{2} - \frac{3}{2}$	835
1	895.093	9.33004 - 121.05066	3d8(a3F)4s - 3d8(a3P)5D	${}^{4}F - {}^{4}D^{\circ}$	7-5	835
15	895.458	23.10828 - 134.78314	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}\mathbf{D} - \mathbf{w}^{2}\mathbf{D}^{\circ}$	5-5	835
5	896,168	23.79618-135.38253	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{2}P)4s4p(^{1}P^{2})$	$^{2}\mathbf{D} - \mathbf{w}^{2}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{3}{2}$	835
2	898,716	10.11566 - 121.38580	$3d^8(a^3F)4s - 3d^8(a^3P)5p$	⁴ F – ⁴ D [•]	$\frac{5}{2} - \frac{3}{2}$	835
5	898.821	23.79618 - 135.05314	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{2}P)4s4p(^{1}P^{*})$	$^{2}D - w^{2}P^{\circ}$	$\frac{1}{3} - \frac{1}{2}$	835
		2011/010 100100011			1 1 1	
0	900.510	23.10828 - 134.15628	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{2}F)4s4n(^{3}P^{\circ})$	$^{2}D - s^{4}D^{0}$	3 - 3	835

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NI II - Continued

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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ¹)	Configurations	Terms	J - J Not	es References
	10	901.007	23.79618 - 134.78314	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}D - w^{2}D^{\circ}$	$\frac{3}{2} - \frac{5}{2}$	835
	2	901 737	10 66389 - 121 56106	$3d^{8}(a^{3}F)4s = 3d^{8}(a^{3}P)5n$	⁴ F – ⁴ D°	3_1	835
	50	901 999	73 10828 - 133 97333	$3d^{8}(a^{1}D)4s = 3d^{7}(a^{2}E)4s4n(^{3}P^{2})$	$^{2}D = s^{4}D^{9}$	\$ 5	835
	1	007.697	25.10828 - 155.97555	50 (a D) + 5 = 50 (a T) + 5 + p(T)	D = 3 D	2 - 2	935
	75	902.007	22 10828 122 85082	$2d^{3}(-1D)A_{2} = 2d^{7}(-2E)A_{2}A_{2}(-3D^{2})$	2D a4D°	5 7	035
	/5	902.996	23.10828 - 133.85083	$3d^{2}(a^{2}D)4s = 3d^{2}(a^{2}F)4s4p(^{2}F)$	$^{-}D - S^{-}D$	$\frac{1}{2} - \frac{1}{2}$	835
	2	904.205	24.78820 - 135.38253	$3d^{\circ}(a^{2}P)4s - 3d'(a^{2}P)4s4p('P')$	*P - w ² P*	$\frac{2}{2} - \frac{2}{2}$	835
	1	904.986	8.39390 - 118.89299	3d ⁸ (a ³ F)4s - 3d ⁸ (a ³ F ₄)4f	⁴ F − 4[¹¹ / ₂]°	$\frac{9}{2} - \frac{11}{2}$	835
	100	905.634	23.10828 - 133.52802	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{2}\mathbf{D} - \mathbf{v}^{4}\mathbf{F}^{\circ}$	$\frac{5}{2} - \frac{7}{2}$	835
	3	905.696	23.79618 - 134.20830	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	${}^{2}\mathbf{D} - \mathbf{w}^{2}\mathbf{F}^{\circ}$	$\frac{3}{2} - \frac{5}{2}$	835
	15	906.123	23.79618 - 134.15628	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}D - s^{4}D^{\circ}$	$\frac{3}{3} - \frac{3}{3}$	835
	2	906.237	25.03638 - 135.38253	$3d^{*}(a^{3}P)4s - 3d^{7}(a^{2}P)4s4n(^{1}P^{\circ})$	${}^{4}\mathbf{P} - \mathbf{w}^{2}\mathbf{P}^{\circ}$	3_3	835
	1	906.730				2 2	835
	{						
	1	906.906	24.78820 - 135.05314	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{2}P)4s4p(^{1}P^{\circ})$	${}^{4}\mathbf{P} - \mathbf{w}^{2}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{1}{2}$	835
	50	907.630	23.79618 - 133.97333	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	² D – s⁴ D °	$\frac{3}{2} - \frac{5}{2}$	835
	10	907.692	8.39390 - 118.56339	3d ⁸ (a ³ F)4s - 3d ⁸ (a ¹ D)5p	⁴ F - ² F [•]	$\frac{9}{2} - \frac{7}{2}$	835
	40	908.258	23.10828 - 133.20930	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{2}\mathbf{D} - \mathbf{v}^{4}\mathbf{F}^{\circ}$	5-5	835
	20	908.584	23.10828 - 133.16992	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	${}^{2}\mathbf{D} - \mathbf{w}^{2}\mathbf{F}^{*}$	$\frac{5}{2} - \frac{7}{2}$	835
	10	909.683	25.03638 - 134.96478	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{4}\mathbf{P} - \mathbf{w}^{2}\mathbf{D}^{\circ}$	$\frac{5}{2} - \frac{3}{2}$	835
	16	011 107	25 02/20 124 50214		40 204	5 5	
	15	911.187	25.03638 - 134.78314	$3d^{(a^{+}P)}4s - 3d^{(a^{+}F)}4s4p(^{+}P^{-})$	$^{*}P - W^{2}D^{*}$		835
	2	913.187	24.78820 - 134.29499	3d^(a'P)4s – 3d^(a'F₄)6f	*P – 4[3]*	$\frac{1}{2} - \frac{1}{2}$	835
	3	913.279	24.78820 - 134.28376	3d*(a'P)4s - 3d'(a'F)4s4p('P°)	*P – s*D°	$\frac{1}{2} - \frac{1}{2}$	835
	75	913.678	24.83593 - 134.28376	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	⁴ P – s ⁴ D °	$\frac{1}{2} - \frac{1}{2}$	835
	15	913.909	24.78820 - 134.20830	$3d^{*}(a^{3}P)4s - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	${}^{4}\mathbf{P} - \mathbf{w}^{2}\mathbf{F}^{\circ}$	$\frac{3}{2} - \frac{5}{2}$	835
	50	914.343	24.78820 - 134.15628	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	4P - s⁴D°	$\frac{3}{2} - \frac{3}{2}$	835
	40	914,743	24.83593 - 134.15628	$3d^{8}(a^{3}P)4s = 3d^{7}(a^{2}F)4s4n(^{3}P^{2})$	4P – s⁴D°	1_3	835
	1	915.471	9 33004 - 118 56339	$3d^{*}(a^{3}F)4s = 3d^{*}(a^{1}D)5n$	${}^{4}\mathbf{F} - {}^{2}\mathbf{F}^{9}$	² / ₁ ² / ₂	835
	75	915 877	24 78820 - 133 97333	$3d^{8}(a^{3}P)4s = 3d^{7}(a^{2}F)4s4n(^{3}P^{2})$	4P - s4D°	1 _ 1 _ 1	835
	30	915 920	8 30300 - 117 57368	$3d^{8}(a^{3}F)Ac = 3d^{7}(a^{2}D)AcAc(^{3}P^{2})$	4E	2 2 2 2 2 2	825
	1	016 440	23 10828 132 22515	3d(a1)As = 3d(aD)AsAp(1D)	2D4D°	2 2 2	035
	10	917.017	933004 - 11837911	$3d^{8}(a^{3}E)/(a - 3d^{8}(a^{1}D))/(a - 3d^{8}(a^{1}D))/(a - 3d^{8}(a^{1}D))/(a - 3d^{8}(a^{1}D))/(a - 3d^{8}(a^{1}D))/(a - 3d^{8}(a^{1}D))/(a - 3d^{1}(a^{1}D))/(a - 3d^{1}(a$	D = V P $4E = 2E^{\circ}$	2 - 2 2 - 2 2 - 2	835
	10	517.017	9.55004 - 110.57911	50 (a 1745 - 50 (a D)5p	r - r	2 - 2	835
	15	917.962	25.03638 - 133.97333	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	⁴ P - s ⁴ D°	$\frac{5}{2} - \frac{5}{2}$	835
	3	918.022					835
	4	918.946					835
	150	918.994	25.03638 - 133.85083	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	4P - s4D°	$\frac{5}{2} - \frac{7}{2}$	835
	10	920.451	9.33004 - 117.97247	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}D)4s4p(^{3}P^{\circ})$	⁴ F − w ⁴ F°	$\frac{7}{2} - \frac{7}{2}$	835
	2	921.228					835
	1	921,299	9.33004 - 117.87278	$3d^{8}(a^{3}F)4s = 3d^{8}(a^{1}D)5n$	4F - 2D°	7_5	835
	75	921,730	25.03638 - 133 52802	$3d^{8}(a^{3}P)4s = 3d^{7}(a^{2}F)4s4r(^{3}P^{2})$	${}^{4}P = v{}^{4}F^{\circ}$	5 1	835
	5	922,176	20100000 100102002		1 - 1 1	2 - 2	835
	15	922 331	24 78820 - 133 20030	$2d^{8}(a^{3}\mathbf{D})Aa = 2d^{7}(a^{2}\mathbf{E})AaAm(^{3}\mathbf{D}^{0})$	4D4E?	3 5	835
	1	922.551	24.78820 - 155.20950	5u(ar)+s=5u(ar)+s+p(r)	F - V F	2 - 2	035
	1	924.710	13.55039 - 121.69255	3d ⁸ (a ³ F)4s - 3d ⁷ (a ² H)4s4p(³ P°)	${}^{2}\mathbf{F} - \mathbf{x}^{2}\mathbf{G}^{\circ}$	$\frac{7}{2} - \frac{9}{2}$	835
	10	924.783	25.03638 - 133.16992	3d*(a'P)4s - 3d ⁷ (a ² G)4s4p('P°)	${}^{4}\mathbf{P} - \mathbf{w}^{2}\mathbf{F}^{*}$	$\frac{2}{2} - \frac{1}{2}$	835
	20	924.912	8.39390 - 116.51206	3d ⁸ (a ³ F)4s - 3d ⁷ (a ² D)4s4p(³ P°)	${}^{4}\mathbf{F} - \mathbf{v}^{4}\mathbf{D}^{\circ}$	$\frac{9}{2} - \frac{7}{2}$	835
	2	925.100					835
	3	925.544					835
	1	925.578	23.79618 - 131.83494	$3d^{(a^{1}D)4s} - 3d^{(a^{4}P)4s4p(^{1}P^{)})$	${}^{2}D - v^{4}P^{\circ}$	3-5	835
	5	927.820	10.66389 - 118.44281	3d*(a ³ F)4s - 3d*(a ¹ D)5p	${}^{4}\mathbf{F} - {}^{2}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{3}{2}$	835
	2	978 052	10 11566 - 117 76301	348(a3E)4a 248(a1D)5-	40 200	5 3	825
	1	070 494	13 55030 . 121 12641	$3d^{3}(a^{3}E)4a^{-3}d^{3}(a^{3}E)4a$		2 - 2	835
		727.300	13,30037 + 121.12341	$3d^{2}(a^{2}F)4s = 3d^{2}(a^{2}F_{2})4t$	·r - 2[5]	$\frac{1}{2} - \frac{1}{2}$	835
	3	929.081	9.33004 - 116.89398	3d"(a"F)4s - 3d'(a"D)4s4p("P")	"F - v"D"	2 - 2	835
	3	929.831	10.11500 - 117.66211	3d°(a°F)4s - 3d′(a°D)4s4p(°P°)	•F - v •D°	$\frac{2}{2} - \frac{3}{2}$	835
	10	930.351					835
	3	930.707	29.07093 - 136.51720	3d"(a'P)4s - 3d"(a'F ₂)6f	² P – 2[1]°	$\frac{1}{2} - \frac{1}{2}$	835

NI II -- Continued

Multiplet Re	el. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	1	931.191	24.83593 - 132.22515	3d8(a3P)4s - 3d7(a4P)4s4p(1P°)	⁴ P - v ⁴ P ^o	$\frac{1}{2} - \frac{3}{2}$		835
	2	931.501	13.55039 - 120.90320	3d ⁸ (a ³ F)4s - 3d ⁸ (a ³ P)5p	² F - ⁴ D ^o	$\frac{7}{2} - \frac{7}{2}$		835
	2	932.321						835
	2	933.339	0.0 - 107.14221	3d ⁹ – 3d°(a ³ F ₂)5p	$g^2D - {}^2D^\circ$	$\frac{2}{2} - \frac{2}{2}$		835
		933.421	0.0 107.09221	249 248(-35)5-	20 20	5 5		835
	1	933.866	0.0 - 107.08221	3d" – 3d"(a"F ₂)5p	g*D - *F*	2 - 2		835
	2	935.085						835
	1	935.200			4- 4-4	0 7		835
	1	936.188	8.39390 - 115.20985	3d°(a°F)4s - 3d′(a*F)4s4p('P*)	"F – x"G"	2 - 2		835
	15	936.704	0.20200 114.05000		45 400	9 11		835
	20	939.276 940.886	8.39390 - 114.85888 9.33004 - 115.61288	$3d^{\circ}(a^{-}F)4s = 3d^{\circ}(a^{-}H)4s4p(^{-}P^{-})$ $3d^{8}(a^{3}F)4s = 3d^{7}(a^{2}H)4s4p(^{3}P^{\circ})$	⁴ F - w ⁴ G ⁶	$\frac{1}{2} - \frac{1}{2}$		835 835
	10	941.972	10.11566 - 116.27581	3d°(a°F)4s - 3d′(a²H)4s4p('P')	*F - w*G*	$\frac{1}{2} - \frac{1}{2}$		835
	4	941.996						835
	2	942.360	10 ((200 11 (75 (02			3 5		835
	2	942.587	10.06389 - 116.75493	$3d^{\circ}(a^{\circ}F)4s = 3d^{\circ}(a^{\circ}H)4s4p(^{\circ}P^{\circ})$ $248(-3P)4s = 247(-2F)4-4-(3P^{\circ})$	$^{2}P - WG^{2}$	$\frac{1}{2} - \frac{1}{2}$		835
	1	944.343	29.07093 - 134.96478	$3d^{\circ}(a^{\circ}P)4s = 3d^{\circ}(a^{\circ}P)4s4p(^{\circ}P^{\circ})$	P - WD	$\frac{1}{2} - \frac{1}{2}$		835
	30	944.034	0.0 - 105.86119	3d" ~ 3d"(a"F3)5p	g-DD	$\bar{2} - \bar{2}$		835
	10	944.842	0.0 - 105.83806	3d ⁹ - 3d ⁸ (a ³ F ₃)5p	$g^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		835
	75	945.965	29.07093 - 134.78314	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}\mathbf{P} - \mathbf{w}^{2}\mathbf{D}^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		835
	15	946.657	1.50694 - 107.14221	$3d^9 - 3d^8(a^3F_2)5p$	$g^2D - {}^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$		835
	3	946.769	32.49953 - 138.12188	3d ⁸ (a ¹ G)4s - 3d ⁸ (a ³ F₄)9p	² G – ⁴ F°	$\frac{9}{2} - \frac{9}{2}$		835
	2	947.195	1.50694 - 107.08221	$3d^9 - 3d^8(a^3F_2)5p$	$g^2D - {}^2F^{\circ}$	$\frac{3}{2} - \frac{2}{2}$		835
	0	949.024	29.59346 - 134.96478	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}P - w^{2}D^{\circ}$	$\frac{1}{2} - \frac{3}{2}$	ĺĺĺ	835
	1	949.137	8.39390 - 113.75304	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{1}P^{\circ})$	⁴F - x⁴G°	$\frac{9}{2} - \frac{9}{2}$		835
	1	952.027	32.52354 - 137.56274	3d ⁸ (a ¹ G)4s - 3d ⁸ (a ³ F ₂)8p	$^{2}G - ^{2}G^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		835
	8	952.266	13.55039 - 118.56339	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{1}D)5p$	${}^{2}\mathbf{F} - {}^{2}\mathbf{F}^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		835
	1	952.340	10.11566 - 115.12000	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{1}P^{\circ})$	${}^{4}\mathbf{F} - \mathbf{x}{}^{4}\mathbf{F}{}^{\circ}$	$\frac{2}{2} - \frac{2}{2}$		835
	10	953.033	8.39390 - 113.32195	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{1}P^{\circ})$	${}^{4}\mathbf{F} - \mathbf{x}{}^{4}\mathbf{F}{}^{\circ}$	$\frac{y}{2} - \frac{y}{2}$		835
	2	953.937	13.55039 - 118.37911	3d*(a'F)4s - 3d*(a'D)5p	² F - ² F °	$\frac{1}{2} - \frac{2}{2}$		835
	1	954.911	9.33004 - 114.05204	3d8(a3F)4s - 3d7(a4F)4s4p(1P*)	⁴ F - x ⁴ F°	$\frac{7}{2} - \frac{7}{2}$		835
	10	955.601	0.0 - 104.64652	3d ⁹ - 3d ⁸ (a ³ F ₄)5p	g²D - ⁴F°	$\frac{2}{2} - \frac{1}{2}$		835
	3	956.912	0.0 - 104.50322	3d° – 3d8(a³F₄)5p	$g^2D - {}^4D^\circ$	$\frac{2}{2} - \frac{2}{2}$		835
	5	959.931	32.49953 - 136.67364	$3d^{8}(a^{1}G)4s - 3d^{8}(a^{3}F_{3})8p$	² G - ² G°	2 - 2		835
	5	960.261	29.07093 - 133.20930	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}P - v^{4}F^{\circ}$	$\frac{2}{2} - \frac{2}{2}$		835
	5	960.269	29.07093 - 133.20930	3d*(a*P)4s - 3d'(a*F)4s4p(*P*)	²P – v⁴F°	$\frac{1}{2} - \frac{1}{2}$		835
	1	961.516	32.52354 - 136.52442	3d8(a1G)4s - 3d8(a3F2)6f	² G – 2[5]°	$\frac{7}{2} - \frac{9}{2}$		835
	1	962.526	32.49953 - 136.39285	3d ⁸ (a ¹ G)4s - 3d ⁸ (¹ D)6p	² G - ² F°	2-2		835
1	1	962.750	32.52354 - 136.39285	3d°(a'G)4s – 3d°('D)6p	'G - 'F'	2-2		835
	15	963.855	22 40052 126 07626	218(10)4, 217(20)4,4-(10)	20	9 9		835
	20 20	965.470 968.784	32.49953 - 136.07626 32.52354 - 135.74606	$3d^{\circ}(a^{\circ}G)4s - 3d^{\circ}(a^{2}F)4s4p(^{2}P^{\circ})$ $3d^{8}(a^{1}G)4s - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}G - v^{2}G^{2}$ $^{2}G - v^{2}G^{2}$	$\frac{1}{2} - \frac{1}{2}$ $\frac{1}{3} - \frac{1}{3}$		835 835
Í								
	50	971.415	32.52354 - 135.46486	$3d^{8}(a^{1}G)4s - 3d^{8}(a^{3}P)4f$	$^{2}G - ^{2}G^{\circ}$	2 - 2		835
	1	973.121	32.49953 - 135.26199	3d ⁸ (a'G)4s - 3d ⁸ (a'F ₄)8p	'G - ⁺G°	$\frac{2}{2} - \frac{2}{2}$		835
	10	977.276						835
	25	978.108						835
	3	980.290	20 10 11 10 10000		20 200	7 7		835
	50	981.768	32.52354 - 134.38082	3d°(a'G)4s - 3d'(a'G)4s4p('P°)	'G − w'G'	2 - 2		835
	3	983.004	32.52354 - 134.25285	3d8(a1G)4s - 3d8(a3F4)6f	² G - 4[3]°	$\frac{7}{2} - \frac{7}{2}$		835
	1	983.431	32.52354 - 134.20830	$3d^{8}(a^{1}G)4s - 3d^{7}(a^{2}G)4s4p(^{1}P^{*})$	$^{2}G - w^{2}F^{\circ}$	$\frac{1}{2} - \frac{3}{2}$		835
	2	983.592	10.11566 - 111.78379	3d ⁸ (a ³ F)4s - 3d ⁷ (a ² G)4s4p(³ P [*])	⁴F – y⁴G*	$\frac{2}{2} - \frac{1}{2}$		835
	10	985.918						835
	2	986.992						835
	4	987.339						835

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NI II - Continued

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fultiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	References
	10	988.338						835
	100	990.626	32.49953 - 133.44575	3d ⁸ (a ¹ G)4s - 3d ⁷ (a ² G)4s4p(¹ P°)	$^{2}G - w^{2}G^{\circ}$	$\frac{9}{2} - \frac{9}{2}$		835
	20	992.516	8.39390 - 109.14805	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}G)4s4p(^{3}P^{\circ})$	⁴F – y⁴F°	$\frac{9}{2} - \frac{9}{2}$		835
	15	993.128	9.33004 - 110.02192	3d ⁸ (a ³ F)4s - 3d ⁷ (a ² G)4s4p(³ P [°])	⁴F – y⁴G°	$\frac{7}{2} - \frac{9}{2}$		835
	1	993.341	32.49953 - 133.16992	$3d^{8}(a^{1}G)4s - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	${}^{2}G - w^{2}F^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		835
	10	994.867	9.33004 - 109.84600	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}G)4s4p(^{3}P^{\circ})$	⁴ F − y ⁴ F°	$\frac{7}{2} - \frac{7}{2}$		835
	30	995.256						835
	4	995.445	10.11566 - 110.57336	3d ⁸ (a ³ F)4s - 3d ⁷ (a ² G)4s4p(³ P [°])	⁴F – y⁴F°	$\frac{5}{2} - \frac{5}{2}$		835
	3	995.453	10.66389 - 111.12054	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{2}G)4s4p(^{3}P^{\circ})$	⁴F – y⁴F°	$\frac{3}{2} - \frac{3}{2}$		835
	1	997.974	13.55039 - 113.75304	3d ⁸ (a ³ F)4s - 3d ⁷ (a ⁴ F)4s4p(¹ P°)	${}^{2}F - x^{4}G^{\circ}$	$\frac{7}{2} - \frac{9}{2}$		835
	5	1004.170				1		835
	8	1005.021						835
	1	1006.712					ļ	835
	10	1008.218					1	835
	20	1016.622				1		835
	8	1016.677						835
	5	1019.067						835
	5	1021.060						835
	3	1023.961	23.79618 - 121.45632	3d ⁸ (a ¹ D)4s - 3d ⁸ (a ³ P)5p	² D - ⁴ S°	3-3		835
	15	1023.999				2 2		835
	50	1024.720	8.39390 - 105.98150	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}P)4s4p(^{3}P^{\circ})$	${}^{4}\mathbf{F} - \mathbf{v}^{6}\mathbf{D}^{\circ}$	<u> ३_म</u>		835
	2	1025.591				2 2		835
	5	1025.641						835
	5	1026.981						835
	20	1028 208						925
	1	1031 306	24 83593 - 121 80034	$3d^{8}(a^{3}\mathbf{P})4s = 3d^{8}(a^{3}\mathbf{P})5n$	${}^{4}\mathbf{P} = {}^{2}\mathbf{D}^{9}$	1_3		835
	2	1032 749	24.05555 - 121.00054	5u (a 1)45 - 5u (a 1)5p	1 - D	2 - 2		835
	10	1033 443	25 03638 - 121 80034	$3d^8(a^3P)4s = 3d^8(a^3P)5p$	${}^{4}P = {}^{2}D^{9}$	2 3	•	835
	15	1034 155	25.05050 - 121.00054	5u (a 1)+3 - 5u (a 1)5p	I - D	2 - 2		835
	10	1034.249	23.10828 - 119.79698	3d*(a1D)4s - 3d*(a3P)5p	${}^{2}D - {}^{4}P^{\circ}$	$\frac{5}{2} - \frac{5}{2}$		835
	,	1036 182	9 33004 - 105 83806	3d*(a ³ E)4s - 3d*(a ³ E.)5p	4E - 2E°	1_1		835
	5	1038 866	9 33004 - 105 58889	$3d^{8}(a^{3}E)4s = 3d^{8}(a^{3}E)5p$	${}^{4}F = {}^{2}G^{\circ}$	2 2		835
	ĩ	1040.668	7.55004 - 105.50007	50 (a 1)45 - 50 (a 1 3)5p	1 - 0	2 - 2		835
	2	1042.704	8 39390 - 104 29823	$3d^{8}(a^{3}E)4s = 3d^{8}(a^{3}E)5n$	⁴ F - ⁴ G°	2 2		835
	30	1044.349	8.39390 - 104 14729	$3d^8(a^3F)4s = 3d^8(a^3F)4s$	⁴ F - ⁴ G°	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		835
	2	1044.871	10.66389 - 106.36930	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{3}F_{2})5p$	${}^{4}\mathbf{F} - {}^{4}\mathbf{F}^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		835
	15	1045.073	8.39390 - 104.08104	3d ⁸ (a ³ F)4s − 3d ⁸ (a ³ F ₂)5n	⁴ F – ⁴ F°	$\frac{9}{2} - \frac{9}{2}$		835
	5	1045.813	10.66389 - 106.28316	$3d^{(a^{3}F)4s} - 3d^{(a^{3}F)4s}$	⁴ F - ⁴ G°	3_3		835
	8	1046.537	10.11566 - 105.66878	$3d^{(a^{3}F)}4s = 3d^{(a^{3}F)}5n$	⁴ F – ⁴ F°	\$_\$		835
	1	1047.497			• •	2 2		835
	6	1048.400	10.11566 - 105.49905	$3d^{8}(a^{3}F)4s = 3d^{8}(a^{3}F)5r$	4F - 4G°	5 _ 7		835
	1	1048.936	23.10828 - 118.44281	3d ⁸ (a ¹ D)4s - 3d ⁸ (a ¹ D)5p	${}^{2}\mathbf{D} - {}^{2}\mathbf{P}^{\circ}$	$\frac{5}{2} - \frac{1}{2}$	1	835
	3	1048 982	24 83593 - 120 16652	3d8(a3D)4e - 3d8(a3D)5n	4P 4P°	13		835
	ĩ	1049.051	10.11566 - 105.43985	$3d^{8}(a^{3}E)4s = 3d^{8}(a^{3}E)5n$	4F _ 4D°	2 2		835
	8	1049 137	9 33004 - 104 64652	$3d^8(a^3F)4s = 3d^8(a^3F)5s$	4E_4E°	$\frac{2}{2}$ $\frac{2}{2}$ $\frac{2}{2}$		835
	100	1049.755	8 39 390 - 103 65303	$3d^{8}(a^{3}E)4s = 3d^{8}(a^{3}E)5p$	4E _ 4D°	$\frac{2}{2}$ $\frac{2}{2}$ $\frac{2}{2}$		835
	3	1050 718	9 33004 104 50222	$3d^8(a^3E)4s = 3d^8(a^3E)4s$	4F - 4D°	2 2 2		835
	10	1052.534	24.78820 - 119.79698	$3d^8(a^3P)4s - 3d^8(a^3P)5p$	⁴ P – ⁴ P°	$\frac{2}{2} - \frac{2}{2}$		835
	,	1052 092	0 33004 104 20222	2d8(a3E)4a 248(a3E)4a	+E 4C*	7 9		075
	2	1052.983	9.33004 - 104.29823	30"(a"F')4s - 30"(a"F4)5p	"F - "G"	$\frac{1}{2} - \frac{1}{2}$		835
	15	1053.729	22 10928 117 07270			5 C		835
	15	1055.246	23.10828 - 117.87278	3d°(a'D)4s - 3d°(a'D)5p	$^{2}D - ^{2}D^{\circ}$	2 - 2		835
	30	1055.291	25.03638 - 119.79698	3d°(a°P)4s – 3d°(a°P)5p	ч Р – Ч	$\frac{2}{2} - \frac{2}{2}$		835
	2	1056.837						835
	1	1062.243						835

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NI II - Continued

lultiplet Rel. In	t. λ_{vac} (in Å)	Levels (in 10^3 cm 3)	Configurations	Terms	J - J	Notes	References
1	1062.965	23.79618 - 117.87278	3d*(a'D)4s - 3d*(a'D)5p	${}^{2}\mathbf{D} - {}^{2}\mathbf{D}^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		835
1	1066.476			1			835
10	1070.590	25.03638 - 118.44281	3d°(a°P)4s - 3d°(a'D)5p	*P – *P*	2 - 2		835
1	1074.224			10 200			835
3	1075.551	24.78820 - 117.76391	$3d^{\circ}(a^{\circ}P)4s = 3d^{\circ}(a^{\circ}D)5p$	$^{4}P - ^{2}D^{4}$	$\frac{1}{2} - \frac{1}{2}$		835
2	1076.006	25.03638 - 117.97247	$3d^{*}(a^{*}P)4s - 3d^{*}(a^{2}D)4s4p(^{*}P^{*})$	*P – w*F*	$\frac{1}{2} - \frac{1}{2}$		835
4	1077.163	25.03638 - 117.87278	3d ^x (a ³ P)4s - 3d ⁸ (a ³ D)5p	${}^{4}\mathbf{P} - {}^{2}\mathbf{D}^{\circ}$	\$ - \$		835
200	1081.035	32.49953 - 125.00344	$3d^{*}(a^{1}G)4s - 3d^{7}(a^{2}H)4s4p(^{3}P^{\circ})$	² G – y ² H°	$\frac{9}{2} - \frac{11}{2}$		835
150	1085.441	32.52354 - 124.65200	$3d^{s}(a^{1}G)4s - 3d^{7}(a^{2}H)4s4p(^{3}P^{\circ})$	² G – y ² H°	$\frac{1}{2} - \frac{9}{2}$		835
4	1086.503	13.55039 - 105.58889	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{3}F_{3})5p$	${}^{2}\mathbf{F} - {}^{2}\mathbf{G}^{\circ}$	$\frac{7}{2} - \frac{9}{2}$		835
4	1091.407	14.99557 - 106.62053	$3d^{s}(a^{3}F)4s - 3d^{s}(a^{3}F_{2})5p$	${}^{2}\mathbf{F} - {}^{2}\mathbf{G}^{\circ}$	$\frac{2}{2} - \frac{7}{2}$		835
1	1099.471	13.55039 - 104.50322	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{3}F_{4})5p$	${}^{2}\mathbf{F} - {}^{4}\mathbf{D}^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		835
2	1101.893						835
5	1101.956	13.55039 - 104.29823	3d*(a ³ F)4s - 3d*(a ³ F ₄)5p	² F − ⁴ G°	$\frac{7}{2} - \frac{9}{2}$	1	835
1	1104.602	13.55039 - 104.08104	$3d^{x}(a^{3}F)4s - 3d^{x}(a^{3}F_{4})5p$	² F - ⁴ F°	$\frac{7}{2} - \frac{9}{2}$		835
1	1105.315						835
30	1108.729						835
1	1109.022						835
2	1114.260						835
40	1116.557	29.07093 - 118.63195	$3d^{8}(a^{3}P)4s = 3d^{8}(a^{1}D)5p$	${}^{2}P - {}^{2}P^{\circ}$	3-1		835
20	1118 404						835
25	1118 547						835
10	1118 921	29 07093 - 118 44281	$3d^{3}(a^{3}P)4s = 3d^{3}(a^{3}D)5p$	${}^{2}P - {}^{2}P^{\circ}$	3_3		835
75	1119.330	32.52354 - 121.86257	$3d^{*}(a^{1}G)4s - 3d^{7}(a^{2}H)4s4p(^{3}P^{\circ})$	² G - x ² G°	$\frac{1}{2} - \frac{1}{2}$		835
125	1121.162	23 40052 131 60355	$2d^{3}(a^{1}(a^{2})) = 2d^{7}(a^{2}U) A_{0} A_{0}(^{3}D^{0})$		2 9		075
123	1121.102	32.49955 - 121.09255	3d(a G)4s - 3d(a G)4s4p(F)	20 - X-0	$\frac{1}{2} - \frac{1}{2}$		833
2	1123.113	29.59346 - 118.63195	3d (a P)4s - 3d (a D)5p	·P - ·P	2 - 2		835
4	1127.112	20.07002 117.76201		2 D 2 D 2	33	1	835
75	1127.480	29.07093 - 117.70391	3d(aF)4s - 3d(aD)3p	P = D	$\frac{1}{2} - \frac{1}{2}$		833
150	1133.730	8 20200 06 52587	$3d^{2}(a^{2}F)4s = 3d^{2}(a^{4}F)4s4p(^{3}P^{2})$	$F = 2^{2}D^{2}$	2 2 2		833
150	1134.333	8.39390 - 90.33387	5u (a r)4s - 5u (a r)4s4p(r)	F - 2 D	2 - 2		635
1	1135.412						835
1	1136.360				7.		835
100	1137.091	9.33004 - 97.27383	3d*(a'F)4s - 3d'(a'F)4s4p('P°)	⁺F – z⁺D°	$\frac{1}{2} - \frac{2}{2}$		835
10	1138.547						835
3	1139.009	51.04546 - 138.84100	3d ⁷ 4s ² – 3d ⁸ (a ³ P)6p	'F - 'D'	$\frac{2}{2} - \frac{1}{2}$		835
75	1139.638	14.99557 - 102.74274	$3d^{*}(a^{+}F)4s - 3d^{-}(a^{+}F)4s4p(^{+}P^{*})$	${}^{2}\mathbf{F} - \mathbf{z}^{2}\mathbf{D}^{\circ}$	$\frac{2}{2} - \frac{3}{2}$		835
75	1140.459	10.11566 - 97.79966	3d*(a ³ F)4s - 3d ⁷ (a ⁴ F)4s4p(³ P°)	⁴ F - z ⁴ D°	$\frac{5}{2} - \frac{3}{2}$		835
2	1141.579						835
1	1141.891						835
50	1143.397	10.66389 - 98.12263	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	⁴ F – z⁴D°	$\frac{3}{2} - \frac{1}{2}$		835
5	1144.874	10 44 380 07 70044	$2 + \frac{3}{2} + $		3.3		835
	1147.033	10.00389 - 97.79900	5u(ar)+s - 5u(ar)+s+p(r)	F - 2 D	2 - 2		633
1	1149.239						835
2	1153.439						835
150	1154.416	8.39390 - 95.01771	$3d^{(a'F)4s} - 3d^{(a'F)4s4p('P')}$	*F – z*G*	$\frac{2}{2} - \frac{2}{2}$		835
2	1156.319						835
1	1157.132	10.11566 - 96.53587	$3d^{*}(a^{*}F)4s - 3d'(a^{*}F)4s4p(^{*}P^{*})$	${}^{4}F - z^{4}D^{\circ}$	2-2		835
100	1158.830	13.55039 - 99.84413	3d^(a'F)4s - 3d'(a'F)4s4p('P°)	⁻F – z⁻G°	$\frac{1}{2} - \frac{1}{2}$		835
150	1159.510	9.33004 - 95.57339	$3d^{(a^{3}F)4s} - 3d^{(a^{4}F)4s4p(^{3}P^{\circ})$	⁴F - z⁴G°	$\frac{2}{2} - \frac{2}{2}$		835
2	1160.776	51.55785 - 137.70726	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{4})8d$	⁴D° - ⁴D	$\frac{1}{2} - \frac{1}{2}$		835
1	1160.823				· ·		835
15	1161.297						835
1	1161.927	32.49953 - 118.56339	$3d^{k}(a^{T}G)4s - 3d^{k}(a^{T}D)5p$	${}^{2}G - {}^{2}F^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		835
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NI II - Continued

Multiplet Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
8	1162.492						835
1	1162.601						835
150	1162.748	8.39390 - 94.39674	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	⁴ F − z ⁴ G°	$\frac{9}{2} - \frac{11}{2}$		835
50	1163.645	10.11566 - 96.05248	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	⁴ F − z ⁴ G°	$\frac{5}{2} - \frac{5}{2}$		835
8	1163.729	23.10828 - 109.03884	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{4}P)4s4p(^{3}P^{\circ})$	${}^{2}\mathbf{D} - \mathbf{z}^{6}\mathbf{P}^{\circ}$	$\frac{5}{2} - \frac{3}{2}$		835
4	1163.880	20110020 107100001					835
150	1164.279	8.39390 - 94.28394	3d*(a3F)4s - 3d7(a4F)4s4p(3P°)	${}^{4}F - z^{4}F^{\circ}$	$\frac{9}{2} - \frac{9}{2}$		835
100	1164.574	13.55039 - 99.41861	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	$^{2}\mathbf{F} - \mathbf{z}^{2}\mathbf{F}^{\circ}$	$\frac{7}{2} - \frac{7}{2}$		835
5	1165.646						835
12	1165,798	10.11566 - 95.89376	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{4}\mathbf{F} - \mathbf{z}^{4}\mathbf{F}^{\circ}$	5-3		835
25	1167.030	9.33004 - 95.01771	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	⁴F – z⁴G°	$\frac{7}{2} - \frac{9}{2}$		835
10	1167.803	51.55785 - 137.18858	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{4})9s$	⁴D° – ⁴F	$\frac{7}{2} - \frac{9}{2}$		835
75	1168.040	14.99557 - 100.60901	$3d^{s}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{2}\mathbf{F} - \mathbf{z}^{2}\mathbf{F}^{\circ}$	2 - 2		835
3	1169.919						835
20	1170.169	10.11566 - 95.57339	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	⁴F – z⁴G°	$\frac{5}{2} - \frac{7}{2}$		835
15	1171.117	10.66389 - 96.05248	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	⁴ F − z ⁴ G°	$\frac{3}{2} - \frac{5}{2}$		835
100	1171.291	9.33004 - 94.70593	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{4}F - z^{4}F^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		835
1	1173.121	23.79618 - 109.03884	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{4}P)4s4p(^{3}P^{\circ})$	² D – z ⁶ P °	$\frac{3}{2} - \frac{3}{2}$		835
50	1173.298	10.66389 - 95.89376	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	4F – z4F°	$\frac{3}{2} - \frac{3}{2}$		835
75	1173.477	10.11566 - 95.33253	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{4}\mathbf{F} - \mathbf{z}^{4}\mathbf{F}^{\circ}$	5-5		835
1	1177.006	51.55785 - 136.51928	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}P)5d$	4 D° - 4F	$\frac{1}{2} - \frac{1}{2}$		835
50	1177.109	9.33004 - 94.28394	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{4}\mathbf{F} - \mathbf{z}^{4}\mathbf{F}^{\circ}$	ž - 9		835
8	1178 224	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				1	835
30	1178.571	14.99557 - 99.84413	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{2}\mathbf{F} - \mathbf{z}^{2}\mathbf{G}^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		835
150	1180 271	13.55039 - 98.27670	$3d^{3}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{2}\mathbf{F} - \mathbf{z}^{2}\mathbf{G}^{\circ}$	7-9		835
30	1181 075	10 66389 - 95 33253	$3d^{8}(a^{3}F)4s = 3d^{7}(a^{4}F)4s4p(^{3}P^{2})$	${}^{4}F - z^{4}F^{\circ}$	3 - 5		835
15	1181 620	23 10828 = 107 73781	$3d^{8}(a^{1}D)4s = 3d^{7}(a^{4}P)4s4p(^{3}P^{2})$	$^{2}D - z^{4}S^{\circ}$	3-3		835
75	1182 169	10,11566 - 94,70593	$3d^{8}(a^{3}F)4s = 3d^{7}(a^{4}F)4s4p(^{3}P^{2})$	${}^{4}F - z^{4}F^{\circ}$	<u><u><u></u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		835
20	1184 512	14 99557 - 99 41861	$3d^{3}(a^{3}F)4s = 3d^{7}(a^{4}F)4s4p(^{3}P^{2})$	$^{2}\mathbf{F} - \mathbf{z}^{2}\mathbf{F}^{\circ}$	<u><u><u></u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		835
3	1184.980	53.36517 - 137.75478	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})8d$	⁴ G° – ⁴ G	⁹ / ₂ - ¹ / ₂		835
2	1185,146	53 36517 - 137 74295	$3d^{8}(a^{3}F)4p = 3d^{8}(a^{3}F_{4})8d$	⁴ G° – ⁴ H	<u></u>	L	835
1	1186 347	51 04546 - 135 33801	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{1})8p$	⁴ F - ⁴ G°	Į į – į	ι	835
8	1186 933	24 78820 - 109 03884	$3d^{8}(a^{3}P)4s = 3d^{7}(a^{4}P)4s4p(^{3}P^{2})$	${}^{4}P - z^{6}P^{9}$	3-3		835
1	1186.993	53.49649 - 137.74295	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{4})8d$	⁴ G° – ⁴ H	باً _ بَا	L	835
20	1187,102	53,49649 - 137,73522	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})8d$	4G° – 4H	ļų_ų	1	835
15	1187.608	24.83593 - 109.03884	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{4}P)4s4p(^{3}P^{\circ})$	⁴ P – z ⁶ P°	$\frac{1}{2} - \frac{3}{2}$		835
1	1190 442	25 03638 - 109 03884	$3d^{8}(a^{3}P)4s = 3d^{7}(a^{4}P)4s4D(^{3}P^{\circ})$	⁴ P – z ⁶ P°	5-3		835
5	1192 306	53 36517 - 137 23628	$3d^{*}(a^{3}F)4n = 3d^{*}(a^{3}F)9s$	4G° - 4F	<u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u>		835
Ő	1192.596	52 73845 - 136 58935	$3d^{8}(a^{3}F)4p = 3d^{8}(a^{3}P)5d$	4D° - 4F	1 1 - I		835
ů ů ř	1192.983	53 36517 - 137 18858	$3d^{8}(a^{3}F)4p = 3d^{8}(a^{3}F_{4})9s$	4G" - 4F	3 - 3		835
2	1193.028	55.56511 151116656			2 2		835
5	1193.267	55.29965 - 139.10305	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₃)8d	² G° – ² H	$\frac{9}{2} - \frac{11}{2}$	ι	835
15	1194 857	53 49649 - 137 18858	$3d^8(a^3F)4n = 3d^8(a^3F)9s$	4G* - 4F	μ_8		835
15	1200 077	55.49049 - 157.10058	5u (a 1)+p = 5u (a 1 4)5s	0 - 1	2 - 2		835
	1200.307	52 72845 126 05053	$3d^{8}(a^{3}E)dn = 3d^{8}(a^{3}E)8c$	4D° - 2F	5 5		835
	1200.307	55 20065 128 56271	$2d^{8}(a^{3}E)/p = 3d^{8}(a^{3}E)/p$	$^{2}C^{\circ}$ ^{2}F	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		835
5	1201.002	52 20595 135 46155	$3d^{7}Ae^{2} = 3d^{8}(e^{3}\mathbf{P})Af$	4F - 2[3]*	2 2 2		835
5	1201.838	52.73845 - 135.94440	$3d^8(a^3F)4p - 3d^8(a^3F_3)7d$	${}^{4}D^{\circ} - {}^{2}F$	$\frac{2}{5} - \frac{7}{2}$		835
	1201 057	54 55705 - 127 75479	3d8(a3E)4n - 2d8(a3E)8d	4F° . 4G	ت ر و		835
3	1201.957	57 73845 - 125 00106	$3d^{8}(a^{3}E)4n = 3d^{8}(a^{3}E)7d$	4D° = 4E	2 2 2		835
10	1202.452	52.75045 ~ 155.90190	5u (a 17+p - 5u (a 13)/u	D-F	2 - 2		835
01	1202.511	53 63462 - 136 76640	3d ⁸ (a ³ E)4p - 3d ⁸ (a ³ D)5d	4D° - 4F	3 5		835
20	1202.911	51 55785 - 124 40727	$3d^{8}(a^{3}E)An = 2d^{8}(a^{3}E)7d$	4D° - 4F	2 2 2 2 2 2		835
16	1205.088	51 55785 - 134.00737	$3d^{8}(a^{3}E)4n = 3d^{8}(a^{3}E)7d$	4D° - 4P	1 1 1		835
13	1203.088	51.55765 - 154.55757	Su(a r) + p = Su(a r)/u		2 - 2		000

NI II - Continued

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	Reference
	1	1205.201	54.26263 - 137.23628	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})9s$	⁴ G° ~ ⁴ F	$\frac{7}{2} - \frac{7}{2}$		835
	20	1205.266	51.55785 - 134.52724	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7d$	⁴D° - ⁴D	$\frac{1}{2} - \frac{1}{2}$		835
	8	1205.314						835
	10	1205.552	24.78820 - 107.73781	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{4}P)4s4p(^{3}P^{\circ})$	${}^{4}P - z^{4}S^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		835
	7	1206.246	24.83593 - 107.73781	3d ⁸ (a ³ P)4s - 3d ⁷ (a ⁴ P)4s4p(³ P°)	⁴ P − z ⁴ S°	$\frac{1}{2} - \frac{3}{2}$		835
	0	1207.567	53.03793 - 135.84941	$3d^{7}4s^{2} - 3d^{8}(a^{3}P_{1})4f$	⁴ F – 1[3]°	$\frac{5}{2} - \frac{7}{2}$		835
	4	1207.620	51.04546 - 133.85304	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{4}\mathbf{F} - \mathbf{v}^{4}\mathbf{F}^{\circ}$	$\frac{9}{2} - \frac{9}{2}$		835
	3	1207.654	51.04546 - 133.85083	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{4}\mathbf{F} - \mathbf{s}^{4}\mathbf{D}^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		835
	1	1208.433	23.10828 - 105.86119	$3d^{8}(a^{1}D)4s - 3d^{8}(a^{3}F_{3})5p$	${}^{2}\mathbf{D} - {}^{2}\mathbf{D}^{\circ}$	$\frac{2}{2} - \frac{2}{2}$		835
	7	1209.170	25.03638 - 107.73781	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{4}P)4s4p(^{3}P^{\circ})$	⁴P – z⁴S°	$\frac{5}{2} - \frac{3}{2}$		835
	1	1209.492	54.55705 - 137.23628	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})9s$	4 F° – ⁴ F	$\frac{9}{2} - \frac{1}{2}$		835
	10	1210.192	54.55705 - 137.18858	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₄)9s	⁴ F° – ⁴F	$\frac{9}{2} - \frac{9}{2}$		835
	3	1210.729	53.36517 - 135.96008	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})7d$	⁴G° – ⁴H	$\frac{9}{2} - \frac{9}{2}$		835
	1	1210.790	53.36517 - 135.95601	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})7d$	⁴ G° – ² H	$\frac{9}{2} - \frac{11}{2}$		835
	1	1211.403	54.17626 - 136.72533	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ P)5d	⁴ D° – ⁴ P	$\frac{1}{2} - \frac{1}{2}$		835
	0	1212.959	55.29965 - 137.74295	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})8d$	² G° – ⁴ H	$\frac{9}{2} - \frac{11}{2}$		835
	7	1213.149						835
	7	1213.361	53.63462 - 136.05053	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})8s$	⁴ D [•] − ² F	$\frac{3}{2} - \frac{5}{2}$		835
	3	1214.104	55.41783 - 137.78250	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₄)8d	⁴ F° – ⁴G	$\frac{7}{2} - \frac{9}{2}$		835
	40	1214.153	52.73845 - 135.10045	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})8s$	${}^{4}D^{\circ} - {}^{2}F$	$\frac{5}{2} - \frac{7}{2}$		835
	1	1214.350	53.63462 - 135.98322	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})8s$	4 D° – 4 F	$\frac{3}{2} - \frac{3}{2}$		835
	100	1217.180	51.55785 - 133.71513	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})8s$	4D° - 4F	$\frac{1}{2} - \frac{9}{2}$		835
	1	1217.692						835
	3	1220.530	52.73845 - 134.67007	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7d$	⁴ D° – ⁴ P	$\frac{5}{2} - \frac{3}{2}$		835
	1	1220.950	52.73845 - 134.64209	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7d$	⁴D° - ⁴F	$\frac{5}{2} - \frac{7}{2}$		835
	1	1221.213	51.55785 - 133.44389	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}P)6s$	${}^{4}D^{\circ} - {}^{4}P$	$\frac{7}{2} - \frac{5}{2}$		835
	1	1221.289	55.01871 - 136.89934	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})7d$	⁴ G° – ⁴ G	5-5		835
	40	1221.992	55.01871 - 136.85244	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})7d$	⁴G° - ⁴F	5 - 3		835
	1	1222.220	55.41783 - 137.23628	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})9s$	4 F° – 4 F	<u>1</u> - 1		835
	20	1222.395	54.17626 - 135.98322	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})8s$	⁴D° – ⁴F	$\frac{1}{2} - \frac{3}{2}$		835
	1	1222.678	54.26263 - 136.05053	3d*(a3F)4p - 3d*(a3F2)8s	⁴ G° – ² F	$\frac{7}{2} - \frac{5}{2}$		835
	1	1222.989	52.20595 - 133.97333	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	⁴ F − s ⁴ D°	$\frac{7}{2} - \frac{5}{2}$	1 1	835
	2	1223.466	53.36517 - 135.10045	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})8s$	⁴ G° − ² F	$\frac{9}{2} - \frac{7}{2}$		835
	5	1223.643	54.26263 - 135.98606	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})7d$	⁴ G° – ⁴ G	1 - 2		835
	1	1223.775	55.01871 - 136.73274	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}P)5d$	⁴ G° - ⁴ F	$\frac{5}{2} - \frac{3}{2}$		835
	75	1224.033	54.26263 - 135.96008	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})7d$	⁴G° - ⁴H	$\frac{7}{2} - \frac{9}{2}$		835
	1	1224.268	54.26263 - 135.94440	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})7d$	⁴ G° - ² F	$\frac{1}{2} - \frac{1}{2}$		835
	2	1224.839	23.79618 - 105.43985	$3d^{8}(a^{1}D)4s - 3d^{8}(a^{3}F_{3})5p$	${}^{2}D - {}^{4}D^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		835
	25	1226.628	8.39390 - 89.91847	$3d^{*}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	⁴ F − z ⁶ G°	$\frac{9}{2} - \frac{9}{2}$		835
	15	1227.267	53.63462 - 135.11672	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})8s$	⁴ D° - ⁴ F	$\frac{3}{2} - \frac{5}{2}$		835
	5	1227.491	13.55039 - 95.01771	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{2}\mathbf{F} - \mathbf{z}^{4}\mathbf{G}^{\circ}$	$\frac{1}{2} - \frac{9}{2}$		835
	0	1228.581	23.10828 - 104.50322	$3d^{8}(a^{1}D)4s - 3d^{8}(a^{3}F_{4})5p$	${}^{2}D - {}^{4}D^{\circ}$	$\frac{5}{2} - \frac{5}{2}$		835
	10	1229.684	52.20595 - 133.52802	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	⁴ F − v ⁴ F°	$\frac{7}{2} - \frac{7}{2}$		835
	8	1230.116	53.36517 - 134.65860	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7d$	⁴ G° – ⁴ G	$\frac{9}{2} - \frac{9}{2}$		835
	1	1230.367	53.36517 - 134.64209	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{4})7d$	⁴ G° - ⁴ F	$\frac{9}{2} - \frac{7}{2}$		835
	40	1230.782	53.36517 - 134.61455	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7d$	⁴ G° – ⁴ G	$\frac{9}{2} - \frac{11}{2}$		835
	50	1230.869	53.36517 - 134.60737	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7d$	⁴ G° - ⁴ F	$\frac{9}{2} - \frac{9}{2}$		835
	25	1230.889	53.36517 - 134.60737	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7d$	⁴ G° − ⁴ F	$\frac{9}{2} - \frac{9}{2}$		835
	100	1231.041	53.36517 - 134.59743	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7d$	⁴G° - ⁴H	$\frac{9}{2} - \frac{11}{2}$		835
	i	1232.107	53.49649 - 134.65860	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7d$	⁴ G° - ⁴ G	<u>1</u> , - ;		835
	-				100 10	Lô tu	1	
	2	1232.773	53.49649 - 134.61455	3d°(a°F)4p - 3d°(a°F ₄)7d	"G" - "G			835
	2	1232.773 1232.886	53.49649 - 134.61455 53.49649 - 134.60737	3d°(a°F)4p - 3d°(a°F₄)7d 3d ⁸ (a³F)4p - 3d ⁸ (a³F₄)7d	'G' - 'G 'G' - 'F	$\frac{11}{2} - \frac{11}{2}$		835 835
	2 3 15	1232.773 1232.886 1233.036	53.49649 - 134.61455 53.49649 - 134.60737 53.49649 - 134.59743	3d°(a°F)4p – 3d°(a°F ₄)7d 3d*(a³F)4p – 3d*(a³F ₄)7d 3d*(a³F)4p – 3d*(a³F ₄)7d	*G* - *G *G* - *F *G* - *H			835 835 835

NI II - Continued

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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	10	1233 484	52 73845 - 133 80976	$3d^8(a^3F)4n = 3d^8(a^3F_*)8s$	⁴ D° – ⁴ F	5 - 1		835
	100	1233.404	9 20 200 90 460 35	$3d^{8}(a^{3}E)Aa = 3d^{7}(a^{4}E)Aa An(^{3}D^{6})$	4F 76°	2 _ 11		835
		1233.337	6.37390 - 67.40033	3d(aT) + s = 3d(aT) + s + p(T)	4C° ² E	2 2 2	1	835
		1234.092	55.01871 - 136.05055	$3d(ar) + p - 3d(ar_2) + s$	$4C^{\circ} - P$	2 - 2		935
	4	1234.375	55.01871 - 130.03145	$3d(a'r)^{4}p - 3d(a'r_{3})/d$	0 - D	2 - 2		935
		1234.659	66 01 0 7 1 126 00/0/	218(30)4 248(30)74	40% 40	5 1		035
	6	1235.069	55.01871 - 135.98606	$3d^{\circ}(a^{\circ}F)4p = 3d^{\circ}(a^{\circ}F_{3})/d$	·G· - 'G	$\frac{1}{2} - \frac{1}{2}$		835
	20	1235.112	55.01871 - 135.98322	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})8s$	⁴G° - ⁴F	$\frac{5}{2} - \frac{3}{2}$		835
	10	1235.405	9.33004 - 90.27530	3d ^s (a ³ F)4s - 3d ⁷ (a ⁴ F)4s4p(³ P [*])	⁺F – z°G°	$\frac{1}{2} - \frac{1}{2}$		835
	0	1236.474	52.73845 - 133.61399	3d8(a3F)4p - 3d8(a3P)6s	⁴ D° – ⁴ P	$\frac{2}{2} - \frac{3}{2}$		835
	25	1236.799	54.26263 - 135.11672	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₃)8s	⁴G° - ⁴F	$\frac{7}{2} - \frac{2}{2}$		835
	10	1237.049	54.26263 - 135.10045	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})8s$	⁴ G° − ² F	$\frac{1}{2} - \frac{1}{2}$		835
	1	1237.247	25.03638 - 105.86119	$3d^{8}(a^{3}P)4s - 3d^{8}(a^{3}F_{3})5p$	⁴ ₽ ² D °	$\frac{5}{2} - \frac{5}{2}$		835
	1	1237.260	56.07526 - 136.89934	3d8(a3F)4p - 3d8(a3F2)7d	⁴F° - ⁴G	$\frac{5}{2} - \frac{5}{2}$		835
	4	1237.961	56.07526 - 136.85244	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})7d$	4 F° – 4 F	$\frac{5}{2} - \frac{3}{2}$		835
	8	1237,976	56.07526 - 136.85244	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})7d$	4 F° – 4 F	5 - 3		835
	1	1238 919	54 26263 - 134 97847	$3d^{8}(a^{3}F)4p = 3d^{8}(a^{3}F)7d$	⁴ G° – ⁴ D	1 2 - 5		835
	25	1230.061	8 39390 - 89 10049	$3d^{8}(a^{3}F)4s = 3d^{7}(a^{4}F)4s4n(^{3}P^{2})$	${}^{4}\mathbf{F} = 7^{9}\mathbf{D}^{9}$	<u>9</u> 1		835
	12	1239.506	55.29965 - 135.97731	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})7d$	$^{2}G^{\circ} - ^{2}G$	$\frac{2}{2} - \frac{2}{2}$		835
		1220 822	55 200(5 125 05(0)	248(-3E)An 248(-3E)74	2 C ° 2H	<u>в</u> 1		025
	00	1239.832	55.29905 - 135.95001	$3d^{2}(a^{2}F)4p = 3d^{2}(a^{2}F_{3})/d$	2 C ² E	$\frac{1}{2} - \frac{1}{2}$		035
	1	1240.012	55.29965 - 135.94440	$3d^{\circ}(a^{\circ}F)4p - 3d^{\circ}(a^{\circ}F_{3})/d$	-G' - F	$\frac{1}{2} - \frac{1}{2}$		835
	2	1240.029			-	7 9		835
	50	1240.877	9.33004 - 89.91847	$3d^{\circ}(a^{*}F)4s - 3d'(a^{*}F)4s4p(^{*}P^{*})$	*F – z°G*	$\frac{1}{2} - \frac{1}{2}$		835
	1	1241.189	55.41783 - 135.98606	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})7d$	* F° - *G	$\frac{1}{2} - \frac{1}{2}$		835
	2	1241.233	53.36517 - 133.92988	$3d^{*}(a^{*}F)4p - 3d^{*}(a^{1}D)5d$	*G° - 2G	$\frac{9}{2} - \frac{1}{2}$		835
	10	1241.320	55.41783 - 135.97731	3d8(a3F)4p - 3d8(a3F3)7d	⁴ F° - ² G	$\frac{7}{2} - \frac{9}{2}$		835
	3	1241.548	23.10828 - 103.65303	3d ⁸ (a ¹ D)4s - 3d ⁸ (a ³ F ₄)5p	${}^{2}D - {}^{4}D^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		835
	10	1241.588	55.41783 - 135.96008	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})7d$	⁴F° – ⁴H	$\frac{7}{2} - \frac{9}{2}$		835
	1	1241.827	55.41783 - 135.94440	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})7d$	${}^{4}F^{\circ} - {}^{2}F$	$\frac{7}{2} - \frac{2}{2}$		835
	30	1242.099	56.37141 - 136.88056	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})7d$	${}^{2}G^{\circ} - {}^{2}H$	2 - 3		835
	6	1242.627	56.42449 - 136.89934	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})7d$	⁴F° - ⁴G	$\frac{3}{2} - \frac{5}{2}$		835
	75	1243.093	53.36517 - 133.80976	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})8s$	4G° - 4F	$\frac{9}{2} - \frac{7}{2}$		835
	6	1243 126						835
	i	1243 345	56 42449 - 136 85244	$3d^{8}(a^{3}E)4p = 3d^{8}(a^{3}E)7d$	4F° – 4F	3 _ 3	1	835
	3	1243.672	10 11566 - 90 52618	$3d^{8}(a^{3}F)4s = 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	4F - 7°G°	2 2		835
	5	1243.848	54 26263 - 134 65860	$3d^{8}(a^{3}F)4p = 3d^{8}(a^{3}F)7d$	4G° - 4G	2 2		835
	3	1243.848	54.26263 - 134.66209	$3d^8(a^3F)4p = 3d^8(a^3F_1)7d$	4° - 4	2^{-2}_{-2}		835
		1244.104	54.20205 - 154.04207	50 (a 1) p = 50 (a 1 1) fu	0 1	2 2		000
	5	1244.255	53.36517 - 133.73498	3d ⁸ (a ³ F)4p - 3d ⁸ (a ¹ D)5d	⁴ G° - ² F	$\frac{9}{2} - \frac{7}{2}$		835
	50	1244.560	53.36517 - 133.71513	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})8s$	⁴G° - ⁴F	$\frac{9}{2} - \frac{9}{2}$		835
	100	1244.811						835
	1	1245.977						835
	150	1246.598	53.49649 - 133.71513	3d*(a3F)4p - 3d*(a3F4)8s	⁴G° - ⁴F	$\frac{11}{2} - \frac{9}{2}$		835
	20	1247.333	53.03793 - 133.20930	$3d^{2}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{4}F - v^{4}F^{\circ}$	$\frac{5}{2} - \frac{5}{2}$		835
	6	1247.509	10.11566 - 90.27530	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	⁴F - z⁰G°	\$ - 7		835
	1	1247,568	57.08055 - 137.23628	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F)9s$	${}^{2}F^{\circ} - {}^{4}F$	Ž - Ž		835
	9	1248.413	54.55705 - 134.65860	$3d^8(a^3F)4p - 3d^8(a^3F)7d$	⁴ F° – ⁴ G	9 9	[835
	10	1248 467	55 01871 - 135 11672	$3d^{8}(a^{3}F)4n = 3d^{8}(a^{3}F)8e$	4G° - 4F	5_5		835
	10	1248 844	54 26263 - 124 22668	$3d^8(a^3F)An = 3d^8(a^3F)Ka$	4G° _ 4[5]°	2 2		835
	100	1249.101	54.55705 - 134.61455	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7d$	4F° - 4G	$\frac{2}{9} - \frac{11}{2}$		835
		1249 212	54 55705 124 60727	3d8(a3E)4n 2d8(a3E \7d	4E° 4E	2 2		935
	0	1249.213	54 55705 124 50742	$3d(a \Gamma)^{4}p = 3d(a \Gamma_{4})/d$ $3d^{8}(a^{3}E)/a = 3d^{8}(a^{3}E)/2d$	Г – Г 4E° 411	2 2		935
	3	1249.309	54.55705 - 134.59743	$30^{\circ}(a^{-}F)^{4}p - 30^{\circ}(a^{-}F_{4})/0$	T - H	2 - 2		035
	6	1250.467	54.55705 - 134.52724	3d°(a°F)4p - 3d°(a°F ₄)7d	"F" – "D	2 - 2		835
	4	1250.685	56.07526 - 136.03143	3d°(a°F)4p - 3d°(a°F ₃)7d	'F' - 'D	2 - 2		835
	1	1250.901						835
	10	1251.394	56.07526 - 135.98606	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{3}F_{3})7d$	'F° - ⁴G	$\frac{2}{2} - \frac{7}{2}$		835
NI II - Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	Reference
	16	1251.438	56.07526 - 135.98322	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})8s$	⁴ F° – ⁴ F	$\frac{5}{3} - \frac{3}{2}$		835
	1	1252.879	57.42016 - 137.23628	$3d^{8}(a^{3}F)4p = 3d^{8}(a^{3}F_{4})9s$	${}^{2}D^{\circ} - {}^{4}F$	1 1 1		835
	50	1253 122	55 29965 - 135 10045	$3d^8(a^3F)4p = 3d^8(a^3F_1)8s$	${}^{2}G^{\circ} - {}^{2}F$	2 1		835
	75	1253.122	8 20 200 88 17188	$2d^{8}(a^{3}E)Aa = 2d^{7}(a^{4}E)AaAn(^{3}D^{9})$	4E -0D*	2 - 2 9 - 2 9 - 2		035
	15	1253.477	0.33034 00.10040	3d(a r) + 8 - 3d(a r) + 8 + p(r)	F - ZD	$\frac{1}{2} - \frac{1}{2}$		835
	4	1253.399	9.33004 - 89.10049	$3d^{\circ}(a^{\circ}F)4s - 3d^{\circ}(a^{\circ}F)4s4p(^{\circ}P^{\circ})$	$F - Z^{\circ}D^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		835
	2	1254.290	54.17626 - 133.90300	3d°(a'F)4p - 3d"(a'D)5d	*D* – *D	$\frac{1}{2} - \frac{2}{2}$		835
	0	1254.346	52.20595 - 131.92877	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})7p$	⁴ F − ² G °	$\frac{7}{2} - \frac{9}{2}$		835
	1	1254.471	24.78820 - 104.50322	$3d^{*}(a^{*}P)4s - 3d^{*}(a^{*}F_{4})5p$	${}^{4}\mathbf{P} - {}^{4}\mathbf{D}^{\circ}$	$\frac{2}{2} - \frac{2}{2}$		835
	50	1254.721	55.41783 - 135.11672	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})8s$	4 F° – 4 F	$\frac{7}{2} - \frac{5}{2}$		835
	7	1254.978	55.41783 - 135.10045	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{3}F_{3})8s$	${}^{4}F^{\circ} - {}^{2}F$	$\frac{7}{2} - \frac{7}{2}$		835
	8	1255.034	56.37141 - 136.05053	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})8s$	${}^{2}G^{\circ} - {}^{2}F$	$\frac{7}{2} - \frac{5}{2}$		835
	6	1255.335	56.37141 - 136.03143	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{3}F_{3})7d$	${}^{2}G^{\circ} - {}^{2}D$	$\frac{7}{2} - \frac{5}{2}$		835
	5	1256.029	51.04546 - 130.66132	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})7p$	⁴F – ⁴G°	3-4		835
	6	1256.187	56 37141 - 135 97731	$3d^{8}(a^{3}F)4n = 3d^{8}(a^{3}F)7d$	${}^{2}G^{\circ} - {}^{2}G$	1 1 1		835
	õ	1256 459	53 60119 - 133 19019	$3d^{7}4s^{2} - 3d^{7}(a^{2}E)4s4n(^{3}P^{2})$	${}^{4}F = v^{4}F^{9}$	3 3		835
	1	1256 709	56 27141 135 04440	$3d^{3}(a^{3}E)/a = 3d^{3}(a^{3}E)/a$	2C° 2E			035
	1	1256.764	50.37141 - 155.94440	3u (a F)4p - 3u (a F3)/u	0 - F	2 = 2		035
	6	1256.764	55.41783 - 134.97847	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7d$	⁴ F° – ⁴ D	$\frac{7}{2} - \frac{5}{2}$		835
	40	1256.930	56.42449 - 135.98322	3d'(a'F)4p - 3d*(a'F ₂)8s	⁺ F° – ⁺ F	2 - 2		835
	8	1257.116	54.26263 - 133.80976	3d ^s (a ³ F)4p - 3d ^s (a ³ F ₄)8s	⁺G° - ⁺F	$\frac{1}{2} - \frac{1}{2}$		835
	2	1257.829						835
	0	1258.303	54.26263 - 133.73498	3d ^s (a ³ F)4p - 3d ^s (a ¹ D)5d	⁴G° - ²F	$\frac{7}{2} - \frac{7}{2}$		835
	1	1259.506						835
	1	1259.886	54.55705 - 133.92988	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{1}D)5d$	⁴ F° - ² G	$\frac{9}{2} - \frac{7}{2}$		835
	1	1261.068	55.29965 - 134.59743	$3d^{x}(a^{3}F)4p - 3d^{x}(a^{3}F_{x})7d$	² G° - 'H	3 - 17		835
	12	1261.786	54.55705 - 133.80976	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{4})8s$	⁴ F° – ⁴ F	$\frac{1}{2} - \frac{1}{2}$		835
	10	1261.975	55.41783 - 134.65860	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F)7d$	⁴ F° – ⁴ G	1 1 - 1		835
	8	1262 239	55 41783 - 134 64209	$3d^{8}(a^{3}E)4p = 3d^{8}(a^{3}E)7d$	⁴ F° – ⁴ F	1 <u>i</u> <u>i</u>	1 1	835
	2	1262.239	54 55705 133 73409	$3d^{3}(a^{3}E)/a = 3d^{3}(a^{1}D)/d$	400 300	2 2 2		925
	100	1263.294	54.55705 - 133.71513	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{4})8s$	*F° – *F	$\frac{2}{2} - \frac{2}{2}$		835
	14	1265 157	56 07526 135 11672	2d ⁸ (a ³ E)4p 2d ⁸ (a ³ E)8a	400 40	5 5		975
	14	1205.157	10.11566 80.10040	3d(a F) + p = 3d(a F) / (a F		2 2		035
	1	1200.005	10.11566 - 89.10049	30 (a F)4s - 30 (a F)4s4p(P)	$F - z^{*}D$	1 2 - 2		835
	8	1266.608	57.08055 - 136.03143	$3d^{(a'F)}4p - 3d^{(a'F)}7d$	$F^{\circ} - D$	2 - 2		835
	6	1267.478	57.08055 - 135.97731	$3d^{(a'F)4p} - 3d^{(a'F_3)7d}$	- F° – G	2 - 2		835
	8	1268.007	57.08055 - 135.94440	$3d^{*}(a^{*}F)4p - 3d^{*}(a^{*}F_{*})7d$	${}^{2}F^{\circ} - {}^{2}F$	$\frac{1}{2} - \frac{1}{2}$		835
	2	1268.359	9.33004 - 88.17188	$3d^{*}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	⁴ F − z ⁶ D°	$\frac{7}{2} - \frac{9}{2}$		835
	1	1269.059	9.33004 - 88.12856	3d*(a ³ F)4s - 3d ⁷ (a ⁴ F)4s4p(³ P°)	⁴ F – z⁰F°	$\frac{7}{2} - \frac{5}{2}$		835
	2	1269.917	56.37141 - 135.11672	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{3}F_{3})8s$	² G° − ⁴ F	$\frac{1}{2} - \frac{5}{2}$		835
	1	1270.061	51.04546 - 129.78207	$3d^{7}4s^{2} - 3d^{7}(a^{4}P)4s4p(^{1}P^{\circ})$	${}^{4}\mathbf{F} - \mathbf{t}^{4}\mathbf{D}^{\circ}$	3 - 7		835
	15	1270.180	56.37141 - 135.10045	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{3})8s$	${}^{2}G^{\circ} - {}^{2}F$	2 - 2		835
	1	1271.993	25.03638 - 103.65303	$3d^{*}(a^{3}P)4s - 3d^{*}(a^{3}F_{*})5p$	⁴ P – ⁴ D°	5 _ 1		835
	1	1272.080	57.42016 - 136.03143	$3d^{*}(a^{*}F)4p - 3d^{*}(a^{*}F_{3})7d$	${}^{2}D^{\circ} - {}^{2}D$	$\frac{5}{2} - \frac{5}{2}$		835
	2	1272.634						835
	2	1273 488	57 42016 - 135 94440	$3d^{8}(a^{3}E)4n = 3d^{8}(a^{3}E)7d$	${}^{2}D^{\circ} = {}^{2}E$	5 2		835
	1	1273 717	55 29965 - 122 80076	$3d^{8}(a^{3}E)4n = 3d^{8}(a^{3}E)8n$	2G° - 4F	2 2 2 2 2 2		835
	2	1274 190	57 42016 - 135 00106	$3d^{8}(a^{3}E)4n = 2d^{8}(a^{3}E)7d$	2D° 4E	2 2		815
	100	1274.100	9 20200 94 97002	3u (a r) + p - 3u (a r)/0 $2d^{3}(a) = 2d^{7}(-4r) + 4 - (3r)^{3}$		2 2		035
	10	1274.802	58.49321 - 136.93682	$3d^{*}(a^{+}F)4p - 3d^{*}(a^{+}F_{2})7d$	$F - Z^{*}F^{*}$ $^{2}F^{*} - ^{2}G$	2-7		835
		1075 (10				, ,		
	10	1275.640 1276.602	55.41783 - 133.80976	3d°(a'F)4p - 3d°(a'F ₄)8s	'F' - 'F	2-2		835 835
	1	1276.859	55.41783 - 133.73526	$3d^{*}(a^{3}F)4p = 3d^{*}(a^{1}D)5d$	${}^{4}F^{\circ} - {}^{2}F$	2 - 4		835
	1	1277 086				2 - 2		835
	20	1277 242	52 73845 - 131 03201	$3d^{8}(a^{3}E)An = 3d^{8}(a^{3}E)Ad$	4D° - 2D	5 5		825
	20	12/1.243	52.75045 - 151.05201			2 2		635
	1	1777 244	56 27141 174 28020			1 4 7		026

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NI II - Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
,	1	1277.617	56.37141 - 134.64209	3d ^s (a ³ F)4p - 3d ^s (a ³ F₄)7d	² G° - ⁴ F	$\frac{7}{2} - \frac{7}{2}$		835
	2	1277.725	52.20595 - 130.47090	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})7p$	⁴ F – ⁴ F°	$\frac{7}{2} - \frac{9}{2}$		835
	18	1277.967	58.70595 - 136.95528	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})7d$	${}^{2}D^{\circ} - {}^{2}P$	3-1		835
	100	1278.637	9.33004 - 87.53809	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	⁴ F − z ⁶ F°	$\frac{1}{3} - \frac{1}{3}$		835
	1	1279.400	53.63462 - 131.79626	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F)6d$	${}^{4}D^{\circ} - {}^{2}F$	$\frac{1}{3} - \frac{5}{3}$		835
	1	1281.056	58.70595 - 136.76649	$3d^{(a^{3}F)4p} - 3d^{(a^{3}P)5d}$	${}^{2}D^{\circ} - {}^{4}F$	3 - 5		835
		1201.000			5.			000
	5	1281.609	52.73845 - 130.76526	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₃)6d	${}^{4}D^{\circ} - {}^{2}F$	$\frac{5}{2} - \frac{7}{2}$		835
	4	1281.704	53.63462 - 131.65583	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6d$	${}^{4}D^{\circ} - {}^{2}P$	$\frac{4}{2} - \frac{1}{2}$		835
	12	1281.723	52.20595 - 130.22587	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})5f$	⁴ F – 3[4]°	$\frac{7}{2} - \frac{7}{2}$		835
	50	1281.834	10.11566 - 88.12856	$3d^{s}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	⁴F – z⁰F°	$\frac{5}{2} - \frac{5}{2}$		835
	2	1282.179	52.73845 - 130.73053	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	⁴ D° – ⁴ F	5-5		835
	1	1282.732	23.79618 - 101.75480	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{2}\mathbf{D} - \mathbf{z}^{2}\mathbf{D}^{\circ}$	3-5		835
	10	1282.825	52.73845 - 130.69135	3d [*] (a ³ F)4p - 3d [*] (a ³ F ₃)6d	${}^{4}\mathbf{D}^{\circ} - {}^{2}\mathbf{P}$	$\frac{2}{2} - \frac{4}{2}$		835
	12	1283.399	10.66389 - 88.58201	$3d^{*}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	⁴F – z⁵F°	$\frac{3}{2} - \frac{3}{2}$		835
	3	1283.731	57.08055 - 134.97847	3d*(a3F)4p - 3d*(a3F4)7d	² F° - ⁴ D	$\frac{1}{2} - \frac{5}{2}$		835
	25	1284.327	51.55785 - 129.41958	$3d^{k}(a^{3}F)4p - 3d^{k}(a^{3}F_{4})6d$	⁴D° - ⁴F	7 - 9		835
	50	1286.338	51.55785 - 129.29791	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{4})6d$	4D° - 4D	$\frac{1}{2} - \frac{1}{2}$		835
	3	1286.396	51.55785 - 129.29451	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})7s$	4D° – 4F	3 - 5		835
	50	1286.561	51.55785 - 129.28450	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F₄)6d	⁴D° – ⁴P	$\frac{1}{2} - \frac{5}{2}$		835
	15	1287.329	57.42016 - 135.10045	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})8s$	${}^{2}D^{\circ} - {}^{2}F$	$\frac{5}{2} - \frac{7}{2}$		835
	8	1287.432]	835
	9	1289.024	57.08055 - 134.65860	3d*(a³F)4p – 3d*(a³F₄)7d	² F° – ⁴G	$\frac{7}{2} - \frac{9}{2}$		835
	3	1289.298	57.08055 - 134.64209	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7d$	² F° – ⁴F	$\frac{1}{2} - \frac{1}{2}$		835
	7	1289.354	56.37141 - 133.92988	3d ⁸ (a ³ F)4p - 3d ⁸ (a ¹ D)5d	${}^{2}G^{\circ} - {}^{2}G$	$\frac{1}{2} - \frac{1}{2}$		835
	11	1280 260	59 40221 126 05052	2d8(a3E)4n 2d8(a3E)9a	2E° 2E	5 5		975
	2	1289.509	20 50246 107 14221	$3d^{8}(a^{3}E) 4a = 3d^{8}(a^{3}E) 5=$	20 20°	2^{-2}_{1}		035
	4	1209.515	23.33340 - 107.14221	$3u(a r) + s = 3u(a r_2) - 5p$		$\frac{1}{7} - \frac{1}{9}$		835
	0	1289.050	9.33004 - 86.87003	$3d^{(a'P)4s} - 3d^{(a'P)4s4p('P')}$	$\mathbf{F} - \mathbf{Z}^{*}\mathbf{F}$	$\frac{2}{5} - \frac{7}{2}$		835
	1	1289.682	56.07526 - 133.61399	3d"(a"P)4p - 3d"(a"P)6s	*F* - *P	2 - 2		835
	1	1290.442	58.49321 - 135.98606	$3d^{\circ}(a^{\circ}F)4p - 3d^{\circ}(a^{\circ}F_{3})7d$	² F [*] − [*] G	$\frac{1}{2} - \frac{1}{2}$		835
	4	1290.908	10.66389 - 88.12856	$3d^{(a'F)}4s - 3d'(a'F)4s4p('P')$	*F – z°F*	$\frac{2}{2} - \frac{2}{2}$		835
	10	1291.251	54.17626 - 131.62045	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6d$	4 D° – 4F	$\frac{1}{2} - \frac{3}{2}$		835
	10	1291.614	10.11566 - 87.53809	$3d^{8}(a^{3}F)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	⁴F – z⁰F°	$\frac{5}{2} - \frac{7}{2}$		835
	2	1292.033	53.63462 - 131.03201	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	${}^{4}D^{\circ} - {}^{2}D$	3-5		835
	2	1292.224	53.36517 - 130.75103	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	4G° – 2H	3 _ H		835
	6	1292.331						835
	5	1292.669						835
		1202 222	50 70505 126 02142		100 10	1.5		
	5	1293.232	58.70595 - 130.03143	$3d^{(a'F)}4p - 3d^{(a'F)}7d$	-DD	2 - 2		835
	0	1293.333	53.03402 - 130.94230	3d"(a'F)4p - 3d"(a'F)6d	"D" – "D	2 - 2		835
	10	1294.500	57.42016 - 134.67007	$3d^{\circ}(a^{*}F)4p - 3d^{\circ}(a^{*}F_{4})7d$	°D° – °P	$\frac{1}{2} - \frac{1}{2}$		835
	2	1294.968	57.42016 - 134.64209	3d°(a`F)4p – 3d°(a`F₄)7d	²D° – ⁴F	$\frac{2}{2} - \frac{1}{2}$		835
	12	1296.126	52 72045 120 04222		454 45			835
	13	1296.950	52.73845 - 129.84233	3d°(a°F)4p - 3d°(a°F₄)6d	"D" – "D	2 - 2		835
	2	1297.087	53.63462 - 130.73053	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	4D° – 4F	$\frac{3}{2} - \frac{5}{2}$		835
	3	1297.417	53.63462 - 130.71085	$3d^{*}(a^{3}F)4p = 3d^{*}(a^{3}F)6d$	${}^{4}D^{\circ} - {}^{4}P$	3_1		835
	1	1297.442			2.	2 2		835
	10	1302 246	29 07093 - 105 86119	$3d^{8}(a^{3}P)As = 3d^{8}(a^{3}F_{1})Sn$	$2\mathbf{p} = 2\mathbf{D}^{\circ}$	3 5		835
	1	1302 603	54 26263 - 131 03201	$3d^8(a^3E)4n = 2d^8(a^3E).6d$	4G° 2D	2 2 2		925
	4	1303.078	52.73845 - 129.47973	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{4})6d$	⁴ D° – ⁴ P	$\frac{2}{5} - \frac{3}{7}$		835
	2	1303.170	52.73845 - 129.47427	3d*(a'F)4p - 3d*(a'F ₄)6d	⁴D° – ⁴F	$\frac{5}{2} - \frac{7}{2}$		835
	0	1303.237	55.01871 - 131.75073	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6d$	4 G [•] − ² G	$\frac{5}{2} - \frac{7}{2}$		835
	5	1303.283	57.08055 - 133.80976	3d8(a3F)4p - 3d8(a3F4)8s	² F° − ⁴ F	$\frac{7}{2} - \frac{7}{2}$		835
	1	1304.555	57.08055 - 133.73498	3d ⁸ (a ³ F)4p - 3d ⁸ (a ¹ D)5d	${}^{2}F^{\circ} - {}^{2}F$	$\frac{1}{2} - \frac{1}{2}$		835
	10	1304.594	55.01871 - 131.67087	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6d$	⁴G° - ⁴G	3-5		835
	6	1305.083	58.49321 - 135.11672	3d*(a3F)4p - 3d*(a3F3)8s	² F° – ⁴ F	3-5		835

NI II - Continued

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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	References
	25	1305.169	55.01871 - 131.63710	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₂)6d	⁴G° - ⁴H	$\frac{5}{2} - \frac{7}{2}$		835
	4	1306.279	54.26263 - 130.81591	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	⁴ G° – ⁴ G	$\frac{7}{2} - \frac{7}{2}$		835
	1	1306.528	54.26263 - 130.80133	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	⁴ G° - ² G	$\frac{7}{2} - \frac{9}{2}$		835
	6	1306.621	52.73845 - 129.27172	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})7s$	${}^{4}D^{\circ} - {}^{2}F$	$\frac{5}{2} - \frac{7}{2}$		835
	10	1307.146	54.26263 - 130.76526	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	${}^{4}G^{\circ} - {}^{2}F$	$\frac{1}{2} - \frac{1}{2}$		835
	50	1307.276	54.26263 - 130.75751	3d8(a3F)4p - 3d8(a3F3)6d	⁴G° - ⁴H	$\frac{7}{2} - \frac{9}{2}$		835
	8	1308.714	58.70595 - 135.11672	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₃)8s	² D° – ⁴ F	$\frac{3}{2} - \frac{5}{2}$		835
10	16	1308.869	0.0 - 76.40203	$3d^9 - 3d^8(a^1G)4p$	$g^2D - {}^2F^{\bullet}$	$\frac{5}{2} - \frac{5}{2}$		835
	0	1309.079	57.42016 - 133.80976	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})8s$	${}^{2}D^{\circ} - {}^{4}F$	$\frac{5}{2} - \frac{7}{2}$		835
	1	1310.358	57.42016 - 133.73498	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{1}D)5d$	${}^{2}D^{\circ} - {}^{2}F$	$\frac{5}{2} - \frac{7}{2}$		835
	15	1310.457	51.55785 - 127.86713	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7s$	⁴ D° – ⁴ F	$\frac{7}{2} - \frac{9}{2}$		835
	1	1311.152	55.41783 - 131.68656	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6d$	${}^{4}\mathbf{F}^{\circ} - {}^{2}\mathbf{H}$	$\frac{1}{2} - \frac{9}{2}$		835
	5	1311.365						835
	7	1313.403	53.36517 - 129.50324	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₄)6d	⁴G° – ⁴G	$\frac{9}{2} - \frac{9}{2}$		835
	2	1313.903	53.36517 - 129.47427	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})6d$	⁴ G° – ⁴ F	$\frac{9}{2} - \frac{7}{2}$		835
	12	1314.771	53.36517 - 129.42403	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})6d$	⁴ G° - ⁴ G	2 - 11		835
	12	1314.847	53.36517 - 129.41958	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})6d$	4G° - 4F	$\frac{9}{2} - \frac{9}{2}$		835
	70	1315.255	53.36517 - 129.39604	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})6d$	⁴G° - ⁴H	$\frac{9}{2} - \frac{11}{2}$		835
	3	1315.558	55.01871 - 131.03201	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	${}^{4}G^{\circ} - {}^{2}D$	5-5		835
	4	1316.502	54.17626 - 130.13519	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})7s$	⁴ D° - ⁴ F	$\frac{1}{2} - \frac{3}{2}$		835
	6	1317.045	53,49649 - 129,42403	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})6d$	⁴ G° – ⁴ G	<u><u> </u></u>		835
	10	1317.122	53.49649 - 129.41958	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})6d$	4G° – 4F	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		835
0	500	1317.220	0.0 - 75.91763	$3d^9 - 3d^8(a^1G)4p$	$g^2D - {}^2F^{\circ}$	3 - 7		835
-	15	1317.531	53.49649 - 129.39604	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})6d$	${}^{4}G^{\circ} - {}^{4}H$	$\frac{11}{2} - \frac{11}{2}$		835
	100	1318.017	53.49649 - 129.36791	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})6d$	⁴G° - ⁴H	<u><u></u><u></u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u>		835
	8	1319.310	55.01871 - 130.81591	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	⁴ G° - ⁴ G	$\frac{5}{2} - \frac{7}{2}$		835
	0	1320.799	55.01871 - 130.73053	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	⁺G° – ⁴F	$\frac{5}{2} - \frac{5}{2}$		835
	3	1321.432	56.07526 - 131.75073	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6d$	⁴ F° − ² G	$\frac{5}{2} - \frac{7}{2}$		835
	2	1321.704	53.63462 - 129.29451	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})7s$	⁴ D° – ⁴ F	$\frac{3}{2} - \frac{5}{2}$		835
	2	1322.825	56.07526 - 131.67087	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6d$	⁴F° - ⁴G	$\frac{5}{2} - \frac{5}{2}$		835
	1	1323.107	54.26263 - 129.84233	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₄)6d	⁴G° - ⁴D	$\frac{7}{2} - \frac{5}{2}$		835
	25	1323.417	56.07526 - 131.63710	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6d$	⁴ F° – ⁴ H	$\frac{5}{2} - \frac{7}{2}$		835
	25	1324.475	55.29965 - 130.80133	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	$^{2}G^{\circ} - ^{2}G$	$\frac{9}{2} - \frac{9}{2}$		835
	1	1325.105	55.29965 - 130.76526	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	${}^{2}G^{\circ} - {}^{2}F$	$\frac{3}{2} - \frac{7}{2}$		835
	1	1325.242	55.29965 - 130.75751	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	² G° – ⁴ H	$\frac{5}{2} - \frac{5}{2}$		835
	100	1325.359	55.29965 - 130.75103	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	${}^{2}G^{\circ} - {}^{2}H$	$\frac{9}{2} - \frac{11}{2}$		835
	4	1325.691	29.07093 - 104.50322	3d*(a ³ P)4s - 3d*(a ³ F ₄)5p	${}^{2}\mathbf{P} - {}^{4}\mathbf{D}^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		835
	7	1326.292	55.41783 - 130.81591	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	4 F° − 4 G	$\frac{7}{2} - \frac{7}{2}$		835
	11	1326.548	55.41783 - 130.80133	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	${}^{4}F^{\circ} - {}^{2}G$	$\frac{7}{2} - \frac{9}{2}$		835
	12	1326.623	56.37141 - 131.75073	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6d$	² G° – ² G	$\frac{7}{2} - \frac{7}{2}$		835
	3	1327.187	58.70595 - 134.05305	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{1}D)5d$	${}^{2}D^{\circ} - {}^{2}D$	$\frac{3}{2} - \frac{5}{2}$		835
	20	1327.319	55.41783 - 130.75751	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{3})6d$	⁴ F° – ⁴ H	$\frac{7}{2} - \frac{9}{2}$		835
	8	1327.730	58.49321 - 133.80976	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F₄)8s	${}^{2}F^{\circ} - {}^{4}F$	$\frac{5}{2} - \frac{7}{2}$		835
	50	1327.755	56.37141 - 131.68656	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6d$	² G° - ² H	$\frac{7}{2} - \frac{9}{2}$		835
	3	1328.847	52.73845 - 127.99156	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{4})7s$	* D ° – *F	$\frac{2}{2} - \frac{1}{2}$		835
	25	1328.964	56.42449 - 131.67087	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6d$	'F° - ⁺G	$\frac{2}{2} - \frac{2}{2}$		835
	13	1329.857	56.42449 - 131.62045	$\frac{3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6d}{3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})7c}$	${}^{4}F^{\circ} - {}^{4}F$	$\frac{2}{2} - \frac{3}{2}$		835
	9	1551.204	55.016/1 - 150.15519	50 (a r)+p - 50 (a r ₂)/s	0 - F	2 - 2		635
	1	1332.706	54.26263 - 129.29791	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})6d$	${}^{4}G^{\circ} - {}^{4}D$	$\frac{1}{2} - \frac{7}{2}$		835
	6	1332.766	54.26263 - 129.29451	$3d^{\circ}(a^{\circ}F)4p - 3d^{\circ}(a^{\circ}F_3)/s$		$\frac{2}{3} - \frac{2}{5}$		833
	7	1332.808	58.70595 - 133.73526	3d°(a'F)4p - 3d°(a'D)5d	$D^{*} - F^{*}$	$\frac{5}{7} - \frac{5}{7}$		835
	3	1333.171	54.26263 - 129.27172	$3d^{\circ}(a^{\circ}F)4p - 3d^{\circ}(a^{\circ}F_3)7s$	G - F	2 - 2		835
	10	1334.101	50.07526 - 131.03201	$3d^{\circ}(a^{\circ}F)4p = 3d^{\circ}(a^{\circ}F_{3})6d$	F - D	$\frac{2}{9} - \frac{2}{9}$		833
	12	1334.287	54.55705 - 129.50324] 3d°(a°F)4p – 3d°(a°F₄)6d	'F' - 'G	$\frac{1}{2} - \frac{1}{2}$		835
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NI II -- Continued

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	7	1334.320						835
	1	1334.656						835
	1	1334.689						835
10	400	1335.203	1.50694 - 76.40203	3d ⁹ - 3d ⁸ (a ¹ G)4p	$g^2D - {}^2F^\circ$	$\frac{3}{2} - \frac{5}{2}$		835
	18	1335.779	54.55705 - 129.41958	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F₄)6d	⁴ F° – ⁴ F	$\frac{9}{2} - \frac{9}{2}$		835
	2	1336.201	54.55705 - 129.39604	3d8(a3F)4p - 3d8(a3F4)6d	⁴ F° − ⁴ H	$\frac{9}{2} - \frac{11}{2}$		835
	1.6	1227.059	54 55705 120 20701	248(a3E)4a 248(a3E)(4	45° 40	2 2		975
	10	1337.938	34.33703 - 129.29791	50 (a'r)4p - 50 (a'r4)60	F-D	$\bar{2} - \bar{2}$		035
	10	1336.193	57 09055 121 70626	2-18(-3E)4= 2-18(-3E)6d	2E° 2E	2 5		835
		1338.402	57.08055 131.79020	$3d^{3}(a^{3}E)4p = 3d^{3}(a^{3}E)6d$	F - F	$\frac{1}{2} - \frac{1}{2}$		835
	5	1339.221	57.08055 - 151.75075	$3d(a \Gamma) + p = 3d(a \Gamma_2) + d(a \Gamma$	$2C^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		633 975
	1	1339.394	56.07526 120.72052	$3d^{2}(a^{3}E)4p = 3d^{2}(a^{3}E)6d$	4E° 4E	2 - 2		035
	3	1339.407	50.07520 - 150.75055	50 (a r)4p - 50 (a r3)60	г - г	2 - 2		833
	15	1340.007	53.36517 - 127.99156	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F₄)7s	4 G° – 4 F	$\frac{9}{2} - \frac{7}{2}$		835
	20	1340.374	57.08055 - 131.68656	$3d^8(a^3F)4p - 3d^8(a^3F_2)6d$	${}^{2}F^{\circ} - {}^{2}H$	$\frac{1}{2} - \frac{9}{2}$		835
	0	1341.226	32.52354 - 107.08221	$3d^{8}(a^{1}G)4s - 3d^{8}(a^{3}F_{2})5p$	${}^{2}G - {}^{2}F^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		835
	20	1342.242	53.36517 - 127.86713	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7s$	4G° – 4F	3-9		835
	10	1343.544	56.37141 - 130.80133	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	${}^{2}G^{\circ} - {}^{2}G$	7-9		835
	2	1343.642	55.41783 - 129.84233	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₄)6d	${}^{4}F^{\circ} - {}^{4}D$	$\frac{7}{2} - \frac{5}{2}$		835
		1244 106	5()7141 120 7(5)(7 7		0.75
		1344.190	56.37141 - 130.76320	$3d^{2}(a^{2}F)4p = 3d^{2}(a^{2}F)5d$	$^{2}G^{2} - ^{4}H$	$\frac{1}{2} - \frac{1}{2}$		835
	50	1344.334	50.3/141 - 130./5/31	$3d^{2}(a^{2}F)4p = 3d^{2}(a^{2}F)30d$ $3d^{2}(a^{3}F)4p = 3d^{2}(a^{3}F)7p$	$4C^{\circ}$ $4E$	$\frac{1}{2} - \frac{1}{2}$		833
	50	1344.014	53.49649 - 127.86/13	$3d^{\circ}(a^{\circ}F)4p = 3d^{\circ}(a^{\circ}F_4)/s$	-2D 45°	$\frac{1}{2} - \frac{1}{2}$		835
	50	1345.882	0.0 - 74.30093	30° – 30°(a°P)4p	g-D - 'S	2 - 2		835
	20	1340.334	55.018/1 - 129.29451	$3d^{(a'F')4p} - 3d^{(a'F')}/s$	'G' - 'F	$\frac{5}{5} - \frac{5}{5}$		835
	- 30	1348.333	23.10828 - 97.27383	$3d^{\circ}(a^{\circ}D)4s = 3d^{\circ}(a^{\circ}F)4s4p(^{\circ}P^{\circ})$	$z D - z D^2$	2 - 2		835
	0	1349.594	55.29965 - 129.39604	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₄)6d	² G° – ⁴ H	$\frac{9}{2} - \frac{11}{2}$		835
	12	1349.791	55.41783 - 129.50324	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})6d$	⁴ F° – ⁴ G	$\frac{7}{2} - \frac{9}{2}$		835
	5	1350.256	56.07526 - 130.13519	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})7s$	⁴ F° − ⁴ F	$\frac{5}{2} - \frac{3}{2}$		835
	10	1350.321	55.41783 - 129.47427	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})6d$	${}^{4}F^{\circ} - {}^{4}F$	$\frac{7}{2} - \frac{7}{2}$		835
	10	1351.287	23.79618 - 97.79966	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	$^{2}D - z^{4}D^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		835
	35	1351.862	55.29965 - 129.27172	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})7s$	${}^{2}\mathbf{G}^{\circ} - {}^{2}\mathbf{F}$	$\frac{9}{2} - \frac{7}{2}$		835
	10	1352.237	57.08055 - 131.03201	$3d^{8}(a^{3}E)4n = 3d^{8}(a^{3}E)6d$	${}^{2}F^{\circ} - {}^{2}D$	1 _ 5		835
	8	1353 606	55 41783 - 129 29451	$3d^{8}(a^{3}E)4p = 3d^{8}(a^{3}E)7e$	⁴ F° - ⁴ F	7 5		835
	15	1353 821	56 37141 - 130 23626	$3d^{8}(a^{3}E)4p = 3d^{8}(a^{3}E)7s$	$^{2}G^{\circ} - ^{2}F$	$\frac{2}{7} = \frac{2}{5}$		835
	2	1354 023	55 41783 - 129 27172	$3d^{8}(a^{3}F)4n = 3d^{8}(a^{3}F)7s$	4F° - F	2 2		835
	10	1355 849				2 2		835
	5	1356.318	54.26263 - 127.99156	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7s$	⁴ G° – ⁴ F	$\frac{7}{2} - \frac{7}{2}$		835
	20	1356 460	57 08055 130 90133	248(a3E)An 248(a3E) (4	2 F ° 2 C	2 9		925
	20	1356 653	56 42449 - 130 13519	$3d^8(a^3E)A_P = 3d^8(a^3E)7c$	4E° 4E	$\frac{2}{3}$ $\frac{2}{3}$		825
	11	1357 132	57 08055 - 130 76526	$3d^8(a^3E)4p = 3d^8(a^3E)6d$	$\Gamma = \Gamma$ $2E^{\circ} = 2E$			835
	5	1357.152	29,07093 - 102,74274	$3d^{8}(a^{3}P)Aa = 3d^{7}(a^{4}F)AaAm(^{3}P^{2})$	$\Gamma - \Gamma$	$\frac{2}{3} - \frac{2}{3}$		825
	25	1358 475	57 42016 - 131 03201	$3d^{8}(a^{3}E)A_{P} = 3d^{8}(a^{3}E)6d$	$2 \mathbf{D}^{\circ} \mathbf{D}$	2 2 2		835
	15	1358.992	57.42010 - 151.05201	50 (a 1)4p - 50 (a 13)60	D - D	2 - 2		835
		12/0.02/	0.2 70/10 07 - 7000		20 10-	3 4		
	14	1300.956	23./9018 - 9/.2/383	3d"(a'D)4s - 3d'(a'F)4s4p('P')	•D - z•D°	2 - 2		835
	5	1361.757	54.55705 - 127.99156	$3d^{\circ}(a^{\circ}F)4p - 3d^{\circ}(a^{\circ}F_{4})7s$	'F' - 'F	$\frac{1}{2} - \frac{1}{2}$		835
	50	1301.885	23.10828 - 96.53587	3d°(a'D)4s - 3d'(a'F)4s4p('P°)	² D − z ³ D°	2 - 2		835
	20	1362.926	57 10017 100 7/10/		200 20	5 7		835
	3	1363.421	57.42016 - 130.76526	3d°(a'F)4p - 3d°(a'F ₃)6d	² D ² - ² F	2 - 2		835
	2	1363.540	32.49953 - 105.83806	3d°(a'G)4s - 3d°(a'F ₃)5p	-GF°	$\frac{2}{2} - \frac{1}{2}$		835
	2	1363.617	24.78820 - 98.12263	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{4}P - z^{4}D^{\circ}$	$\frac{3}{2} - \frac{1}{2}$		835
	1	1363.861						835
	25	1364.067	54.55705 - 127.86713	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7s$	${}^{4}F^{\circ} - {}^{4}F$	$\frac{9}{2} - \frac{9}{2}$		835
	25	1364.202	58.49321 - 131.79626	3d8(a3F)4p - 3d8(a3F2)6d	${}^{2}F^{\circ} - {}^{2}F$	$\frac{5}{2} - \frac{5}{2}$		835
	1	1364.440						835
	20	1364.505	24.83593 - 98.12263	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{4}P - z^{4}D^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		835

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NI II - Continued

Aultiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm 1)	Configurations	Terms	J - J	Notes	References
	2	1364.793	57.42016 - 130.69135	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6d$	${}^{2}\mathbf{D}^{\circ} - {}^{2}\mathbf{P}$	$\frac{5}{2} - \frac{3}{2}$		835
	25	1365.048	58.49321 - 131.75073	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{2})6d$	${}^{2}F^{\circ} - {}^{2}G$	$\frac{5}{2} - \frac{7}{2}$		835
	4	1365.760	56.07526 - 129.29451	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{3}F_{3})7s$	⁴ F° – ⁴ F	$\frac{5}{2} - \frac{5}{2}$		835
	5	1366.947	57.08055 - 130.23626	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})7s$	${}^{2}F^{\circ} - {}^{2}F$	$\frac{7}{2} - \frac{5}{2}$		835
	20	1367.067	29.59346 - 102.74274	$3d^{*}(a^{3}P)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{2}\mathbf{P} - \mathbf{z}^{2}\mathbf{D}^{\circ}$	$\frac{1}{2} - \frac{3}{2}$		835
	1	1367.394	56.37141 - 129.50324	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{4})6d$	² G° – ⁴G	$\frac{7}{2} - \frac{9}{2}$		835
	10	1368.171	58.70595 - 131.79626	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{2})6d$	${}^{2}D^{\circ} - {}^{2}F$	$\frac{3}{7} - \frac{5}{7}$		835
	1	1369.560						835
	20	1369.651	24.78820 - 97.79966	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{4}P - z^{4}D^{\circ}$	3-3	1	835
	500	1370.136	0.0 - 72.98565	$3d^9 - 3d^8(a^3P)4p$	$g^2 D - {}^2 P^\circ$	5 - 3		835
	25	1370.549	24.83593 - 97.79966	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{2})$	$^4P - z^4D^\circ$	1 - 3		835
	4	1370.804	58.70595 - 131.65583	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{2})6d$	${}^{2}\mathbf{D}^{\circ} - {}^{2}\mathbf{P}$	$\frac{1}{2} - \frac{1}{2}$		835
	1	1371 733	56 37141 - 129 27172	$3d^{8}(a^{3}E)4n = 3d^{8}(a^{3}E)7e$	$^{2}G^{\circ} - ^{2}F$	1_1		835
	4	1373 746	1 50694 - 74 30093	$3d^{9} - 3d^{8}(a^{3}\mathbf{P})An$	~2D 45°	$\frac{2}{3}$ $\frac{2}{3}$		035
0	150	1374.075	1.50694 74.30095	$3d^{9} - 3d^{8}(a^{3}D)Am$	gD = 3	$2 - \frac{1}{2}$		835
,	50	1374.073	1.50094 - 74.28555	$3\mathbf{U} = 3\mathbf{U} (\mathbf{a} \mathbf{r}) 4 \mathbf{p}$ $2\mathbf{d}^{3} (\mathbf{c}^{3} \mathbf{E}) 4 \mathbf{c} = 2\mathbf{d}^{7} (\mathbf{c}^{4} \mathbf{E}) 4 \mathbf{c} 4 \mathbf{r} (3 \mathbf{P}^{2})$	gD3	$\frac{1}{2} - \frac{1}{2}$		835
	10	1373.022	29.07093 - 101.73480	50 (a r)45 - 30 (a r)454p(*P*)	°P - Z°D*	2 - 2		835
	7	1377.912	55.41783 - 127.99156	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})7s$	⁴F° – ⁴ F	$\frac{7}{2} - \frac{7}{2}$		835 835
		1270 670			100 100			
	1	1378.578	58.49321 - 131.03201	$3d^{(a'F)} = 3d^{(a'F)} = 3d^{(a'F)}$	F – D	$\frac{2}{2} - \frac{2}{2}$		835
	50	1379.586	24.78820 - 97.27383	$3d^{*}(a^{P})4s - 3d^{7}(a^{F})4s4p(^{P})$	$^{4}P - z^{4}D^{\circ}$	$\frac{2}{2} - \frac{2}{2}$		835
	12	1379.980	23.10828 - 95.57339	$3d^{3}(a^{T}D)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	$^{2}D - z^{4}G^{\circ}$	$\frac{2}{2} - \frac{1}{2}$		835
	2	1380.440						835
	20	1380.793	57.42016 - 129.84233	3d*(a³F)4p - 3d*(a³F₄)6d	$^{2}D^{\circ} - ^{4}D$	2 - 2		835
	200	1381.295	1.50694 - 73.90325	3d° – 3d*(a³P)4p	$g^2D - {}^2P^\circ$	$\frac{1}{2} - \frac{1}{2}$		835
	6	1381.423	51.04546 - 123.43460	$3d^{2}4s^{2} - 3d^{8}(a^{3}F_{4})6p$	⁴ F - ² G°	2-2		835
	4	1381.694	0.0 - 72.37542	$3d^{\circ} - 3d^{*}(a^{3}P)4p$	$g^2D - {}^2D^\circ$	$\frac{5}{2} - \frac{3}{2}$		835
	2	1382.695	58.49321 - 130.81591	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{3}F_{3})6d$	² F° – ⁴G	5 - 7		835
	1	1383.356						835
	0	1383.966	23.79618 - 96.05248	$3d^{(a)}D)4s - 3d^{(a)}F)4s4p(^{3}P^{(a)})$	$^{2}D - z^{4}G^{\circ}$	3-5		835
	12	1384.327	25.03638 - 97.27383	$3d^{x}(a^{1}P)4s - 3d^{7}(a^{4}F)4s4p(^{1}P^{\circ})$	${}^{4}\mathbf{P} - \mathbf{z}{}^{4}\mathbf{D}^{\circ}$	3-2		835
	I	1385.179						835
	6	1385.216	57.08055 - 129.27172	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F)7s$	${}^{2}F^{\circ} - {}^{2}F$	<u><u>z</u>_<u>z</u></u>		835
	1	1386.063	32 49953 - 104 64652	$3d^{8}(a^{1}G)4s = 3d^{8}(a^{3}F_{1})5n$	${}^{2}G - {}^{4}F^{9}$	2 2		835
	10	1387 745	57 42016 - 129 47973	$3d^{8}(a^{3}E)An = 3d^{8}(a^{3}E)Ad$	2D° 4P	2 2 2		835
	5	1287 851	57.42016 129.47975	$3d(a^{1})+p = 3d(a^{1})+3d(a^{1})$	2D° 4F	2 2 2		835
	1	1388 796	59 70595 120 71095	3d(a T)+p = 3d(a T)+0d $3d^8(a^3E)/dp = 2d^8(a^3E)/dd$		$\frac{2}{3}$ $\frac{2}{1}$		035
	1	1500.790	58.70595 - 150.71085	50 (a F)4p - 50 (a F),60	D - F	$\bar{2} - \bar{2}$		833
	2	1391.761	57.42016 - 129.27172	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})7s$	$^{2}D^{\circ} - ^{2}F$	$\frac{5}{2} - \frac{7}{2}$		835
	100	1393.330	0.0 - 71.77083	3d - 3d(a'P)4p	$g^{2}D - D^{2}$	2 - 2		835
	12	1393.867	58.49321 - 130.23626	$3d^{(a'F)}4p - 3d^{(a'F_2)}/s$	F - F	2 - 2		835
	10	1396.695	23.10828 - 94.70593	$3d^{(a'D)}4s - 3d^{(a'F)}4s4p(^{P'})$	$^{\circ}D - z^{\circ}F^{\circ}$	5-5		835
	14	1396.790	32.52354 - 104.08104	$3d^{*}(a^{1}G)4s - 3d^{*}(a^{3}F_{3})5p$	² G – ⁴ F°	7-3		835 835
	2	1397.858	29.07093 - 100.60901	3d^(a`P)4s - 3d/(a*F)4s4p(`P*)	$^{2}P - z^{2}F^{\circ}$	2 - 2		835
	3	1398.009	58.70595 - 130.23626	$3d^{*}(a^{*}F)4p - 3d^{*}(a^{*}F_{2})7s$	${}^{2}\mathbf{D}^{\circ} - {}^{2}\mathbf{F}$	2 - 2		835
	40	1398.612	25.03638 - 96.53587	3d*(a'P)4s - 3d'(a'F)4s4p('P')	$^{4}P - z^{4}D^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		835
	16	1398.758	57.42016 - 128.91281	$3d^{*}(a^{+}F)4p - 3d^{*}(a^{+}F_{4})5g$	$^{2}D^{\circ} - ^{4}P$	$\frac{2}{2} - \frac{2}{2}$		835
8	80 12	1399.026	1.50694 - 72.98565	$3d^{4} - 3d^{8}(a^{3}P)4p$	$g^2D - {}^2P^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		835 835
	12	.577.501						055
	30	1400.644	51.04546 - 122.44122	3d ⁷ 4s ² - 3d ⁸ (a ³ F ₄)6p	⁴ F − ⁴ F°	$\frac{9}{2} - \frac{9}{2}$		835
	20	1402.379	61 04647 100 100FT		40 400	9 11		835
	7	1406.970	51.04546 - 122.12057	3d′4s² – 3d°(a'F₄)6p	"F - "G"	$\frac{2}{2} - \frac{11}{2}$		835
	10	1408.796				1	1	835
	10				1		1 1	
	15	1409.612						835

NI II - Continued

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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	100	1411.071	1.50694 - 72.37542	3d ⁹ - 3d ⁸ (a ³ P)4p	$g^2D - {}^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$		835
	30	1412.868	0.0 - 70.77812	$3d^9 - 3d^8(a^3P)4p$	$g^2D - {}^4D^\circ$	$\frac{5}{2} - \frac{7}{2}$		835
	10	1413.679			-			835
	15	1414.299	0.0 - 70.70677	$3d^9 - 3d^8(a^3P)4p$	$g^2D - {}^4D^\circ$	$\frac{5}{2} - \frac{3}{2}$		835
	1	1414.444	66.57971 - 137.27822	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)5d$	${}^{4}\mathbf{P}^{\circ} - {}^{2}\mathbf{P}$	3-3		835
	20	1415.728	0.0 - 70.63546	$3d^{\circ} - 3d^{\circ}(a^{3}P)4p$	$g^2D - {}^4D^\circ$	$\frac{5}{2} - \frac{5}{2}$		835
					-			
	1	1415.846				i i		835
	12	1416.060	51.55785 - 122.17542	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})5d$	${}^{4}D^{\circ} - {}^{2}F$	$\frac{7}{2} - \frac{5}{2}$		835
	0	1416.660	58.70595 - 129.29451	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{1})7s$	2 D° - 4 F	3-5		835
	10	1417.007	57,42016 - 127,99156	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{4})7s$	${}^{2}D^{\circ} - {}^{4}F$	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>	1	835
	1	1417 553	24 78820 - 95 33253	$3d^{8}(a^{3}P)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{4}\mathbf{P} - \mathbf{z}^{4}\mathbf{F}^{\circ}$	3 - 5		835
	10	1417.699	25 03638 - 95 57339	$3d^{*}(a^{3}P)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{2})$	${}^{4}P - z^{4}G^{\circ}$	3 - 3		835
	10		20100000 70107007					
	5	1420 674	66 57134 - 136 96075	$3d^{8}(a^{3}P)4p = 3d^{8}(a^{3}P)5d$	4P° - 4P	5 - 5		835
	18	1420.843	66 57971 - 136 96075	$3d^{8}(a^{3}P)4n = 3d^{8}(a^{3}P)5d$	4P° _ 4P	3_5		835
	10	1421.013	66 57134 136 89934	$3d^{8}(a^{3}P)4n = 3d^{8}(a^{3}P)5d$	⁴ P ° _ ⁴ P	2 3		835
	0	1421.713	00.57154 - 150.87954	50 (a 1)+p = 50 (a 1)50	1 - 1	2 2 2		835
-	16	1422.320	1 50604 71 77083	$3d^9 = 3d^8(a^3\mathbf{P})4\mathbf{p}$	$\sigma^2 D = {}^2 D^{\circ}$	3_5		835
/	10	1423.212	52 20595 122 44122	$3d^{7}4s^{2} - 3d^{8}(a^{3}F)6p$	$4\mathbf{F} - 4\mathbf{F}^{\circ}$	2 - 2 7 - 2		835
	11	1423.780	32.20393 - 122.44122	50 45 - 50 (a r4)6p	F = F	2 - 2		
		1422.004						925
		1423.994	(7.03103 137.31103	2d8(a3D)4m 2d8(a3D)5d	4D° 2D	1 1 1		935
	3	1424.890	67.03102 - 137.21193	30 (a P)4p - 30 (a P)30	F - F	2 - 2		035
	10	1425.025		2174 2 2184 35 345	41 26230	9 7		035
	0	1425.579	51.04546 - 121.19232	$3d^{4}4s^{2} - 3d^{2}(a^{2}F_{2})4I$	F = 2[3]	$\frac{1}{2} - \frac{1}{2}$		033
	3	1425.604	66.57971 - 136.72533	3d'(a'P)4p - 3d'(a'P)5d	P-P	2 - 2		833
	3	1426.783						635
		1427 449						925
	1	1427.448				1		035
	10	1427.782	(= 02102 12 (00024		400 40	1 3		833
	8	1431.270	67.03102 - 136.89934	$3d^{(a'P)4p} - 3d^{(a'P)5d}$	$^{4}P^{2} - ^{4}P^{2}$	$\frac{1}{2} - \frac{1}{2}$		833
	25	1431.492	51.04546 - 120.90320	$3d^{2}4s^{2} - 3d^{2}(a^{2}P)5p$	F - D	$\frac{1}{2} - \frac{1}{2}$		833
		1433.745	66.57971 - 136.32755	3d"(a"P)4p - 3d"(a"P)5d	"P" – "D	2 - 2		835
	1	1433.893						835
								075
	1	1434.317			400 40	5 5		835
	12	1434.373	66.57134 - 136.28860	3d"(a"P)4p - 3d"(a"P)5d	P - D	$\frac{1}{2} - \frac{1}{2}$		835
	14	1434.493	66.57971 - 136.29083	$3d^{\circ}(a^{\circ}P)4p - 3d^{\circ}(a^{\circ}P)5d$	$^{4}P^{2} - ^{4}D$	$\frac{1}{2} - \frac{1}{2}$		835
	12	1434.546	66.57971 - 136.28860	$3d^{\circ}(a^{\circ}P)4p = 3d^{\circ}(a^{\circ}P)5d$	$P^{*} - D$	$\begin{bmatrix} 5 & -5 \\ 1 & 3 \end{bmatrix}$		833
		1434.688	67.03102 - 136.73274	$3d^{\circ}(a^{\circ}P)4p - 3d^{\circ}(a^{\circ}P)3d$	P - F	$\frac{5}{2} - \frac{7}{2}$		833
	1	1434.837	67.03102 - 136.72533	3d (a P)4p - 3d (a P)3d	$\mathbf{P} - \mathbf{P}$	2 - 2		833
		1425 240	25 02(28 04 70502	248(-3D)4- 247(-4E)4-4-(3D ⁹)	4D -4E*	5 7		0.75
	5	1435.348	23.03030 - 94./0393	$3d^{(a''')+8} = 3d^{(a''')+8} + 3d^{(a''')} + 3d^{(a''')+8} = 3d^{(a'''')+8} + 3d^{(a'''')+8} = 3d^{(a'''')+8} + 3d^{(a''''')+8} = 3d^{(a''''')+8} = 3d^{(a''''')+8} = 3d^{(a''''')+8} = 3d^{(a''''')+8} = 3d^{(a'''''')+8} = 3d^{(a''''''')+8} = 3d^{(a''''''')+8} = 3d^{(a'''''''')+8} = 3d^{(a''''''''')+8} = 3d^{(a''''''''''''''''''''''''''''''''''''$		2 - 2		835
	50	1430.105	09.37134 - 130.20146	50 (a r)4p - 50 (a r)50	F - D	2 - 2		835
	8	1439.094	66 57124 126 05052	248(03D)4p 248(03E)90	4D° 2E	5 5		835
		1439.283	66.57134 - 136.05053	$3d^{2}(a^{2}P)4p = 3d^{2}(a^{2}P_{2})\delta S$	$4\mathbf{P} - \mathbf{F}$	$\frac{1}{2} - \frac{1}{2}$		033
	8	1439.352	66.57971 - 136.05450	$3d^{2}(a^{2}P)4p = 3d^{2}(a^{2}P_{3})/d$ $2d^{2}(a^{3}D)4p = 2d^{2}(a^{3}P_{3})/d$	4P° 4D	$\frac{1}{2} - \frac{1}{2}$		033
	13	1443.080	67.03102 - 136.32755	3d (a P)4p - 3d (a P)3d	F-D	$\frac{1}{2} - \frac{1}{2}$	1	635
	10	1442 939	67.02102 126.20092	248(0 ³ D)4m 248(- ³ D)64	4p° 4p	11		825
	10	1443.838	67.03102 - 136.29083	3d"(a"P)4p - 3d"(a"P)3d	P - D	2 - 2		833
		1444.940	1 50/04 - 50 50/33	219 218(-30)4-	20 40	3 3	1	833
	13	1445.098	1.50694 - 70.70677	30° – 30°(a°P)4p	g.DD.	2 - 2		835
	14	1445.460			20 400	3 .		835
	20	1446.589	1.50694 - 70.63546	3d ⁷ – 3d ⁶ (a ³ P)4p	$g^2D - D^*$	2 - 2		835
8	14	1450.005	0.0 - 68.96565	3d' – 3d'(a'D)4p	g'D - 'P'	2 - 2		835
					4- 4- 4	, .		
	15	1452.558	52.20595 - 121.05066	3d'4s ² – 3d ⁸ (a'P)5p	"F - "D"	$\frac{1}{2} - \frac{2}{2}$		835
	15	1453.359	68.15431 - 136.96075	3d'(a'D)4p - 3d'(a'P)5d	'D' - 'P	2 - 2		835
	2	1454.292	53.03793 - 121.80034	$3d^{7}4s^{2} - 3d^{8}(a^{3}P)5p$	*F - 2D*	2 - 2	ł	835
7	200	1454.852	0.0 - 68.73598	3d" - 3d"(a'D)4p	g ² D - ² D°	2 - 2		835
	16	1456.913						835
	5	1457.359	68.28162 - 136.89934	3d°(a'D)4p - 3d ⁸ (a'P)5d	'₽" – *P	$\frac{1}{2} - \frac{3}{2}$		835
	1		F		1	1	1	

NI II - Continued

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	Reference
	4	1457.863	67.69464 - 136.28860	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}P)5d$	² F° - ⁴ D	$\frac{5}{2} - \frac{5}{2}$		835
	4	1458.170	52.73845 - 121.31789	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₃)5d	⁴D° - ⁴G	$\frac{5}{2} - \frac{7}{2}$		835
	4	1458.342	68.15431 - 136.72533	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}P)5d$	${}^{2}D^{\circ} - {}^{4}P$	$\frac{3}{2} - \frac{1}{2}$		835
	4	1459.459						835
	1	1459.611						835
	1	1459.640	53.63462 - 122.14499	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})5d$	⁴ D° – ⁴ G	$\frac{3}{2} - \frac{5}{2}$		835
	12	1459.715	67.69464 - 136.20146	3d ⁸ (a ¹ D)4p - 3d ⁸ (a ³ P)5d	² F° - ⁴ D	$\frac{5}{2} - \frac{7}{2}$		835
	9	1459.809	52.73845 - 121.24090	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	${}^{4}D^{\circ} - {}^{2}F$	$\frac{5}{2} - \frac{7}{2}$		835
	6	1460.078	52.73845 - 121.22780	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	4D° - 4F	$\frac{5}{2} - \frac{5}{2}$		835
	1	1460.136	51.55785 - 120.04495	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₄)5d	⁴ D° – ⁴ G	$\frac{7}{2} - \frac{9}{2}$		835
	1	1460.312	53.63462 - 122.11294	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})5d$	${}^{4}\mathbf{D}^{\circ} - {}^{2}\mathbf{P}$	$\frac{3}{2} - \frac{1}{2}$		835
	2	1460.408	68.13121 - 136.60479	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}F_{2})6g$	² F° – 2[4]°	$\frac{7}{2} - \frac{7}{2}$		835
	8	1461.840	66.57134 - 134.97847	3d ⁸ (a ³ P)4p - 3d ⁸ (a ³ F₄)7d	${}^{4}P^{\circ} - {}^{4}D$	$\frac{5}{2} - \frac{5}{2}$		835
	8	1462.482	52.73845 - 121.11559	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	${}^{4}D^{\circ} - {}^{2}P$	$\frac{5}{2} - \frac{3}{2}$		835
	20	1462.944	51.55785 - 119.91333	3d8(a3F)4p - 3d8(a3F4)5d	⁴ D° − ⁴ F	$\frac{7}{2} - \frac{9}{2}$		835
	14	1463.113	53.03793 - 121.38580	$3d^{7}4s^{2} - 3d^{8}(a^{3}P)5p$	4F - 4D°	$\frac{5}{2} - \frac{3}{2}$		835
	8	1464.301	67.69464 - 135.98606	3d ⁸ (a ¹ D)4p - 3d ⁸ (a ³ F ₃)7d	${}^{2}F^{\circ} - {}^{4}G$	$\frac{5}{2} - \frac{7}{2}$		835
	10	1464.369	67.69464 - 135.98322	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}F_{2})8s$	² F° – ⁴ F	$\frac{5}{2} - \frac{3}{2}$		835
7	60	1467.265	0.0 - 68.15431	3d ⁹ - 3d ⁸ (a ¹ D)4p	$g^2D - {}^2D^\circ$	$\frac{5}{2} - \frac{3}{2}$		835
	10	1467.637	68.15431 - 136.29083	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}P)5d$	${}^{2}D^{\circ} - {}^{4}D$	$\frac{3}{2} - \frac{1}{2}$		835
	10	1467.694	68.15431 - 136.28860	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}P)5d$	${}^{2}D^{\circ} - {}^{4}D$	$\frac{3}{2} - \frac{5}{2}$		835
6	100	1467.762	0.0 - 68.13121	$3d^{\circ} - 3d^{\circ}(a^{\dagger}D)4p$	$g^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		835
	30	1468.268	51.55785 - 119.66529	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})5d$	⁴ D° – ⁴ P	$\frac{7}{2} - \frac{5}{2}$		835
	25	1468.465	51.55785 - 119.65625	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})5d$	${}^{4}D^{\circ} - {}^{4}D$	$\frac{7}{2} - \frac{7}{2}$		835
	10	1469.200	53.63462 - 121.69902	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	⁴ D° – ⁴ D	$\frac{3}{2} - \frac{3}{2}$		835
	3	1469.601	68.28162 - 136.32755	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}P)5d$	${}^{2}P^{\circ} - {}^{4}D$	$\frac{1}{2} - \frac{3}{2}$		835
	1	1469.847						835
	1	1470.322	53.03793 - 121.05066	$3d^{7}4s^{2} - 3d^{8}(a^{3}P)5p$	⁴ F – ⁴ D°	$\frac{5}{2} - \frac{5}{2}$		835
	2	1470.386	68.28162 - 136.29083	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}P)5d$	${}^{2}P^{\circ} - {}^{4}D$	$\frac{1}{2} - \frac{1}{2}$	1 1	835
	5	1470.666	68.73598 - 136.73274	$3d^{*}(a^{T}D)4p - 3d^{*}(a^{3}P)5d$	${}^{2}D^{\circ} - {}^{4}F$	$\frac{5}{2} - \frac{3}{2}$		835
	10	1471.466	66.57971 - 134.53937	3d ⁸ (a ³ P)4p - 3d ⁸ (a ³ F₄)7d	⁺P° – ⁴P	$\frac{3}{2} - \frac{5}{2}$		835
	1	1471.961	54.17626 - 122.11294	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{2})5d$	${}^{4}D^{\circ} - {}^{2}P$	$\frac{1}{2} - \frac{1}{2}$		835
	10	1472.571	54.17626 - 122.08479	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})5d$	⁴ D° – ⁴ F	$\frac{1}{2} - \frac{3}{2}$		835
	5	1472.835	68.15431 - 136.05053	$3d^{s}(a^{1}D)4p - 3d^{s}(a^{3}F_{2})8s$	${}^{2}D^{\circ} - {}^{2}F$	$\frac{3}{2} - \frac{5}{2}$		835
	2	1472.889	51.04546 - 118.93953	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})4f$	⁴ F − 4[5]°	$\frac{9}{2} - \frac{11}{2}$		835
	1	1473.249	68.15431 - 136.03143	$3d^{*}(a^{T}D)4p - 3d^{*}(a^{T}F_{3})7d$	${}^{2}\mathbf{D}^{\circ} - {}^{2}\mathbf{D}$	$\frac{3}{2} - \frac{5}{2}$		835
	1	1474.312	51.04546 - 118.87411	3d ⁷ 4s ² - 3d ⁸ (a ³ F₄)4f	⁴F - 4[3]°	$\frac{9}{2} - \frac{7}{2}$		835
	4	1474.597	53.36517 - 121.18055	3d*(a3F)4p - 3d*(a3F3)5d	${}^{4}G^{\circ} - {}^{2}H$	$\frac{9}{2} - \frac{11}{2}$		835
	2	1474.901						835
	1	1474.910	68.96565 - 136.76649	3d [*] (a ¹ D)4p - 3d [*] (a ³ P)5d	² P° – ⁴ F	$\frac{3}{2} - \frac{5}{2}$		835
	3	1475.270	53.60119 - 121.38580	$3d^{7}4s^{2} - 3d^{8}(a^{3}P)5p$	⁴ F - ⁴ D°	$\frac{3}{2} - \frac{3}{2}$		835
	1	1475.645	68.96565 - 136.73274	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}P)5d$	${}^{2}P^{\circ} - {}^{4}F$	$\frac{3}{2} - \frac{3}{2}$		835
	3	1475.734	70.35894 - 138.12188	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})9p$	² G - ⁴ F°	$\frac{9}{2} - \frac{9}{2}$		835
	2	1475.801	68.96565 - 136.72533	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}P)5d$	${}^{2}P^{\circ} - {}^{4}P$	$\frac{1}{2} - \frac{1}{2}$		835
	25	1476.043	54.17626 - 121.92516	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})5d$	⁺ D° – ⁴ D	2 - 2		835
	1	1477.063	68.28162 - 135.98322	$3d^{*}(a^{1}D)4p - 3d^{*}(a^{3}F_{2})8s$	$^{2}P^{\circ} - {}^{4}F$	$\frac{1}{2} - \frac{3}{2}$		835
6	4	1477.227	0.0 - 67.69464 68.15657 - 135.84941	$3d^9 - 3d^8(a^1D)4p$ $3d^74s^2 - 3d^8(a^3P)4f$	$g^2D - {}^2F^{\circ}$ ${}^4P - 1(3)^{\circ}$	$\frac{2}{2} - \frac{2}{2}$		835 835
			50.10007 100.04941		x = 1[3]	2 - 2		000
	10	1479.443	53.63462 - 121.22780	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	⁴ D° – ⁴ F	$\frac{3}{2} - \frac{5}{2}$		835 835
	30	1480 331	68 73598 - 136 28860	$3d^{8}(a^{1}D)4n = 3d^{8}(a^{3}P)5d$	${}^{2}D^{\circ} - {}^{4}D$	5_5		835
	75	1481 001	51 04546 - 118 56330	$3d^{7}4s^{2} = 3d^{8}(a^{1}D)5n$	${}^{4}F = {}^{2}F^{9}$	$\frac{2}{9}$ $\frac{2}{2}$		835
	0	1481 210	51.04540 - 116.50559	50 48 - 50 (a D)5p	1 - F	2 - 2		835
	15	1481 560	66 57134 - 134 06776	3d8(a3D)4p 3d8(aD)5d	4D° 2D	5 3		825

NI II - Continued

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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	References
	15	1481.744	66.57971 - 134.06776	3d ⁸ (a ³ P)4p - 3d ⁸ (a ¹ D)5d	${}^{4}\mathbf{P}^{\circ} - {}^{2}\mathbf{P}$	$\frac{3}{2} - \frac{3}{2}$		835
	12	1481.883	66.57134 - 134.05305	3d ⁸ (a ³ P)4p - 3d ⁸ (a ³ D)5d	${}^{4}\mathbf{P}^{\circ} - {}^{2}\mathbf{D}$	$\frac{5}{2} - \frac{5}{2}$	Ì	835
	4	1481.898	53.63462 - 121.11559	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	${}^{4}D^{\circ} - {}^{2}P$	$\frac{3}{2} - \frac{3}{2}$		835
	10	1481.982	53.63462 - 121.11190	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	4D° – 4P	$\frac{1}{2} - \frac{1}{2}$		835
	100	1482.240	68.73598 - 136.20146	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}P)5d$	${}^{2}D^{\circ} - {}^{4}D$	5 - 1		835
	8	1482 393	1 50694 - 68 96565	$3d^9 = 3d^8(a^1D)4n$	$a^2 D = {}^2 P^{\circ}$	3 3		835
	0	1402.375	1.50074 - 08.50505	50 - 50 (a D)+p	gD-1	2-2		000
	40	1483.277	23.10828 - 90.52618	$3d^{8}(a^{1}D)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	$^{2}D - z^{6}G^{\circ}$	$\frac{5}{2} - \frac{5}{2}$		835
	15	1483.554	52.73845 - 120.14417	3d*(a'F)4p - 3d*(a'F ₄)5d	⁴D° – ⁴D	$\frac{2}{2} - \frac{2}{2}$		835
	1	1483.760						835
	25	1484.227	66.57971 - 133.95485	3d ⁸ (a ³ P)4p - 3d ⁸ (a ¹ D)5d	${}^{4}P^{\circ} - {}^{2}P$	$\frac{3}{2} - \frac{1}{2}$		835
	1	1484.592	66.57134 - 133.92988	3d ⁸ (a ³ P)4p - 3d ⁸ (a ¹ D)5d	⁴ P° − ² G	$\frac{5}{2} - \frac{7}{2}$	1	835
	10	1485.185	66.57134 - 133.90300	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{1}D)5d$	4 P° − 2 D	$\frac{5}{2} - \frac{3}{2}$		835
	60	1485.375	66.57971 - 133.90300	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{1}D)5d$	${}^{4}P^{\circ} - {}^{2}D$	3-3		835
	2	1485 987	68 73598 - 136 03143	$3d^{8}(a^{1}D)4p = 3d^{8}(a^{3}E_{1})7d$	$^{2}D^{\circ} - ^{2}D$	1 1 1		835
	5	1486 372	66 57971 - 133 85773	$3d^8(a^3P)4n = 3d^8(a^3P)6c$	⁴ P ° - ⁴ P	3_1		835
	7	1496 669	52 73845 120 00286	$2d^{8}(a^{3}E)4n = 2d^{8}(a^{3}E)5d$	4D° 4E	2 - 2 5 Z		835
	50	1487.242	52.75845 - 120.00280	$3u(a \Gamma) + p = 3u(a \Gamma_4) + 3u$		2 - 2		835
	50	1487.242	00.5/134 - 133.809/6	$3d^{\circ}(a^{\circ}P)4p - 3d^{\circ}(a^{\circ}F_{4})8s$	P - F	$\frac{1}{2} - \frac{1}{2}$		835
	5	1487.438	1.50694 - 68.73598	3d° – 3d°(a'D)4p	g°D – °D°	$\frac{2}{2} - \frac{2}{2}$		835
7	6	1487.455	1.50694 - 68.73598	3d ⁹ – 3d ⁸ (a ¹ D)4p	$g^2D - {}^2D^\circ$	$\frac{3}{2} - \frac{5}{2}$		835
	5	1487.778						835
	2	1487.970						835
	1	1488.109						835
	16	1488.730	52.73845 - 119.90972	$3d^{8}(a^{3}F)4p = 3d^{8}(a^{3}F_{4})5d$	4D° – 4P	5-3		835
	5	1488.845	68.73598 - 135.90196	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}F_{3})7d$	² D ° – ⁴ F	$\frac{5}{2} - \frac{5}{2}$		835
	100	1488 896	66 57134 - 133 73408	$3d^{8}(a^{3}D)dn = 3d^{8}(a^{1}D)5d$	4D° 2F	5 1		825
	25	1480.070	66 57071 122 72526	$3d(a^{2}P)4p = 3d(a^{2}D)3d$ $3d^{8}(a^{3}P)4p = 3d^{8}(a^{3}D)5d$	$\Gamma = \Gamma$ 4D° 2E	2 - 2 3 5		035
	55	1489.079	55 01971 122 14400	3d(aT)+p = 3d(aD)/3d $2d^{3}(a^{3}E)/4a = 2d^{3}(a^{3}E)/5d$	$\mathbf{r} = \mathbf{r}$	2 - 2 5 5		035
	5	1489.729	55.018/1 - 122.14499	$30^{\circ}(a^{\circ}r)^{4}p - 30^{\circ}(a^{\circ}r_{2})^{3}0$	$\frac{1}{10}$	$\frac{1}{2} - \frac{1}{2}$		835
		1490.262	68.15657 - 135.25892	3d ¹ 4s ² - 3d ² (a ² P)4s4p(¹ P ²)	$P = V^2 D^2$	2 - 2		835
	2	1491.176	55.018/1 - 122.08025	3d"(a'F)4p - 3d"(a'G)4d	"G" - "F	2 - 2		835
	4	1491.308	54.26263 - 121.31789	$3d^{\circ}(a^{\circ}F)4p = 3d^{\circ}(a^{\circ}F_{3})5d$	"G" – "G	$\frac{1}{2} - \frac{1}{2}$		835
	4	1491.588	66.57134 - 133.61399	3d ⁸ (a ³ P)4p - 3d ⁸ (a ³ P)6s	⁴ P° – ⁴ P	$\frac{5}{2} - \frac{3}{2}$		835
	6	1491.776	66.57971 - 133.61399	3d ⁸ (a ³ P)4p - 3d ⁸ (a ³ P)6s	⁴ P° – ⁴ P	$\frac{3}{2} - \frac{3}{2}$		835
	3	1491.823	54.26263 - 121.29467	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	⁴ G° – ² G	$\frac{7}{2} - \frac{9}{2}$		835
	40	1491.899	55.01871 - 122.04729	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})5d$	4G° 4H	3-7		835
	15	1493.022	54.26263 - 121.24090	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	4G° − 2F	$\frac{1}{2} - \frac{1}{2}$		835
	2	1493.315	54.26263 - 121.22780	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	⁴ G° - ⁴ F	$\frac{1}{2} - \frac{5}{2}$		835
	50	1494.151	54,26263 - 121,19034	$3d^{8}(a^{3}F)4p = 3d^{8}(a^{3}F_{3})5d$	4G° - 4H	2_9		835
	6	1494,236	67.03102 - 133.95485	$3d^{8}(a^{3}P)4p = 3d^{8}(a^{3}D)5d$	4P° - 2P	1_1		835
	10	1494 701	67 88016 - 134 78314	$3d^{7}4s^{2} - 3d^{7}(s^{2}F)4s4n(^{3}P^{\circ})$	${}^{4}P = w^{2}D^{2}$	2 2		835
	40	1495 383	66 57134 - 133 44389	$3d^{8}(a^{3}P)An = 3d^{8}(a^{3}P)Ac$	4D° 4D	2 - 2 5 5		835
	20	1495 570	66 57971 - 133 44389	$3d^{8}(a^{3}P)Ap = 3d^{8}(a^{3}P)Ac$	4D° 4D	2 2 2		835
	10	1496.308	67.03102 - 133.86221	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)6s$	$^{4}P^{\circ} - ^{2}P$	$\frac{2}{1} - \frac{2}{2}$		835
		1407 400	(7.03102 102.05772		400 40	, ,		025
	2	1496.409	67.03102 - 133.85773	$3d^{\circ}(a^{\circ}P)4p - 3d^{\circ}(a^{\circ}P)6s$	*P* - *P	$\frac{1}{2} - \frac{1}{2}$		835
	1	1496.463	68.15431 - 134.97847	3d°(a'D)4p – 3d ⁸ (a'F₄)7d	² D° – ⁴ D	2 - 2		835
	1	1498.734	55.41783 - 122.14071	3d*(a'F)4p - 3d*(a'F ₂)5d	${}^{4}\mathbf{F}^{\circ} - {}^{2}\mathbf{H}$	$\frac{1}{2} - \frac{9}{2}$		835
	15	1499.704	53.36517 - 120.04495	3d ⁸ (a ³ F)4p – 3d ⁸ (a ³ F₄)5d	⁴ G° – ⁴ G	$\frac{9}{2} - \frac{9}{2}$		835
7	200	1500.437	1.50694 - 68.15431	3d ⁹ – 3d ⁸ (a ¹ D)4p	$g^2D - {}^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$		835
	7	1500.651	53.36517 - 120.00286	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₄)5d	⁴ G° − ⁴ F	$\frac{9}{2} - \frac{7}{2}$		835
	20	1501.885	67.03102 - 133.61399	3d ⁸ (a ³ P)4p - 3d ⁸ (a ³ P)6s	⁴ P° – ⁴ P	$\frac{1}{2} - \frac{3}{2}$		835
	6	1501.962	0.0 - 66.57971	3d° - 3d8(a3P)4p	$g^2D - {}^4P^\circ$	$\frac{5}{2} - \frac{3}{2}$		835
	75	1502.150	0.0 - 66.57134	$3d^9 - 3d^8(a^3P)4p$	$g^2D - {}^4P^\circ$	3-3		835
	20	1502,669	53.49649 - 120.04495	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F).5d$	⁴ G° - ⁴ G	<u>π</u> _§		835
	7	1503,123	51.04546 - 117 57368	$3d^{7}4s^{2} - 3d^{7}(a^{2}D)4s4n(^{3}P^{2})$	${}^{4}\mathbf{F} = \mathbf{w}^{4}\mathbf{F}^{9}$	2 2		835
	12	1503,209	53.36517 - 119 88947	$3d^{8}(a^{3}F)4n = 3d^{8}(a^{3}F)5d$	4G° - 4G	§_1		835
				56 (a x) 1p - 54 (a x 4)54		2 - 2		000

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Multiplet	Rel. Int.	λ _{ac} (in Å)	Levels (in 10^3 cm $^{-1}$)	Configurations	Terms	J-J N	otes	References
	75	1504.485	53.36517 - 119.83300	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})5d$	⁴ G° – ⁴ H	<u> 위 - 부</u>		835
	5	1504.590	70.74870 - 137.21193	$3d^{*}(a^{3}P)4p - 3d^{*}(a^{3}P)5d$	${}^{4}D^{\circ} - {}^{2}P$	$\frac{1}{3} - \frac{1}{3}$		835
	13	1505.642	53.49649 - 119.91333	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{3}F_{4})5d$	4G° - 4F	<u>п</u> - §		835
	16	1506.184	53 49649 - 119 88947	$3d^{(a^{3}F)4p} - 3d^{(a^{3}F)4p}$	${}^{4}G^{\circ} - {}^{4}G$	<u>ů</u> <u>ů</u>	ļ	835
	25	1506.585	67 88016 - 134 25605	$3d^{7}4s^{2} - 3d^{8}(a^{3}F)6f$	$^{+}\mathbf{P} = 4[2]^{\circ}$	3 5		835
	7	1506.851	01100010 101120000		· ·(-)			835
					200 200			
	10	1506.968	67.69464 - 134.05305	$3d^{(a'D)4p} - 3d^{(a'D)5d}$	$^{2}F^{*} - ^{2}D$	2 - 2		835
	5	1506.995	52.20595 - 118.56339	$3d^{2}4s^{2} - 3d^{2}(a^{2}D)5p$	$^{\circ}F = ^{\circ}F^{\circ}$	2 - 2		835
	18	1507.465	53.49649 - 119.83300	$3d^{(a'F)4p} - 3d^{(a'F_4)5d}$	*G* - *H	$\frac{11}{2} - \frac{11}{2}$		835
	15	1507.961	70.35894 - 136.67364	$3d^{2}4s^{2} - 3d^{2}(a^{3}F_{3})8p$	² G - ² G"	$\frac{2}{2} - \frac{2}{2}$	1	835
	10	1508.249						835
	7	1508.262	70.63546 - 136.93682	3d*(a'P)4p - 3d*(a'F ₂)7d	*D° – ′ G	$\frac{2}{2} - \frac{1}{2}$	-	835
	10	1508.315	55.01871 - 121.31789	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{3})5d$	4G° - 4G	$\frac{5}{2} - \frac{7}{2}$		835
	7	1508.352						835
	4	1508.498	53.36517 - 119.65625	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{4})5d$	⁴ G° – ⁴ D	$\frac{9}{2} - \frac{7}{2}$		835
	100	1508.816	53.49649 - 119.77360	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})5d$	⁴G° - ⁴H	ų_ų		835
	1	1509.113	70.63546 - 136.89934	$3d^{*}(a^{3}P)4p - 3d^{*}(a^{3}P)5d$	⁴ D° – ⁴ P	3-3		835
	12	1509.308	68.70976 - 134.96478	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{4}\mathbf{P} - \mathbf{w}^{2}\mathbf{D}^{\circ}$	$\frac{1}{2} - \frac{3}{2}$		835
		1500 245	70 70(77 12(0(075		4D° 4D	3 5	1	0.7.5
	8	1509.345	/0./06// - 136.960/5	3d"(a"P)4p ~ 3d"(a"P)5d	'D' - 'P	$\frac{2}{5} - \frac{2}{5}$		835
	4	1509.602	68.73598 - 134.97847	$3d^{(a'D)4p} - 3d^{(a'F_4)7d}$	-DD	2 - 2		835
	100	1509.767	67.69464 - 133.92988	3d"(a'D)4p - 3d"(a'D)5d	F - G	2 - 2		835
	1	1510.067	55.01871 - 121.24090	3d^(a'F)4p - 3d^(a'F ₃)5d	"G" – "F	$\frac{2}{2} - \frac{2}{2}$		835
	16	1510.232						835
	4	1510.366	55.01871 - 121.22780	3d*(a`F)4p - 3d*(a`F ₃)5d	⁺G° - ⁺F	$\frac{2}{2} - \frac{2}{2}$		835
	3	1510.690	56.07526 - 122.27005	$3d^{x}(a^{3}F)4p - 3d^{x}(a^{3}F_{2})5d$	⁴ F° - ² G	$\frac{5}{2} - \frac{7}{2}$		835
	5	1510.741	70.70677 - 136.89934	$3d^{*}(a^{3}P)4p - 3d^{*}(a^{3}P)5d$	4D° – 4P	$\frac{3}{2} - \frac{3}{2}$		835
	75	1510.859	1.50694 - 67.69464	$3d^{\circ} - 3d^{\circ}(a^{\dagger}D)4p$	$g^2D - F^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		835
	8	1511.185	52.20595 - 118.37911	$3d^{7}4s^{2} - 3d^{8}(a^{1}D)5p$	${}^{4}F - {}^{2}F^{\circ}$	$\frac{1}{2} - \frac{5}{2}$		835
	3	1511.314	67.69464 - 133.86221	$3d^{*}(a^{T}D)4p - 3d^{*}(a^{3}P)6s$	${}^{2}F^{\circ} - {}^{2}P$	$\frac{5}{2} - \frac{3}{2}$		835
	10	1511.467						835
		1512 227	60 16667 124 20276	2474-2 247(-2E)4-4-(3P)	tD of D*	3 1		925
		1512.237	08.13037 - 134.28370	$3d^{2}4s^{2} - 3d^{2}(a^{2}F)^{4}s^{4}p(F)$	P-SD	$\frac{1}{2} - \frac{1}{2}$		035
	11	1512.742	/1.45//4 - 13/.562/4	$3d^{2}4s^{2} - 3d^{2}(a^{2}F_{2})8p$	-GG	2 - 2		835
	11	1513.016	67.88016 - 133.97333	3d'4s' - 3d'(a'F)4s4p('P')	$\mathbf{P} - \mathbf{s} \cdot \mathbf{D}^{*}$	2-2		835
		1513.550	56.07526 - 122.14499	3d [°] (a [°] F)4p - 3d [°] (a [°] F ₂)5d	"F" - "G	$\frac{1}{2} - \frac{1}{2}$	1	835
	15	1513.783	70.70677 – 136.76649	$3d^{(a'P)4p} - 3d^{(a'P)5d}$	*D* - *F	2 - 2		835
	50	1514.222	67.69464 - 133.73526	3d^(a'D)4p - 3d^(a'D)5d	$^{2}\mathbf{F}^{\bullet} - ^{2}\mathbf{F}$	2 - 2		835
	10	1514.336						835
	80	1514.372	70.35894 - 136.39285	3d ⁷ 4s ² - 3d [*] (¹ D)6p	${}^{2}G - {}^{2}F^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		835
	17	1514.411						835
	5	1514.552	70.70677 - 136.73274	3d [*] (a ³ P)4p - 3d [*] (a ³ P)5d	⁴ D° - ⁴ F	$\frac{3}{2} - \frac{3}{2}$		835
	6	1514.633						835
	2	1514.644						835
	8	1514.856	68 96565 - 134 97847	$3d^{3}(a^{1}D)4n = 3d^{3}(a^{3}E)7d$	2P° - 4D	3 _ 5		835
	15	1515 157	68 15657 - 134 15628	$3d^{7}4e^{2} = 3d^{7}(a^{2}F)AeAn(^{3}P^{6})$	4P_ e4D*	3 3		835
	25	1515.260	55 29965 - 121 20467	$3d^{8}(a^{3}E)4n = 3d^{8}(a^{3}E)5d$		2 2 2		835
	23	1515.209	23 10828 - 90 10040	$3d^{8}(a^{\dagger}D)Aa = 3d^{7}(a^{4}E)AaAm(^{3}D^{6})$	20-0	2 2 2 1 2 1		835
	6	1515.529	23.10020 - 03.10049	$3d^{8}(a^{3}D)An = 2d^{8}(a^{3}D)Ad$	⁴ D° - ⁴ F	$\frac{2}{1}$ $\frac{2}{3}$		835
	1	1515.692	70.74870 - 136.72533	$3d^{*}(a^{3}P)4p - 3d^{*}(a^{3}P)5d$	⁴ D° - ⁴ P	$\frac{2}{1} - \frac{2}{1}$		835
	30	1515.791	56.07526 - 122.04729	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{2})5d$	${}^{4}F^{\circ} - {}^{4}H$	$\frac{2}{2} - \frac{1}{2}$		835
	40	1515.825	67.88016 - 133.85083	3d'4s' - 3d'(a'F)4s4p('P')	'P - s'D'	$\frac{5}{2} - \frac{1}{2}$		835
	17	1516.048	68.28162 - 134.24196	3d*(a'D)4p - 3d*(a'P)6s	² P° - ² P	2 - 2		835
	50	1516.215	70.63546 - 136.58935	$3d^{*}(a^{3}P)4p - 3d^{*}(a^{3}P)5d$	⁴D° – ⁴F	$\frac{2}{2} - \frac{1}{2}$		835
	1 20							
	3	1516.503	55.29965 - 121.24090	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{3}F_{3})5d$	² G° - ² F	$\frac{9}{2} - \frac{7}{2}$		835

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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	1 - 1	Notes	References
	40	1517.480	56.37141 - 122.27005	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})5d$	² G° - ² G	$\frac{7}{2} - \frac{7}{2}$		835
	100	1517,894	55.29965 - 121.18055	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F)5d$	${}^{2}G^{\circ} - {}^{2}H$	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		835
	15	1517 984	55 41783 - 121 29467	$3d^{8}(a^{3}E)4p = 3d^{8}(a^{3}E)5d$	${}^{4}F^{2} - {}^{2}G$	1_9		835
	40	1510 271	69 15657 122 07222	$3d^{7}4c^{2} = 3d^{7}(c^{2}E)/(c^{4}E)^{3}D^{\circ}$	4D o ⁴ D°	2 2 2		835
	40	1519.571	68.13037 - 133.97333	$30.45 - 30.(a \Gamma)454p(\Gamma)$		2^{-2}		035
	15	1519.513	55.41/83 - 121.22/80	$3d^{\circ}(a^{\circ}F)4p - 3d^{\circ}(a^{\circ}F_{3})5d$	$\mathbf{F} - \mathbf{F}$	$\frac{1}{2} - \frac{1}{2}$		835
	4	1519.745	68.15431 - 133.95485	3d^(a'D)4p - 3d*(a'D)5d	² D° – ² P	$\frac{1}{2} - \frac{1}{2}$		835
	100	1519.935	68.13121 - 133.92291	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{1}D)5d$	² F° − ² G	$\frac{7}{2} - \frac{9}{2}$		835
	2	1520.008		_			ļļ	835
	4	1520.077	68.28162 - 134.06776	$3d^{*}(a^{1}D)4p - 3d^{*}(a^{1}D)5d$	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{P}$	$\frac{1}{2} - \frac{3}{2}$		835
	14	1520 168	54 26263 - 120 04495	$3d^{8}(a^{3}E)4p = 3d^{8}(a^{3}E)5d$	4G° - 4G	2 9		835
	10	1520.100	32,40052 08,27670	3d(aT)+p = 3d(aT4)3d $3d^{8}(aC)Aa = 2d^{7}(a^{4}E)AaAm(^{3}D^{9})$	20 -20	2 2 9 9		935
	10	1520.294	32.49933 - 98.27670	30 (a G)4s - 30 (a F)4s4p(F)	479 411	2 2		833
	30	1520.392	55.41783 - 121.19034	$3d^{(a'F)4p} - 3d^{(a'F_3)5d}$	'F - 'H	$\frac{1}{2} - \frac{1}{2}$		835
	40	1520.467	56.37141 - 122.14071	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})5d$	² G° – ² H	$\frac{7}{2} - \frac{9}{2}$		835
	10	1520.932	67.69464 - 133.44389	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}P)6s$	${}^{2}F^{\circ} - {}^{4}P$	5-5		835
	20	1520.944	68 15431 - 133 90300	$3d^{8}(a^{\dagger}D)4p = 3d^{8}(a^{\dagger}D)5d$	${}^{2}D^{\circ} - {}^{2}D$	3-3		835
	100	1521 110	70 77812 136 51028	$3d^{8}(a^{3}D)Ap = 3d^{8}(a^{3}D)Sd$	4D° 4E	2 2		835
	16	1521.119	56 42440 122 14400	348(-37)(a + 1)(a + 1		2^{-2}_{3-5}		035
	15	1521.596	30.42449 - 122.14499	$3d^{2}(a^{2}F)4p = 3d^{2}(a^{2}F_{2})5d^{2}$	$\mathbf{F} = \mathbf{G}$	$\frac{1}{2} - \frac{1}{2}$		833
	18	1521.673	70.35894 – 136.07626	$3d'4s^2 - 3d'(a^2F)4s4p(^3P^3)$	²G – v²G°	$\frac{1}{2} - \frac{1}{2}$		835
	12	1521.889	68.15431 - 133.86221	3d ⁸ (a ¹ D)4p - 3d ⁸ (a ³ P)6s	${}^{2}D^{\circ} - {}^{2}P$	$\frac{3}{2} - \frac{3}{2}$		835
	10	1521.992	68.15431 - 133.85773	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}P)6s$	${}^{2}D^{\circ} - {}^{4}P$	3-1		835
	2	1522 506	53 63462 - 119 31544	$3d^{8}(a^{3}F)4n = 3d^{8}(a^{3}F_{3})6s$	${}^{4}D^{\circ} - {}^{2}F$	3 5		835
	ñ	1522.500	53 63462 119 31 544	$3d^{8}(a^{3}E)An = 3d^{8}(a^{3}E)An$	4D° 2E	2 2		925
	10	1522.517	53.03402 - 119.31344	$3u(a r) + p = 3u(a r_2) + os$	D - r	2 2 2		035
	30	1522.509	08.13121 - 133.80976	3d (a D)4p - 3d (a F ₄)8s	F - F	$\frac{5}{2} - \frac{5}{2}$	{	833
	10	1522.691	68.28162 - 133.95485	$3d^{(a'D)4p} - 3d^{(a'D)5d}$	'P' - 'P	2-2		835
	12	1522.846	52.20595 - 117.87278	3d ⁷ 4s ² - 3d ⁸ (a ¹ D)5p	${}^{4}F - {}^{2}D^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		835
	11	1522.990	56.42449 - 122.08479	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})5d$	⁴ F° – ⁴ F	$\frac{3}{2} - \frac{3}{2}$		835
	3	1523,102	56.42449 - 122.08025	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{1}G)4d$	${}^{4}F^{\circ} - {}^{2}F$	3 5		835
	6	1523 160	70.63546 - 136.28860	$3d^{8}(a^{3}P)4p = 3d^{8}(a^{3}P)5d$	⁴ D° – ⁴ D	\$_\$		835
	20	1523.100	67 89016 122 52800	$2d^{7}Ar^{2} = 2d^{7}(r^{2}\Sigma)ArArr(^{3}D^{0})$	$4\mathbf{D} = \mathbf{D}$	2 2 2		035
	50	1525.278	07.88010 - 133.32802	30 45° - 30 (a'F)454p('P')		$\frac{1}{2} - \frac{1}{2}$		833
	15	1523.897	/0./06// - 130.32/55	$3d^{(a'P)4p} - 3d^{(a'P)5d}$	'D' – 'D	2 - 2		835
	50	1524.302	68.13121 - 133.73498	3d ⁸ (a ¹ D)4p - 3d ⁸ (a ¹ D)5d	${}^{2}F^{\circ} - {}^{2}F$	$\frac{1}{2} - \frac{1}{2}$		835
	4	1524.758	70.70677 - 136.29083	3d ⁸ (a ³ P)4p - 3d ⁸ (a ³ P)5d	⁴ D° – ⁴ D	$\frac{3}{2} - \frac{1}{2}$		835
	22	1524.834	68.15431 - 133.73526	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{1}D)5d$	${}^{2}D^{\circ} - {}^{2}F$	3 - 5		835
	14	1524.996	68 96565 - 134 53937	$3d^{8}(a^{3}D)4n = 3d^{8}(a^{3}E)7d$	$^{2}P^{\circ} = ^{4}P$	3 5	1	835
	8	1525 422	5273845 - 11829417	$3d^{8}(a^{3}E)Ap = 3d^{8}(a^{3}E)Ac$	$4D^{\circ} - 2E$	\$_1 \$_1		835
	4	1526.480	70.77812 - 136.28860	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)5d$	⁴ D° - ⁴ D	$\frac{2}{2} - \frac{2}{2}$		835
		1.000 0000			1770 1 -			
	20	1526.999	54.55705 - 120.04495	3d°(a°F)4p - 3d°(a°F4)5d	⁺F~ – *G	$\frac{1}{2} - \frac{1}{2}$		835
	15	1527.497	51.04546 - 116.51206	3d'4s' - 3d'(a'D)4s4p('P')	*F - v⁴D°	$\frac{2}{2} - \frac{1}{2}$		835
	1	1527.661	68.15431 – 133.61399	3d ⁸ (a ¹ D)4p - 3d ⁸ (a ³ P)6s	²D° – ⁴P	$\frac{3}{2} - \frac{3}{2}$		835
	18	1527.968	68.70976 - 134.15628	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	⁴P – s⁴D°	$\frac{1}{2} - \frac{3}{2}$		835
	3	1528.158]		835
	22	1528.508	70.77812 - 136.20146	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)5d$	4D° - 4D	$\frac{1}{2} - \frac{1}{2}$		835
	1	1529 702	70 62546 126 05052	248(-3D)4- 248(-3E)9-	4D9 2E	5 5		975
	1	1520.703	70.03340 - 130.03033	JU (a F)4p - JO (a F2)8S	U - F			633
	4	1529.148	/0.63546 - 136.03143	$3d^{\circ}(a^{\circ}P)4p - 3d^{\circ}(a^{\circ}F_{3})7d$	*D* - 2D	2 - 2		835
	0	1529.812	52.20595 - 117.57368	$3d'4s^2 - 3d'(a^2D)4s4p(^3P^{\circ})$	⁴F - w⁴F°	$\frac{1}{2} - \frac{9}{2}$		835
	18	1530.080	54.55705 - 119.91333	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₄)5d	⁴ F° – ⁴F	$\frac{9}{2} - \frac{9}{2}$		835
	10	1530.428	53.03793 - 118.37911	$3d^{7}4s^{2} - 3d^{8}(a^{1}D)5p$	${}^{4}\mathbf{F} - {}^{2}\mathbf{F}^{\circ}$	5 - 5		835
	75	1530.636	54.55705 - 119.88947	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})5d$	⁴ F° – ⁴G	$\frac{9}{2} - \frac{11}{2}$		835
	30	1530 663	68 73598 - 134 06776	$3d^{8}(a^{1}D)4n = 3d^{8}(a^{1}D)5d$	² D° - ² P	5 3		835
	16	1530.005	60.73500 134.05205			2 2 2		0JJ 915
	10	1530.993	00./3370 - 134.03303	30 (a.D)4p - 30 (a.D)30	ע- ע	2 - 2	J	833
	3	1531.288	ł					835
	1	1531.336						835
	14	1531.408						835
	18	1531.640	68.15431 - 133.44389	3d ⁸ (a ¹ D)4p - 3d ⁸ (a ³ P)6s	²D° − ⁴P	$\frac{3}{2} - \frac{5}{2}$		835

NI II - Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	1	1531.720	70.35894 - 135.64510	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})6f$	² G – 3[5]°	$\frac{9}{2} - \frac{11}{2}$		835
	16	1531.952	54.55705 - 119.83300	3d ⁸ (a ³ F)4p – 3d ⁸ (a ³ F₄)5d	⁴F° – ⁴H	$\frac{9}{2} - \frac{11}{2}$		835
	20	1531.972	51.55785 - 116.83315	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})6s$	4 D° – 4 F	$\frac{7}{2} - \frac{9}{2}$		835
	14	1532.741	56.07526 - 121.31789	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	⁴F° – ⁴ G	$\frac{5}{2} - \frac{7}{2}$		835
	17	1533.669						835
	12	1533.885	68.73598 - 133.92988	3d ^s (a ¹ D)4p - 3d ^s (a ¹ D)5d	${}^{2}D^{\circ} - {}^{2}G$	$\frac{5}{2} - \frac{7}{2}$		835
	20	1533.991	57.08055 - 122.27005	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})5d$	${}^{2}F^{\circ} - {}^{2}G$	$\frac{1}{2} - \frac{1}{2}$		835
	5	1534.424						835
	12	1534 484						835
	11	1534.546	56.07526 - 121.24090	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	${}^{4}F^{\circ} - {}^{2}F$	$\frac{5}{2} - \frac{7}{2}$		835
	1	1534 628	50.07520 121.21070					835
	10	1534.861	56.07526 - 121.22780	3d*(a ³ F)4p - 3d*(a ³ F ₃)5d	${}^{4}\mathbf{F}^{\circ} - {}^{4}\mathbf{F}$	$\frac{5}{2} - \frac{5}{2}$		835
	2	1535 083						835
	12	1535.005	68 73598 - 133 86221	$3d^{(a^{1}D)4n} = 3d^{(a^{3}P)6s}$	${}^{2}D^{\circ} - {}^{2}P$	5_3		835
	12	1535.477	70 35894 - 135 46486	$3d^{7}4s^{2} - 3d^{8}(a^{3}P)4f$	$2^{2}G = 2^{2}G^{2}$	2 <u>7</u>		835
	30	1536.051	68 96565 - 134 06776	$3d^{8}(a^{1}D)4n = 3d^{8}(a^{1}D)5d$	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{P}$	3 3		835
	15	1536.118	54 55705 119 65625	$3d^{8}(a^{3}E)4p = 3d^{8}(a^{3}E)5d$	⁴ F° – ⁴ D	2 2		835
	13	1536.367	71.45774 - 136.54650	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{2})6f$	${}^{2}G - 2[4]^{\circ}$	$\frac{2}{7} - \frac{2}{7}$		835
		10001001			()			
	20	1536.398	68.96565 - 134.05305	$3d^{*}(a^{T}D)4p - 3d^{*}(a^{T}D)5d$	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{D}$	$\frac{2}{2} - \frac{2}{2}$		835
	15	1536.717	68.73598 - 133.80976	$3d^{\kappa}(a^{\dagger}D)4p - 3d^{\kappa}(a^{\dagger}F_{4})8s$	$^{2}D^{\circ} - {}^{4}F$	$\frac{2}{2} - \frac{1}{2}$		835
	25	1536.746	1.50694 - 66.57971	3d ⁹ – 3d ⁸ (a ³ P)4p	$g^2D - {}^4P^\circ$	$\frac{3}{2} - \frac{3}{2}$		835
	10	1536.779						835
	12	1536.944	1.50694 - 66.57134	3d° - 3d ⁸ (a ³ P)4p	$g^2D - {}^4P^\circ$	$\frac{3}{2} - \frac{5}{2}$		835
	12	1537.038	57.08055 - 122.14071	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{3}F_{2})5d$	${}^{2}\mathbf{F}^{\circ} - {}^{2}\mathbf{H}$	$\frac{7}{2} - \frac{9}{2}$		835
	20	1537.216	54.26263 - 119.31544	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6s$	${}^{4}G^{\circ} - {}^{2}F$	$\frac{1}{2} - \frac{5}{2}$		835
	2	1537.322	67.88016 - 132.92797	$3d^{7}4s^{2} - 3d^{8}(a^{1}D_{2})4f$	⁴ P − 2[2]°	$\frac{5}{2} - \frac{3}{2}$		835
	15	1537.477	70.35894 - 135.40067	$3d^{7}4s^{2} - 3d^{8}(a^{3}P_{2})4f$	${}^{2}G - 2[4]^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		835
	1	1537.776	72.98565 - 138.01453	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}F_{*})8d$	${}^{2}P^{\circ} - {}^{4}D$	$\frac{3}{2} - \frac{5}{2}$		835
	25	1537.859						835
	6	1538.022]		835
	30	1538 388						835
1	30	1538.483	68,73598 - 133,73498	$3d^{*}(a^{\dagger}D)4p - 3d^{*}(a^{\dagger}D)5d$	${}^{2}D^{\circ} - {}^{2}F$	$\frac{5}{2} - \frac{7}{2}$		835
	4	1538.567	71.77083 - 136.76649	$3d^{*}(a^{3}P)4p - 3d^{*}(a^{3}P)5d$	${}^{2}D^{\circ} - {}^{4}F$	3-3		835
	0	1538.722	68.96565 - 133.95485	$3d^{*}(a^{T}D)4p - 3d^{*}(a^{T}D)5d$	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{P}$	3-1		835
	3	1538 831	55.01871 - 120.00286	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{4})5d$	⁴ G° - ⁴ F	3-3		835
	1	1538.956	70.35894 - 135.33801	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})8p$	${}^{2}G - {}^{4}G^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		835
	15	1539 649						835
	10	1539.731	56.37141 - 121.31789	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	2 G° – ⁴G	$\frac{7}{2} - \frac{7}{2}$		835
	2	1539.949	68.96565 - 133.90300	$3d^{*}(a^{T}D)4p - 3d^{*}(a^{T}D)5d$	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{D}$	3-3		835
	ĩ	1540.015	53 03793 - 117 97247	$3d^{7}4s^{2} - 3d^{7}(a^{2}D)4s4p(^{3}P^{\circ})$	${}^{4}\mathbf{F} - \mathbf{w}^{4}\mathbf{F}^{\circ}$	\$ - 7		835
	25	1540 281	56 37141 - 121 29467	$3d^{*}(a^{3}F)4p = 3d^{*}(a^{3}F)5d$	${}^{2}G^{\circ} - {}^{2}G$	$\frac{1}{7} - \frac{1}{9}$		835
	1	1540.656	50.57141 - 121.29467	50 (0 1)+p = 50 (0 1)50	0 0	2 2		835
	25	1540 760	70 27540 127 27800	2d8(a ³ D)4p 2d8(a ³ D)5d	² D ⁹ - ² P	3 3		815
	35	1540.700	2.37342 - 137.27822 69.06565 133.96331	3d(a + p + p - 3d(a + p))da $3d^{8}(a + p)da$ $3d^{8}(a + p)da$	$2\mathbf{p}^{\circ}$ $2\mathbf{p}$	2 2		835
	4	1540.908	00.90303 - 133.80221	Ju (a D)+p - Ju (a r)05	1	2 - 2		835
	14	1541.324	69 73509 133 61300	3d8(a)D)4p = 3d8(a)B)6a	$^{2}D^{\circ} - ^{4}P$	5 3		835
	11	1541.530	66 27141 121 24000	$3d_{(a}^{3}E)/p = 3d_{(a}^{3}E_{(a)}Sd_{(a)}^{3}E_{(a)}$	$^{2}G^{\circ} - ^{2}F$	2 2		835
	4	1541.801	75.14948 - 140.00876	$3d^{8}(a^{1}G)4p - 3d^{8}(a^{1}G)6s$	2 H° – 2 G	$\frac{2}{9} - \frac{2}{7}$		835
		1.6.10.60.1			202 20	5 7		025
	1	1542.024	57.42016 - 122.27005	$3d^{(a+1)4p} = 3d^{(a+1)2p}$	40 - 0	2 - 2		835
	18	1542.208	53.60119 - 118.44281	30'4s" - 30"(a'D)5p	$\mathbf{F} - \mathbf{P}$	$\frac{1}{2} - \frac{1}{2}$		835
	2	1542.238	53.60119 - 118.44281	30'4s" - 30"(a'D)5p	P ~ 'P'	2 - 2		835
	3	1542.263		a.7.) a.w. !=	410 2004			835
	1	1542.388	53.03793 - 117.87278	3d'4s" - 3d°(a'D)5p	$F - D^{\circ}$	2 - 2		835
	3	1542.401	71.77083 - 136.60479	$3d^{\circ}(a^{\circ}P)4p - 3d^{\circ}(a^{\circ}F_{2})6g$	² D [•] - 2[4] [•]	2 - 2		835

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NI II - Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	References
	15	1542.773	71,77083 - 136,58935	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)5d$	² D° – ⁴ F	$\frac{5}{2} - \frac{7}{2}$		835
	1	1543 132	56 42449 - 121 22780	$3d^8(a^3F)4n = 3d^8(a^3F_1)5d$	4°F° - 4°F	1 1		835
	2	1543.806		54 (41) 10 54 (413)54		2 2		835
	2	1544.272	57 42016 122 17542	$3d^{8}(a^{3}E)An = 3d^{8}(a^{3}E)Sd$	2D° 2E	5 5		835
	5	1544.275	55 41793 120 14417	$3d(aT) + p = 3d(aT_2) + 3d^8(a^3E) + 3d^8($		2 2 2		835
	5	1544.908	53.41783 - 120.14417	$3d^{2}(a^{2}r)^{4}p = 3d^{2}(a^{2}r_{4})^{3}d$	$\mathbf{F} = \mathbf{D}$	2 - 2		033
	10	1544.980	53.03/93 - 117.76391	30°48° - 30°(a°D)5p	F - D	$\bar{2} - \bar{2}$		835
	30	1545.408	68.73598 - 133.44389	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}P)6s$	² D° – ⁴ P	5-5		835
	12	1545 453			_	1 ° °		835
	16	1545 717						835
	5	1545 881	52 20595 - 116 89398	$3d^{7}Ae^{2} - 3d^{7}(a^{2}D)AeAn(^{3}P^{\circ})$	${}^{4}\mathbf{F} = v^{4}\mathbf{D}^{9}$	1_1		835
	1	1546.053	53 63462 - 118 31482	$3d^{8}(a^{3}E)An = 3d^{8}(a^{3}E)An$	${}^{4}D^{\circ} - {}^{4}F$	3 5		835
		1546.070	53.63462 - 118.51482	$3d^8(a^3E)/m = 3d^8(a^3E)/m$	4D° 4E	2 2 2		925
	-	1340.070	55.05402 - 118.51482	50 (a 174p - 50 (a 13)0s	D - 1	2 - 2		055
	15	1547.337	55.41783 - 120.04495	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F₄)5d	⁴F° - ⁴G	$\frac{7}{2} - \frac{9}{2}$		835
	13	1547.407	53.03793 - 117.66211	$3d^{7}4s^{2} - 3d^{7}(a^{2}D)4s4p(^{3}P^{\circ})$	${}^{4}F - v^{4}D^{\circ}$	$\frac{5}{2} - \frac{3}{2}$		835
	5	1547.513						835
	3	1547.547	71.45774 - 136.07626	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}G - v^{2}G^{\circ}$	3-3		835
	16	1548 344	55.41783 - 120.00286	$3d^{8}(a^{3}F)4n - 3d^{8}(a^{3}F_{4})5d$	⁴ F° – ⁴ F	2 1		835
	7	1548.416	55.41765 - 120.00280	54 (41) (21) 54 (414) 54		2 2		835
	1	1549.588	55.29965 - 119.83300	3d8(a3F)4p - 3d8(a3F4)5d	² G° – ⁴ H	$\frac{9}{2} - \frac{11}{2}$		835
	0	1549.818	72.37542 - 136.89934	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)5d$	${}^{2}D^{\circ} - {}^{4}P$	$\frac{3}{2} - \frac{1}{2}$		835
	4	1549.964	71.77083 - 136.28860	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)5d$	${}^{2}D^{\circ} - {}^{4}D$	5-5		835
	3	1550,479	71.45774 - 135.95409	$3d^{7}4s^{2} - 3d^{8}(a^{3}P_{0})4f$	² G - 0[3]°	1-1		835
	2	1550.495	55.41783 - 119.91333	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})5d$	${}^{4}F^{\circ} - {}^{4}F$	1 - 2		835
	10	1550.912	68.96565 - 133.44389	3d ⁸ (a ¹ D)4p - 3d ⁸ (a ³ P)6s	$^{2}\mathbf{P}^{\circ}-^{4}\mathbf{P}$	$\frac{3}{2} - \frac{5}{2}$		835
	5	1552.276						835
	0	1553.012	72.37542 - 136.76649	3d*(a'P)4p - 3d*(a'P)5d	² D° – *F	$\frac{2}{2} - \frac{2}{2}$		835
	4	1553.346						835
	5	1554.108						835
	50	1554.124	67.88016 - 132.22515	$3d^{7}4s^{2} - 3d^{7}(a^{4}P)4s4p(^{1}P^{\circ})$	$^{4}P - v^{4}P^{\circ}$	$\frac{5}{2} - \frac{3}{2}$	1	835
	8	1554.293	70.77812 - 135.11672	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}F_{3})8s$	⁴ D° − ⁴ F	$\frac{7}{2} - \frac{5}{2}$		835
	8	1554 332	52 73845 - 117 07470	$3d^{8}(a^{3}E)An = 3d^{8}(a^{3}E)An$	4D° - 4F	5 1		835
	6	1554 509	66 57134 - 130 90065	$3d^{8}(a^{3}P)An = 3d^{8}(a^{1}P)Ac$		2 2 2		825
	2	1554.509	60.37134 - 130.90003	3u(ar)+p - 3u(aD) 0s	$\mathbf{F} = \mathbf{D}$	$\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$		833
	16	1555.002	52.20595 - 110.51200	30'45" - 30'(a*D)454p(*P')	$2\mathbf{p}^{\circ} - \mathbf{V}^{\circ}\mathbf{D}$	$\frac{5}{3} - \frac{5}{2}$		835
	10	1555.598	72.98303 - 137.27822	$3d^{2}(a^{2}P)4p = 3d^{2}(a^{2}P)3d^{2}$	$\mathbf{P} - \mathbf{P}$	2 - 2		833
	00	1555.490	71.43774 - 133.74000	$30'4s^2 - 30'(a^2F)4s4p(P')$		$\frac{1}{2} - \frac{1}{2}$		835
	•	1333.383	75.72168 - 140.00617	30 (a C)4p - 30 (a C)6s	-n - 0	2 - 2		633
	13	1555.957	51.55785 - 115.82712	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}P)4d$	4D° - 4F	$\frac{7}{2} - \frac{7}{2}$		835
	7	1556.350						835
	10	1556.766				ļ		835
	4	1556.997	72.98565 - 137.21193	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)5d$	$^{2}\mathbf{P}^{\circ} - ^{2}\mathbf{P}$	$\frac{3}{2} - \frac{1}{2}$		835
	1	1557.194	68.70976 - 132.92797	$3d^{7}4s^{2} - 3d^{8}(a^{1}D_{2})4f$	⁴ P – 2[2]°	1-3		835
	12	1557.290	57.08055 - 121.29467	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	${}^{2}\mathbf{F}^{\circ} - {}^{2}\mathbf{G}$	$\frac{1}{2} - \frac{1}{2}$		835
	1	1557.380						835
	10	1558.087	51.55785 - 115.73915	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ P)4d	⁴ D° – ⁴ F	$\frac{7}{2} - \frac{9}{2}$		835
	12	1558.443						835
	2	1558.501	51.04546 - 115.20985	$3d^{7}4s^{2} - 3d^{7}(a^{4}F)4s4p(^{1}P^{\circ})$	⁴ F - x ⁴ G°	$\frac{9}{2} - \frac{7}{2}$		835
	5	1558.544	53.60119 - 117.76391	$3d^{7}4s^{2} - 3d^{8}(a^{2}D)5p$	${}^{4}\mathbf{F} - {}^{2}\mathbf{D}^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		835
	15	1558.597	57.08055 - 121.24090	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	${}^{2}F^{\circ} - {}^{2}F$	$\frac{7}{2} - \frac{7}{2}$		835
	40	1660 666						0.25
	40	1558.055						835
	18	1559.159			2000 1	7 0		835
		1559.822	57.08055 - 121.19034	3d°(a°F)4p - 3d°(a°F3)5d	'F' - 'H	2 - 2		835
	0	1560.341	75.91763 - 140.00617	3d°(a'G)4p - 3d°(a'G)6s	"F" – "G	$\frac{2}{2} - \frac{2}{2}$		835
	25	1560.459			100 10	5.		835
	10	1560.517	55.01871 - 119.10006	$3d^{\circ}(a^{*}F)4p - 3d^{\circ}(a^{*}F_{2})6s$	"G" – "F	2 - 2		835

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NI II - Continued

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	Reference
	4	1560.562						835
	5	1560.796	52.20595 - 116.27581	$3d^{7}4s^{2} - 3d^{7}(a^{2}H)4s4p(^{3}P^{\circ})$	⁴F – w⁴G°	$\frac{1}{2} - \frac{1}{2}$		835
1	15	1560.831	68.15657 - 132.22515	$3d^{7}4s^{2} - 3d^{7}(a^{4}P)4s4p(^{1}P^{\circ})$	${}^{4}P - v^{4}P^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		835
	4	1560.935	25.03638 - 89.10049	$3d^{*}(a^{3}P)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{4}P - z^{6}D^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		835
	4	1561.015	53.60119 - 117.66211	$3d^{7}4s^{2} - 3d^{7}(a^{2}D)4s4p(^{3}P^{\circ})$	${}^{4}F - v^{4}D^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		835
	15	1561.229	54.26263 - 118.31482	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{3})6s$	⁴G° – ⁴F	$\frac{1}{2} - \frac{5}{2}$		835
	2	1561.733	54.26263 - 118.29417	3d*(a3F)4p - 3d*(a3F3)6s	⁴ G° – ² F	$\frac{7}{2} - \frac{7}{2}$		835
	11	1561.968	70.35894 - 134.38082	$3d^{7}4s^{2} - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	${}^{2}G - w^{2}G^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		835
	18	1562.329	70.63546 - 134.64209	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}F_{4})7d$	4D° - 4F	\$ - Ī		835
	7	1563.111	72.98565 - 136.96075	$3d^{*}(a^{3}P)4p - 3d^{*}(a^{3}P)5d$	${}^{2}P^{\circ} - {}^{4}P$	3 - 5		835
	50	1563.376	68.15657 - 132.12070	$3d^{7}4s^{2} - 3d^{7}(a^{4}P)4s4p(^{1}P^{\circ})$	⁴ P − v ⁴ P°	3-1		835
	120	1563.604	51.04546 - 115.00025	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{3}P^{\circ})$	${}^{4}F - w^{4}D^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		835
	1	1563.837						835
	15	1564.273	56.07526 - 120.00286	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{3}F_{4})5d$	⁺F° – ⁺F	$\frac{5}{2} - \frac{7}{2}$		835
	8	1564.389	70.35894 - 134.28166	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})6f$	² G – 4[5]°	$\frac{9}{2} - \frac{11}{2}$		835
	1	1565.001	55.41783 - 119.31544	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{3}F_{2})6s$	${}^{4}F^{\circ} - {}^{2}F$	$\frac{7}{2} - \frac{5}{2}$		835
	20	1565.399		· · · · ·				835
	3	1565.970		· ·				835
	7	1566.019	53.03793 - 116.89398	$3d^{7}4s^{2} - 3d^{7}(a^{2}D)4s4p(^{3}P^{\circ})$	${}^{4}F - v^{4}D^{\circ}$	$\frac{5}{2} - \frac{5}{2}$		835
	1	1566.890	57.42016 - 121.24090	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{3}F_{3})5d$	${}^{2}D^{\circ} - {}^{2}F$	$\frac{5}{2} - \frac{7}{2}$		835
	15	1567.069	51.04546 - 114.85888	$3d^{7}4s^{2} - 3d^{7}(a^{2}H)4s4p(^{3}P^{\circ})$	⁴F – w⁴G°	$\frac{9}{2} - \frac{11}{2}$		835
	10	1567.220	57.42016 - 121.22780	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{3}F_{3})5d$	² D° – ⁴F	$\frac{5}{2} - \frac{5}{2}$		835
	3	1567.298	71.45774 - 135.26199	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})8p$	<u>-</u> G - ⁴G°	$\frac{1}{2} - \frac{9}{2}$		835
	10	1567.323						835
	12	1567.336						835
	3	1567.370	71.45774 - 135.25892	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{1}P^{\circ})$	${}^{2}G - v^{2}D^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		835
	1	1567.872	72.98565 - 136.76649	$3d^{*}(a^{*}P)4p - 3d^{*}(a^{*}P)5d$	² P° – ⁴ F	$\frac{3}{2} - \frac{5}{2}$		835
	4	1567.966	58.49321 - 122.27005	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{3}F_{2})5d$	² F° – ² G	$\frac{5}{2} - \frac{7}{2}$	• •	835
	1	1568.698	72.98565 - 136.73274	3d [*] (a ³ P)4p - 3d [*] (a ³ P)5d	${}^{2}P^{\circ} - {}^{4}F$	$\frac{3}{2} - \frac{3}{2}$		835
	16	1569.172	66.57971 - 130.30697	$3d^{*}(a^{*}P)4p - 3d^{*}(a^{*}F_{*})5g$	⁴ P° - 3[2]°	$\frac{3}{2} - \frac{3}{2}$		835
	1	1569.415						835
	13	1569.624	53.36517 - 117.07470	$3d^{x}(a^{t}F)4p - 3d^{x}(a^{t}F_{4})6s$	⁴G° – ⁴F	$\frac{9}{2} - \frac{7}{2}$		835
	2	1569.972	57.42016 - 121.11559	$3d^{(a'F)}4p - 3d^{(a'F_3)}5d$	² D° - ² P	$\frac{5}{2} - \frac{3}{2}$		835
	10	1570.302	58.49321 - 122.17542	$3d^{s}(a^{t}F)4p - 3d^{s}(a^{t}F_{2})5d$	${}^{2}F^{\circ} - {}^{2}F$	3-3		835
	60	1570.392	68.15657 - 131.83494	$3d^{7}4s^{2} - 3d^{7}(a^{4}P)4s4p(^{1}P^{\circ})$	${}^{4}\mathbf{P} - \mathbf{v}{}^{4}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		835
	3	1570.512	56.37141 - 120.04495	$3d^{*}(a^{*}F)4p - 3d^{*}(a^{*}F_{4})5d$	² G° – ⁴ G	$\frac{7}{2} - \frac{9}{2}$		835
	1	1570.701	68.13121 - 131.79626	$3d^{x}(a^{1}D)4p - 3d^{x}(a^{3}F_{2})6d$	² F° – ² F	$\frac{1}{2} - \frac{5}{2}$		835
	1	1570.879		-		1		835
	12	1571.145						835
	12	1571.162						835
	10	1571.257						835
	2	1571.532	56.37141 - 120.00286	$3d^{*}(a^{*}F)4p - 3d^{*}(a^{*}F_{4})5d$	² G° - ⁴F	$\frac{1}{2} - \frac{1}{2}$		835
	2	1571.550	56.37141 - 120.00286	3d [×] (a ³ F)4p – 3d [×] (a ³ F₄)5d	² G° – ⁴F	$\frac{1}{2} - \frac{1}{2}$		835
	4	1572.018						835
	4	1572.062						835
	25	1572.540	58.49321 - 122.08479	$3d^{(a'F)4p} - 3d^{(a'F_2)5d}$	² F° – ⁴ F	$\frac{5}{2} - \frac{3}{2}$		835
	4	1572.646	58.49321 - 122.08025	3d*(a'F)4p - 3d*(a'G)4d	${}^{2}F^{\circ} - {}^{2}F$	$\frac{5}{2} - \frac{5}{2}$		835 835
	1	1314.793						000
	10	1573.071	E1 EE70E 11E 00134	2386-3534-2386-1038-		1 2 9		835
	18	1574.202	51.55785 - 115.08136	$30^{1}(a^{1}f')4p = 30^{1}(a^{1}G')3s$ $3474a^{2} = 2474a^{4}D(4a^{4}A^{1})b^{4}$	40 - 'G	$\frac{5}{1}$	1	033 975
4	100	1574.423	08./09/0 - 132.22515	$30'4s^2 - 30'(a^2P)4s4p('P')$	$\mathbf{r} - \mathbf{v}^{T}\mathbf{P}^{T}$	2 2		033
	20	15/4.942	/0.35894 - 133.85304	$30^{\circ}48^{\circ} - 30^{\circ}(a^{\circ}F)484p(^{\circ}P^{\circ})$	-U - V'F' 4D° 2D	1 1		833 878
	5	15/4.976	/0./48/0 - 134.24196	$3d^{\circ}(a^{\circ}P)4p = 3d^{\circ}(a^{\circ}P)6s$	D = P	2 - <u>2</u>		833
}	16	15/5.003	/0.35894 - 133.85083	30'4s' - 30'(a'F)4s4p('P')	"G – S'D'	$1 \overline{2} - \overline{2}$	ı	833

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NI II - Continued

Multiplet Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
15	1575.090						835
1	1575.559	58,70595 - 122,17542	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})5d$	${}^{2}D^{\circ} - {}^{2}F$	3-5		835
9	1575.597	53.36517 - 116.83315	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{4})6s$	⁴ G° – ⁴ F	2 - 9		835
1	1576 747		00 (11) (p 00 (114) 00	· ·	2 2		835
30	1577 015	68 70976 - 132 12070	$3d^{7}4s^{2} - 3d^{7}(a^{4}P)4s4p(^{1}P^{\circ})$	$4\mathbf{P} = \mathbf{v}^4\mathbf{P}^\circ$	1_1		835
16	1577 115	52 20595 115 61288	$3d^{7}4s^{2} - 3d^{7}(s^{2}H)AsAn(^{3}P^{\circ})$	$4\mathbf{F} = \mathbf{v}^{\dagger}\mathbf{G}^{\ast}$	$\frac{2}{2}$ $\frac{2}{9}$		935
10	15/7.115	52.20595 - 115.01288	$3d^{2}4s^{2} - 3d^{2}(a^{2}H)4s4p(^{2}P^{2})$	F-wG	2 - 2		835
7	1577.210						835
14	1577.933	58.70595 - 122.08025	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{1}G)4d$	${}^{2}D^{\circ} - {}^{2}F$	$\frac{3}{2} - \frac{5}{2}$		835
20	1578.865	53.49649 - 116.83315	3d ⁸ (a ³ F)4p – 3d ⁸ (a ³ F₄)6s	⁴ G° – ⁴ F	$\frac{11}{2} - \frac{9}{2}$		835
60	1578.990						835
18	1579.073						835
18	1579.563	73.90325 - 137.21193	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)5d$	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{P}$	$\frac{1}{2} - \frac{1}{2}$		835
17	1570 701						975
17	1579.791	55 010 21 110 21 402		100 15			835
2	1579.877	55.01871 - 118.31482	$3d^{\circ}(a^{\circ}F)4p - 3d^{\circ}(a^{\circ}F_{3})6s$	"G" - "F	1		835
3	1579.959	53.60119 - 116.89398	$3d'4s^2 - 3d'(a^2D)4s4p(^{\circ}P^{\circ})$	$F - v^4 D^\circ$	2-2		835
8	1580.588	70.63546 - 133.90300	$3d^{*}(a^{*}P)4p - 3d^{*}(a^{+}D)5d$	$^{4}D^{\circ} - ^{2}D$	$\frac{2}{2} - \frac{2}{2}$		835
1	1580.674						835
2	1580.698	66.57971 - 129.84233	$3d^{*}(a^{3}P)4p - 3d^{*}(a^{3}F_{4})6d$	${}^{4}P^{\circ} - {}^{4}D$	$\frac{3}{2} - \frac{5}{2}$		835
6	1581.085	67.69464 - 130.94236	$3d^{*}(a^{\dagger}D)4p = 3d^{*}(a^{\dagger}D)6s$	${}^{2}F^{\circ} - {}^{2}D$	5_3		835
25	1581 334	53 03793 - 116 27581	$3d^{7}Ae^{2} - 3d^{7}(a^{2}H)AeAn(^{3}P^{\circ})$	$\frac{1}{4}\mathbf{F} = \mathbf{w}^{4}\mathbf{G}^{2}$	2 <u>2</u> 2 <u>7</u>		825
10	1581 704	67 88016 121 10218	$3d^{7}4s^{2} - 3d^{8}(s^{3}E)$	4D 2(2)*	2 2		835
10	1501.004	67.88016 - 131.10318	$3d 4s^2 - 3d (a F_2) 5f$	P - 2[2]	2-2		835
0	1581.826	52./3845 - 115.956/1	$3d^{(a'F)}4p - 3d^{(a'P)}4d$	*D* - *F	2-2		835
2	1582.135	67.69464 - 130.90065	$3d^{\circ}(a'D)4p - 3d^{\circ}(a'D)6s$	F' - D	2 - 2		835
0	1582.373	70.70677 - 133.90300	3d^(a^P)4p - 3d^(a'D)5d	*D° - ² D	$\frac{3}{2} - \frac{3}{2}$		835
2	1582.571						835
10	1582.689				1		835
17	1583.051	70.35894 - 133.52802	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{2}G - v^{4}F^{\circ}$	3-3		835
1	1583.398	70.70677 - 133.86221	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)6s$	${}^{4}D^{\circ} - {}^{2}P$	3 - 3		835
10	1583.436	53.60119 - 116.75493	$3d^{7}4s^{2} - 3d^{7}(a^{2}H)4s4p(^{3}P^{\circ})$	${}^{4}F = W^{4}G^{\circ}$	1 1 1		835
15	1583.509	70.70677 - 133.85773	$3d^{*}(a^{3}P)4p - 3d^{*}(a^{3}P)6s$	⁴ D ° – ⁴ P	3-1		835
					1		
10	1584.530						835
16	1584.563	70.74870 - 133.85773	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)6s$	⁴ D° – ⁴ P	$\frac{1}{2} - \frac{1}{2}$		835
1	1584.761	68.13121 - 131.23283	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}F_{2})5g$	² F° – 2[4]°	$\frac{7}{2} - \frac{7}{2}$		835
200	1585.117	70.35894 - 133.44575	$3d^{7}4s^{2} - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	$^{2}G - w^{2}G^{\circ}$	$\frac{9}{2} - \frac{9}{2}$		835
4	1585.702	57.08055 - 120.14417	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{4})5d$	² F° – ⁴ D	$\frac{7}{2} - \frac{5}{2}$		835
4	1586.677	56.07526 - 119.10006	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6s$	⁴F° – ⁴ F	$\frac{5}{2} - \frac{3}{2}$		835
3	1587 138	51 04546 - 114 05204	$3d^{7}4s^{2} - 3d^{7}(s^{4}E)AsAn(^{1}P^{\circ})$	${}^{4}\mathbf{F} = \mathbf{x}^{4}\mathbf{F}^{\circ}$	2 1		925
8	1587 207	52,20595 - 115,20985	$3d^{7}4e^{2} - 3d^{7}(e^{4}E)AeAe(P^{0})$	4F - 400	2 2		835
19	1587 443	55 29965 - 118 20417	$\frac{3d^8(a^3F)An}{3d^8(a^3F)An} = \frac{3d^8(a^3F)An}{3d^8(a^3F)An}$	2G° 2E	$\frac{2}{9}$ $\frac{2}{7}$		935
18	1507.445	70 62546 122 61200	$3d(ar)^{4}p - 3d(ar)^{6}bs$	40° - 1	$\frac{1}{2} - \frac{1}{2}$		835
35	1587.845	70.03340 - 133.01399	$3d^{(a'P)4p} - 3d^{(a'P)6s}$	$^{1}D^{2} - ^{1}P$	2 - 2		835
15	1588.369	70.77812 - 133.73526	$3d^{*}(a^{*}F)^{4}p = 3d^{*}(a^{*}F_{4})^{3}d^{*}(a^{*}B)^{4}p = 3d^{*}(a^{*}D)^{5}d^{*}(a^{*}B)^{4}p = 3d^{*}(a^{*}D)^{5}d^{*}(a^{*}B)^{4}p = 3d^{*}(a^{*}B)^{5}d^{*}(a^{*}B)^{5}d^{*}(a^{*}B)^{4}p = 3d^{*}(a^{*}B)^{5}d^{*}(a^$	$^{4}D^{9} - ^{2}F$			835
		100110000			2-2		000
10	1588.464	68.15657 - 131.11019	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{2})5f$	⁴ P - 2[2]°	$\frac{3}{2} - \frac{3}{2}$		835
9	1588.715	56.37141 - 119.31544	3d*(a'F)4p - 3d*(a'F ₂)6s	${}^{2}G^{\circ} - {}^{2}F$	$\frac{1}{2} - \frac{5}{2}$		835
20	1588.798						835
40	1589.061	68.28162 - 131.21185	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}F_{2})5g$	² P° – 2[2]°	$\frac{1}{2} - \frac{3}{2}$		835
80	1589.116	74.28333 - 137.21193	3d*(a ³ P)4p - 3d*(a ³ P)5d	${}^{2}S^{\circ} - {}^{2}P$	$\frac{1}{2} - \frac{1}{2}$		835
200	1589.246	71.45774 - 134.38082	3d ⁷ 4s ² - 3d ⁷ (a ² G)4s4p(¹ P°)	$^{2}G - w^{2}G^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		835
5	1589.474	52 20595 - 115 12000	3d ² 4e ² - 3d ² (e ⁴ E)4e4r(1D ^e)	4E4E°	2 5		835
	1580 647	74 20002 127 21102	$3d^{+}75 = 3d^{-}(a^{+}\Gamma)^{+}754p(\Gamma^{+})$	F - X F	$\frac{1}{2} - \frac{1}{2}$		035
1	1507.54/	74.30093 - 137.21193	3d(a'')+p = 3d(a'') > 3d	5 - P	$\frac{1}{2} - \frac{1}{2}$		835
3	1589.503	/4.30093 - 13/.21193	3d"(a"P)4p - 3d"(a"P)5d	-S' - 'P	2 - 2		835
20	1589.644	/0./06// - 133.61399	3d"(a'P)4p - 3d"(a'P)6s	*D* - *P	2 - 2		835
80	1589.772	52.20595 - 115.10809	$3d'4s' - 3d'(a^2P)4s4p(^1P^*)$	'F - w⁴D°	2 - 2		835
8	1589.903	55.41783 - 118.31482	$3d^{*}(a^{*}F)4p - 3d^{*}(a^{*}F_{3})6s$	⁴ F° – ⁴F	$\frac{1}{2} - \frac{5}{2}$		835
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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	7	1589.948						835
	0	1590.422	55.41783 - 118.29417	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})6s$	${}^{4}F^{\circ} - {}^{2}F$	$\frac{1}{2} - \frac{1}{2}$		835
	10	1590.529						835
	1	1590.703	70.74870 - 133.61399	3d*(a'P)4p - 3d*(a'P)6s	⁴ D° – ⁴ P	$\frac{1}{2} - \frac{2}{2}$		835
	50	1591.041	13.55039 - 76.40203	3d*(a ³ F)4s - 3d*(a ¹ G)4p	${}^{2}F - {}^{2}F^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		835
	16	1591.099						835
	10	1591.350						835
	80	1591.415	71.45774 - 134.29499	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})6f$	² G – 4[3]°	$\frac{1}{2} - \frac{5}{2}$		835
	2	1591.732	58.49321 - 121.31789	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F)5d$	²F° – ⁴G	3-1		835
	200	1592 080	70 35894 - 133 16992	$3d^{7}4s^{2} - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	$^{2}G - w^{2}F^{\circ}$	2 - 1		835
	15	1592 144	70 63546 - 133 44389	$3d^{8}(a^{3}P)4n = 3d^{8}(a^{3}P)6s$	⁴ D° - ⁴ P	\$_ <u>\$</u>	ļ	835
	25	1592.248	71.45774 - 134.26207	$3d^74s^2 - 3d^8(a^3F_4)6f$	² G - 4[4]°	$\frac{1}{2} - \frac{1}{2}$		835
		1000 470	51 (555 (134) 5005		20 45278	7 7		016
	50	1592.479	/1.45//4 - 134.25285	$30'4s^2 - 30'(a^2F_4)0I$	-G-4[3]	$\frac{1}{2} - \frac{1}{2}$		833
	15	1592.502	52.20595 - 115.00025	$3d'4s^2 - 3d'(a^2P)4s4p(^3P^*)$	*F - w*D*	$\frac{1}{2} - \frac{1}{2}$		835
	1	1592.662	68.15431 - 130.94236	3d°(a'D)4p - 3d°(a'D)6s	$^{2}D^{\circ} - ^{2}D$	$\frac{2}{2} - \frac{2}{2}$		835
	1	1593.132	68.13121 - 130.90065	3d*(a'D)4p - 3d*(a'D)6s	2 F° - 2 D	$\frac{1}{2} - \frac{2}{2}$		835
	15	1593.200						835
	15	1593.522						835
	150	1593.611	71.45774 - 134.20830	$3d^{7}4s^{2} - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	${}^{2}G - w^{2}F^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		835
	40	1593.698	53.03793 - 115.78506	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{3}P^{2})$	${}^{4}\mathbf{F} - \mathbf{t}^{2}\mathbf{D}^{\circ}$	\$ _ 3		835
	1	1594 019	58 49321 - 121 22780	$3d^{8}(a^{3}F)4n - 3d^{8}(a^{3}F_{1})5d$	² F° – ⁴ F	\$_\$		835
	6	1504 297	57 42016 120 14417	$3d^{8}(a^{3}E)(n-3d^{8}(a^{3}E))5d$	2D° 4D	2 - 2 5 5	1	835
	25	1594.287	57.42016 - 120.14417	5u (a r)4p - 5u (a r4)5u	D - D	2 - 2		035
	35	1594.340	((57134 120 28450	148(-3D)A- 148(-3D)A4	4D° 4D	5 5		033
	1	1594.575	66.5/134 - 129.28450	30°(a°P)4p - 30°(a°F₄)60	°P - P	2 - 2		833
	12	1594.703	51.04546 - 113.75304	$3d^{7}4s^{2} - 3d^{7}(a^{4}F)4s4p(^{1}P^{\circ})$	⁴F – x⁴G°	$\frac{9}{2} - \frac{9}{2}$		835
	1	1595.332						835
	8	1595.519	56.42449 - 119.10006	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6s$	⁴ F ° − ⁴ F	$\frac{3}{2} - \frac{3}{2}$		835
	70	1595.608	74.28333 - 136.95528	$3d^{*}(a^{3}P)4p - 3d^{*}(a^{3}F_{2})7d$	${}^{2}S^{\circ} - {}^{2}P$	$\frac{1}{2} - \frac{1}{2}$		835
	70	1595.768	70.77812 - 133.44389	$3d^{*}(a^{3}P)4p - 3d^{*}(a^{3}P)6s$	⁴ D° – ⁴ P	$\frac{7}{2} - \frac{5}{2}$		835
	15	1595.919	74.30093 - 136.96075	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)5d$	⁴ S° – ⁴ P	$\frac{3}{2} - \frac{5}{2}$		835
	60	1596.074	74 30093 - 136 95528	$3d^8(a^3P)4n - 3d^8(a^3F_3)7d$	⁴ S° – ² P	3-1		835
	1	1596 874	58 49321 - 121 11559	$3d^{8}(a^{3}F)4p = 3d^{8}(a^{3}F)5d$	${}^{2}\mathbf{F}^{\circ} - {}^{2}\mathbf{P}$	2 2		835
	1	1597.031	74 28333 136 80034	$3d^{8}(a^{3}P)Ap = 3d^{8}(a^{3}P)Sd$	$^{2}S^{\circ} = ^{4}P$			835
	1	1597.031	74.28555 - 150.89954	50 (a 1)4p = 50 (a 1)50	5-1	2 - 2		835
	25	1597.101	74 30003 136 80034	2 48(- 3D) 4. 2 48(- 3D) 5 4	40° 40	3 3		035
	9	1597.484	74.30093 - 130.89934	$3d^{2}(a^{2}P)4p = 3d^{2}(a^{2}P)5d$	3 - P	$\frac{1}{2} - \frac{1}{2}$		835
	7	1597.886	57.42016 - 120.00286	3d"(a°F)4p – 3d"(a°F₄)5d	-D F	2-2		835
	40	1598.282	73.89373 - 136.46110	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{1}P^{\circ})$	$^{2}P - v^{2}D^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		835
	4	1598.315						835
	30	1598.371	71.77083 - 134.33446	$3d^{*}(a^{3}P)4p - 3d^{*}(a^{3}F_{+})6g$	² D° – 4[2]°	$\frac{2}{2} - \frac{3}{2}$		835
	18	1598.860						835
	40	1599.251						835
	12	1599.282	53.03793 - 115.56598	$3d^{7}4s^{2} - 3d^{7}(a^{4}F)4s4p(^{1}P^{\circ})$	⁴F – x⁴G°	$\frac{5}{2} - \frac{5}{2}$		835
	1	1599.439	58.70595 - 121.22780	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{3})5d$	² D° – ⁴F	$\frac{3}{2} - \frac{5}{2}$		835
	10	1599 549	54,55705 - 117,07470	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F)6s$	⁴ F° – ⁴ F	3 - 1		835
	25	1599 603	71 45774 - 133 97333	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}G - s^{4}D^{\circ}$	7 - 5		835
	10	1600 268	57 42016 - 119 90972	$3d^{8}(a^{3}F)4n = 3d^{8}(a^{3}F)5d$	${}^{2}D^{\circ} - {}^{4}P$	5 3		835
	18	1600.565	57.42010 115.50572	54 (41) 10 54 (414)54	5.	2 2		835
	3	1600.753	54.26263 - 116.73251	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ P)4d	⁴G° – ⁴P	$\frac{7}{2} - \frac{5}{2}$		835
		1 (0) 0 :		a 174 2 a 184 las 240	20 05 020	99		035
	16	1601.045	70.35894 - 132.81816	$3d'4s^2 - 3d'(a'D_2)4f$	'G – 2[4]°	$\frac{2}{2} - \frac{2}{2}$		835
	10	1601.240	67.88016 - 130.33178	$3d'4s^2 - 3d'(a^*P)4s4p('P^*)$	$\mathbf{P} - \mathbf{t}^* \mathbf{D}^*$	$\frac{1}{2} - \frac{2}{2}$		835
	8	1601.288	74.28333 - 136.73274	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)5d$	<u></u> 'S° - 'F	$\frac{1}{2} - \frac{2}{2}$		835
	3	1601.400				_		835
	1	1601.518	9.33004 - 71.77083	3d ⁸ (a ³ F)4s - 3d ⁸ (a ³ P)4p	${}^{4}F - {}^{2}D^{\circ}$	$\frac{1}{2} - \frac{5}{2}$		835
		,						
	4	1601.742	74.30093 - 136.73274	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)5d$	⁴ S° − ⁴ F	$\frac{3}{2} - \frac{3}{2}$		835

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Multiplet	Rei. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	10	1601.928	74.30093 - 136.72533	3d ⁸ (a ³ P)4p - 3d ⁸ (a ³ P)5d	⁴ S° – ⁴ P	$\frac{3}{2} - \frac{1}{2}$		835
	12	1602.209	68.15657 - 130.57042	$3d^{7}4s^{2} - 3d^{7}(a^{4}P)4s4p(^{1}P^{\circ})$	$^{4}P - t^{4}D^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		835
	1	1602.679	71.45774 - 133.85304	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{2}G - v^{4}F^{\circ}$	2 - 2		835
	20	1602.973	8.39390 - 70.77812	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{3}P)4p$	⁴ F ~ ⁴ D°	2 - 1		835
	1	1603 224	53 36517 - 115 73915	$3d^8(a^3F)4n = 3d^8(a^3P)4d$	4C° - 4F	2 2		835
	20	1603.410	13 55039 - 75 91763	$3d^8(a^3F)Ac = 3d^8(a^1G)Ac$	$2\mathbf{F}$, $2\mathbf{F}^{\circ}$	2^{-2}		825
	20	1003.410	15.55039 - 75.91705	50 (a 17)45 - 50 (a 074p	F ~ F	2 - 2		835
	25	1603.555				1		835
	16	1603.728	68.70976 - 131.06385	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{2})5f$	⁴ P – 2[1]°	$\frac{1}{2} - \frac{1}{2}$		835
	5	1603.917	52.73845 - 115.08536	3d ⁸ (a ³ F)4p - 3d ⁸ (a ¹ G)5s	$^{4}D^{\circ} - ^{2}G$	$\frac{2}{2} - \frac{1}{2}$		835
	2	1604.394	67.88016 - 130.20889	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})5f$	⁴ P − 3[3]°	$\frac{5}{2} - \frac{7}{2}$		835
	18	1604.482						835
	5	1604.570	53.63462 - 115.95671	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ P)4d	${}^{4}D^{\circ} - {}^{4}F$	$\frac{3}{2} - \frac{5}{2}$		835
	3	1604 696	67 88016 - 130 19723	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{2})5f$	4P - 3[2]°	5_3		835
	0	1605.027	67.88016 - 130.19725	$3d^{7}4s^{2} - 3d^{8}(s^{3}E) > 5f$	4D 2[2]	$\frac{2}{5}$ $\frac{2}{5}$		035
		1605.027	07.88010 - 130.18439	$30.48^{\circ} - 30.(a \Gamma_3)31$	P = 3[2]	$\frac{1}{2} - \frac{1}{2}$		835
	4	1605.217	/1.//083 - 134.06//6	$3d^{(a'P)4p} - 3d^{(a'D)5d}$	$^{2}D^{2} - ^{2}P$	$\frac{2}{2} - \frac{2}{2}$		835
	35	1605.744	51.04546 - 113.32195	$3d'4s^2 - 3d'(a^2F)4s4p('P^2)$	*F - x*F*	$\frac{1}{2} - \frac{1}{2}$		835
	3	1605.795						835
	60	1605.910						835
	12	1606.280						835
	30	1606 469						835
	0	1606 605	56 07526 119 31492	$2d^{8}(a^{3}E)(a) = 2d^{8}(a^{3}E)(a)$	400 40	5 5		935
	15	1606.093	50.07520 - 118.51482	5u (a F)4p - 5u (a F3)6s	Г - Г	2 - 2		835
	15	1606.729						835
	18	1606.902						835
	1	1607.477						835
	20	1607.849						835
	3	1607.987	68.13121 - 130.32094	$3d^{8}(a^{1}D)4p - 3d^{8}(a^{3}F_{3})5g$	${}^{2}F^{\circ} - 3[4]^{\circ}$	$\frac{7}{2} - \frac{7}{2}$		835
	60	1608.134	53.60119 - 115.78506	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{3}P^{\circ})$	${}^{4}\mathbf{F} - \mathbf{t}^{2}\mathbf{D}^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		835
	80	1608.177	32,52354 - 94,70593	$3d^{8}(a^{1}G)4s - 3d^{7}(a^{4}F)4s4p(^{3}P^{\circ})$	${}^{2}\mathbf{G} - \mathbf{z}^{4}\mathbf{F}^{9}$	1 1	ł	835
	4	1608 244				2 2		835
	30	1608.358	68.15657 - 130.33178	$3d^{7}4s^{2} - 3d^{7}(a^{4}P)4s4p(^{1}P^{\circ})$	${}^{4}\mathbf{P} - t^{4}\mathbf{D}^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		835
	25	1609 442	52 02702 115 20005		45 400	5 7		0.0.5
	25	1608.442	53.03793 - 115.20985	$3d^{4}s^{2} - 3d^{2}(a^{4}F)4s4p(^{4}P^{2})$	$^{*}F - x^{*}G^{*}$	2 - 2		835
	1	1608.708	76.40203 - 138.56371	$3d^{(a'G)4p} - 3d^{(a'F_3)9s}$	${}^{2}\mathbf{F}^{\circ} - {}^{2}\mathbf{F}$	2 - 2		835
	1	1609.343	52.73845 - 114.87488	$3d^{*}(a^{*}F)4p - 3d^{*}(a^{*}P)4d$	⁴D° – ⁴D	$\frac{2}{2} - \frac{2}{2}$		835
	12	1609.474	71.77083 - 133.90300	$3d^{*}(a^{*}P)4p - 3d^{*}(a^{+}D)5d$	$^{2}D^{\circ} - ^{2}D$	$\frac{2}{2} - \frac{3}{2}$		835
	20	1610.102	67.88016 - 129.98805	$3d^{7}4s^{2} - 3d^{7}(a^{4}P)4s4p(^{1}P^{\circ})$	$^{4}P - t^{4}D^{\circ}$	$\frac{5}{2} - \frac{5}{2}$		835
	18	1610.532	71.77083 - 133.86221	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)6s$	$^{2}D^{\circ} - ^{2}P$	$\frac{5}{2} - \frac{3}{2}$		835
	8	1611.061	68.15657 - 130.22752	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})5f$	⁴ P - 3[3]°	$\frac{3}{2} - \frac{5}{2}$		835
	6	1611.079	53.03793 - 115.10809	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{1}P^{\circ})$	${}^{4}\mathbf{F} - \mathbf{w}^{4}\mathbf{D}^{\circ}$	3-3		835
	2	1611.238						835
	25	1611.390						835
	2	1611 927						835
	ĩ	1612.163	68.15657 - 130.18439	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})5f$	⁴ P - 3[2]°	$\frac{3}{2} - \frac{5}{2}$		835
						, .		
	20	1612.450	68.15657 - 130.17403	$3d'4s^2 - 3d^8(a^3F_3)5f$	*P - 3[1]°	$\frac{2}{2} - \frac{3}{2}$		835
	2	1613.132	53.60119 - 115.59225	$3d^{7}4s^{2} - 3d^{7}(a^{4}F)4s4p(^{1}P^{\circ})$	${}^{4}F - x^{4}F^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		835
	60	1613.216	71.45774 – 133.44575	$3d^{7}4s^{2} - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	$^{2}G - w^{2}G^{\circ}$	$\frac{7}{2} - \frac{9}{2}$		835
	20	1613.820	53.60119 - 115.56598	$3d^{7}4s^{2} - 3d^{7}(a^{4}F)4s4p(^{1}P^{\circ})$	${}^{4}F - x^{4}G^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		835
	1	1613.949						835
	2	1614.218						835
	10	1614 495						025
	20	1614 924						833
	30	1614.824	6()7141		200 10	7 7		835
	90	1614.911	56.3/141 - 118.29417	$3d^{\circ}(a^{\circ}F)4p - 3d^{\circ}(a^{\circ}F_{3})6s$	'G' - 'F	2 - 2		835
	120	1615.459	67.88016 - 129.78207	3d'4s' - 3d'(a*P)4s4p('P°)	*P - t*D*	$\frac{2}{2} - \frac{1}{2}$		835
	9	1615.704						835
	15	1616.387	72.37542 - 134.24196	3d ⁸ (a ³ P)4p - 3d ⁸ (a ³ P)6s	$^{2}\mathbf{D}^{\circ} - ^{2}\mathbf{P}$	$\frac{3}{2} - \frac{1}{2}$		835
	1	1	1	I	1		1	

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NI II - Continued

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	Reference
	2	1616.456						835
	25	1616.536	68.70976 - 130.57042	$3d^{7}4s^{2} - 3d^{7}(a^{4}P)4s4p(^{1}P^{\circ})$	${}^{4}P - t{}^{4}D^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		835
	25	1616.917	52.20595 - 114.05204	$3d^{7}4s^{2} - 3d^{7}(a^{4}F)4s4p(^{1}P^{\circ})$	${}^{4}F - x^{4}F^{\circ}$	$\frac{1}{2} - \frac{7}{2}$		835
	2	1616.993	71.77083 - 133.61399	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)6s$	² D° – ⁴ P	$\frac{5}{2} - \frac{3}{2}$		835
	50	1617.088						835
	40	1617.144						835
	40	1617.299	53.03793 - 114.86935	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{3}P^{\circ})$	${}^{4}F - w^{4}D^{\circ}$	$\frac{5}{2} - \frac{3}{2}$		835
	20	1618.950	76.72736 - 138.49584	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{1}P^{\circ})$	${}^{2}\mathbf{H} - \mathbf{w}^{2}\mathbf{G}^{\circ}$	$\frac{11}{2} - \frac{9}{2}$		835
	1	1619.193	73.89373 - 135.65293	$3d^{7}4s^{2} - 3d^{8}(a^{3}P_{2})4f$	² P – 2[1]°	$\frac{3}{2} + \frac{3}{2}$		835
	6	1619.395	71.45774 - 133.20930	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{2}G - v^{4}F^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		835
	7	1619.607						835
	20	1619.857						835
	6	1619.964	73.89373 - 135.62359	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})6f$	² P - 3[2]°	$\frac{3}{2} - \frac{3}{2}$		835
	5	1619.989	-					835
	18	1620.331	53.36517 - 115.08136	$3d^{s}(a^{3}F)4p - 3d^{s}(a^{1}G)5s$	⁴ G° ² G	$\frac{9}{2} - \frac{9}{2}$		835
	1	1620.428	71.45774 - 133.16992	$3d^{7}4s^{2} - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	${}^{2}G - w^{2}F^{\circ}$	3 - 3		835
	3	1620.842						835
	1	1620.946	72.37542 - 134.06776	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{1}D)5d$	${}^{2}\mathbf{D}^{\circ} - {}^{2}\mathbf{P}$	$\frac{3}{2} - \frac{3}{2}$		835
	40	1621.460	71.77083 - 133.44389	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)6s$	² D° - ⁴P	5-5		835
	6	1621 880	55,41783 - 117,07470	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{1})6s$	⁴ F° − ⁴ F	<u>1</u> - <u>1</u>		835
	18	1621.926	10.11566 - 71.77083	$3d^{*}(a^{*}F)4s - 3d^{*}(a^{*}P)4p$	${}^{4}F - {}^{2}D^{\circ}$	5-5		835
	80	1622,106						835
	2	1622.164						835
	20	1622.796	68.70976 - 130.33178	$3d^{7}4s^{2} - 3d^{7}(a^{4}P)4s4p(^{1}P^{\circ})$	${}^{4}\mathbf{P} - t^{4}\mathbf{D}^{\circ}$	$\frac{1}{2} - \frac{3}{2}$		835
	1	1622.923						835
	1	1622.981	51,55785 - 113,17296	$3d^{(a)}F)4p - 3d^{(a)}D)4d$	⁴ D° - ² G	$\frac{7}{2} - \frac{9}{2}$		835
	60	1624 084	71.45774 - 133.03100	$3d^{7}4s^{2} - 3d^{8}(a^{1}D_{2})4f$	${}^{2}G - 2[5]^{\circ}$	Ž - 2		835
	20	1624,172	70.35894 - 131.92877	$3d^{2}4s^{2} - 3d^{8}(a^{3}F_{1})7p$	² G - ² G°	$\frac{3}{2} - \frac{3}{2}$		835
	0	1624.435						835
	16	1624.773	52.20595 - 113.75304	$3d^{2}4s^{2} - 3d^{2}(a^{4}F)4s4p(^{1}P^{\circ})$	⁴ F − x ⁴ G°	$\frac{7}{2} - \frac{9}{2}$		835
	25	1625.233						835
	2	1625.288	72.37542 - 133.90300	$3d^{s}(a^{3}P)4p - 3d^{s}(a^{1}D)5d$	${}^{2}D^{\circ} - {}^{2}D$	$\frac{3}{2} - \frac{3}{2}$		835
	12	1626.161						835
	20	1626.309	73.89373 - 135.38253	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{1}P^{\circ})$	$^{2}\mathbf{P} - \mathbf{w}^{2}\mathbf{P}^{\circ}$	3-3		835
	15	1626.320	73.89373 - 135.38253	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{1}P^{\circ})$	$^{2}\mathbf{P} - \mathbf{w}^{2}\mathbf{P}^{\circ}$	3-3		835
	6	1626.366	72.37542 - 133.86221	3d [*] (a'P)4p - 3d [*] (a'P)6s	${}^{2}\mathbf{D}^{\circ} - {}^{2}\mathbf{P}$	$\frac{3}{2} - \frac{3}{2}$		835
	12	1626.961	68.70976 - 130.17403	$3d^{7}4s^{2} - 3d^{*}(a^{3}F_{3})5f$	⁴P - 3[1]°	<u>+</u> _+		835
	12	1627.396	9.33004 - 70.77812	$3d^{s}(a^{3}F)4s - 3d^{s}(a^{3}P)4p$	⁴ F - ⁴ D°	$\frac{1}{2} - \frac{1}{2}$		835
	4	1627.656	58.70595 - 120.14417	$3d^{*}(a^{3}F)4p - 3d^{*}(a^{3}F_{4})5d$	${}^{2}D^{\circ} - {}^{4}D$	$\frac{1}{2} - \frac{5}{2}$		835
	15	1628.126	66.57134 - 127.99156	$3d^{s}(a^{t}P)4p - 3d^{s}(a^{t}F_{4})7s$	⁴ P° – ⁴ F	$\frac{5}{2} - \frac{7}{2}$		835
	10	1628.497	14.99557 - 76.40203	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{3}G)4p$	${}^{2}F - {}^{2}F^{\circ}$	2 - 2		835
	15	1628.726						835
	20	1628.810	76.72736 - 138.12188	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})9p$	${}^{2}H - {}^{4}F^{\circ}$	$\frac{11}{2} - \frac{9}{2}$		835
	100	1629.282	51.04546 - 112.42219	$3d^{7}4s^{2} - 3d^{7}(a^{4}F)4s4p(^{1}P^{\circ})$	¹F – x⁴G°	2 - 11 2 - 2		835
	11	1629.445						835
	70	1629.591	73.89373 - 135.25892	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{1}P^{\circ})$	$^{2}\mathbf{P} - \mathbf{v}^{2}\mathbf{D}^{\circ}$	$\frac{1}{2} - \frac{5}{2}$		835
	1	1629.718	71.45774 - 132.81816	$3d^{7}4s^{2} - 3d^{*}(a^{1}D_{2})4f$	² G – 2[4]°	$\frac{7}{2} - \frac{9}{2}$		835
	20	1630.130						835
	10	1630.356	53.63462 - 114.97019	3d*(a3F)4p - 3d*(a3P)4d	⁴ D° – ⁴ D	$\frac{3}{2} - \frac{1}{2}$		835
	25	1631.024						835
	12	1631.182	9.33004 - 70.63546	$3d^{s}(a^{3}F)4s - 3d^{s}(a^{3}P)4p$	⁴F - ⁴D°	$\frac{7}{2} - \frac{5}{2}$		835
	15	1632.152	53.60119 - 114.86935	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{3}P^{\circ})$	⁴ F − w ⁴ D [•]	$\frac{1}{2} - \frac{1}{2}$		835
	1 13							
	30	1632.171	53.60119 - 114.86935	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{3}P^{\circ})$	⁴ F - w ⁴ D [•]	$\frac{3}{2} - \frac{3}{2}$		835

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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	6	1632.488	72.98565 - 134.24196	3d ⁸ (a ³ P)4p - 3d ⁸ (a ³ P)6s	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{P}$	$\frac{3}{2} - \frac{1}{2}$		835
	2	1632.960	72.37542 - 133.61399	3d8(a3P)4p - 3d8(a3P)6s	${}^{2}D^{\circ} - {}^{4}P$	$\frac{3}{2} - \frac{3}{2}$		835
	4	1633.189						835
	10	1633.625	57.08055 - 118.29417	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ F ₃)6s	${}^{2}\mathbf{F}^{\circ} - {}^{2}\mathbf{F}$	$\frac{1}{2} - \frac{1}{2}$		835
	35	1633.988			<u> </u>			835
	30	1635.070	73.89373 – 135.05314	3d'4s² - 3d'(a²P)4s4p('P°)	$^{2}\mathbf{P} - \mathbf{w}^{2}\mathbf{P}^{*}$	$\frac{1}{2} - \frac{1}{2}$		835
	100	1635.340	55.01871 - 116.16776	3d ⁸ (a ³ F)4p - 3d ⁸ (a ³ P)4d	⁴G° – ⁴F	$\frac{5}{2} - \frac{3}{2}$		835
	1	1636.068						835
	4	1636.231	52.20595 - 113.32195	3d ⁷ 4s ² - 3d ⁷ (a ⁴ F)4s4p('P°)	⁴ F − x ⁴ F°	$\frac{7}{2} - \frac{9}{2}$		835
	3	1636.488	10.66389 - 71.77083	3d ⁸ (a ³ F)4s - 3d ⁸ (a ³ P)4p	${}^{4}F - {}^{2}D^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		835
	20	1637.072						835
	2	1637.140	72.98565 - 134.06776	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{1}D)5d$	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{P}$	<u>1</u> - 1		835
	10	1637.267						835
	100	1637.439	73.89373 - 134.96478	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}\mathbf{P} - \mathbf{w}^{2}\mathbf{D}^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		835
	20	1637.509	72.37542 - 133.44389	3d ⁸ (a ³ P)4p - 3d ⁸ (a ³ P)6s	² D° – ⁴ P	3-3		835
	300	1637.589	70.35894 - 131.42432	$3d^{7}4s^{2} - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	2 G – x ² H °	⁹ / ₂ - ¹¹ / ₂		835
	4	1638.963	53.03793 - 114.05204	3d ⁷ 4s ² - 3d ⁷ (a ⁴ F)4s4p(¹ P ^o)	${}^{4}\mathbf{F} - \mathbf{x}^{4}\mathbf{F}^{\circ}$	\$ - 7		835
	8	1639.987						835
	7	1640.769	67.88016 - 128.82715	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{1})5f$	⁴ P – 4[3]°	\$_1		835
	10	1641.418	67.88016 - 128.80323	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})5f$	${}^{4}P - 4[2]^{\circ}$	\$_\$		835
	20	1642.299						835
	40	1642.324	73.89373 - 134.78314	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}\mathbf{P} - \mathbf{w}^{2}\mathbf{D}^{\circ}$	3-5		835
	15	1642.351						835
	5	1642.670	72.98565 - 133.86221	3d*(a ³ P)4p - 3d*(a ³ P)6s	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{P}$	$\frac{3}{2} - \frac{3}{2}$		835
	2	1642.739	57.42016 - 118.29417	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F)6s$	${}^{2}D^{\circ} - {}^{2}F$	3-1		835
	2	1642.792	70.74870 - 131.62045	$3d^{(a^{3}P)4p} - 3d^{(a^{3}F)6d}$	4 D° - 4F	1 - 1		835
	80	1643.271	71.45774 - 132.31198	$3d^{7}4s^{2} - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	${}^{2}\mathbf{G} - \mathbf{x}^{2}\mathbf{H}^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		835
	20	1643.334	67.88016 - 128.73203	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})5f$	⁴ P − 4[1]°	2 - 3		835
	14	1644.040						835
	6	1644.137	58.49321 - 119.31544	3d8(a3F)4p - 3d8(a3F2)6s	${}^{2}F^{\circ} - {}^{2}F$	\$ - 2		835
	o	1645.654	54.17626 - 114.94242	3d [*] (a ³ F)4p - 3d [*] (a ³ P)4d	4 D° – 4 D	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		835
	10	1647.637						835
	3	1648.353						835
	1	1648.381	68.15657 - 128.82223	3d ⁷ 4s ² - 3d ⁸ (a ³ F ₄)5f	⁴ P − 4[2]°	$\frac{3}{2} - \frac{3}{2}$		835
	13	1649.396	72.98565 - 133.61399	3d ⁸ (a ³ P)4p - 3d ⁸ (a ³ P)6s	² P ° – ⁴ P	$\frac{3}{2} - \frac{3}{2}$		835
	3	1649.905	58.70595 - 119.31544	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{3}F_{2})6s$	${}^{2}D^{\circ} - {}^{2}F$	$\frac{3}{2} - \frac{5}{2}$		835
	14	1650.412	10.11566 - 70.70677	3d ⁸ (a ³ F)4s - 3d ⁸ (a ³ P)4p	⁴ F - ⁴ D°	$\frac{5}{2} - \frac{3}{2}$		835
	4	1650.636						835
	10	1650.835	68.15657 - 128.73203	3d ⁷ 4s ² - 3d ⁸ (a ³ F ₄)5f	⁴ P − 4{1]°	$\frac{3}{2} - \frac{3}{2}$		835
	13	1652.270						835
	3	1652.355	10.11566 - 70.63546	3d*(a3F)4s - 3d*(a3P)4p	⁴ F − ⁴ D°	$\frac{5}{2} - \frac{5}{2}$	1	835
	3	1652.477						835
	10	1652.726						835
	15	1652.839						835
	18	1653.369				1		835
	10	1653.687	71.45774 - 131.92877	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})7p$	${}^{2}G - {}^{2}G^{\circ}$	$\frac{7}{2} - \frac{9}{7}$		835
	10	1653.779						835
	1	1654.667						835
	1	1655.749						835
	0	1655.903	73.89373 - 134.28376	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}P - s^{4}D^{\circ}$	$\frac{3}{2} - \frac{1}{2}$	1	835
	3	1656.840	73.89373 - 134.24972	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})6f$	${}^{2}P - 4[1]^{\circ}$	$\frac{1}{3} - \frac{1}{3}$		835
	2	1657.273				· '		835
	10	1657.313	73.90325 - 134.24196	3d*(a3P)4p - 3d*(a3P)6s	$^{2}P^{\circ} - ^{2}P$	$\frac{1}{2} - \frac{1}{2}$		835
	20	1661.018	77.33247 - 137.53596	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})7f$	² D - 4[4]°	$\frac{5}{2} - \frac{7}{2}$		835
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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	3	1662.063				1		835
	20	1662.423						835
	25	1662.892						835
	16	1663.563	70.35894 - 130.47090	$3d^{2}4s^{2} - 3d^{6}(a^{3}F_{4})7p$	4G - *F*	$\frac{1}{2} - \frac{1}{2}$		835
	10	1664.316	10.66389 - 70.74870	$3d^{\circ}(a^{3}F)4s - 3d^{\circ}(a^{3}P)4p$	$^{\circ}F - ^{\circ}D^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		835
	2	1664.384	79.92388 - 140.00617	3d°(a'G)4p - 3d°(a'G)6s	-GG	2 - 2		835
	8	1664.459	73.89373 - 133.97333	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}P - s^{4}D^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		835
	4	1665.477	10.66389 - 70.70677	3d°(a'F)4s – 3d°(a'P)4p	•F - •D•	$\frac{1}{2} - \frac{1}{2}$		835
	1	1005.800	(8 7007(128 72202	2474-2 2484-372 166	400 40130	1 3		832
	0	1666 828	57 08055 117 07470	$3d^{8}(a^{3}E)Ap = 3d^{8}(a^{3}E)Ac$	2E°_4E	2^{-2}_{1}		835
	4	1667 930	73 90325 - 133 85773	$3d^{8}(a^{3}P)An = 3d^{8}(a^{3}P)6s$	² P° _ ⁴ P	2 - 2 1 - 1		835
	•	1007.550	13.90323 - 133.03773	50 (a 1)+p - 50 (a 1)65		2 - 2		030
	1	1668.122	52.73845 - 112.68630	3d ⁸ (a ³ F)4p - 3d ⁸ (a ¹ D)4d	⁴D° – ² F	$\frac{5}{2} - \frac{5}{2}$		835
	7	1670.935	70.35894 – 130.20562	3d ⁷ 4s ² - 3d ⁸ (a ³ F ₃)5f	² G – 3[5]°	$\frac{9}{2} - \frac{11}{2}$		835
	12	1671.514	77.73679 - 137.56274	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{2})8p$	$^{2}H - ^{2}G^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		835
	10	1674.000	8.39390 - 68.13121	3d ⁸ (a ³ F)4s - 3d ⁸ (a ¹ D)4p	$^{4}F - ^{2}F^{\circ}$	$\frac{9}{2} - \frac{1}{2}$		835
	3	1676.317	57.42016 - 117.07470	3d8(a3F)4p - 3d8(a3F4)6s	² D° – ° F	$\frac{3}{2} - \frac{1}{2}$		835
	2	1676.671						835
	1	1677.297	74.28333 - 133.90300	3d ⁸ (a ³ P)4p - 3d ⁸ (a ¹ D)5d	${}^{2}S^{\circ} - {}^{2}D$	$\frac{1}{2} - \frac{3}{2}$		835
	5	1678.447	74.28333 - 133.86221	3d ⁸ (a ³ P)4p - 3d ⁸ (a ³ P)6s	² S° – ² P	$\frac{1}{2} - \frac{3}{2}$		835
	10	1678.476	52.20595 - 111.78379	$3d^{7}4s^{2} - 3d^{7}(a^{2}G)4s4p(^{3}P^{\circ})$	⁴F – y⁴G°	$\frac{1}{2} - \frac{1}{2}$		835
	1	1678.941	74.30093 - 133.86221	3d ⁸ (a ³ P)4p - 3d ⁸ (a ³ P)6s	⁴ S° – ² P	$\frac{3}{2} - \frac{3}{2}$		835
	7	1679.068	74.30093 - 133.85773	3d ⁸ (a ³ P)4p - 3d ⁸ (á ³ P)6s	4S° – 4P	$\frac{1}{2} - \frac{1}{2}$		835
	70	1684.952	76.72736 - 136.07626	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}H - v^{2}G^{\circ}$	$\frac{11}{2} - \frac{9}{2}$		835
	8	1685.465	74.28333 - 133.61399	3d8(a3P)4p - 3d8(a3P)6s	² S° – ⁴ P	$\frac{1}{2} - \frac{3}{2}$		835
	9	1685.965	74.30093 - 133.61399	3d ⁸ (a ³ P)4p - 3d ⁸ (a ³ P)6s	4S° – 4P	$\frac{3}{2} - \frac{3}{2}$		835
	9	1686.934						835
	12	1690.814	74.30093 - 133.44389	$3d^{8}(a^{3}P)4p - 3d^{8}(a^{3}P)6s$	4S° – 4P	$\frac{1}{2} - \frac{5}{2}$		835
	11	1691.231	77.33247 - 136.46110	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{1}P^{\circ})$	$^{2}D - v^{2}D^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		835
	10	1693.177	77.33247 - 136.39285	3d ⁷ 4s ² - 3d ⁸ (¹ D)6p	$^{2}D - ^{2}F^{\circ}$	$\frac{2}{2} - \frac{1}{2}$		835
	2	1694.384	73.89373 - 132.91215	$3d^{7}4s^{2} - 3d^{8}(a^{1}D_{2})4f$	² P – 2[2]°	$\frac{3}{2} - \frac{5}{2}$		835
	8	1695.594	51.04546 - 110.02192	$3d^{7}4s^{2} - 3d^{7}(a^{2}G)4s4p(^{3}P^{\circ})$	⁴F - y⁴G°	$\frac{9}{2} - \frac{9}{2}$		835
	1	1695.897				2		835
	2	1696.527			_			835
	4	1698.400	76.72736 - 135.60630	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})6f$	² H – 3[6]°	$\frac{11}{2} - \frac{13}{2}$		835
	2	1699.772	76.72736 - 135.55880	3d'4s ² - 3d ⁸ (a'P)4f	4H - *G*	$\frac{11}{2} - \frac{2}{2}$		835
	1	1700.665	51.04546 - 109.84600	3d ⁷ 4s ² - 3d ⁷ (a ² G)4s4p(³ P°)	⁴F - y⁴F°	$\frac{9}{2} - \frac{7}{2}$		835
	2	1701.504	57.42016 - 116.19147	3d8(a3F)4p - 3d8(a3P)4d	$^{2}D^{\circ} - ^{2}F$	$\frac{5}{2} - \frac{5}{2}$		835
	1	1702.150	71.45774 - 130.20690	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})5f$	² G – 3[5]°	$\frac{1}{2} - \frac{9}{2}$		835
_	7	1702.265	53.03793 - 111.78379	$3d^{7}4s^{2} - 3d^{7}(a^{2}G)4s4p(^{3}P^{\circ})$	⁴ F − y ⁴ G°	$\frac{1}{2} - \frac{1}{2}$		835
5	25	1703.408 1704.54	0.0 – 58.70595	3d° – 3d°(a°F)4p	g ² D - ² D°	2 - 2		835 089
	11	1705.581						835
	8	1705.739			277 401			835
	2	1706.170	76.72736 - 135.33801	$3d'4s^2 - 3d^2(a^3F_4)8p$	$^{2}H - ^{2}G^{2}$	$\frac{1}{2} - \frac{1}{2}$		835
	25	1708.380	/6./2/36 - 135.26199	30'45" ~ 30'(a'F4)8p	-n - G	$\overline{2} - \overline{2}$		833
4	200	1708.570	0.0 - 58.49321	3d ⁹ - 3d ⁸ (a ³ F)4p	$g^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{5}{2}$		835
		1810.00-		a 17 / 3 a 18 / 3	20 45-20	9 11		075
	3	1/10.032	70.35894 - 128.83711	30'45" - 30"(a ² F4)5f 2d ⁷ 45 ² - 2d ⁷ (c ² C)4c4-(3P ⁰)	^G – 4[6]° 4⊑ – •4⊑°	2 - 2		835 835
	2	1716 149	32.20393 - 110.37330	$50.45 - 50.(a^{-}C)^{454}p(^{-}P)$	г-уг	2 - 2		835
	1	1717 700	77 73679 - 135 95409	3d ⁷ ds ² - 3d ⁸ (a ³ D-)4f	2H - 0(3)	9_1		835
	5	1719.906	11.13017 - 133.73407	JU 78 - JU (4 F0/71	11 - 0[3]	2 - 2		835
		1117.700				1	1	
	15	1721.092	51.04546 - 109.14805	$3d^{7}4s^{2} - 3d^{7}(a^{2}G)4s4n(^{3}P^{\circ})$	⁴ F − v ⁴ F°	2 - 2		835

NI II - Continued

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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	1	1722.113	77.33247 - 135.40067	$3d^{7}4s^{2} - 3d^{8}(a^{3}P_{2})4f$	² D - 2[4]°	$\frac{5}{2} - \frac{7}{2}$		835
	2	1722.646	77.33247 - 135.38253	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{1}P^{\circ})$	$^{2}D - w^{2}P^{\circ}$	$\frac{5}{2} - \frac{3}{2}$		835
	20	1723.859	77.73679 - 135.74606	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{2}H - v^{2}G^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		835
	1	1723.957						835
	1	1724.818						835
	4	1726.324	77.33247 - 135.25892	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{1}P^{\circ})$	$^{2}D - v^{2}D^{\circ}$	$\frac{5}{2} - \frac{5}{2}$		835
	1	1728.022	77 73679 - 135.60620	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})6f$	²H – 3[[∐]]°	8_11		835
	2	1728 133	11.15017 155.00020		II 9[2]	2 2		835
	6	1728 625						835
	1	1732 620						835
	8	1734 904	52 20595 - 109 84600	$3d^{7}4s^{2} - 3d^{7}(a^{2}G)4s4p(^{3}P^{\circ})$	${}^{4}\mathbf{F} = \mathbf{v}^{4}\mathbf{F}^{\circ}$	7 7		835
	5	1735.135	77.33247 – 134.96478	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{2})$	$^{2}D - w^{2}D^{\circ}$	$\frac{2}{5} - \frac{3}{2}$		835
					45 450			
	3	1738.059	53.03793 - 110.57336	$3d'4s^2 - 3d'(a^2G)4s4p(^3P^3)$	$F - y^{*}F^{*}$	2 - 2		835
	12	1738.311	70.35894 - 127.88586	3d'4s ² – 3d°(a'G)5p	² G - ² G ^o	$\frac{1}{2} - \frac{1}{2}$		835
	1	1738.549	53.60119 - 111.12054	$3d'4s^2 - 3d'(a^2G)4s4p(^3P^3)$	*F - y*F*	$\frac{1}{2} - \frac{1}{2}$		835
	4	1738.793	76.72736 - 134.23844	$3d^{2}4s^{2} - 3d^{6}(a^{3}F_{4})6f$	${}^{2}\mathbf{H} - 4[{}^{12}_{2}]^{\circ}$	$\frac{11}{2} - \frac{13}{2}$		835
_	30	1740.619	77.33247 - 134.78314	$3d'4s^2 - 3d'(a^2F)4s4p(^3P^3)$	$^{2}D - w^{2}D^{\circ}$			835
5	1000	1741.547	0.0 - 57.42016	3d* - 3d°(a3F)4p	g'D – 'D'	$\frac{1}{2} - \frac{1}{2}$		835
	1	1746.989	9.33004 - 66.57134	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{3}P)4p$	⁴ F - ⁴ P°	$\frac{7}{2} - \frac{5}{2}$		835
	500	1748.285	1.50694 - 58.70595	$3d^{9} - 3d^{8}(a^{3}F)4p$	$g^2D - {}^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$		835
	300	1751.911	0.0 - 57.08055	3d ⁹ - 3d ⁸ (a ³ F)4p	$\overline{g^2D} - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		835
	50	1754.808	1.50694 - 58.49321	$3d^9 - 3d^8(a^3F)4p$	$g^2D - {}^2F^\circ$	$\frac{3}{2} - \frac{5}{2}$		835
	2	1756.829	77.33247 - 134.25285	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})6f$	² D – 4[3]°	$\frac{5}{2} - \frac{7}{2}$		835
	1	1763.097	76.72736 - 133.44575	$3d^{7}4s^{2} - 3d^{7}(a^{2}G)4s4p(^{1}P^{\circ})$	$^{2}H - w^{2}G^{\circ}$	$\frac{11}{2} - \frac{9}{2}$		835
	2	1769.940	70.35894 - 126.85797	3d ⁷ 4s ² - 3d ⁸ (a ¹ G)5p	$^{2}G - ^{2}H^{\circ}$	<u>₹_</u>		835
	4	1771.865	71.45774 - 127.89533	$3d^{7}4s^{2} - 3d^{8}(a^{1}G)5p$	${}^{2}G - {}^{2}G^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		835
	1	1772.197	78.95545 - 135.38253	$3d^{7}4s^{2} - 3d^{7}(a^{2}P)4s4p(^{1}P^{\circ})$	$^{2}\mathbf{D} - \mathbf{w}^{2}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		835
	25	1773.949	0.0 - 56.37141	$3d^9 - 3d^8(a^3F)4p$	$g^2D - {}^2G^\circ$	$\frac{5}{2} - \frac{7}{2}$		835
2	1	1783.317	0.0 - 56.07526	$3d^9 - 3d^8(a^3F)4p$	$g^2D - {}^4F^\circ$	$\frac{5}{2} - \frac{5}{2}$		835
5	100	1788.485	1.50694 - 57.42016	3d ⁹ – 3d ⁸ (a ³ F)4p	$g^2D - {}^2D^o$	$\frac{3}{2} - \frac{5}{2}$		835
	1	1789.640	77.33247 - 133.20930	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	${}^{2}D - v^{4}F^{\circ}$	3-3		835
	1	1791.219	78.95545 - 134.78314	$3d^{7}4s^{2} - 3d^{7}(a^{2}F)4s4p(^{3}P^{\circ})$	$^{2}\mathbf{D} - \mathbf{w}^{2}\mathbf{D}^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		835
	1	1804.451				[* *		835
2	30	1804.473	0.0 - 55.41783	$3d^9 - 3d^8(a^3F)4p$	g ² D - ⁴ F°	5-7		835
	2	1808.330	57.42016 - 112.71975	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{1}D)4d$	${}^{2}D^{\circ} - {}^{2}F$	$\frac{5}{2} - \frac{7}{2}$		835
	30	1812.065	13.55039 - 68.73598	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{1}D)4p$	${}^{2}F - {}^{2}D^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		835
	1	1817.112						835
2	1	1820.916	1.50694 - 56.42449	$3d^{9} - 3d^{8}(a^{3}F)4p$	$g^2D - {}^4F^\circ$	$\frac{3}{2} - \frac{3}{2}$		835
	1	1825.068	51.04546 - 105.83806	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})5p$	${}^{4}F - {}^{2}F^{\circ}$	<u>9</u> - 7		835
	1	1832.144	13.55039 - 68.13121	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{1}D)4p$	${}^{2}F - {}^{2}F^{\circ}$	$\frac{7}{2} - \frac{7}{2}$		835
2	1	1832.566	1.50694 - 56.07526	$3d^9 - 3d^8(a^3F)4p$	$g^2D - {}^4F^\circ$	$\frac{3}{2} - \frac{5}{2}$		835
	5	1833.403	51.04546 - 105.58889	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})5p$	⁴ F − ² G°	$\frac{9}{2} - \frac{9}{2}$		835
	1	1837.744	52.20595 - 106.62053	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{2})5p$	⁴ F - ² G°	$\frac{7}{2} - \frac{7}{2}$		835
	2	1837.985	75.91763 - 130.32472	$3d^{8}(a^{1}G)4p - 3d^{8}(a^{3}F_{1})5g$	² F° - 3[5]°	$\frac{2}{3} - \frac{2}{3}$		835
	1	1842.889	0.0 - 54.26263	$3d^9 - 3d^8(a^3F)4p$	$g^2D - {}^4G^\circ$	<u><u>s</u> - <u>7</u></u>		835
	2	1852.522	58.70595 - 112.68630	$3d^{8}(a^{3}F)4p - 3d^{8}(a^{1}D)4d$	${}^{2}D^{\circ} - {}^{2}F$	3-5		835
	2	1852.875	14.99557 - 68.96565	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{1}D)4p$	${}^{2}F - {}^{2}P^{\circ}$	5-3		835
	6	1857.587				2 2		835
	1	1860.689	76 72736 - 130 47090	$3d^74s^2 - 3d^8(a^3E)7r$	² H - ⁴ E°	ц_2		835
	1	1860.796	14.99557 - 68 73598	$3d^8(a^3F)4s = 3d^8(a^1D)4n$	${}^{2}\mathbf{F} - {}^{2}\mathbf{D}^{9}$	5 5		835
	6	1864.558	52.20595 - 105.83806	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{2})5n$	${}^{4}F - {}^{2}F^{\circ}$	2 2		835
	5	1865.637	51.04546 - 104.64652	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{1})5p$	⁴ F - ⁴ F°	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		835
	5	1866.499	67.88016 - 121.45632	$3d^{7}4s^{2} - 3d^{8}(a^{3}P)sn$	⁴ P - ⁴ S°	2 2		835
	8	1870.460	52.20595 - 105.66878	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{1})5p$	4F - 4F°	$\frac{2}{7} - \frac{2}{5}$		835
	Ŭ		100.00070	50 15 50 (u 1 3)5P		2 - 2		000

NI II - Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	3	1875.069	53.03793 - 106.36930	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{2})5p$	⁴ F - ⁴ F°	$\frac{5}{2} - \frac{3}{2}$		835
	1	1876.180	68.15657 - 121.45632	$3d^{7}4s^{2} - 3d^{8}(a^{3}P)5p$	⁴ P - ⁴ S°	$\frac{3}{2} - \frac{3}{2}$		835
	2	1876.418	52.20595 - 105.49905	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})5p$	⁴ F − ⁴ G°	$\frac{1}{2} - \frac{1}{2}$		835
	40	1877.838	51.04546 - 104.29823	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})5p$	⁴ F - ⁴ G°	$\frac{9}{2} - \frac{9}{2}$		835
	2	1878.103	53.03793 - 106.28316	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{2})5p$	4F - 4G°	$\frac{5}{2} - \frac{5}{2}$		835
	25	1881.155	14.99557 - 68.15431	$3d^{8}(a^{3}F)4s - 3d^{8}(a^{1}D)4p$	${}^{2}\mathbf{F} - {}^{2}\mathbf{D}^{\bullet}$	$\frac{5}{2} - \frac{3}{2}$		835
	4	1883.170	51.04546 - 104.14729	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})5p$	⁴ F − ⁴ G°	$\frac{9}{2} - \frac{11}{2}$		835
	20	1885.525	51.04546 104.08104	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})5p$	⁴ F – ⁴ F°	$\frac{9}{2} - \frac{9}{2}$		835
	12	1886.043	13.55039 - 66.57134	3d*(a ³ F)4s - 3d*(a ³ P)4p	${}^{2}F - {}^{4}P^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		835
	1	1893.600	23.10828 - 75.91763	$3d^{s}(a^{1}D)4s - 3d^{s}(a^{1}G)4p$	${}^{2}D - {}^{2}F^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		835
	6	1895.082	53.60119 - 106.36930	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{2})5p$	⁴ F - ⁴ F°	$\frac{3}{2} - \frac{3}{2}$		835
1	2	1896.147	0.0 - 52.73845	$3d^{\circ} - 3d^{*}(a^{3}F)4p$	$g^2D - {}^4D^\circ$	$\frac{5}{2} - \frac{5}{2}$, 835
	4	1900.025	53.03793 - 105.66878	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})5p$	⁴F - ⁴F°	$\frac{5}{2} - \frac{5}{2}$		835
	15	1900.865	51.04546 - 103.65303	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})5p$	⁴ F – ⁴ D°	$\frac{9}{2} - \frac{7}{2}$		835
	2	1900.921	23.79618 - 76.40203	3d*(a1D)4s - 3d*(a1G)4p	$^{2}D - ^{2}F^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		835
	1	1907.612	53.60119 - 106.02279	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{2})5p$	${}^{4}F - {}^{4}D^{\circ}$	$\frac{3}{2} - \frac{1}{2}$		835
	1	1908.326	53.03793 - 105.43985	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})5p$	⁴ F - ⁴ D [•]	$\frac{5}{2} - \frac{3}{2}$		835
	2	1912.146	52.20595 - 104.50322	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})5p$	⁴ F - ⁴ D°	$\frac{7}{2} - \frac{5}{2}$		835
	1	1920.582	53.60119 - 105.66878	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})5p$	⁴ F − ⁴ F °	$\frac{3}{2} - \frac{5}{2}$		835
	2	1927.707	52.20595 - 104.08104	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})5p$	⁴ F - ⁴ F°	$\frac{7}{2} - \frac{9}{2}$		835
	1	1929.063	53.60119 - 105.43985	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{3})5p$	⁴ F − ⁴ D°	$\frac{3}{2} - \frac{3}{2}$		835
	1	1930.493						835
	1	1937.661	53.03793 - 104.64652	3d ⁷ 4s ² - 3d ⁸ (a ³ F ₄)5p	⁴ F - ⁴ F°	\$ - 7		835
	2	1938.579	14.99557 - 66.57971	$3d^{(a^{3}F)4s} - 3d^{(a^{3}P)4p}$	² F – ⁴ P°	$\frac{5}{2} - \frac{3}{2}$		835
	10	1939.901						835
	2	1943.060	53.03793 - 104.50322	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})5p$	4F - 4D°	2 - 2		835
	2	1943.744	52.20595 - 103.65303	$3d^{7}4s^{2} - 3d^{8}(a^{3}F_{4})5p$	⁴ F – ⁴ D°	$\frac{7}{2} - \frac{7}{2}$		835
	40	1953.407	23.10828 - 74.30093	3d ⁸ (a ¹ D)4s - 3d ⁸ (a ³ P)4p	${}^{2}D - {}^{4}S^{\circ}$	$\frac{5}{2} - \frac{3}{2}$		835
	1	1954.709	76.72736 - 127.88586	3d ⁷ 4s ² - 3d ⁸ (a ¹ G)5p	² H - ² G°	$\frac{11}{2} - \frac{9}{2}$		835
	8	1965.357	25.03638 - 75.91763	3d*(a ³ P)4s - 3d*(a ¹ G)4p	${}^{4}\mathbf{P} - {}^{2}\mathbf{F}^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		835
	15	1980.010	23.79618 - 74.30093	3d ^x (a ¹ D)4s - 3d ^x (a ³ P)4p	² D – ⁴ S°	$\frac{3}{2} - \frac{3}{2}$		835
	3	1980.699	23.79618 - 74.28333	3d ^x (a ¹ D)4s - 3d ^x (a ³ P)4p	${}^{2}D - {}^{2}S^{\circ}$	$\frac{3}{2} - \frac{1}{2}$		835
	2	1993.570	66.57134 - 116.73251	3d*(a ³ P)4p - 3d*(a ³ P)4d	⁴ P° – ⁴ P	$\frac{5}{2} - \frac{5}{2}$		835
	1	1993.906	66.57971 - 116.73251	3d*(a ³ P)4p - 3d*(a ³ P)4d	⁴ P° - ⁴ P	$\frac{3}{2} - \frac{5}{2}$		835
	15	1995.723	23.79618 - 73.90325	3d ^s (a ¹ D)4s - 3d ^s (a ³ P)4p	$^{2}\mathbf{D} - ^{2}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{1}{2}$		835

NICKEL III (Ni ²⁺), Z = 28 Ground State $1s^22s^22p^63s^23p^63d^8(^3F_4)$ (26 electrons) Ionization Potential 284 900 cm⁻¹; 35.32 eV

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm $^{-1}$)	Configurations	Terms	J - J	Notes	References
	0	615.164	· · · ·	, ,				661
	5	615.554	14.0316 - 176.48710	$3d^{8} - 3d^{7}(b^{2}D)4p$	$a^{1}D - {}^{3}P^{\circ}$	2 – 2		661
	15	625.306	16.6616 - 176.58320	$3d^{*} - 3d^{7}(b^{2}D)4p$	$a^{3}P - {}^{3}P^{\circ}$	2 – 1		661
	100	625.682	16.6616 - 176.48710	$3d^{8} - 3d^{7}(b^{2}D)4p$	a ³ P - ³ P°	2 - 2		661
	15	625.938	16.9778 - 176.73640	$3d^{8} - 3d^{7}(b^{2}D)4p$	$a^{3}P - {}^{3}P^{\circ}$	1-0		661
	10	626.548	16.9778 - 176.58320	$3d^{8} - 3d^{7}(b^{2}D)4p$	$a^{3}P - {}^{3}P^{\circ}$	1 - 1		661
	30	626.923	16.9778 - 176.48710	$3d^{*} - 3d^{7}(b^{2}D)4p$	$a^{3}P - {}^{3}P^{\circ}$	1 - 2		661
	15	627.541	17.2307 - 176.58320	$3d^{8} - 3d^{7}(b^{2}D)4p$	$a^{3}P - {}^{3}P^{\circ}$	0 - 1		661
	500	630.711	23.1087 - 181.6584	$3d^{8} - 3d^{7}(b^{2}D)4p$	a'G - 'F°	4 - 3		661
	1	635.406	0.0 - 157.37542	$3d^{*} - 3d^{7}(a^{2}F)4p$	ga ³ F – ¹ G°	4 - 4		661
	15	637.057	0.0 - 156.97208	$3d^{8} - 3d^{7}(a^{2}F)4p$	ga'F - 'F°	4 - 4		661
	200	637.535	0.0 - 156.85300	$3d^{8} - 3d^{7}(a^{2}F)4p$	$ga^{3}F - D^{\circ}$	4 - 3		661

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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	2	637.703	0.0 - 156.80870	$3d^8 - 3d^7(a^2F)4p$	$ga^{3}F - {}^{3}G^{\circ}$	4 - 5		661
	10	639.338	0.0 - 156.41120	$3d^8 - 3d^7(a^2F)4p$	$ga^{3}F - {}^{3}F^{\circ}$	4-3		661
	5	641.689	0.0 - 155.84140	$3d^8 - 3d^7(a^2F)4p$	$ga^{3}F - {}^{3}G^{\circ}$	4 - 4		661
	100	641 866	1.3607 - 157.15427	$3d^8 - 3d^7(a^2F)4p$	$ga^{3}F - {}^{3}D^{\circ}$	3-2		661
	1	642 611	1 3607 - 156 97208	$3d^8 - 3d^7(a^2F)4n$	$ga^{3}F - {}^{3}F^{\circ}$	3-4		661
	0	644.488	1.3607 - 156.52287	$3d^8 - 3d^7(a^2F)4p$	$ga^{3}F - {}^{3}F^{\circ}$	3 - 2		661
					- 			
	20	644.948	1.3607 - 156.41120	$3d^8 - 3d^7(a^2F)4p$	$ga^{3}F - {}^{3}F^{\circ}$	3-3		661
	30	645.305	2.2696 - 157.23516	30° - 30 (a°F)4p	$ga^3F - ^3D^3$	2-1		001
	2	645.632	2.2696 - 157.15427	$3d^{\circ} - 3d^{\circ}(a^{\circ}F)4p$	$ga^3F - ^3D^3$	2-2		001
	1	646.890	2.2696 - 156.85300	3d° – 3d′(a²F)4p	$ga^{3}F - ^{3}D^{2}$	2 - 3		601
	0	647.319	1.3607 - 155.84140	30° - 30° (a°F)4p	ga°F - 'G'	3-4		001
	3	648.271	2.2696 - 156.52287	3d° – 3d'(a°F)4p	ga'F - 'F'	2-2		001
	2	648.745	2.2696 - 156.41120	$3d^8 - 3d^7(a^2F)4p$	$ga^{3}F - {}^{3}F^{\circ}$	2 - 3		661
	2	649.006	1.3607 - 155.44330	$3d^8 - 3d^7(a^2F)4p$	$ga^{3}F - {}^{3}G^{\circ}$	3 - 3		661
	2	650.701	53.70393 - 207.38210	3d7(a4F)4s - 3d6(a5D)4s4p	⁵ F - ⁵ F°	5-4		661
	30	652.652	53.70393 - 206.92518	$3d^{7}(a^{4}F)4s - 3d^{6}(a^{5}D)4s4p$	⁵ F - ⁵ F°	5 - 5		661
	1	652.837	2.2696 - 155.44330	$3d^8 - 3d^7(a^2F)4p$	$ga^{3}F - {}^{3}G^{\circ}$	2 - 3		661
	10	653.496						661
				a. 18 - ā. 17 / 750 d				
	10	654.445	2.2696 - 155.07100	3d° - 3d'(a°F)4p	ga'F - 'D'	2-2		001
	5	654.768	54.65783 - 207.38210	$3d^{2}(a^{2}F)4s = 3d^{2}(a^{2}D)4s4p$	F - F	4-4		001
	0	655.120	61.33858 - 213.97967	$3d'(a^{2}F)4s - 3d'(a^{2}D)4s4p$	F - F	4-3		001
	1	656.431	55.40629 - 207.74430	3d'(a*F)4s - 3d°(a*D)4s4p	F - F	3-3		001
		656.724	54.65783 - 206.92518	3d'(a*F)4s - 3d°(a'D)4s4p	F - F	4-5		001
	1	657.304	62.60558 - 214.7440	3d'(a*F)4s - 3d°(a'D)4s4p	"F - "F"	3-2		661
	0	657.668	55.95221 - 208.0057	3d ⁷ (a ⁴ F)4s - 3d ⁶ (a ⁵ D)4s4p	5F - 5F°	2 - 2		661
	0	657.998	55.40629 - 207.38210	3d ⁷ (a ⁴ F)4s - 3d ⁶ (a ⁵ D)4s4p	⁵ F - ⁵ F°	3 - 4		661
	0	658.810	55.95221 - 207.74430	3d7(a4F)4s - 3d6(a5D)4s4p	⁵ F - ⁵ F°	2 - 3		661
	30	660.079	61.33858 - 212.8377	3d7(a4F)4s - 3d6(a5D)4s4p	${}^{3}F - {}^{3}F^{\circ}$	4 - 4	i i	661
	10	660.620	62.60558 - 213.97967	3d7(a4F)4s - 3d6(a5D)4s4p	${}^{3}F - {}^{3}F^{\circ}$	3 - 3		661
	5	661.061	63.47193 - 214.7440	3d7(a4F)4s - 3d6(a5D)4s4p	${}^{3}F - {}^{3}F^{\circ}$	2 - 2		661
	200	(12.24)	(1 22050 212 2125	247(-4E)4a 246(a5D)4a4m	35 300	4 2		661
	200	002.300	61.33838 - 212.3123	3d(aF)4s - 3d(aD)4s4p $2d^{2}(a^{4}E)4s - 2d^{6}(a^{5}D)4s4p$	F - D	4-5		661
	100	003.308	53.70393 - 204.40412	$3d^{2}(a^{2}\Gamma)4s - 3d^{2}(a^{2}D)4s4p$	F - D	3-4		661
	100	004.851	02.00538 - 213.0108	3d(a'F)4s - 3d(a'D)4s4p $3d^{7}(-^{4}E)4a - 3d^{9}(a^{5}D)4a4p$	F - D	3-2		661
	20	000.41/	54.05/85 - 204./1495	$3d(a^{2}F)4s = 3d(a^{2}D)4s4p$ $3d^{2}(a^{4}F)4a = 3d^{6}(a^{5}D)4a4p$		4-3		661
	50	667 783	54 65783 - 204 40412	3d(a r) + s - 3d(a D) + s + p $3d^{7}(a^{4}F) + s - 3d^{6}(a^{5}D) + s + p$	⁵ F- ⁵ D ^o	4 - 4		661
		0011105						
	1	667.976	62.60558 - 212.3125	3d ⁷ (a ⁴ F)4s - 3d ⁶ (a ⁵ D)4s4p	${}^{3}\mathbf{F} - {}^{3}\mathbf{D}^{\circ}$	3 - 3		661
	10	668.195	55.40629 - 205.06251	3d ⁷ (a ⁴ F)4s - 3d ⁶ (a ⁵ D)4s4p	${}^{5}\mathbf{F} - {}^{5}\mathbf{D}^{\circ}$	3 - 2		661
	1	668.697	63.47193 - 213.0168	3d'(a ⁴ F)4s - 3d ⁶ (a ⁵ D)4s4p	³ F - ³ D°	2 – 2		661
	5	669.458	55.95221 - 205.32700	$3d'(a^{4}F)4s - 3d^{6}(a^{5}D)4s4p$	°F – °D°	2 - 1		661
	5	669.755	55.40629 - 204.71493	$3d'(a^{*}F)4s - 3d^{\circ}(a^{3}D)4s4p$	³ F - ³ D°	3-3	ł	661
	0	670.440	56.30824 - 205.46600	3d'(a*F)4s - 3d°(a3D)4s4p	⁷ F – ⁷ D [*]	1-0		661
	2	670.640	55.95221 - 205.06251	3d ⁷ (a ⁴ F)4s - 3d ⁶ (a ⁵ D)4s4p	⁵ F - ⁵ D°	2 - 2		661
	0	671.065	56.30824 - 205.32700	$3d^{7}(a^{4}F)4s - 3d^{6}(a^{5}D)4s4p$	⁵ F - ⁵ D°	1-1		661
	500	676.941	14.0316 - 161.75489	$3d^8 - 3d^7(a^2F)4p$	$a^{1}D - {}^{1}F^{\circ}$	2 - 3		661
	5	682.947	55.40629 - 201.82946	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)5p$	5F - 5D°	3 - 3		661
	10	683,186	53.70393 - 200.07635	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)5p$	⁵ F - ⁵ F°	5 - 4		661
	10	683.455	55.40629 - 201.72523	3d ⁷ (a ⁴ F)4s - 3d ⁷ (a ⁴ F)5p	⁵ F – ⁵ F°	3 - 2		661
		(02.500						
	10	683.590	53 70393 100 01009	3d ⁷ (a ⁴ E)4s 2d ⁷ (a ⁴ E)5n	5E. 5E.	5 5		661
	100	680 210	16 6616 - 161 75490	$3d^8 + 2d^7(a^2E)An$	3D E	2 2		661
	200	700 169	14.0316 - 156.85200	3u - 3u (a - r) + p $3d^8 - 2d^7 (a^2 F) + n$		2-3		661
	1	701 261	0.0 - 142 57560	$3d^8 = 3d^7(a^2H)/a$	a D - D	1 5		661
	100	701 779	14 0316 - 156 52287	$3d^8 - 3d^7(a^2E)An$	a ¹ D. ³ E ^o	2 2		661
	100	/01.//0	14.0310 - 130.32207	5u – 5u (a r)4p	aD-F	2-2		001

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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	0	705.991	1.3607 - 143.00270	3d ⁸ - 3d ⁷ (a ² H)4p	ga ³ F - ³ H°	3-4		661
	0	707.754	2.2696 - 143.56016	$3d^8 - 3d^7(a^2D)4p$	$ga^{3}F - {}^{3}P^{\circ}$	2 - 2		661
	5	708.853	1.3607 - 142.43395	$3d^8 - 3d^7(a^2D)4p$	ga ³ F - ¹ D°	3 - 2		661
	100	709.027	14.0316 - 155.07100	3d* - 3d7(a2F)4p	$a^{\dagger}D - {}^{\dagger}D^{\circ}$	2 - 2		661
	20	711.518	0.0 - 140.54452	$3d^8 - 3d^7(a^2D)4p$	$ga^{3}F - {}^{3}F^{\circ}$	4 - 3		661
	100	711.772	16.6616 - 157.15427	$3d^8 - 3d^7(a^2F)4p$	$a^{3}P - {}^{3}D^{\circ}$	2 - 2		661
	100	712.976	16.9778 - 157.23516	$3d^{x} - 3d^{7}(a^{2}F)4p$	$a^{3}P - {}^{3}D^{\circ}$	1 - 1		661
	300	713 332	0.0 - 140.18465	$3d^8 - 3d^7(a^2D)4p$	$ga^{3}F - {}^{3}F^{\circ}$	4-4		661
	300	713 385	16 9778 - 157, 15427	$3d^{8} - 3d^{7}(a^{2}F)4p$	$a^{3}P - {}^{3}D^{\circ}$	1 - 2		661
	100	714 254	17 2307 - 157 23516	$3d^8 - 3d^7(a^2F)4p$	$a^{3}P - {}^{3}D^{\circ}$	0 - 1		661
	100	714 965	17.2507 - 157.25510					661
	100	715.563	16.6616 - 156.41120	3d ^x - 3d ⁷ (a ² F)4p	$a^{3}P - {}^{3}F^{\circ}$	2 – 3		661
	20	716 608	16 9778 - 156 52287	$3d^8 - 3d^7(a^2F)4p$	$a^{3}P - {}^{3}F^{\circ}$	1 - 2		661
	20	717 318	10.7778 - 150.52287	50 50 (a1),p		· -		661
	10	718 287	62 60558 - 201 82946	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)5n$	${}^{3}\mathbf{F} - {}^{5}\mathbf{D}^{\circ}$	3 - 3		661
	500	718 480	13607 - 14054452	$3d^{2} - 3d^{7}(a^{2}D)4n$	$ga^3F - {}^3F^\circ$	3-3		661
	100	718 674	22696 - 14141410	$3d^{x} - 3d^{7}(a^{2}P)4n$	$e^{3}F - P^{\circ}$	2 - 1		661
	15	720.337	1.3607 - 140.18465	$3d^{*} - 3d^{7}(a^{2}D)4p$	$ga^{3}F - {}^{3}F^{\circ}$	3 - 4		661
	200	721.250	22 1097 161 75 490	248 247/-25)4n		4 2		661
	200	721.259	23.1087 - 101.73489	30 - 30 (a r) + p		4-5		661
12	100	721.418	2.2090 - 140.88340	3d - 3d (a D) + p $2d^8 - 2d^7 (a^2 D) 4 p$	ga F - F	1 3		661
12	300	722.094	0.0 - 138.48740	$3d^{2} - 3d(a^{2}D)4p$	$ga^{T} - D$	4-3		661
	3	724.155	16.97/8 - 155.07100	30° – 30 (a°r)4p		1-2		661
	20	724.471	0.0 - 138.03090	$3d^{2} - 3d(a^{2}H)4p$	ga F - G	4-4		001
12	250	725.196	1.3607 - 139.25370	3d" - 3d'(a-D)4p	ga F - D	3 - 2		001
	2	725.806						661
	15	727.313	1.3607 - 138.85220	3d ⁸ – 3d'(a ² H)4p	ga`F - `G°	3 - 3		661
12	100	729.249	1.3607 - 138.48740	$3d^{*} - 3d^{7}(a^{2}D)4p$	ga'F - 'D°	3 – 3		661
	500	729.820	0.0 - 137.02020	$3d^{*} - 3d^{7}(a^{2}H)4p$	ga'F - 'G°	4 - 5		661
	50	730.014	2.2696 - 139.25370	$3d^{8} - 3d^{7}(a^{2}D)4p$	ga'F - 'D°	2 - 2		661
11	250	730.109	0.0 - 136.96700	$3d^{*} - 3d^{7}(a^{2}P)4p$	ga'F - 'D°	4 - 3		661
	150	731.481	2.2696 - 138.97920	3d* - 3d7(a2D)4p	ga ³ F - ³ D°	2 - 1		661
	400	731.696	1.3607 - 138.03090	$3d^{8} - 3d^{7}(a^{2}H)4p$	ga ³ F - ³ G°	3 - 4		661
	300	732.158	2.2696 - 138.85220	3d ^x – 3d ⁷ (a ² H)4p	ga ³ F - ³ G°	2 - 3		661
	20	733.807						661
12	5	734.100	2.2696 - 138.48740	$3d^8 - 3d^7(a^2D)4p$	ga ³ F - ³ D°	2 - 3		661
11	50	737.419	1.3607 - 136.96700	$3d^{x} - 3d^{2}(a^{2}P)4p$	ga'F - 'D°	3 – 3		661
11	200	738.258	1.3607 - 136.81320	3d [×] - 3d ² (a ² P)4p	$ga^{3}F - {}^{3}D^{\circ}$	3 - 2		661
11	100	740.235	2.2696 - 137.36236	$3d^{x} - 3d^{2}(a^{2}P)4p$	$ga^{3}F - {}^{3}D^{\circ}$	2 – 1		661
	30	740.620	0.0 - 135.02320	$3d^{8} - 3d^{7}(a^{2}G)4p$	ga ³ F – ¹ F°	4 - 3		661
11	3	742.391	2.2696 - 136.96700	$3d^{*} - 3d^{7}(a^{2}P)4p$	ga ³ F - ³ D°	2 - 3		661
1	2	743.275	2.2696 - 136.81320	$3d^{*} - 3d^{7}(a^{2}P)4p$	ga ³ F - ³ D°	2 - 2		661
	100	743.955	0.0 - 134.41477	$3d^{*} - 3d^{7}(a^{2}G)4p$	ga ³ F - ³ G°	4 - 4		661
	5	744.400	0.0 - 134.33479	3d [×] - 3d ⁷ (a ² G)4p	ga ³ F - ³ G°	4 - 3		661
	100	744.784	23.1087 - 157.37542	$3d^{*} - 3d^{7}(a^{2}F)4p$	a'G - 'G°	4 - 4		661
	40	745.058	0.0 - 134.21760	$3d^{*} - 3d^{7}(a^{2}G)4p$	ga ³ F - ¹ H°	4 - 5		661
	50	746.319	1.3607 - 135.35033	$3d^{*} - 3d^{7}(a^{4}P)4p$	ga ³ F - ³ P°	3 - 2		661
	30	747.015	23.1087 - 156.97208	$3d^{*} - 3d^{7}(a^{2}F)4p$	$a^{3}G - {}^{3}F^{\circ}$	4 – 4		661
	20	747.213	2.2696 - 136.09870	$3d^{8} - 3d^{7}(a^{4}P)4p$	ga ³ F - ³ P°	2 - 1		661
	3	747,697	23,1087 - 156,85300	$3d^{*} - 3d^{7}(a^{2}F)4p$	$a^{1}G - {}^{3}D^{\circ}$	4 - 3		661
9	300	747,989	0.0 - 133.69200	$3d^{8} - 3d^{7}(a^{2}G)4p$	$ga^{3}F - {}^{3}G^{\circ}$	4-5		661
6	200	749,677	0.0 - 133.39094	$3d^8 - 3d^7(a^4P)4p$	$ga^{3}F - D^{\circ}$	4 - 3		661
0	300	750.053	0.0 - 133.32470	$3d^8 - 3d^7(a^2G)4n$	ga ³ F - 'G'	4-4		661
4	150	750 983	0.0 - 133.15850	$3d^{8} - 3d^{7}(a^{2}G)4n$	$ga^{3}F - {}^{3}F^{\circ}$	4-3		661
8	150	751 333	0.0 - 133.09589	$3d^{8} - 3d^{7}(a^{4}P)4n$	ga'F - 'P'	4-3		661
0	150	, 51.555	0.0 - 100.0000					
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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
9	150	751.573	1.3607 - 134.41477	$3d^8 - 3d^7(a^2G)4p$	ga ³ F - ³ G°	3 – 4		661
9	200	752.023	1.3607 - 134.33479	$3d^8 - 3d^7(a^2G)4p$	ga ³ F - ³ G°	3 - 3		661
4	100	752.603	1.3607 - 134.23190	$3d^8 - 3d^7(a^2G)4p$	$ga^{3}F - {}^{3}F^{\circ}$	3 - 2		661
•	30	753.252	2.2696 - 135.02320	$3d^8 - 3d^7(a^2G)4p$	$ga^{3}F - F^{\circ}$	2 - 3		661
	10	753.378	231087 - 15584140	$3d^8 - 3d^7(a^2F)4n$	$a^{1}G - {}^{3}G^{\circ}$	4-4		661
5	100	756.687	0.0 - 132.15650	$3d^8 - 3d^7(a^2G)4p$	$Pa^{3}F = {}^{3}H^{\circ}$	4 - 4		661
5	100	/50.00/	0.0 - 152.15050	54 54 (a O)Ap	541 11			001
0	50	757 201	2 2696 - 134 33479	$3d^8 - 3d^7(a^2G)4n$	$\mathbf{r}\mathbf{a}^{3}\mathbf{F} = {}^{3}\mathbf{G}^{2}$	2-3		661
6	5	757 397	1 3607 - 133 39094	$3d^8 = 3d^7(a^4P)4n$	$ra^{3}F = {}^{3}D^{\circ}$	3_3		661
U	10	757 689	71 28410 203 36052	$3d^{2}(a^{4}B)Ac = 3d^{2}(a^{4}E)5p$	${}^{5}\mathbf{D} = {}^{3}\mathbf{E}^{9}$	2_3		661
4	200	757.009	2 2606 124 22100	3d(a r) + s = 3d(a r) + 3d(a r) + s = 3d(a r) + 3d(a	$I = I^{\circ}$	2-3		661
-	150	758 020	14 0216 145 05015	$3d^{*} - 3d^{7}(a^{2}D)4p$		2 - 2		661
4	150	738.039	1 2607 122 15950	3d = 3d (a D) + p	aD - F	2 - 1		661
4	250	136.133	1.3007 - 133.13830	50 – 50 (a C)+p	ga I' - I'	3-3		001
4	250	758 773	0.0 - 131.79202	$3d^8 - 3d^7(a^2G)4n$	$ga^3 F = {}^3 F^\circ$	4 - 4	1	661
8	100	759.098	1 3607 - 133 09589	$3d^8 = 3d^7(a^4P)4n$	$\mathbf{r}\mathbf{a}^{3}\mathbf{F} = {}^{5}\mathbf{P}^{6}$	3_3		661
0	100	760.074	1.5007 - 155.05589	5 u - 5 u (a 1)+p	ga i = i	5-5	Ì	661
	10	760.024	0.0 131 50050	2d ⁸ 2d ⁷ (a ² C)4p	an ³ E ³ U ⁹	1 5		661
0	10	760.432	1 2607 122 81826	$3d^{8} - 3d^{7}(a^{4}D)An$	$ga^{3}E^{5}D^{9}$	2 2		661
0		760.064	1.3007 - 132.81820	3d = 3d (a F) + p	gar - r	3 - 2		661
8	3	/02.951	2.2090 - 133.33970	30 – 30 (a r)+p	gar - r	2-1		100
		762 212	2 2606 122 27670	2-18 2-17(-2D)4-	an ³ E ³ D ⁹	2.		441
	100	763.313	2.2096 - 133.27670	$3d^2 - 3d(a^2F)4p$	gar - P	2-1		601
4	100	764.014	2.2696 - 133.15850	$3d^{2} - 3d^{2}(a^{2}G)4p$	ga F – F	2-3		001
8	50	764.354	2.2696 - 133.09589	3d" - 3d'(a'P)4p	ga F - P	2 - 3		001
	50	765.726	14.0316 - 144.62455	$3d^{\circ} - 3d^{\circ}(a^{\circ}D)4p$	$a^{\dagger}D - P^{\dagger}$	2 - 1		001
8	3	766.000	2.2696 - 132.81826	$3d^{2} - 3d^{2}(a^{2}P)4p$	ga'F - 'P'	2-2		001
4	100	766.693	1.3607 - 131.79202	3d" - 3d'(a-G)4p	ga"F – "F"	3 - 4		001
	5	767.400	0.0 - 130.31230	$3d^8 - 3d^7(a^4P)4p$	$ga^{3}F - {}^{5}D^{\circ}$	4 - 4		661
	2	767.901	115.27226 - 245.49536	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F_{12})5g$	³ G° – ∛[¹]°	5-6		661
	400	770.216	14.0316 - 143.86480	$3d^{8} - 3d^{7}(a^{2}D)4p$	a'D - 'F°	2 - 3		661
	200	772.040	14.0316 - 143.56016	$3d^8 - 3d^7(a^2D)4p$	$a^{1}D - {}^{3}P^{\circ}$	2 - 2		661
	100	773.464	16.6616 - 145.95015	$3d^{8} - 3d^{7}(a^{2}D)4p$	$a^{3}P - P^{\circ}$	$\frac{1}{2} - 1$		661
	5	775.364	16.9778 - 145.95015	$3d^{8} - 3d^{7}(a^{2}D)4p$	$a^{3}P - {}^{1}P^{\circ}$	1 - 1		661
	5	776.884	17.2307 - 145.95015	$3d^{8} - 3d^{7}(a^{2}D)4p$	$a^{3}P - {}^{1}P^{\circ}$	0 - 1		661
	100	777.181	52.5320 - 181.2034	$3d^{*} - 3d^{7}(b^{2}D)4p$	a'S - 'P°	0 - 1		661
	500	778.806	14.0316 - 142.43395	$3d^{8} - 3d^{7}(a^{2}D)4p$	$a^{1}D - {}^{1}D^{\circ}$	2 - 2		661
	30	780.572	16.9778 - 145.08845	$3d^{8} - 3d^{7}(a^{2}D)4p$	a ³ P – ³ P°	1 – 0		661
	50	781.486	16.6616 - 144.62455	$3d^{8} - 3d^{7}(a^{2}D)4p$	a ³ P - ³ P°	2 - 1		661
	30	783.419	2.2696 - 129.91310	$3d^{8} - 3d^{7}(a^{4}P)4p$	ga ³ F - ⁵ D°	2 – 2		661
					1			
	200	785.020	14.0316 - 141.41410	3d [*] – 3d [*] (a ² P)4p	a'D - 'P'	2 - 1		661
	20	786.145	16.6616 - 143.86480	3d° – 3d′(a²D)4p	a'P - 'F'	2-3		661
	300	788.039	16.6616 - 143.56016	$3d^{n} - 3d^{n}(a^{*}D)4p$	a P - P	2 - 2		001
	200	788.298	14.0316 - 140.88540	$3d^{\circ} - 3d'(a^{2}D)4p$	a'D - F'	2 - 2		661
	20	790.000	16.9778 - 143.56016	$3d^{2} - 3d^{2}(a^{2}D)4p$	a'P - 'P'	1-2		661
	20	790.450	14.0316 - 140.54452	3d" - 3d'(a²D)4p	a'D – 'F'	2 - 3		661
	30	797 092	16 9778 - 142 43395	$3d^8 - 3d^7(e^2D)4n$	$a^{3}P = {}^{1}D^{9}$	1_2		661
	2	798 572	14 0316 - 130 25370	$3d^{8} - 3d^{7}(a^{2}D)Ap$	$a^{1} - D^{2}$	2 2		661
	100	800 332	14.0316 - 138.97920	$3d^{2} - 3d(a^{2}D)Ap$	aD - D	2 - 2		661
	20	801.145	14.0316 - 138.85220	$3d^{8} - 3d^{7}(a^{2}H)An$		2 - 1		661
	100	801 501	16.6616 - 141.41410	$3d^8 - 3d^7(a^2D)A_{P}$		2-3		661
	200	803.400	14 0316 - 139 49740	3u = 3u (a + 7) + p $3d^8 = 3d^7 (a^2 T) / 4 =$		2-1		661
	20	003.490	14.0310 - 138.46740	5u – 5u (a-12)4p	a D - D	2-3		001
	3	803.612	16.9778 - 141.41410	3d ⁸ − 3d ⁷ (a ² P)4p	a ³ P – ¹ P°	1-1		661
	200	805.007	16.6616 - 140.88515	$3d^8 - 3d^7(a^2P)4n$	$a^{3}P - {}^{3}S^{\circ}$	2 - 1		661
	20	805,263	17.2307 - 141.41410	$3d^8 - 3d^7(a^2P)4n$	a ³ P ~ ¹ P°	0-1		661
	100	807.055	16 9778 - 140 88515	$3d^8 = 3d^7(a^2 \mathbf{P})4\mathbf{n}$	a ³ P_ ³ S°	1_1_1		661
	30	807.213	16 6616 - 140 54452	$3d^{8} = 3d^{7}(a^{2}D)4n$	$a^{3}P = {}^{3}F^{\circ}$	2_2	1	661
	10	808 711	17 2307 - 140 88515	$3d^8 = 3d^7(a^2 \mathbf{D}) \Delta \mathbf{n}$	a ³ D_ ³ S ^o	0-1		661
	10	300.711	17.2507 - 140.00515	Ju → Ju (a r)+p	a1 - 5	0-1		001

NI III - Continued

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Aultiplet	Rel. Int.	$\lambda_{\rm vac}$ (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	Reference
	500	811.568	23.1087 - 146.32580	3d ⁸ - 3d ⁷ (a ² H)4p	a'G - 'H°	4-5		661
	10	813.426	14.0316 - 136.96700	$3d^8 - 3d^7(a^2P)4p$	$a^{\dagger}D - {}^{3}D^{\circ}$	2 - 3		661
	5	815.718	16.6616 - 139.25370	$3d^8 - 3d^7(a^2D)4p$	$a^{3}P - {}^{3}D^{\circ}$	2 - 2		661
	5	817 544	16 6616 - 138 97920	$3d^8 - 3d^7(a^2D)4p$	$a^{3}P - {}^{3}D^{\circ}$	2 - 1		661
	20	817 833	16.0010 - 130.07920 16.9778 - 139.25370	$3d^8 - 3d^7(a^2D)4p$	$a^{3}P - {}^{3}D^{\circ}$	1-2		661
1	1	818.389	16.6616 - 138.85220	$3d^8 - 3d^7(a^2H)4p$	$a^{3}P - {}^{3}G^{\circ}$	2 - 3		661
1	10	810.227	14 0316 136 00870	3d ⁸ 3d ⁷ (a ⁴ D)4n	a ¹ D ³ P°	2 - 1		661
ļ	10	819.237	14.0310 - 130.03870	$3d^8 - 3d(a r) + p$	aD = 1 $a^{3}D^{-3}D^{-3}$	2 - 1		661
1	50	819.005	16.616 128.49740	3d = 3d (a D) 4p	$a \mathbf{r} = \mathbf{D}$	1-1		661
	50	820.851	10.0010 - 138.48740	$3d = 3d (a^2D)^4p$	$a^{3}P = D$	2-3		661
	15	821.373	17.2307 - 138.97920	$3d^{2} - 3d^{2}(a^{2}D)4p$	$a^{P} - D$	0-1		001
	20	824.292 824.850	14.0316 - 135.35033	3d" - 3d'(a'P)4p	a'D - "P"	2 - 2		661 661
				218 217 2014				
	10	825.300	16.9778 – 138.14648	3d° - 3d'(a²P)4p	a'P - 'S'	1 – 0		661
1	500	826.138	23.1087 - 144.15300	3d* - 3d'(a ² H)4p	a'G – 'G°	4 - 4		661
	200	826.501	14.0316 - 135.02320	$3d^8 - 3d^7(a^2G)4p$	a'D - 'F°	2 – 3		661
	2	827.792	82.27726 - 203.07846	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{4}F)5p$	³ D - ⁵ D°	1-0		661
	100	828.109	23.1087 - 143.86480	$3d^8 - 3d^7(a^2D)4p$	a ⁱ G – ⁱ F°	4 – 3		661
1	3	828.491	16.6616 - 137.36236	$3d^{8} - 3d^{7}(a^{2}P)4p$	$a^{3}P - {}^{3}D^{\circ}$	2 - 1		661
	10	830.666	16.9778 - 137.36236	$3d^{8} - 3d^{7}(a^{2}P)4p$	$a^{3}P - {}^{3}D^{\circ}$	1 - 1		661
1	100	831.229	16.6616 - 136.96700	$3d^8 - 3d^7(a^2P)4p$	$a^{3}P - {}^{3}D^{\circ}$	2 - 3		661
	5	831.487						661
	5	832 284	16 6616 - 136 81320	$3d^8 - 3d^7(a^2P)4p$	$a^{3}P - {}^{3}D^{\circ}$	2 - 2		661
	20	834.058	10.0010 - 150.01520 23 1087 - 143 00270	$3d^8 - 3d^7(a^2H)4n$	$a^{1}G = {}^{3}H^{\circ}$	4 - 4		661
	20	837.025	14.0316 - 133.50097	$3d^{8} - 3d^{7}(a^{4}P)4p$	$a^{1}D - {}^{3}D^{\circ}$	2 - 2		661
	50	997.944	14 4414 124 00070	2.48 2.47(-47) 4-	-3D 3D*	1 2 1		661
	50	837.200	16.6616 - 136.09870	3d - 3d (a P) + p	ar - r	2-1		661
	5	839.478	16.9778 - 136.09870	3d" - 3d'(a'P)4p		1-1		001
	20	841.256	17.2307 - 136.09870	3d* - 3d'(a*P)4p	a P - P	0 - 1		661
	2	841.825	82.17260 - 200.96297	3d'(a ² D)4s - 3d'(a ⁴ F)5p	'D - 'F°	3 - 3		661
3	500	842.142	0.0 - 118.74525	$3d^{k} - 3d^{7}(a^{4}F)4p$	ga'F - 'D°	4 – 3		661
	50	842.546	16.6616 - 135.35033	3d ⁸ - 3d ⁷ (a ⁴ P)4p	$a^{3}P - {}^{3}P^{\circ}$	2 – 2		661
	50	844.787	16.9778 - 135.35033	3d [*] - 3d ⁷ (a ⁴ P)4p	$a^{3}P - {}^{3}P^{\circ}$	1 - 2		661
	100	844.859	16.6616 - 135.02320	$3d^8 - 3d^7(a^2G)4p$	$a^{3}P - F^{\circ}$	2 - 3		661
3	400	845.242	1.3607 - 119.66954	$3d^8 - 3d^7(a^4F)4p$	$ga^{3}F - {}^{3}D^{\circ}$	3 – 2		661
3	300	847.433	2.2696 - 120.27232	$3d^8 - 3d^7(a^4F)4p$	$ga^{3}F - {}^{3}D^{\circ}$	2 - 1		661
-	5	849.810	16.6616 - 134.33479	$3d^{*} - 3d^{7}(a^{2}G)4p$	$a^{3}P - {}^{3}G^{\circ}$	2 - 3		661
	15	851.521	23.1087 - 140.54452	$3d^8 - 3d^7(a^2D)4p$	$a^1G - {}^3F^{\bullet}$	4 - 3		661
1	15	851 788	2 2696 - 119 66954	3d ⁸ - 3d ⁷ (a ⁴ F)4p	$ga^{3}F - {}^{3}D^{\circ}$	2 - 2		661
2	10	852 867	0.0 - 117.25080	$3d^8 - 3d^7(a^4F)4p$	$ga^3F - F^{\circ}$	4 - 3		661
2	5	853 308	16 6616 - 133 83954	$3d^8 - 3d^7(a^4P)4n$	$a^{3}P - {}^{3}D^{\circ}$	2-1		661
	2	855 710	16.0010 - 133.03954 16.0778 - 133.83954	$3d^8 - 3d^7(a^4P)4n$	$a^{3}P - {}^{3}D^{\circ}$	1_1_1		661
	100	855 022	14 0216 120 86250	$3d^8 - 3d^7(a^4 P)A_P$	$a^{\dagger}D = 3S^{\circ}$	1 - 1 2 - 1		661
2	50	855.506	1.3607 – 118.11495	$3d^{8} - 3d^{7}(a^{4}F)4p$	$a^3F - {}^3F^\circ$	3 - 2		661
	50	056 694	16 6616 122 20004	2.48 2.4 ⁷ (o ⁴ D)4m	• ³ D ³ D*	1 2 2		661
	200	850.084	10.0010 - 135.35054	3d = 3d (a r) + p $2d^8 = 2d^7 (a^4 F) + p$	$a \Gamma = D$			661
1	200	857.087	0.0 - 110.07439	$3d^2 - 3d(ar)4p$	gar - O	4-4		661
	50	857.550	1/.2307 - 133.83934	3d = 3d (a P)4p		1 1 2		661
	20	858.198	16.9778 - 133.50097	3d - 3d (a P)4p	a' P = D	1-2		601
	20 20	858.861 859.387	16.6616 - 133.09589 16.9778 - 133.33970	$3d^{8} - 3d^{7}(a^{4}P)4p$ $3d^{8} - 3d^{7}(a^{4}P)4p$	$a^{3}P - {}^{5}P^{\circ}$	1-1		661
					300 3000			
	50	859.854	16.9778 - 133.27670	3d° - 3d'(a'P)4p	a'P - 'P'	1-1		001
1	150	860.238	1.3607 - 117.60635	3d° - 3d'(a*F)4p	ga F - G	3-3		001
2	300	860.642	0.0 - 116.19193	3d* - 3d ⁷ (a*F)4p	ga'F - 'F°	4-4		661
	10	860.905	16.6616 - 132.81826	3d ⁸ - 3d ⁷ (a ⁴ P)4p	a'P - 5P°	2 - 2		661
2	300	862.882	1.3607 - 117.25080	$3d^8 - 3d^7(a^4F)4p$	ga'F – 'F°	3 - 3		661

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NI III - Continued

Multiplat	Pal Int) (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Tarms	тт	Notes	Pafarancas
Multiplet	Kel. Int.	Avac (III A)	Levels (III 10 Ciff 7)	Configurations	Terms	J - J	Notes	Kelerences
1	50	867.023	2.2696 - 117.60635	3d ⁸ – 3d ⁷ (a ⁴ F)4p	$ga^{3}F - {}^{3}G^{\circ}$	2 – 3		661
1	100	867.194	1.3607 - 116.67439	3d ⁸ - 3d ⁷ (a ⁴ F)4p	ga ³ F - ³ G°	3 – 4		661
1	300	867.508	0.0 - 115.27226	$3d^{8} - 3d^{7}(a^{4}F)4p$	$ga^{3}F - {}^{3}G^{\circ}$	4 - 5		661
2	200	869.702	2.2696 - 117.25080	$3d^8 - 3d^7(a^4F)4p$	$ga^{3}F - {}^{3}F^{\circ}$	2 – 3		661
	10	869.926	23.1087 - 138.06040	$3d^8 - 3d^7(a^2H)4p$	$a^1G - {}^3I^\circ$	4 - 5		661
2	200	870.845	1.3607 - 116.19193	$3d^8 - 3d^7(a^4F)4p$	$ga^{3}F - {}^{3}F^{\circ}$	3 - 4		661
					-			
	150	875.641	16.6616 - 130.86350	3d ⁸ – 3d ⁷ (a ⁴ P)4p	$a^{3}P - {}^{3}S^{\circ}$	2 – 1		661
		877.852	23.1087 - 137.02020	$3d^8 - 3d^7(a^2H)4p$	a ¹ G - ³ G°	4 - 5		661
	30	878.078	16.9778 - 130.86350	$3d^8 - 3d^7(a^4P)4p$	$a^{3}P - {}^{3}S^{\circ}$	1 - 1		661
	50	879.471	0.0 - 113.70512	$3d^8 - 3d^7(a^4F)4p$	ga ³ F - ⁵ G°	4 - 4		661
	20	880.028	17.2307 - 130.86350	$3d^8 - 3d^7(a^4P)4p$	$a^{3}P - {}^{3}S^{\circ}$	0 - 1		661
	20	882.642	16.6616 - 129.95795	$3d^8 - 3d^7(a^4P)4p$	$a^{3}P - {}^{5}D^{\circ}$	2 - 1		661
	50	883.849	0.0 - 113.14092	$3d^8 - 3d^7(a^4F)4p$	ga ³ F - ⁵ G°	4 - 5		661
	3	885,103	16.9778 - 129.95795	$3d^8 - 3d^7(a^4P)4p$	$a^{3}P - {}^{5}D^{\circ}$	1-1		661
	2	885 455	0.0 - 112.93543	$3d^8 - 3d^7(a^4F)4n$	$ga^{3}F = {}^{5}D^{\circ}$	4-3		661
	10	886 924	13607 - 11411020	$3d^8 - 3d^7(a^4F)4p$	$ga^{3}F = {}^{5}G^{\circ}$	3_3		661
	5	890 131	1 3607 - 113 70512	$3d^8 - 3d^7(a^4F)Ap$	$ga^{3}F = G^{\circ}$	3-3		661
	2	892 041	2 2696 114 37101	$3d^8 - 3d^7(a^4E)/a^{10}$	gal - G	3-4		661
	,	392.041	2.2090 - 114.37101	50 – 50 (a 17)4p	gal - G	2-2		001
	50	893 533	23 1087 - 135 02320	$3d^8 - 3d^7(a^2G)4n$	$a^{1}G - {}^{1}F^{\circ}$	4 - 3		661
	100	900.008	23,1087 - 134,21760	$3d^8 - 3d^7(a^2G)Ap$	alG IH	4 5		661
	50	904.204	23.1087 133.69200	$3d^8 - 3d^7(a^2G)4p$		4-5		661
12	20	969 100	16 0778 120 27222	$3d^{2} - 3d(a^{2}G)4p$		4-5		661
13	20	908.100	10.9778 - 120.27232	$3d^{2} - 3d(ar)/4p$	a P - D	1-1		001
13	30	970.478	17.2307 - 120.27232	$3d^{2} - 3d^{2}(a^{2}F)4p$	$a^{T}P - D^{T}$	0-1		001
15	20	970.790	10.0010 - 119.00934	3d" - 3d (a'F)4p	a"P - "D"	2-2		001
13	300	973 786	16 9778 - 119 66954	$3d^8 - 3d^7(a^4 E)4p$	a ³ P - ³ D ^o	1 . 2		661
13	400	979 589	16 6616 - 118 74525	$3d^8 - 3d^7(a^4E)Ap$	$a^{3}P - ^{3}D^{\circ}$	1 - 2 2 3		661
15	100	1205 244	53 70303 130 31230	3u - 3u (a T) + p $2d^{7}(a^{4}E)Aa - 2d^{7}(a^{4}P)Aa$		2-3		661
	100	1305.344	55.70393 - 150.51250	50 (a r)48 - 50 (a r)4p	F - D	5 - 4		001
	10	1313.085	54 (5792 120 21220	2 476 455 4 2 476 455 4	55 550			001
	10	1321.804	54.65785 - 150.51250	3d(a'r)4s - 3d(a'r)4p	F = D	4 - 4	-	001
		1521.94	0.0 - 75.04001	3d - 3d (a G)4s	ga F – G	4 - 4	F,P	375,1108
	75	1328.084	54.65783 - 129.95400	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}P)4p$	⁵ F - ⁵ D°	4 - 3		661
	2	1330.787						661
		1331.14	0.0 - 75.12365	$3d^8 - 3d^7(a^2G)4s$	$ga^{3}F - {}^{3}G$	4 - 5	F.P	375,1108
	3	1331.153	81.68680 - 156.80870	$3d^{7}(a^{2}H)4s - 3d^{7}(a^{2}F)4p$	³ H - ³ G°	6 - 5	- ,-	661
		1335.53	1.3607 - 76.23725	$3d^8 - 3d^7(a^2G)4s$	$ga^{3}F - {}^{3}G$	3-3	F.P	375,1108
	10	1341.421	55.40629 - 129.95400	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}P)4p$	⁵ F - ⁵ D°	3 - 3	- ,-	661
	50	1342.148	55.40629 - 129.91310	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}P)4p$	${}^{5}\mathbf{F} - {}^{5}\mathbf{D}^{\circ}$	3 - 2		661
		1346.15	1.3607 - 75.64661	$3d^8 - 3d^7(a^2G)4s$	$ga^{3}F - {}^{3}G$	3 - 4	F,P	375,1108
	30	1351.256	55.95221 - 129.95795	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}P)4p$	⁵ F - ⁵ D°	2 - 1	,-	661
		1351.94	2.2696 - 76.23725	$3d^8 - 3d^7(a^2G)4s$	$ga^{3}F - {}^{3}G$	2 - 3	F.P	375.1108
	20	1352.052	55.95221 - 129.91310	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}P)4p$	⁵ F - ⁵ D°	2 - 2	- /-	661
	20	1353.512	56.30824 - 130.19005	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}P)4p$	⁵ F - ⁵ D°	1 - 0		661
		1355.69	1.3607 - 75.12365	$3d^8 - 3d^7(a^2G)4s$	$ga^{3}F - {}^{3}G$	3 - 5	F,P	375,1108
	50	1357.802	56.30824 - 129.95795	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}P)4p$	⁵ F - ⁵ D°	1 - 1		661
	3	1362.783						661
		1362.82	2.2696 - 75.64661	$3d^8 - 3d^7(a^2G)4s$	$ga^{3}F - {}^{3}G$	2 - 4	F.P	375.1108
	10	1365.151	110.21280 - 183.46488	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ F° - ⁵ D	5 - 4	,-	661
	5	1374.491						661
	10	1374.660	112.40165 - 185.14723	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ F° – ⁵ D	1 - 0		661
	15	1376.183	112.40165 - 185.06715	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ F° – ⁵ D	1 - 2		661
	15	1377.077	82.82640 - 155.44330	$3d^{7}(a^{2}H)4s - 3d^{7}(a^{2}F)4p$	${}^{3}H - {}^{3}G^{\circ}$	4 - 3		661
	10	1382.077	111.22120 - 183.57558	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ F° – ⁵ P	3 - 2		661
	3	1387.870	61.33858 - 133.39094	3d7(a4F)4s - 3d7(a4P)4p	${}^{3}\mathbf{F} - {}^{3}\mathbf{D}^{\circ}$	4 - 3		661
	5	1388.629						661
					1	1	1	

NI III - Continued

Multiplet	Rel. Int.	$\lambda_{\rm vac}$ (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	1	1389.149	61.33858 - 133.32470	3d7(a4F)4s - 3d7(a2G)4p	${}^{3}\mathbf{F} - {}^{1}\mathbf{G}^{\circ}$	4 - 4		661
	20	1389.735	110.37135 - 182.32713	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ F° – ⁵ G	4 – 5		661
	30	1392.377	111.22120 - 183.04145	3d ⁷ (a ⁴ F)4p - 3d ⁷ (a ⁴ F)4d	⁵ F° – ⁵ G	3 - 4		661
	10	1395.459	111.91453 - 183.57558	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ F [°] – ⁵ P	2 – 2		661
	15	1401.214	111.22120 - 182.58783	3d ⁷ (a ⁴ F)4p - 3d ⁷ (a ⁴ F)4d	⁵ F° – ⁵ F	3 - 2		661
	15	1403.113	110.21280 - 181.48295	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ F° – ⁵ F	5 – 4		661
	10	1405.279	116.19193 - 187.35188	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	${}^{3}\mathbf{F}^{\circ} - {}^{3}\mathbf{F}$	4 - 4		661
	10	1405.421	111.89865 - 183.05220	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ D° - ³ G	4 - 5		661
	3	1406.061	111.91453 - 183.03525	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ F° – ⁵ F	2 - 1		661
	50	1406.250	110.37135 - 181.48295	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	${}^{5}F^{\circ} - {}^{5}F$	4 – 4		661
	15	1409.000	114.09560 - 185.06715	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ D° – ⁵ D	1 – 2		661
	2	1409.471						661
	5	1409.974	112.93543 - 183.85972	3d ⁷ (a ⁴ F)4p - 3d ⁷ (a ⁴ F)4d	⁵ D° – ³ G	3 - 4		661
	10	1410.126	157.37542 - 228.29097	$3d^{7}(a^{2}F)4p - 3d^{7}(a^{4}F)6s$	³ G° – ³ F	4 - 3		661
	15	1410.344	112.93543 - 183.83947	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	${}^{5}D^{\circ} - {}^{3}D$	3 - 3		661
	3	1410.446	111.89865 - 182.79820	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)5s$	⁵ D° - ⁵ F	4 - 4		661
	5	1410.642	117.25080 - 188.14054	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	${}^{3}F^{\circ} - {}^{3}F$	3 - 3		661
	50	1412.304	110.21280 - 181.01908	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ F° – ⁵ F	3 - 5		661
	5	1413.211	63.47193 - 134.23190	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{2}G)4p$	${}^{3}\mathbf{F} - {}^{3}\mathbf{F}^{\circ}$	2 - 2		661
	3	1413.938	113.65147 - 184.37568	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ D° - ⁵ P	2 – 1		661
	20	1414.389	112.93543 - 183.63776	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ D° – ⁵ G	3 - 3		661
	15	1414.916	155.44330 - 226.11880	$3d^{7}(a^{2}F)4p - 3d^{7}(a^{4}F)5d$	³ G° - ⁵ F	3-4		661
	3	1415.467	110.37135 - 181.01908	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ F° - ⁵ F	4-5		661
	5	1415.909	111.89865 - 182.52469	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ D ° – ⁵ P	4 - 3		661
	75	1416.956	114.37101 - 184.94495	$3d^{2}(a^{4}F)4p - 3d^{2}(a^{4}F)4d$	⁵ G° - ⁵ H	2 - 3		661
	2	1417.249						661
	2	1417.387	62.60558 - 133.15850	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{2}G)4p$	${}^{3}F - {}^{3}F^{\circ}$	3 - 3		661
	20	1417.736	117.60635 - 188.14054	$3d^{2}(a^{4}F)4p - 3d^{2}(a^{4}F)4d$	${}^{3}G^{\circ} - {}^{3}F$	3 - 3		661
	10	1417.841	112.93543 - 183.46488	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ D° – ⁵ D	3 – 4		661
	3	1418.105						661
	5	1418.292	118.11495 - 188.62287	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	${}^{3}F^{\circ} - {}^{3}F$	2 - 2		661
	10	1419 382	61.33858 - 131.79202	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{2}G)4p$	${}^{3}\mathbf{F} - {}^{3}\mathbf{F}^{\circ}$	4 - 4		661
	75	1420 448	114 11020 - 184 51075	$3d^{7}(a^{4}E)4n = 3d^{7}(a^{4}E)4d$	°G° - [°] H	3-4		661
	10	1421 082	114.11020 104.51075	su (u i) p su (u i) iu				661
	2	1422.002	156 97208 - 227 28870	$3d^{7}(a^{2}E)4n = 3d^{7}(a^{4}E)6s$	${}^{3}F^{\circ} - {}^{5}F$	4-4	· .	661
	10	1423 722	$114\ 37101 - 184\ 60957$	$3d^{7}(a^{4}F)4p = 3d^{7}(a^{4}F)5s$	5G° - 5F	2 - 1		661
	10	1423.722	11.07101 10.00507	54 (41) (p 54 (41) 55				
	100	1424.511 1425 737	113.70512 - 183.90488	3d ⁷ (a ⁴ F)4p - 3d ⁷ (a ⁴ F)4d	⁵ G° – ⁵ H	4 – 5		661 661
	5	1427.087	153,25635 - 223,32977	3d ⁶ 4s ² - 3d ⁷ (a ⁴ Fsc))4f	⁵ D - ∜[⁷]°	4 - 3		661
	20	1427 639			- 121			661
	3	1427.914						661
	200	1428.870	113.14092 - 183.12619	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ G° – ⁵ H	5 - 6		661
	10	1430 438	113.70512 - 183.61267	$3d^{2}(a^{4}E)4p - 3d^{2}(a^{4}E)5s$	⁵ G° - ⁵ F	4 - 3		661
	10	1430.630						661
	30	1434.133	114.11020 - 183.83947	$3d^{2}(a^{4}F)4p - 3d^{2}(a^{4}F)4d$	⁵ G° - ³ D	3-3		661
	200	1434.306	112.78785 - 182.50830	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ G° – ⁵ H	6 - 7	1	661
	2	1434,446						661
	10	1435.609	113.14092 - 182.79820	3d7(a4F)4p - 3d7(a4F)5s	⁵ G° - ⁵ F	5 – 4		661
	2	1438 152	115,27226 - 184,80562	$3d^{7}(a^{4}F)4p = 3d^{7}(a^{4}F)4d$	³ G° – ³ H	5-5		661
	20	1439.809	11112.220 101.00002					661
	3	1439.938	116,19193 - 185,63913	$3d^{7}(a^{4}F)4p = 3d^{7}(a^{4}F)4d$	${}^{3}F^{\circ} - {}^{3}H$	4 - 4		661
	2	1441 159	110.17175 - 105.05715	50 (a 1)+p - 50 (a 1)+0		7 = 4		661
	5	1442 235	113 70512 - 183 04145	$3d^{7}(a^{4}F)4n = 3d^{7}(a^{4}F)4d$	'G' - 'G	4_4		661
	40	1445 374	62 60558 - 131 79202	$3d^{7}(a^{4}F)4s = 3d^{7}(a^{2}G)4r$	${}^{3}\mathbf{F} - {}^{3}\mathbf{F}^{\circ}$	3-4		661
	+0	1775.577	02.00550 - 151.77202	50 (a 1)+5 - 50 (a 0)+p		5 - 4		

NI III - Continued

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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	2	1446.154						661
35	15	1446.748	111.89865 - 181.01908	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	⁵ D° – ⁵ F	4 - 5		661
	30	1448.175	112.78785 - 181.84000	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	5G° – 5G	6-6		661
	200	1451.504	115.27226 - 184.16657	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	³ G° - ³ H	5 - 6		661
	20	1452 532				-		661
	20	1453.603						661
	50	1453.882						661
	10	1457,430	116 19193 - 184 80562	$3d^{7}(a^{4}E)4p = 3d^{7}(a^{4}E)4d$	³ F° – ³ H	4 - 5		661
	10	1457 575	118,74525 - 187,35188	$3d^{7}(a^{4}E)4p = 3d^{7}(a^{4}E)4d$	³ D° – ³ F	3-4		661
	50	1457 820	110.74525 - 187.55188	50 (a 1)+p = 50 (a 1)+0		J - 4		661
	50	1457.027	116 67420 195 24915	$2d^{7}(a^{4}E)An = 2d^{7}(a^{4}E)Sa$	C° F	4 2		661
	10	1438.284	110.07439 - 183.24813	3d(a r) + p - 3d(a r) - 3s		4-3		661
	10	1401.049	101.75489 - 250.10990	50 (a'r)4p - 50 (a'r)50	r - r	3-4		501
	5	1462.239	117.25080 - 185.63913	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	³ F° – ³ H	3 - 4		661
	2	1464.778	120.27232 - 188.54282	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	${}^{3}D^{\circ} - {}^{3}P$	1 – 1		661
	5	1464.989						661
36	10	1465.606	112.78785 - 181.01908	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	5G° - 5F	6 - 5		661
	5	1466 027				1		661
	5	1466.156						661
	3	1469.836						661
	2	1470 642	117 25080 - 185 24815	$3d^{7}(a^{4}E)4n = 3d^{7}(a^{4}E)5e$	³ E° – ³ E	3 - 3		661
	2	1471 468	118 11495 - 186 07340	$3d^{7}(a^{4}E)4p = 3d^{7}(a^{4}E)5s$	$^{3}\mathbf{F}^{\circ} - ^{3}\mathbf{F}$	2_2		661
	5	1471.400	116 19193 - 184 03762	$3d^{7}(a^{4}E)Ap = 3d^{7}(a^{4}E)Se$	3 E° 3 E	1 1		661
	5	1473.939	110.66054 197.40339	3d(aT) + p = 3d(aT) + 3s $3d^{2}(a^{4}E) + a^{2}d^{2}(a^{4}E) + d^{2}d^{2}$	3D° 3D	2 2		661
27	15	1474.402	115 27226 192 05220	3d(a T) + p = 3d(a T) + d $2d^{7}(a^{4}E) A = 2d^{7}(a^{4}E) A d$		2-2		661
37	15	1473.308	115.27220 ~ 185.05220	50 (a r)+p - 50 (a r)+0	0 - 0	3-3		001
	5	1475.662						661
	3	1476.527						661
38	10	1477.801	116.19193 - 183.85972	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	³ F° – ³ G	4 - 4		661
	10	1478.252	116.19193 - 183.83947	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	${}^{3}F^{\circ} - {}^{3}D$	4 - 3		661
	10	1478.854						661
	5	1481.923						661
	10	1483.044	118.11495 - 185.54370	3d ⁷ (a ⁴ F)4p - 3d ⁷ (a ⁴ F)4d	${}^{3}\mathbf{F}^{\circ} - {}^{3}\mathbf{D}$	2 - 1		661
	3	1484.268	117.25080 - 184.62354	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	${}^{3}F^{\circ} - {}^{3}D$	3 - 2		661
	3	1486.456						661
37	3	1488.424	116.67439 - 183.85972	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	${}^{3}G^{\circ} - {}^{3}G$	4 - 4		661
	1	1491.111	75.12365 - 142.18780	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{2}H)4p$	³ G - ³ H°	5-6		661
	2	1491.309	115.27226 - 182.32713	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	3G° - 3G	5 - 5		661
	10	1491.899						661
	30	1492.622						661
	30	1492.990						661
38	20	1495.641	116.19193 - 183.05220	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	${}^{3}F^{\circ} - {}^{3}G$	4 - 5		661
	5	1498.338	117.60635 - 184.34650	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	³ G° - ³ G	3-3		661
	3	1501.063			- 0			661
38	5	1501 311	117 25080 - 183 85972	$3d^{7}(a^{4}E)4n = 3d^{7}(a^{4}E)4d$	³ F° - ³ G	3-4		661
20	2	1503 850	111.20000 105.05712	50 (a1) ip 50 (a1) iu	1 0	5-4		661
	5	1505.050						661
27	1	1506 519	116 67420 182 05220	$2d^{7}(a^{4}E)A = 2d^{7}(a^{4}E)Ad$		4 5	i i	661
37	10	1500.516	116.07439 - 183.03220	3d(a'r)4p - 3d(a'r)4d		4-5		001
	10	1512.040	110.19193 - 182.32713	$3d^{2}(a^{2}F)4p = 3d^{2}(a^{2}F)4d$	F - G	4-5		661
	2	1324.891	119.00934 - 183.24813	30 (a'r)4p - 30 (a'r)3s	"D - "F	2-3		001
	5	1526.305						661
	3	1529.096	119.66954 - 185.06715	$3d'(a^{4}F)4p - 3d'(a^{4}F)4d$	'D° - 'D	2 – 2		661
	5	1536.246	118.74525 - 183.83947	$3d^{7}(a^{4}F)4p - 3d^{7}(a^{4}F)4d$	³ D° - ³ D	3 - 3		661
	50	1540.759	79.25011 - 144.15300	3d ⁷ (a ² G)4s - 3d ⁷ (a ² H)4p	¹ G - ¹ G°	4 - 4		661
	20	1547.641	79.25011 - 143.86480	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{2}D)4p$	${}^{1}G - {}^{1}F^{\circ}$	4 - 3		661
	10	1552.365	79.14301 - 143.56016	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{2}D)4p$	${}^{3}\mathbf{P} - {}^{3}\mathbf{P}^{\circ}$	2 – 2		661
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NI III -- Continued

Multiplet	Rel. Int.	λ _{νac} (in Å)	Levels (in 10^3 cm $^{-1}$)	Configurations	Terms	J - J	Notes	Reference
	2	1555.598	71.06735 - 135.35033	3d7(a4P)4s - 3d7(a4P)4p	⁵ P - ³ P°	3 - 2		661
	3	1568.269						661
	5	1568.569	79.25011 - 143.00270	3d ⁷ (a ² G)4s - 3d ⁷ (a ² H)4p	¹ G ~ ³ H°	4 – 4		661
		1575.50	0.0 - 63.47193	3d ⁸ – 3d ⁷ (a ⁴ F)4s	ga ³ F - ³ F	4 – 2	F,P	375,1108
	15	1579.999	79.14301 - 142.43395	3d ⁷ (a ² P)4s - 3d ⁷ (a ² D)4p	³ P – ¹ D°	2 – 2		661
	1	1586.909	76.23725 - 139.25370	3d ⁷ (a ² G)4s - 3d ⁷ (a ² D)4p	³ G – ³ D°	3 – 2		661
	2	1589.625	75.12365 - 138.03090	3d7(a2G)4s - 3d7(a2H)4p	³ G - ³ G°	5-4		661
	3	1597.077	76.23725 - 138.85220	3d7(a2G)4s - 3d7(a2H)4p	${}^{3}G - {}^{3}G^{\circ}$	3 – 3	i i	661
		1597.30	0.0 - 62.60558	$3d^{*} - 3d^{7}(a^{4}F)4s$	ga ³ F - ³ F	4 - 3	F,P	375,1108
	3	1597.899	78.30354 - 140.88515	3d7(a4P)4s - 3d7(a2P)4p	${}^{3}P - {}^{3}S^{\circ}$	2 – 1		661
	15	1598.073	71.06735 - 133.64258	3d7(a4P)4s - 3d7(a2P)4p	⁵ P - ³ P°	3 - 2		661
	10	1600.294	53.70393 - 116.19193	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	⁵ F - ³ F °	5 - 4		661
	2	1601.025	121.41160 - 183.87200	$3d^{7}(b^{2}D)4s - 3d^{7}(b^{2}D)4p$	${}^{3}\mathbf{D} - {}^{3}\mathbf{D}^{\circ}$	2 - 2		661
	15	1602.505	78.48243 - 140.88515	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{2}P)4p$	${}^{3}\mathbf{P} - {}^{3}\mathbf{S}^{\circ}$	1 - 1	i 1	661
	300	1604.537	71.06735 - 133.39094	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{4}P)4p$	⁵ P - ³ D ^o	3 - 3		661
	5	1607.000	78.65755 - 140.88515	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{2}P)4p$	${}^{3}P - {}^{3}S^{\circ}$	0 - 1		661
	100	1609.876	71.38410 - 133.50097	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{4}P)4p$	⁵ P - ³ D ^o	2 - 2		661
		1610.01	1.3607 - 63.47193	$3d^{*} - 3d^{7}(a^{4}F)4s$	ga ³ F - ³ F	3 - 2	F,P	375,1108
	20	1610 534	71 06735 - 133 15850	$3d^{7}(a^{4}P)4s = 3d^{7}(a^{2}G)4n$	⁵ P - ³ F°	3_3		661
	30	1612 165	71.06735 - 133.09589	$3d^{7}(a^{4}P)As = 3d^{7}(a^{4}P)An$	5P_5P	3_3		661
17	10	1612.105	54 65783 - 116 67439	$3d^{7}(a^{4}F)4s = 3d^{7}(a^{4}F)4n$	5 - 3 C°			661
17	30	1612 730	71 38410 - 133 39094	$3d^{7}(a^{4}P)Aa = 3d^{7}(a^{4}P)Ap$	5P 3D*	2 2		661
	1	1612.750	71 84242 133 83054	$3d^{7}(a^{4}P)Aa = 3d^{7}(a^{4}P)Ap$		2-3		661
	2	1615.597	75.12365 - 137.02020	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{2}H)4p$	³ G - ³ G°	5 - 5		661
	15	1619 127	71 94242 122 64250	2d7(afD)4a 2d7(a2D)4a	5D 3D*			(()
	20	1618 801	71 39410 123 15950	3d(a r) 4s - 3d(a r) 4p $3d^{2}(a^{4}D) 4a - 3d^{2}(a^{2}C) 4p$	5D 3E°	1 - 2		661
	20	1619 414	71.06735 - 132.81826	3d(a + p) + s = 3d(a + p) + p $3d^{7}(a + p) + a = 3d^{7}(a + p) + p$	5D 5D°	2-3		661
	20	1619.414	70 14201 140 89515	3d(a r)48 - 3d(a r)4p $2d^{2}(a^{2}R)4a - 2d^{2}(a^{2}R)4a$		3 - 2		661
	100	1670.443	71 38410 123 00590	3d(ar) + 8 = 3d(ar) + p $3d^{2}(a^{4}P) + a = 3d^{2}(a^{4}P) + p$	5D 5D°	2-1		661
	50	1621.830	71.84242 - 133.50097	$3d^{2}(a^{4}P)4s - 3d^{2}(a^{4}P)4p$	⁵ P - ³ D°	1 - 2		661
17	50	1621.042	55 05221 117 60625	2d7(a4E)4a 2d7(a4E)4a	E C.			661
17	25	1621.942	55.95221 - 117.00055 92.03245 144.62455	3d(a r) 4s - 3d(a r) 4p $2d^{7}(a^{2}D) 4a - 2d^{7}(a^{2}D) 4a$		2-3	(i	001
17	33	1623.622	83.03345 - 144.62455	$3d^{2}(a^{2}D)4s = 3d^{2}(a^{2}D)4p$	D - P	2-1		001
17	20	1624.220	53./0393 - 115.2/226	3d(a'F)4s - 3d(a'F)4p	F - G	5-5		001
	100	1626.096	71.84242 - 133.33970	$3d'(a^{+}P)4s - 3d'(a^{+}P)4p$	$\mathbf{P} - \mathbf{P}^{*}$	1-1		661
	3	1627.751	71.38410 - 132.81826	$3d'(a^{*}P)4s - 3d'(a^{*}P)4p$	$^{3}P - ^{3}P^{*}$	2 - 2		661
	25	1029.000	82.1/200 - 143.30010	30 (a-D)45 - 30 (a-D)4p	D- P	3-2		001
	3	1630.120	84.60410 - 145.95015	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{2}D)4p$	$^{1}\mathbf{P} - ^{1}\mathbf{P}^{\circ}$	1 - 1		661
		1630.30	0.0 - 61.33838	$3d^{2} - 3d^{2}(a^{2}F)4s$	ga F - F	4-4	F,P	3/5,1108
	2	1630.602	82.82640 - 144.15300	$3d'(a^2H)4s - 3d'(a^2H)4p$	H - G	4-4		001
	2	1631.479	79.25011 - 140.54452	$3d'(a^{-}G)4s - 3d'(a^{-}D)4r$	'G - 'F'	4-3		661
17	100	1631.754	82.27726 - 143.56016 55.40629 - 116.67439	3d ⁷ (a ² D)4s - 3d ⁷ (a ² D)4p 3d ⁷ (a ⁴ F)4s - 3d ⁷ (a ⁴ F)4p	D - P 'F - 'G'	1 - 2 3 - 4		661 661
		1622.70	1 2607 (2 60550					
		1632.79	1.3007 - 62.60558	30" - 30'(a'F)4s	ga F - F	3-3	F,P	375,1108
		1633.92	2.2696 - 63.47193	$3d^{2} - 3d^{2}(a^{2}F)4s$	ga'F - 'F	2 - 2	F,P	375,1108
	3	1635./17	79.74922 - 140.88515	$3d'(a^2P)4s - 3d'(a^2P)4p$	$^{\circ}P - ^{\circ}S^{\circ}$	1-1		661
	25	1639.996	71.84242 - 132.81826	$3d'(a^{*}P)4s - 3d'(a^{*}P)4p$	P - P	1 - 2		661
	1	1644.466						661 661
17	100	1640 221		a 17/ 4mm a 17/ 4mm a				
17	100	1649.771	54.65783 - 115.27226	3d'(a*F)4s - 3d'(a*F)4p	'F - 'G°	4 – 5		661
	300	1652.866	81.08080 - 142.18780	3d'(a ⁻ H)4s – 3d'(a ⁻ H)4p	'Н – 'Н'	6 - 6		661
	200	1653.119	85.83420 - 146.32580	3d'(a'H)4s - 3d'(a'H)4p	'H - 'H°	5 - 5		661
	250	1656.126	82.19380 - 142.57560	$3d'(a^2H)4s - 3d'(a^2H)4p$	'H – 'H°	5 - 5		661
		1657.39	2.2696 - 62.60558	$3d^{8} - 3d^{7}(a^{4}F)4s$	ga 'F - 'F	2 - 3	F,P	375,1108

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NI III - Continued

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	200	1661.786	82.82640 - 143.00270	$3d^{7}(a^{2}H)4s - 3d^{7}(a^{2}H)4p$	$^{3}H - ^{3}H^{\circ}$	4 - 4		661
	1	1662.311	82.27726 - 142.43395	$3d^{2}(a^{2}D)4s - 3d^{2}(a^{2}D)4p$	${}^{3}D - {}^{1}D^{\circ}$	1 - 2		661
	20	1665.859				1	!	661
	20	1666.102	84.60410 - 144.62455	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{2}D)4p$	¹ P - ³ P°	1 - 1		661
	20	1666.828	82.19380 - 142.18780	$3d^{7}(a^{2}H)4s - 3d^{7}(a^{2}H)4p$	³ H - ³ H°	5-6		661
	2.	1667.28	1.3607 - 61.33858	$3d^8 - 3d^2(a^4F)4s$	$ga^{3}F - {}^{3}F$	3 - 4	F.P	375,1108
		1007.20	1.5007 01.55050		6		- ,-	,
	50	1672.213						661
	10	1673.659	82.82640 - 142.57560	3d ⁷ (a ² H)4s - 3d ⁷ (a ² H)4p	³ H – ³ H°	4 - 5		661
	1	1676.054	78.48243 - 138.14648	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{2}P)4p$	${}^{3}P - {}^{1}S^{\circ}$	1 - 0		661
	10	1680.532	79.74922 - 139.25370	3d ⁷ (a ² P)4s - 3d ⁷ (a ² D)4p	$^{3}P - ^{3}D^{\circ}$	1 – 2		661
16	10	1682.029	54.65783 - 114.11020	3d ⁷ (a ⁴ F)4s - 3d ⁷ (a ⁴ F)4p	⁵ F – ⁵ G°	4 – 3		661
16	1	1682.443	53.70393 - 113.14092	3d ⁷ (a ⁴ F)4s - 3d ⁷ (a ⁴ F)4p	⁵ F – ⁵ G°	5 - 5		661
	2	1683 471	83 03345 - 142 43395	$3d^{7}(a^{2}D)4s = 3d^{7}(a^{2}D)4n$	³ D – ¹ D°	2_2		661
	30	1683 688	97 84160 - 157 23516	$3d^{2}(a^{2}F)4s = 3d^{2}(a^{2}F)4r$	${}^{3}\mathbf{F} = {}^{3}\mathbf{D}^{2}$	2 - 1	1	661
	1	1684 515	77.04100 - 157.25510	50 (a 1) 15 - 50 (a 1) 4p				661
	5	1685 085	79 14301 - 138 48740	$3d^{7}(a^{2}P)4s = 3d^{7}(a^{2}D)4n$	$^{3}P - ^{3}D^{\circ}$	2-3		661
	3	1685 546	78 30354 - 137 63160	$3d^{7}(a^{4}P)4s = 3d^{7}(a^{2}P)4p$	$^{3}P - ^{1}D^{\circ}$	2 - 2		661
	5	1685.077	07 84160 157 15427	$3d^{7}(a^{2}E)4s = 3d^{7}(a^{2}E)4p$	$^{3}\mathbf{F} = ^{3}\mathbf{D}^{\circ}$	2-2		661
	5	1005.977	97.84100 - 157.15427	50 (a 1)+5 - 50 (a 1)+p	I - D	2-2		001
	75	1686.216	86.64588 - 145.95015	3d ⁷ (a ² D)4s - 3d ⁷ (a ² D)4p	'D - 'P°	2 – 1		661
25	400	1687.897	71.06735 - 130.31230	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{4}P)4p$	⁵ P – ⁵ D°	3 – 4		661
	5	1689.121						661
	1	1689.596						661
	20	1690.372	97.99581 - 157.15427	$3d^{7}(a^{2}F)4s - 3d^{7}(a^{2}F)4p$	${}^{3}F - {}^{3}D^{\circ}$	3 - 2		661
	5	1690.634	78.48243 - 137.63160	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{2}P)4p$	³ P – ¹ D°	1 – 2		661
	15	1600 074	08 22702 - 157 27542	$2d^{7}(a^{2}E)Aa = 3d^{7}(a^{2}E)Aa$	F-G	4 4		661
	1 15	1601 275	76.23773 - 137.37 3 42	50 (a 1)48 - 50 (a 1)4p	1.2.0			661
	2	1602 210	75 12265 - 134 21760	3d ⁷ (a ² G)4a 3d ⁷ (a ² G)4a	G H	5 5		661
16	1000	1692.219	75.12505 - 154.21700	3d(a G)4s - 3d(a G)4p $2d^{2}(a^{4}E)4a - 2d^{2}(a^{4}E)4p$	0-H	5-5		661
10	1000	1692.514	2 2606 61 2285	3d(a r) + s - 3d(a r) + p		3-0	ED	275 1109
16	1	1693 559	54 65783 - 113 70512	$3d^{7}(a^{4}E)Ae = 3d^{7}(a^{4}E)An$	sar = r	4 4	1,1	661
10		1095.559	54.05785 - 115.70512	5u (a 1)+s = 5u (a 1)+p	1-0			001
	5	1694.307	71.84242 - 130.86350	3d ⁷ (a ⁴ P)4s - 3d ⁷ (a ⁴ P)4p	⁵ P - ³ S°	1 - 1		661
	2	1694.582	97.84160 - 156.85300	$3d^{7}(a^{2}F)4s - 3d^{7}(a^{2}F)4p$	³ F - ³ D°	2 – 3		661
	30	1695.599	97.99581 - 156.97208	$3d^{7}(a^{2}F)4s - 3d^{7}(a^{2}F)4p$	³ F - ³ F°	3 - 4		661
16	5	1695.910	55.40629 - 114.37101	3d ⁷ (a ⁴ F)4s - 3d ⁷ (a ⁴ F)4p	⁵ F – ⁵ G°	3 - 2		661
	5	1696.195	84.60410 - 143.56016	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{2}D)4p$	${}^{1}P - {}^{3}P^{\circ}$	1 – 2		661
25	50	1698.176	71.06735 - 129.95400	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{4}P)4p$	⁵ P - ⁵ D°	3 – 3		661
	5	1698.381	78,48243 - 137,36236	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{2}P)4p$	$^{3}P - ^{3}D^{\circ}$	1-1		661
	10	1699.024	97.99581 - 156.85300	$3d^{7}(a^{2}F)4s = 3d^{7}(a^{2}F)4p$	${}^{3}\mathbf{F} - {}^{3}\mathbf{D}^{\circ}$	3 - 3		661
	8	1699.349	71.06735 - 129.91310	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{4}P)4p$	⁵ P - ⁵ D°	3 - 2		661
	10	1701.081	76.23725 - 135.02320	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{2}G)4n$	${}^{3}G - {}^{1}F^{\circ}$	3 - 3		661
30	60	1701.599	75.64661 - 134.41477	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{2}G)4n$	³ G - ³ G°	4-4		661
	10	1702.591	98.23793 - 156.97208	$3d^{7}(a^{2}F)4s - 3d^{7}(a^{2}F)4p$	${}^{3}\mathbf{F} - {}^{3}\mathbf{F}^{\circ}$	4 - 4		661
16		1702.447		217.4534 217.4534	5. 50			
16	50	1703.467	55.40629 - 114.11020	3d'(a'F)4s - 3d'(a'F)4p	F-G	3-3		661
	3	1703.925	75.64661 - 134.33479	3d'(a'G)4s - 3d'(a'G)4p	G - G	4 - 3		661
	10	1704.128	97.84160 - 156.52287	3d'(a'F)4s - 3d'(a'F)4p	'F - 'F'	2 - 2		661
	60	1704.641	78.30354 - 136.96700	3d'(a'P)4s - 3d'(a'P)4p	°D° – Y	2 - 3		661
	10	1706.041	98.23793 - 156.85300	3d'(a'F)4s - 3d'(a'F)4p	·F – ·D°	4-3		661
	15	1706.246	82.27726 - 140.88540	3d'(a'D)4s - 3d'(a'D)4p	'D - 'F'	1 - 2		661
25	10	1707.242	71.38410 - 129.95795	3d ⁷ (a ⁴ P)4s - 3d ⁷ (a ⁴ P)4p	⁵ P - ⁵ D°	2 - 1		661
25	200	1707.346	71.38410 - 129.95400	3d7(a4P)4s - 3d7(a4P)4p	⁵ P - ⁵ D°	2 - 3		661
30	200	1707.426	75.12365 - 133.69200	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{2}G)4p$	³ G - ³ G*	5 - 5		661
25	50	1708.552	71.38410 - 129.91310	3d7(a4P)4s - 3d7(a4P)4p	⁵ P - ⁵ D°	2 - 2		661
16	800	1709.901	54.65783 - 113.14092	3d7(a4F)4s - 3d7(a4F)4p	5F - 5G°	4 - 5		661
16	10	1711.779	55.95221 - 114.37101	3d7(a4F)4s - 3d7(a4F)4p	5F - 5G*	2-2		661
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NI III - Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	1 - 1	Notes	References
	5	1712.893	83.03345 - 141.41410	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{2}P)4p$	³ D - ¹ P°	2 - 1		661
	10	1713.864	71.84242 - 130.19005	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{4}P)4p$	⁵ P – ⁵ D°	1 – 0		661
	100	1714.698	85.83420 - 144.15300	$3d^{7}(a^{2}H)4s - 3d^{7}(a^{2}H)4p$	'H – 'G°	5-4		661
16	650	1715.303	55.40629 - 113.70512	3d7(a4F)4s - 3d7(a4F)4p	⁵ F - ⁵ G°	3 - 4		661
15	100	1715.931	54.65783 = 112.93543	3d ⁷ (a ⁴ F)4s - 3d ⁷ (a ⁴ F)4p	⁵ F – ⁵ D°	4 - 3		661
15	75	1716.886	55.40629 - 113.65147	3d ⁷ (a ⁴ F)4s - 3d ⁷ (a ⁴ F)4p	⁵ F – ⁵ D°	3 - 2		661
	20	1718.184	75.12365 - 133.32470	3d ⁷ (a ² G)4s - 3d ⁷ (a ² G)4p	³ G – ¹ G°	5-4		661
15	150	1718.365	53.70393 - 111.89865	3d ⁷ (a ⁴ F)4s - 3d ⁷ (a ⁴ F)4p	⁵ F - ⁵ D°	5 - 4		661
30	20	1718.873	76.23725 - 134.41477	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{2}G)4p$	³ G - ³ G°	3 - 4		661
20	20	1719.008	98.23793 - 156.41120	$3d^{7}(a^{2}F)4s - 3d^{7}(a^{2}F)4p$	${}^{3}F - {}^{3}F^{\circ}$	4 - 3		661
16	500	1719 458	55.95221 - 114.11020	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	⁵ F - ⁵ G°	2 - 3		661
15	50	1719.892	55.95221 - 114.09560	3d ⁷ (a ⁴ F)4s - 3d ⁷ (a ⁴ F)4p	⁵ F - ⁵ D°	2 - 1		661
25	20	1720 708	71.84242 - 129.95795	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{4}P)4p$	⁵ P - ⁵ D°	1-1		661
30	200	1721.256	76 23725 - 134 33479	$3d^{7}(a^{2}G)4s = 3d^{7}(a^{2}G)4n$	³ G - ³ G°	3-3		661
50	200	1721.250	10.23723 - 134.33477	50 (a 0)45 - 50 (a 0)4p	0.0			661
	15	1722.038	71 84242 - 129 91310	$\frac{1}{1}$ $3d^{7}(a^{4}P)4s = 3d^{7}(a^{4}P)4p$	⁵ P - ⁵ D°	1-2		661
16	400	1722.038	56 30824 - 114 37101	$3d^{7}(a^{4}F)4s = 3d^{7}(a^{4}F)4p$	⁵ F - ⁵ G°	1-2		661
20	20	1722.285	75 64661 133 60200	$3d^{2}(a^{2}G)Ae = 3d^{2}(a^{2}G)Ap$	³ G - ³ G	4_5		661
30	20	1722.790	75.04001 - 155.05200	50 (a C)+s = 50 (a C)+p	0-0	4-5		001
	150	1723.793	82.17260 - 140.18465	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{2}D)4p$	${}^{3}D - {}^{3}F^{\circ}$	3 – 4		661
28	75	1724.291	76.23725 - 134.23190	3d ⁷ (a ² G)4s - 3d ⁷ (a ² G)4p	${}^{3}\mathbf{G} - {}^{3}\mathbf{F}^{\circ}$	3 - 2		661
15	50	1724.523	56.30824 - 114.29545	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	⁵ F - ⁵ D°	1-0		661
	20	1727.640	79.74922 - 137.63160	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{2}P)4p$	${}^{3}\mathbf{P} - {}^{1}\mathbf{D}^{\circ}$	1 – 2		661
	1	1728.127						661
	20	1728.738	97.99581 - 155.84140	3d ⁷ (a ² F)4s - 3d ⁷ (a ² F)4p	³ F - ³ G°	3 - 4		661
	2	1729.219	84.60410 - 142.43395	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{2}D)4p$	'P - 'D°	1 – 2		661
	20	1729.384	79.14301 - 136.96700	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{2}P)4p$	${}^{3}\mathbf{P} - {}^{3}\mathbf{D}^{\circ}$	2-3		661
	10	1730.255	78.30354 - 136.09870	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{4}P)4p$	${}^{3}\mathbf{P} - {}^{3}\mathbf{P}^{\circ}$	2 - 1		661
15	75	1730.483	56.30824 - 114.09560	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	⁵ F - ⁵ D°	1-1		661
	2	1731.733						661
15	250	1733.129	55.95221 - 113.65147	3d ⁷ (a ⁴ F)4s - 3d ⁷ (a ⁴ F)4p	° F – ` D °	2 - 2		661
	50	1733.762	75.64661 - 133.32470	3d7(a2G)4s - 3d7(a2G)4p	³ G – ¹ G°	4 – 4		661
	2	1735.628	78.48243 - 136.09870	3d ⁷ (a ⁴ P)4s - 3d ⁷ (a ⁴ P)4p	$^{3}\mathbf{P} - ^{3}\mathbf{P}^{\circ}$	1 – 1		661
	5	1735.713	79.74922 - 137.36236	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{2}P)4p$	³ P - ³ D°	1 - 1		661
	50	1736.011	98.23793 - 155.84140	3d ⁷ (a ² F)4s - 3d ⁷ (a ² F)4p	${}^{3}F - {}^{3}G^{\circ}$	4 – 4		661
	50	1736.051	97.84160 - 155.44330	$3d^{7}(a^{2}F)4s - 3d^{7}(a^{2}F)4p$	${}^{3}\mathbf{F} - {}^{3}\mathbf{G}^{\circ}$	2 - 3		661
	2	1736.569						661
15	500	1738.252	55.40629 112.93543	3d ⁷ (a ⁴ F)4s - 3d ⁷ (a ⁴ F)4p	⁵ F – ⁵ D°	3 - 3		661
28	300	1738.785	75.64661 - 133.15850	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{2}G)4p$	${}^{3}G - {}^{3}F^{\circ}$	4 – 3		661
	5	1739.747	121.80245 - 179.28200	$3d^{7}(b^{2}D)4s - 3d^{7}(b^{2}D)4p$	${}^{3}D - {}^{3}F^{\circ}$	3 – 4		661
	1	1739.979						661
	15	1740.671	75.64661 - 133.09589	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{4}P)4p$	³ G ~ ⁵ P°	4 - 3		661
	10	1740.718	97.99581 - 155.44330	$3d^{7}(a^{2}F)4s - 3d^{7}(a^{2}F)4p$	${}^{3}\mathbf{F} - {}^{3}\mathbf{G}^{\circ}$	3 - 3		661
	30	1740.944	82.19380 - 139.63390	$3d^{7}(a^{2}H)4s - 3d^{7}(a^{2}H)4p$	${}^{3}H - {}^{1}I^{\circ}$	5 - 6		661
21	300	1741.963	61.33858 - 118.74525	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	${}^{3}\mathbf{F} - {}^{3}\mathbf{D}^{\circ}$	4 - 3		661
15	1	1743.903	56.30824 - 113.65147	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	⁵ F - ⁵ D°	1 - 2		661
	1	1745.436						661
15	550	1747.011	54.65783 - 111.89865	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	⁵ F - ⁵ D°	4 - 4		661
	1	1747.356	97.84160 - 155.07100	$3d^{7}(a^{2}F)4s - 3d^{7}(a^{2}F)4p$	${}^{3}\mathbf{F} - {}^{1}\mathbf{D}^{\circ}$	2 – 2		661
	50	1747.680	86.64588 - 143.86480	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{2}D)4n$	¹ D - ¹ F°	2 - 3		661
	1	1749.203	85.83420 - 143.00270	$3d^{7}(a^{2}H)4s - 3d^{7}(a^{2}H)4p$	'H – ³ H°	5 - 4		661
21	300	1752.427	62.60558 - 119.66954	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	${}^{3}F - {}^{3}D^{\circ}$	3 - 2		661
21	400	1753 011	75,12365 - 132,16860	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{2}G)4n$	³ G - ³ H°	5-6		661
	2	1753 150	121 41160 - 178 45150	$3d^{7}(h^{2}D)4s = 3d^{7}(h^{2}D)4n$	${}^{3}\mathbf{D} - {}^{3}\mathbf{F}^{\circ}$	2-3		661
29	10	1753 377	75 12365 - 132 15650	$3d^{7}(a^{2}G)4s = 3d^{7}(a^{2}G)4n$	³ G - ³ H°	5-4		661
27	10	1155.511	13.12505 - 152.15050		U. I.			

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NI III -- Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	1	1755.757	79.14301 – 136.09870	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{4}P)4p$	³ P – ³ P°	2 - 1		661
	2	1756 201	76 22725 122 15850	2d7(c2C)4c 2d7(c2C)4r		2 2		661
	25	1757 024	70.23723 - 133.13830 96.64599 143.56016	3d(a O) + s - 3d(a O) + p $3d^{2}(a^{2}D) Aa - 3d^{2}(a^{2}D) Aa$		3-3		661
	10	1759 469	80.04388 - 143.30010	$3d^{2}(a^{2}D)4s = 3d^{2}(a^{2}D)4p$ $3d^{2}(a^{4}D)4a = 2d^{2}(a^{4}D)4a$	D - P	2-2		001
		1758.408	78.48243 - 135.35033	$3d^{2}(a^{2}P)4s = 3d^{2}(a^{2}P)4p$	P - P	1-2		661
	3	1758.940	78.48243 - 135.33490	3d'(a'P)4s - 3d'(a'P)4p	³ P - ³ P ²	1-0		661
	20	1760.260	84.60410 - 141.41410	3d ⁷ (a ² P)4s - 3d ⁷ (a ² P)4p	' Ρ – ' Ρ °	1 – 1		661
21	150	1760.560	63.47193 - 120.27232	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	³ F - ³ D°	2 – 1		661
	20	1762.394	80.62110 - 137.36236	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{2}P)4p$	${}^{3}P - {}^{3}D^{\circ}$	0 - 1		661
	2	1763.069	78.30354 - 135.02320	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{2}G)4p$	³ P – ¹ F °	2 – 3		661
	20	1763.607	82.27726 - 138.97920	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{2}D)4p$	${}^{3}D - {}^{3}D^{\circ}$	1-1		661
14	800	1764.688	53.70393 - 110.37135	3d ⁷ (a ⁴ F)4s - 3d ⁷ (a ⁴ F)4p	⁵ F - ⁵ F°	5 – 4		661
	1	1765.229						661
	10	1766 387	121,19293 - 177,80560	$3d^{7}(h^{2}D)4s = 3d^{7}(h^{2}D)4n$	$^{3}D - ^{3}F^{\circ}$	1-2		661
14	500	1767 938	54 65783 - 111 22120	$3d^{7}(a^{4}E)4s = 3d^{7}(a^{4}E)4n$	⁵ F - ⁵ F°	4 - 3		661
14	1000	1769 634	53 70393 - 110 21280	$3d^{7}(a^{4}F)4s = 3d^{7}(a^{4}F)4p$	5F - 5F°	5_5	р	661
14	200	1769 653	55 40629 - 111 91453	$3d^{7}(a^{4}F)4s = 3d^{7}(a^{4}F)4p$	5F - 5F°	3-2	P	661
14	200	1770 153	55 40629 - 111 89865	$3d^{7}(a^{4}E)As = 3d^{7}(a^{4}E)An$	5F - 5D°	3-2	•	661
		1770.155	55.40025 - 111.85805	50 (a 1)+5 - 50 (a 1)+p	I- D	3-4		001
14	100	1771.492	55.95221 - 112.40165	3d ⁷ (a ⁴ F)4s - 3d ⁷ (a ⁴ F)4p	⁵ F - ⁵ F°	2 – 1		661
	1	1772.499						661
27	40	1773.788	75.12365 - 131.50050	3d ⁷ (a ² G)4s - 3d ⁷ (a ² G)4p	${}^{3}G - {}^{3}H^{\circ}$	5 – 5		661
	10	1774.640	79.74922 - 136.09870	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{4}P)4p$	${}^{3}P - {}^{3}P^{\circ}$	1 – 1		661
	2	1774.992						661
	150	1775.750	82.17260 - 138.48740	3d ⁷ (a ² D)4s - 3d ⁷ (a ² D)4p	${}^{3}\mathbf{D} - {}^{3}\mathbf{D}^{\circ}$	3 - 3		661
	400	1776.068	81.68680 - 137.99140	3d7(a2H)4s - 3d7(a2H)4p	³ H - ³ I°	6 - 7		661
	30	1776.802	84.60410 - 140.88515	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{2}P)4p$	${}^{1}P - {}^{3}S^{\circ}$	1 – 1		661
	10	1777.227	61.33858 - 117.60635	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	${}^{3}F - {}^{3}G^{\circ}$	4 – 3		661
	10	1778.583	125.43355 - 181.6584	$3d^{7}(b^{2}D)4s - 3d^{7}(b^{2}D)4p$	¹ D ¹ F°	2 - 3		661
	30	1778.730	83.03345 - 139.25370	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{2}D)4p$	${}^{3}D - {}^{3}D^{\circ}$	2 - 2		661
	20	1779.127	79.14301 – 135.35033	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{4}P)4p$	${}^{3}\mathbf{P} - {}^{3}\mathbf{P}^{\circ}$	2 – 2		661
21	30	1779.442	63.47193 - 119.66954	3d7(a4F)4s - 3d7(a4F)4p	${}^{3}\mathbf{F} - {}^{3}\mathbf{D}^{\circ}$	2 - 2		661
	1	1779.607						661
	15	1781.088	75.64661 - 131.79202	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{2}G)4p$	³ G - ³ F°	4 - 4		661
21	50	1781.279	62.60558 - 118.74525	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	${}^{3}\mathbf{F} - {}^{3}\mathbf{D}^{\circ}$	3 - 3		661
14	60	1782.747	56.30824 - 112.40165	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	⁵ F - ⁵ F°	1 – 1		661
	75	1784.882	82.82640 - 138.85220	3d ⁷ (a ² H)4s - 3d ⁷ (a ² H)4p	${}^{3}H - {}^{3}G^{\circ}$	4 - 3		661
14	60	1786.927	55.95221 - 111.91453	3d7(a4F)4s - 3d7(a4F)4p	⁵ F - ⁵ F°	2 - 2		661
	2	1787.456	83.03345 - 138.97920	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{2}D)4p$	${}^{3}D - {}^{3}D^{\circ}$	2 – 1		661
27	200	1788.301	76.23725 - 132.15650	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{2}G)4p$	³ G - ³ H°	3 – 4		661
	150	1788.502	61.33858 - 117.25080	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	${}^{3}F - {}^{3}F^{\circ}$	4 - 3		661
	3	1789.888	82.27726 - 138.14648	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{2}P)4p$	${}^{3}D - {}^{1}S^{\circ}$	1-0		661
	5	1789.983	82.19380 - 138.06040	3d7(a2H)4s - 3d7(a2H)4p	³ H - ³ I°	5 - 5		661
27	250	1790.402	75.64661 - 131.50050	$3d^{2}(a^{2}G)4s - 3d^{2}(a^{2}G)4n$	³ G - ³ H°	4 - 5		661
	200	1790.934	82,19380 - 138,03090	$3d^{2}(a^{2}H)Ac = 3d^{2}(a^{2}H)Ac$	³ H - ³ C ²	5_4		661
14	200	1791 644	55 40629 - 111 22120	$3d^{7}(a^{4}F)4s = 3d^{7}(a^{4}F)4n$	5E_5E°	3.3		661
14	200	1792 513	86 64588 - 142 43395	$3d^{7}(a^{2}D)Ac = 3d^{7}(a^{2}D)Ac$		3-3		661
	100	1792.013	79 25011 - 135 02320	$3d^{2}(a^{2}G)As = 3d^{2}(a^{2}G)Ap$		2 - 2		661
	1	1793.972	79.25011 - 155.02520	50 (a 0)45 - 50 (a 0)4p	0-r	4-3		661
14	200	1794.904	54.65783 - 110.37135	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	⁵ F - ⁵ F°	4 – 4		661
	20	1795.192	81.68680 - 137.39130	3d ⁷ (a ² H)4s - 3d ⁷ (a ² H)4p	${}^{3}H - {}^{3}I^{\circ}$	6 - 6		661
14	20	1798.366	56.30824 - 111.91453	3d7(a4F)4s - 3d7(a4F)4p	⁵ F - ⁵ F°	1 – 2		661
	5	1799.023	79.74922 - 135.33490	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{4}P)4p$	${}^{3}\mathbf{P} - {}^{3}\mathbf{P}^{\circ}$	1-0		661
14	20	1800.031	54.65783 - 110.21280	3d7(a4F)4s - 3d7(a4F)4p	⁵ F - ⁵ F°	4 - 5		661
	1	1800.404	121.19293 - 176.73640	$3d^{7}(b^{2}D)4s - 3d^{7}(b^{2}D)4p$	${}^{3}D - {}^{3}P^{\circ}$	1-0		661

NI III - Continued

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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
20	50	1801.506	62.60558 - 118.11495	3d ⁷ (a ⁴ F)4s - 3d ⁷ (a ⁴ F)4p	³ F - ³ F°	3 - 2		661
	2	1802.546	80.62110 - 136.09870	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{4}P)4p$	³ P - ³ P°	0 - 1		661
	1	1803.615						661
	30	1804.394	101.95490 - 157.37542	$3d'(a^2F)4s - 3d'(a^2F)4p$	'F - 'G°	3 - 4		661
	30	1806.457	78.48243 – 133.83954	$3d'(a^{+}P)4s - 3d'(a^{+}P)4p$	$^{3}P - ^{3}D^{3}$	1-1		661
	30	1806.550	82.27726 - 137.63160	$3d'(a^2D)4s - 3d'(a^2P)4p$	·D – ·D*	1 – 2		661
	50	1807.056	78.30354 - 133.64258	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{2}P)4p$	${}^{3}\mathbf{P} - {}^{3}\mathbf{P}^{\circ}$	2 - 2		661
	300	1807.245	81.68680 - 137.02020	$3d'(a^2H)4s - 3d'(a^2H)4p$	³ H - ³ G ³	6-5		661
	5	1809.200	63.47193 - 118.74525	$3d'(a^{*}F)4s - 3d'(a^{*}F)4p$	[°] F - [°] D	2 - 3		661
14	15	1809.335	55.95221 - 111.22120	$3d'(a^{*}F)4s - 3d'(a^{*}F)4p$	$\mathbf{F} - \mathbf{F}$	2-3		661
	150	1810.489	82.82640 - 138.06040	$3d'(a^2H)4s - 3d'(a^2H)4p$	$H - I^{-}$	4-5		661
	200	1811.689	/8.30354 - 133.50097	30'(a'P)4s - 30'(a'P)4p	·P - D	2 - 2		001
	10	1812.190	78.65755 - 133.83954	3d7(a4P)4s - 3d7(a4P)4p	$^{3}P - ^{3}D^{\circ}$	0 - 1		661
	3	1812.539	121.41160 - 176.58320	$3d^{7}(b^{2}D)4s - 3d^{7}(b^{2}D)4p$	${}^{3}D - {}^{3}P^{\circ}$	2 - 1		661
	20	1812.769	79.25011 - 134.41477	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{2}G)4p$	¹ G - ³ G°	4 – 4		661
	1	1814.082						661
	20	1815.307	78.30354 - 133.39094	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{4}P)4p$	$^{3}P - ^{3}D^{\circ}$	2 - 3		661
	15	1815.398	79.25011 – 134.33479	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{2}G)4p$	'G - 'G°	4 - 3		661
	2	1815.650						661
	1	1816.990	78.30354 - 133.33970	3d ⁷ (a ⁴ P)4s - 3d ⁷ (a ⁴ P)4p	${}^{3}P - {}^{5}P^{\circ}$	2 – 1		661
	15	1817.598	101.95490 - 156.97208	$3d^{7}(a^{2}F)4s - 3d^{7}(a^{2}F)4p$	${}^{1}F - {}^{3}F^{*}$	3 - 4		661
	300	1819.275	79.25011 - 134.21760	3d7(a2G)4s - 3d7(a2G)4p	¹ G – ¹ H°	4 – 5		661
14	3	1819.325	55.40629 - 110.37135	3d7(a4F)4s - 3d7(a4F)4p	⁵ F – ⁵ F°	3 – 4		661
	25	1822.918	78.48243 - 133.33970	3d ⁷ (a ⁴ P)4s - 3d ⁷ (a ⁴ P)4p	³ P - ³ P°	1 – 1		661
20	800	1823.061	61.33858 - 116.19193	3d7(a4F)4s - 3d7(a4F)4p	${}^{3}F - {}^{3}F^{\circ}$	4 - 4		661
	1	1823.936	82.19380 - 137.02020	3d ⁷ (a ² H)4s - 3d ⁷ (a ² H)4p	${}^{3}H - {}^{3}G^{\circ}$	5 - 5		661
	20	1825.084	78.30354 - 133.09589	3d ⁷ (a ⁴ P)4s - 3d ⁷ (a ⁴ P)4p	${}^{3}P - {}^{5}P^{\circ}$	2 - 3		661
	15	1828.279	129.91310 - 184.60957	3d ⁷ (a ⁴ P)4p - 3d ⁷ (a ⁴ F)5s	⁵ D° ~ ⁵ F	2 – 1		661
	15	1828.672	121.80245 - 176.48710	$3d^{7}(b^{2}D)4s - 3d^{7}(b^{2}D)4p$	$^{3}D - ^{3}P^{\circ}$	3 - 2		661
		1829.56	0.0 - 54.65783	$3d^{*} - 3d^{7}(a^{+}F)4s$	ga ³ F - ⁵ F	4 – 4	F,P	375,1108
20	400	1830.006	62.60558 - 117.25080	3d ⁷ (a ⁴ F)4s - 3d ⁷ (a ⁴ F)4p	${}^{3}F - {}^{3}F^{\circ}$	3 - 3		661
20	200	1830.075	63.47193 - 118.11495	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	${}^{3}\mathbf{F} - {}^{3}\mathbf{F}^{\bullet}$	2 - 2		661
	15	1830.859	78.65755 - 133.27670	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{2}P)4p$	${}^{3}\mathbf{P} - {}^{3}\mathbf{P}^{\circ}$	0 – 1		661
	5	1831.578	83.03345 - 137.63160	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{2}P)4p$	${}^{3}D - {}^{1}D^{\circ}$	2 - 2		661
	1	1831.850						661
	20	1833.669	82.27726 - 136.81320	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{2}P)4p$	³ D - ³ D°	1 – 2		661
	15	1834.381	78.30354 - 132.81826	3d ⁷ (a ⁴ P)4s - 3d ⁷ (a ⁴ P)4p	${}^{3}\mathbf{P} - {}^{5}\mathbf{P}^{\circ}$	2 - 2		661
	20	1834.890	79.14301 - 133.64258	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{2}P)4p$	${}^{3}P - {}^{3}P^{\circ}$	2 - 2		661
	30	1836.843	79.25011 - 133.69200	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{2}G)4p$	¹ G – ¹ G°	4 - 5		661
	1	1839.092	84.60410 - 138.97920	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{2}D)4p$	P - 'D'	1-1		661
	40	1840.421 1841 866	133.15850 - 187.49338	3d'(a ² G)4p - 3d'(a ⁴ F)4d	⁵ F° – ⁵ P	3 - 2		661 661
		1011.000				ĺ		
34	50	1843.406	79.14301 - 133.39094	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{4}P)4p$	³ P - ³ D°	2 – 3		661
	1	1843.689	86.64588 - 140.88540	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{2}D)4p$	D - F	2 - 2		661
	15	1845.141	79.14301 - 133.33970	$3d'(a^2P)4s - 3d'(a^4P)4p$	$^{3}\mathbf{P} - ^{3}\mathbf{P}^{*}$	2 - 1		661
19	650	1847.275	63.47193 - 117.60635	$3d'(a^{+}F)4s - 3d'(a^{+}F)4p$	F - G	2-3		661
	100	1849.319 1849.473	79.25011 - 133.32470 62.60558 - 116.67439	$3d^{7}(a^{4}G)4s - 3d^{7}(a^{4}G)4p$ $3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	³ F - ³ G°	4-4		661
19	75	1849.540	1 3607 - 55 40620	3d8 3d7(04E)40	σa ³ Ε – ⁵ Ε	3_2	FP	661 375 1108
	30	1853 480	79 14301 - 133 09589	$3d^{7}(a^{2}P)4s = 3d^{7}(a^{4}P)4n$	$^{3}\mathbf{P} = ^{5}\mathbf{P}^{\circ}$	2 - 3	•,•	661
19	800	1854 149	61 33858 - 115 27226	$3d^{7}(a^{4}F)4s = 3d^{7}(a^{4}F)4r$	³ F - ³ G°	4 - 5		661
	1	1855.525	79.74922 - 133.64258	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{2}P)4n$	³ P - ³ P°	1-2		661
				() ()-P		1	1	
	1	1855.755	101.95490 - 155 84140	$3d^{7}(a^{2}F)4s = 3d^{7}(a^{2}F)4r$	F - ³ G°	3-4		661

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NI III - Continued

Aultiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	0	1857.158	79.25011 - 133.09589	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{4}P)4p$	¹ G - ⁵ P°	4 - 3		661
	300	1858.750	85.83420 - 139.63390	3d7(a2H)4s - 3d7(a2H)4p	${}^{I}H - {}^{I}I^{\circ}$	5 - 6		661
	2	1859.480	63.47193 - 117.25080	3d7(a4F)4s - 3d7(a4F)4p	${}^{3}F - {}^{3}F^{\circ}$	2 - 3		661
		1862.06	0.0 - 53.70393	$3d^8 - 3d^7(a^4F)4s$	$ga^{3}F - {}^{5}F$	4 - 5	F.P	375,1108
		1862.80	2 2696 - 55 95221	$3d^8 - 3d^7(a^4F)4s$	$ga^{3}F - {}^{5}F$	2 - 2	F.P	375,1108
	3	1866.008	79.74922 - 133.33970	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{4}P)4p$	$^{3}P - ^{5}P^{\circ}$	1 - 1	- ,-	661
	5	1866 163	62 60558 - 116 19193	$3d^{7}(a^{4}E)4s = 3d^{7}(a^{4}E)4e$	³ F - ³ F°	3_4		661
	2	1860.105	02.00558 - 110.19195	50 (a 1)45 - 50 (a 1)4p	1 - 1	5-4		661
	3	1867.700	70 74000 133 07(70	2 17/ 2014 2 17/ 2014	in ine			001
	20	1868.201	/9./4922 - 133.2/6/0	$3d(a^{-}P)4s = 3d(a^{-}P)4p$	$\mathbf{P} - \mathbf{P}$	1 - 1		001
	_	18/6.27	1.3607 - 54.65783	3d" - 3d'(a'F)4s	ga F - F	3-4	F,P	375,1108
	5	1879.063	80.62110 - 133.83954	3d'(a ² P)4s - 3d'(a ⁴ P)4p	³ P - ³ D ³	0 - 1		661
	5	1880.498	82.17260 - 135.35033	3d'(a2D)4s - 3d'(a2P)4p	³ D - ³ P°	3 - 2		661
		1881.94	2.2696 - 55.40629	3d ⁸ - 3d ⁷ (a ⁴ F)4s	ga ³ F - ⁵ F	2 - 3	F,P	375,1108
	25	1882.686	79.74922 - 132.8648	$3d^{7}(a^{2}P)4s - 3d^{7}(a^{2}P)4p$	${}^{3}P - {}^{3}P^{\circ}$	1 – 0		661
	1	1884.723	82.27726 - 135.33490	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{4}P)4p$	³ D - ³ P°	1 - 0		661
	10	1885.864						661
	15	1890.155	79.25011 - 132.15650	$3d^{7}(a^{2}G)4s - 3d^{7}(a^{2}G)4p$	¹ G - ³ H°	4-4		661
	5	1895.479		· · · · · · · · · · · · · · · · · · ·				661
	1	1899 098						661
	50	1902 607	78 30354 - 130 86350	3d7(a4D)4e 3d7(a4D)4-	30 300	2 1	Ì	661
	10	1002.007	70.30334 - 130.00330	Ju(a I) + s = Ju(a I) + p $2d^{2}(a^{2}C) A = 2d^{2}(a^{2}C) A =$				661
	15	1903.262	79.25011 - 131.79202	$30^{\circ}(a^{\circ}G)4s = 30^{\circ}(a^{\circ}G)4p$	G - F	4-4		001
	3	1909.091	/8.48243 - 130.86350	3d'(a'P)4s - 3d'(a'P)4p	°P - °S	1-1		001
	30	1913.890					ł	661
	3	1914.076						661
	1	1914.75	85.83420 - 138.06040	3d7(a2H)4s - 3d7(a2H)4p	¹ H - ³ I°	5 - 5		661
	1	1914.919	82.19380 - 134.41477	3d ⁷ (a ² H)4s - 3d ⁷ (a ² G)4p	${}^{3}H - {}^{3}G^{\circ}$	5 - 4]	661
	5	1915.409						661
	5	1915.497	78.65755 - 130.86350	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{4}P)4p$	${}^{3}P - {}^{3}S^{\circ}$	0 - 1		661
	2	1915.834	85.83420 - 138.03090	$3d^{7}(a^{2}H)4s - 3d^{7}(a^{2}H)4p$	¹ H - ³ G°	5-4		661
	1	1922.91						661
	5	1923 463	83 03345 - 135 02320	$3d^{7}(a^{2}D)4a = 3d^{7}(a^{2}G)4a$	³ D - ¹ F°	2.1		661
18	200	1030 431	61 33858 113 14092	$3d^{7}(a^{4}E)Aa = 3d^{7}(a^{4}E)Aa$	35 50	1 5		661
10	200	1930.431	70 14101 120 86150	$3u (a \Gamma) 4s - 3u (a \Gamma) 4p$		4-5	n	001
		1933.47	79.14301 - 130.86350	$3d'(a^2P)4s - 3d'(a^2P)4p$	P - S	2-1	Р	3/5
1	5	1935.947	78.30354 - 129.95795	$3d^{2}(a^{+}P)4s - 3d^{2}(a^{+}P)4p$	P - D	2 - 1		001
	2	1936.10	78.30354 - 129.95400	3d'(a*P)4s – 3d'(a*P)4p	·P - 'D'	2 - 3	ļ .	661
	3	1939.40	82.27726 - 133.83954	3d'(a ² D)4s – 3d'(a ⁴ P)4p	, D – ,D,	1 - 1		661
	100	1939.588	85.83420 - 137.39130	3d'(a2H)4s - 3d'(a2H)4p	³ H - ³ I°	5 - 6		661
	0	1941.41	82.82640 - 134.33479	3d7(a2H)4s - 3d7(a2G)4p	³ H - ³ G°	4 - 3		661
18	0	1941.58	62.60558 - 114.11020	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4D$	³ F - ⁵ G°	3 - 3		661
	0	1942.64	176.48710 - 227.96302	$3d^{7}(b^{2}D)4p - 3d^{7}(a^{4}F)5d$	³ P° – ⁵ G	2 - 3		661
	10	1942.886	82,17260 - 133,64258	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{2}P)4p$	${}^{3}D - {}^{3}P^{\circ}$	3 - 2		661
	2	1944.36	78.48243 - 129.91310	3d ⁷ (a ⁴ P)4s - 3d ⁷ (a ⁴ P)4p	$^{3}P - ^{5}D^{\circ}$	1 - 2		661
	1	1946.81						661
	5	1950.00				1		661
24	100	1052 540	71 06735 122 28240	147(-4D)4- 217(4D)4	SP SO	1 2 2		001
44	200	1932,340	/1.00/33 - 122.28240	30'(a'P)4s - 30'(a'P)4p	P - S	3-2		100
	0	1955.74	82.19380 - 133.32470	3d'(a*H)4s - 3d'(a*G)4p	"H - 'G"	5-4		661
	3	1956.402	/9.74922 - 130.86350	3d'(a'P)4s - 3d'(a'P)4p	°P – °S°	1 - 1		661
18	20	1956.964	62.60558 - 113.70512	3d'(a*F)4s - 3d'(a*F)4p	'F - 'G°	3 - 4		661
	5	1961.324	86.64588 - 137.63160	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{2}P)4p$	${}^{1}\mathbf{D} - {}^{1}\mathbf{D}^{\circ}$	2 - 2		661
	2	1963.73	82.17260 - 133.09589	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{4}P)4p$	³ D - ⁵ P°	3 - 3		661
24	100	1964.689	71.38410 - 122.28240	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{4}P)4n$	⁵ P - ⁵ S ^o	2-2		661
	3	1968.053		· · · · · · · · · · · · · · · · · · ·		- -		661
	n	1969.62						661
	ñ	1970 54						661
	v	1710.34						001

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NI III - Continued

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	References
	15	1974.493	82.17260 - 132.81826	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{4}P)4p$	³ D - ⁵ P°	3 - 2		661
18	15	1974.780	63.47193 - 114.11020	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	³ F - ⁵ G°	2 - 3		661
	1	1977.84	61.33858 - 111.89865	$3d^{7}(a^{4}F)4s - 3d^{7}(a^{4}F)4p$	³ F - ⁵ D°	4 - 4		661
	2	1980.248	82.82640 - 133.32470	$3d^{7}(a^{2}H)4s - 3d^{7}(a^{2}G)4p$	${}^{3}H - {}^{1}G^{\circ}$	4 - 4		661
24	50	1982.538	71.84242 - 122.28240	$3d^{7}(a^{4}P)4s - 3d^{7}(a^{4}P)4p$	⁵ P - ⁵ S°	1 - 2		661
	1	1987.83	83.03345 - 133.33970	$3d^{7}(a^{2}D)4s - 3d^{7}(a^{4}P)4p$	${}^{3}D - {}^{5}P^{\circ}$	2 – 1		661
	10	1993.362						661

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NICKEL IV (Ni ³⁺), Z = 28 Ground State $1s^22s^22p^63s^23p^63d^7({}^4F_{9/2})$ (25 electrons) Ionization Potential [443 000] cm⁻¹; [54.9] eV

Multiplet l	Rel. Int.	$\lambda_{\rm vac}$ (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	References
	330	392.680	0. – 254.6634	$3d^{7} - 3d^{6}(b^{3}P)4p$	$ga^4F - {}^4D^\circ$	$\frac{9}{2} - \frac{7}{2}$		903
	320	393.236	0 254.3000	$3d^7 - 3d^6(b^3F)4p$	ga ⁴ F - ⁴ F°	$\frac{9}{2} - \frac{9}{2}$		903
	120	394.526	1.1897 - 254.6634	$3d^{7} - 3d^{6}(b^{3}P)4p$	ga ⁴ F – ⁴ D°	$\frac{1}{2} - \frac{1}{2}$		903
	20	395.087	1.1897 - 254.3000	$3d^7 - 3d^6(b^3F)4p$	$ga^4F - {}^4F^\circ$	$\frac{1}{2} - \frac{9}{2}$		903
	130	395.369	1.1897 - 254.1237	$3d^{7} - 3d^{6}(b^{3}F)4p$	$ga^4F - {}^4F^\circ$	$\frac{7}{2} - \frac{5}{2}$		903
1	200	396.127	1.1897 - 253.6391	3d ⁷ - 3d ⁶ (b ³ F)4p	ga ⁴ F – ⁴ F°	$\frac{7}{2} - \frac{7}{2}$		903
	40	397.557	2.0425 - 253.5793	3d ⁷ - 3d ⁶ (b ³ F)4p	ga4F - 4F°	$\frac{5}{2} - \frac{3}{2}$		903
ł	140	397.967	2.0425 - 253.3262	$3d^{7} - 3d^{6}(b^{3}P)4p$	$ga^4F - ^4D^\circ$	$\frac{5}{2} - \frac{5}{2}$		903
	60	398.473	2.6211 - 253.5793	3d ⁷ – 3d ⁶ (b ³ F)4p	$ga^4F - {}^4F^\circ$	$\frac{1}{2} - \frac{3}{2}$		903
	120	398.521	2.0425 - 252.9754	3d ⁷ – 3d ⁶ (b ³ P)4p	ga⁴F - ⁴D°	$\frac{5}{2} - \frac{3}{2}$		903
	50	398.886	2.6211 - 253.3262	3d ⁷ - 3d ⁶ (b ³ P)4p	ga⁴F – ⁴D°	$\frac{3}{2} - \frac{5}{2}$		903
	110	399.444	2.6211 - 252.9754	$3d^7 - 3d^6(b^3P)4p$	ga⁴F – ⁴D°	$\frac{3}{2} - \frac{3}{2}$		903
	80	399.487	2.0425 - 252.3540	$3d^{7} - 3d^{6}(b^{3}P)4p$	$ga^4F - {}^4P^\circ$	$\frac{5}{2} - \frac{5}{2}$		903
	230	401.299					i	903
	20	407.035	2.0425 - 247.7317	3d ⁷ - 3d ⁶ (b ³ F)4p	ga⁴F - ⁴G°	$\frac{2}{2} - \frac{7}{2}$	Q	903
	20	407.967						903
	60	412.460	19.8296 - 262.2755	$3d^7 - 3d^6(b^1G)4p$	$a^2G - {}^2G^\circ$	$\frac{9}{2} - \frac{9}{2}$		903
	240	413.331	0. – 241.9390	3d ⁷ – 3d ⁶ (b ³ F)4p	ga4F – 4D°	$\frac{9}{2} - \frac{1}{2}$		903
	140	415.588	1.1897 – 241.8179	$3d^{7} - 3d^{6}(b^{3}F)4p$	ga⁴F - ⁴D°	$\frac{7}{2} - \frac{5}{2}$		903
	110	417.547	2.0425 - 241.5400	3d ⁷ – 3d ⁶ (b ³ F)4p	ga ⁴ F – ⁴ D°	$\frac{5}{2} - \frac{3}{2}$		903
	90	418.703	19.8296 - 258.6728	3d ⁷ – 3d ⁶ (b ¹ G)4p	$a^2G - {}^2H^\circ$	$\frac{9}{2} - \frac{9}{2}$	Q	903
	230	418.785	43.8586 - 282.6452	$3d^{7} - 3d^{6}(b^{1}D)4p$	$a^2F - ^2D^\circ$	$\frac{2}{2} - \frac{2}{2}$		903
	180	418.866	43.4375 - 282.1795	$3d^{7} - 3d^{6}(b^{1}D)4p$	$a^2F - ^2D^\circ$	$\frac{2}{2} - \frac{3}{2}$		903
	60	419.198	2.6211 - 241.1724	$3d^{7} - 3d^{6}(b^{3}P)4p$	ga⁴F – ⁴D°	$\frac{3}{2} - \frac{1}{2}$		903
	120	421.543						903
	50	421.608	19.8296 - 257.0180	3d ⁷ – 3d ⁶ (b ³ F)4p	$a^2G - {}^2F^\circ$	2 + 2		903
	250	422.747	18.1186 – 254.6634	3d ⁷ - 3d ⁶ (b ³ P)4p	a ⁴ P - ⁴ D°	$\frac{2}{2} - \frac{4}{2}$		903
	60	422.924	20.9476 - 257.4064	3d ⁷ – 3d ⁶ (b ³ F)4p	$a^2G - F^{\circ}$	$\frac{1}{2} - \frac{2}{2}$	Q	903
	80	423.713	18.1186 - 254.1237	3d ⁷ – 3d ⁶ (b ³ F)4p	$a^{4}P - {}^{4}F^{\circ}$	$\frac{1}{2} - \frac{2}{2}$		903
	.80	423.765						903
	60	423.806						903
	60	423.921						903
	40	424.122						903
	100	424.158	18.3668 - 254.1237	$3d^{7} - 3d^{6}(b^{3}F)4p$	a⁴P - ⁴F°	$\frac{3}{2} - \frac{5}{2}$		903
	490	424.405	26.6491 – 262.2755	3d ⁷ – 3d ⁶ (b ¹ G)4p	$a^2H - {}^2G^\circ$	$\frac{11}{2} - \frac{9}{2}$		903
	120	424.583	18.1186 - 253.6391	3d ⁷ - 3d ⁶ (b ³ F)4p	a ⁴ P - ⁴ F°	$\frac{5}{2} - \frac{7}{2}$		903
				1	1	1	[

NI IV - Continued

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	100	425.148	18.3668 - 253.5793	3d ⁷ - 3d ⁶ (b ³ F)4p	a ⁴ P - ⁴ F°	$\frac{1}{2} - \frac{3}{2}$		903
	20	425.197				1		903
	40	425.593	18.3668 - 253.3262	3d ⁷ – 3d ⁶ (b ³ P)4p	a⁴P – ⁴D°	$\frac{3}{2} - \frac{2}{2}$		903
	380	425.782	27.6776 - 262.5387	3d ⁷ – 3d ⁶ (b ¹ G)4p	$a^2H - {}^2G^\circ$	$\frac{9}{2} - \frac{7}{2}$		903
	110	426.230	18.9584 - 253.5793	3d ⁷ – 3d ⁶ (b ³ F)4p	a⁴P – ⁴F°	$\frac{1}{2} - \frac{3}{2}$]	903
	70	426.924	18.1186 - 252.3540	$3d^{7} - 3d^{6}(b^{3}P)4p$	$a^4P - {}^4P^\circ$	$\frac{5}{2} - \frac{5}{2}$		903
	50	427.308	18.9584 - 252.9754	3d ⁷ - 3d ⁶ (b ³ P)4p	a ⁴ P - ⁴ D°	$\frac{1}{2} - \frac{3}{2}$		903
	170	427 372	18 3668 - 252 3540	$3d^7 - 3d^6(b^3P)4p$	$a^4P - {}^4P^\circ$	3 5		903
	230	428 420	26 6491 - 260 0651	$3d^7 - 3d^6(b^1G)4p$	$a^{2}H = {}^{2}H^{0}$	<u> </u>		903
	40	420.420	20.0491 - 200.0031	54 × 54 (0 G)4p	a 11 - 11	2 - 2		903
	150	429.017	27 6776 260 3555	3d7 3d6(b1C)/m	a ² H ² E ^o	2 2		903
	150	429.773	27.0770 - 200.3333	3d = 3d (0 G) + p		2^{-2}		903
	60	430.994	20.0491 - 238.0728	3a° - 3a°(6°G)4p	a-nn	2 - 2		903
	410	432.880	18.1186 - 249.1300	3d ⁷ - 3d ⁶ (b ³ P)4p	a ⁴ P - ⁴ S°	$\frac{5}{2} - \frac{3}{2}$		903
	200	432.912	27.6776 - 258.6728	$3d^7 - 3d^6(b^1G)4p$	$a^2H - {}^2H^\circ$	2 - 2		903
	260	433.345	(8.3668 - 249.1300	$3d^7 - 3d^6(b^3P)4p$	$a^4P - {}^4S^\circ$	3-3		903
	140	434 461	18 9584 - 249 1300	$3d^7 - 3d^6(b^3P)4n$	$a^4P - {}^4S^\circ$	1 - 3		903
	60	434 938	27.0965 - 257.0180	$3d^7 - 3d^6(b^3E)4p$	$a^2D - {}^2F^\circ$	5 1		903
	80	438.185	27.0903 - 237.0100	54 54 (61)10		2 - 2		903
		100.011				11 0		
	150	439.261	26.6491 - 254.3000	3d′ – 3d°(b'F)4p	a'H – 'F'	1 2 - 2		903
	100	442.552	27.6776 - 253.6391	3d' - 3d°(b'F)4p	a²H – ⁴ F°	$\frac{9}{2} - \frac{1}{2}$		903
	190	444.178	0. – 225.1369	3d ⁷ - 3d ⁶ (a ³ D)4p	ga⁴F – ⁴D°	$\frac{9}{2} - \frac{7}{2}$		903
	570	444.208	26.6491 - 251.7736	3d ⁷ – 3d ⁶ (b ³ F)4p	a ² H - ² G°	$\frac{11}{2} - \frac{9}{2}$		903
	540	444.747	27.6776 - 252.5230	3d ⁷ – 3d ⁶ (b ³ F)4p	$a^2H - {}^2G^\circ$	$\frac{9}{2} - \frac{7}{2}$		903
	120	446.281	0 224.0753	$3d^7 - 3d^6(a^1G)4p$	$ga^4F - {}^2F^\circ$	$\frac{9}{2} - \frac{7}{2}$		903
	610	446 778	18 1186 - 241 9390	$3d^7 - 3d^6(h^3F)4n$	$a^4P = {}^4D^\circ$	5_1		903
	180	447 029	18 1186 - 241 8179	$3d^7 = 3d^6(b^3E)4p$	$a^4P - {}^4D^\circ$	5 5		903
	460	447.523	1 1807 224 6457	$3d^7 = 3d^6(a^3D)/a^2$	aT = D	2 2 2		903
	190	447.323	1.1677 - 224.0457	$3d^7 = 3d(a D)^4p$	ga P = D	2 - 2 3 3		903
	70	440.079	1 1907 - 224 0212	3u = 3u (0 F) + p	$a \mathbf{r} - \mathbf{D}$	2 - 2		903
	20	448.779	18.3668 - 241.1724	$3d^{7} - 3d^{6}(b^{3}P)4p$	ga' F - F $a^4 P - ^4 D^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
	20	449.238	2.0425 - 224.6457	$3d^{7} - 3d^{6}(a^{3}D)4p$	ga⁴F - ⁴D°	$\frac{2}{2} - \frac{2}{2}$		903
	160	449.273	18.9584 - 241.5400	3d ⁷ - 3d ⁶ (b ³ F)4p	a⁴P – ⁴D°	$\frac{1}{2} - \frac{3}{2}$		903
	180	450.017	18.9584 - 241.1724	3d ⁷ – 3d ⁶ (b ³ P)4p	a⁴P – ⁴D°	$\frac{1}{2} - \frac{1}{2}$		903
	120	450.183	2.0425 - 224.1740	3d ⁷ – 3d ⁶ (a ³ D)4p	ga⁴F – ⁴D°	$\frac{5}{2} - \frac{3}{2}$		903
	30	451.009	18.3668 - 240.0942	$3d^7 - 3d^6(a^1F)4p$	$a^4P - {}^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$		903
	20	451.363	2.6211 - 224.1740	$3d^{7} - 3d^{6}(a^{3}D)4p$	ga⁴F – ⁴D°	$\frac{3}{2} - \frac{3}{2}$		903
	210	451.500						903
	40	451.690	2.6211 - 224.0213	$3d^7 - 3d^6(a^3D)4n$	$ga^4F - {}^4F^\circ$	3 - 5	0	903
	50	452.157	2.6211 - 223 7854	$3d^7 = 3d^6(a^3D)4n$	$\sigma a^4 F = {}^4 D^9$	$\frac{2}{3}$ 1	×	903
	40	452.157	1 1897 - 222 3333	$3d^{7} - 3d^{6}(a^{3}D)4p$	ga^4F $^4D^\circ$	1 5		903
	200	452.212	1.1677 - 222.5555	50 ~ 50 (a D)+p	ga 1 - 1	2 - 2		903
	30	452.714	18.1186 - 239.0087	3d ⁷ - 3d ⁶ (a ¹ F)4p	$a^4P - {}^2D^\circ$	$\frac{5}{2} - \frac{5}{2}$		903
	80	453.227	18.3668 - 239.0087	$3d^{7} - 3d^{6}(a^{1}F)4p$	$a^4P - {}^2D^\circ$	$\frac{3}{2} - \frac{5}{2}$		903
	70	454.432	27.6776 - 247.7317	3d ⁷ - 3d ⁶ (b ³ F)4p	a²H – ⁴G°	$\frac{9}{2} - \frac{7}{2}$		903
	60	456.361	19.8296 - 238.9578	$3d^{7} - 3d^{6}(a^{1}F)4p$	$a^2G - {}^2G^\circ$	$\frac{9}{2} - \frac{9}{2}$		903
	190	456.419	43.4375 - 262.5387	$3d^{7} - 3d^{6}(b^{1}G)4p$	$a^2F - {}^2G^\circ$	$\frac{5}{2} - \frac{7}{2}$		903
	50	456.913	0 218.8606	$3d^7 - 3d^6(a^3H)4p$	$ga^4F - {}^2H^\circ$	<u><u><u>3</u></u> - <u><u>1</u></u></u>		903
	120	457.293	43.8586 - 262.5387	3d ⁷ – 3d ⁶ (b ¹ G)4p	$a^2F - C^{\circ}G^{\circ}$	$\frac{7}{2} - \frac{7}{2}$		903
	350	457 850	43 8586 - 262 2755	3d7 . 3d6/61C3/4-	$a^2 E^2 C^{\circ}$	1 2		903
	170	457.050	-73.0300 - 202.2733	347 - 346(L3T2)40		$2 - \frac{1}{2}$ 3 - 5		3U3 003
	1/0	430.330	23.0469 - 241.81/9	30° - 30°(b°F)4p	a-r - D	2 - 2		903
i	260	459.164	43.4373 - 261.2263	3d – 3d°(b'G)4p	a'F - 'F'	$\frac{1}{2} - \frac{2}{2}$		903
	210	461.010	43.4375 - 260.3555	3d′ – 3d°(b'G)4p	a ² F - ² F°	$\frac{1}{2} - \frac{1}{2}$		903
	110	461.061	24.6514 - 241.5400	$3d' - 3d^{6}(b^{3}F)4p$	$a^2P - {}^4D^\circ$	$\frac{1}{2} - \frac{3}{2}$		903
	120	461.082	24.6514 - 241.5400	$3d^7 - 3d^6(b^3F)4n$	$a^2P - {}^4D^\circ$	1 1 - 3	0	903

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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	60	461.764						903
	80	461.832	20.9476 - 237.4803	$3d^{7} - 3d^{6}(a^{1}F)4p$	$a^2G - {}^2G^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
	150	461.907	43.8586 - 260.3555	3d ⁷ – 3d ⁶ (b ¹ G)4p	$a^2F - {}^2F^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
	340	462.009	27.0965 - 243.5420	3d ⁷ – 3d ⁶ (a ¹ F)4p	$a^2D - {}^2F^\circ$	$\frac{2}{2} - \frac{1}{2}$		903
	120	462.058	27.0965 - 243.5201	3d ⁷ – 3d ⁶ (a ¹ F)4p	$a^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{5}{2}$		903
	80	463.527	0. – 215.7361	3d ⁷ - 3d ⁶ (a ³ G)4p	ga⁴F – ⁴H°	$\frac{9}{2} - \frac{9}{2}$		903
	70	463.588						903
	20	463.708	18.3668 - 234.0195	$3d^7 - 3d^6(a^1S)4p$	$a^4P - {}^2P^\circ$	$\frac{3}{2} - \frac{3}{2}$		903
	110	464.160	24.6514 - 240.0942	3d ⁷ - 3d ⁶ (a ¹ F)4p	$a^2P - {}^2D^\circ$	$\frac{1}{2} - \frac{3}{2}$		903
	210	464.309	2.0425 - 217.4143	3d ⁷ - 3d ⁶ (a ³ F)4p	$ga^4F - ^2D^\circ$	$\frac{5}{2} - \frac{5}{2}$		903
	250	464.334	23.6489 - 239.0087	$3d^{7} - 3d^{6}(a^{1}F)4p$	$a^2P - {}^2D^\circ$	$\frac{3}{2} - \frac{5}{2}$		903
	160	464.423	2.6211 - 217.9397	3d ⁷ - 3d ⁶ (a ³ F)4p	$ga^4F - {}^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$, 903
	80	464.483	0. – 215.2929	3d ⁷ - 3d ⁶ (a ³ G)4p	ga⁴F – ⁴G°	$\frac{9}{7} - \frac{7}{7}$		903
	440	465.307	0 - 214.9105	$3d^7 - 3d^6(a^3G)4p$	$ga^4F - {}^4G^\circ$	2 - 2		903
	180	465.504	67.3600 - 282.1795	$3d^7 - 3d^6(b^1D)4p$	$b^2D - D^2$	3-3		903
	220	465.673	28 7777 - 243 5201	$3d^7 - 3d^6(a^{T}F)4p$	$a^2D - {}^2F^\circ$	3 - 5		903
	210	465 862	67.9898 - 282.6452	$3d^{7} - 3d^{6}(h^{1}D)4p$	$b^2D - {}^2D^\circ$	\$_\$		903
	310	466.009	0. – 214.5874	3d ⁷ - 3d ⁶ (a ³ H)4p	$ga^4F - {}^2H^\circ$	$\frac{2}{2} - \frac{2}{2}$		903
		444.124	1 1907 - 215 7245	247 246(-30)4-	4E 411º	7 1		002
	110	400.124	1.1897 - 215.7245	3d - 3d (a O)4p	gar - n	$\frac{2}{7}$	V V	903
	220	400.372	1.1897 - 215.5108	3d = 3d (a G)4p $3d^7 = 3d(a^3G)4p$	gar - r	2 - 2 2 - 1		903
	200	407.001	0 214.1010	3d - 3d (a C)4p $2d^7 - 2d^{6}b^{3}E^{3}A_{-}$	2E 2E°	2 2 2		903
	300	467.373	43.4375 - 257.4064	$3d^{2} - 3d(0^{2}r)4p$	$a^{+}F - F$	$\frac{1}{2} - \frac{1}{2}$		903
	30	467.495	18.3008 - 232.2727	$3d^{2} - 3d(a^{2}D)4p$	$a^{+}P - F$	2 - 2		903
	280	467.856	0 213./39/	3d" – 3d"(a F)4p	ga F - 'G	2 - 2		903
	130	468.149	0 213.6069	3d ⁷ - 3d ⁶ (a ³ G)4p	$ga^{4}F - {}^{2}H^{\circ}$	$\frac{9}{2} - \frac{11}{2}$		903
	230	468.318	1.1897 - 214.7181	3d' - 3d°(a'G)4p	ga*F - *G*	2 - 2		903
	380	468.395	2.0425 - 215.5413	3d' - 3d°(a'G)4p	ga'F – 'F°	2 - 2		903
	560	468.437	2.0425 - 215.5168	3d' - 3d°(a'G)4p	ga⁴F - ⁴F°	$\frac{2}{2} - \frac{2}{2}$		903
	630	468.586	0. – 213.4086	3d' – 3d°(a'G)4p	ga⁴F – ⁴F°	$\frac{2}{2} - \frac{2}{2}$		903
	200	468.931	2.0425 - 215.2929	3d' – 3d⁵(a'G)4p	ga⁴F - ⁴G°	$\frac{2}{2} - \frac{4}{2}$		903
	420	469.133	43.8586 - 257.0180	3d ⁷ – 3d*(b ³ F)4p	$a^2F - {}^2F^\circ$	$\frac{7}{2} - \frac{7}{2}$		903
	20	469.193	0. – 213.1311	3d ⁷ - 3d ⁶ (a ³ F)4p	ga⁴F – ² F°	$\frac{9}{2} - \frac{7}{2}$		903
	30	469.492	27.0965 - 240.0942	3d ⁷ - 3d ⁶ (a ¹ F)4p	$a^2D - {}^2D^\circ$	$\frac{5}{2} - \frac{3}{2}$		903
	670	469.669	1.1897 - 214.1010	3d ⁷ - 3d ⁶ (a ³ G)4p	ga⁴F – ⁴F°	$\frac{1}{2} - \frac{1}{2}$		903
	360	469.706	2.6211 - 215.5168	3d ⁷ - 3d ⁶ (a ³ G)4p	ga⁴F - ⁴F°	$\frac{3}{2} - \frac{5}{2}$		903
	70	470.000	28.7777 - 241.5400	3d ⁷ – 3d ⁶ (b ³ F)4p	$a^2D - {}^4D^\circ$	$\frac{3}{2} - \frac{3}{2}$		903
	20	470.084	18.3668 - 231.0918	3d ⁷ - 3d ⁶ (a ¹ D)4p	a ⁴ P - ² D°	3-5		903
	140	470.124	19.8296 - 232.5395	$3d^{7} - 3d^{6}(a^{1}D)4p$	$a^2G - {}^2F^*$	$\frac{3}{2} - \frac{7}{2}$		903
	440	470.194	2.0425 - 214.7181	$3d^7 - 3d^6(a^3G)4p$	ga⁴F – ⁴G°	$\frac{5}{2} - \frac{5}{2}$		903
	20	470.301			-			903
	340	470.407	2.0425 - 214.6228	$3d^{7} - 3d^{6}(a^{3}F)4p$	ga⁴F – ² G°	$\frac{5}{2} - \frac{7}{2}$		903
	230	470.473	1.1897 - 213.7397	3d ⁷ - 3d ⁶ (a ³ F)4p	$ga^4F - {}^2G^\circ$	$\frac{7}{2} - \frac{9}{2}$		903
	530	471.016	26.6491 - 238.9578	3d ⁷ - 3d ⁶ (a ¹ F)4p	$a^2H - {}^2G^\circ$	<u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u>		903
	140	471.071	0 212.2818	$3d^{7} - 3d^{6}(a^{3}F)4p$	ga⁴F – ⁴G°	3 - 7		903
	630	471.211	1.1897 - 213.4086	$3d^{7} - 3d^{4}(a^{3}G)4p$	ga⁴F – ⁴F°	7 - 9		903
	650	471.236	0 212.2070	$3d^{7} - 3d^{6}(a^{3}F)4p$	ga⁴F – ⁴G°	<u>1</u>		903
	520	471,360	0 212.1509	$3d^{7} - 3d^{6}(a^{3}F)4p$	ga⁴F - ⁴G°	2-2		903
	490	471.476	2.6211 - 214.7181	3d ⁷ – 3d ⁶ (a ³ G)4p	ga⁴F – ⁴G°	$\frac{1}{2} - \frac{5}{2}$		903
	510	471 565	2 0425 - 214 1010	$3d^7 - 3d^6(a^3G)4n$	$ga^4F - {}^4F^\circ$	5_7		903
	210	471 825	1.1897 - 213 1311	$3d^7 - 3d^6(a^3F)4n$	$ga^4F - {}^2F^\circ$	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		903
	410	471.825	27 0965 - 230 0097	$3d^{7} - 3d^{6}(a^{1}F)An$	$a^2D - ^2D^2$	5 5		903
	140	4/1.074	42 4275 255 0440	2d ⁷ 2d ⁶ /L ³ D)/m	$a^2 E^2 D^2$	2 2 2		903
	140	472.338	45.4575 - 255.0040	2d ⁷ 2d ⁶ (a ¹ D)4a	$a^2 G^2 F^2$			903
	20	472.008	20.7470 - 252.5595	$3d^7 = 3d(a D)^4p$	a = F	2 2 2		903
	350	4/3.104	2.0425 - 213.4121	30° - 30°(a°F)4p	gar - G	2 - 2		903

 $\mathbf{NI} \ \mathbf{IV} - \mathbf{Continued}$

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	References
	410	473.225	28.7777 - 240.0942	$3d^{7} - 3d^{6}(a^{1}F)4p$	$a^2D - {}^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$		903
	40	473.308	27 6776 - 238 9578	$3d^{7} - 3d^{6}(a^{1}F)4n$	$a^2H - {}^2G^\circ$	2 - 2		903
	560	473 727	1 1897 - 212 2818	$3d^7 - 3d^6(a^3F)4n$	$\sigma a^4 F = {}^4 G^\circ$	1 1 1		903
	320	473.963	0 - 210.9875	$3d^7 - 3d^6(a^3H)An$	$ra^4 F = {}^2 I^\circ$	2 <u>1</u>		903
	520	473.903	1 1807 212 1500	$3d^{2} - 3d(a^{2}H)4p$	ga T = T	2 - 2 I 9		903
	360	474.017	1.1897 - 212.1309	3d = 3u(a F)4p	ga = -G	2 - 2 2 5		903
	350	4/4.399	2.6211 - 213.4121	30° - 30°(a°F)4p	ga F - G	2-2		903
	440	475.351	23.6489 - 234.0195	3d ⁷ - 3d ⁶ (a ¹ S)4p	$a^2P - {}^2P^\circ$	$\frac{3}{2} - \frac{3}{2}$		903
	580	475.649	2.0425 - 212.2818	3d ⁷ – 3d°(a ³ F)4p	ga⁴F - ⁴G°	$\frac{2}{2} - \frac{4}{2}$		903
	80	475.855	20.9476 - 231.0918	3d ⁷ – 3d ⁶ (a ³ D)4p	$a^2G - ^2D^\circ$	$\frac{1}{2} - \frac{5}{2}$		903
	530	475.912	0 210.1218	3d ⁷ – 3d ⁶ (a ³ F)4p	ga⁴F - ⁴D°	$\frac{9}{2} - \frac{7}{2}$		903
	480	476.6 4 0	27.6776 - 237.4803	3d ⁷ - 3d ⁶ (a ¹ F)4p	$a^2H - {}^2G^\circ$	$\frac{9}{2} - \frac{7}{2}$		903
	530	476.970	2.6211 - 212.2759	3d ⁷ - 3d ⁶ (a ³ F)4p	$ga^4F - {}^2F^\circ$	$\frac{3}{2} - \frac{5}{2}$		903
	50	477 240	43 4375 - 252 9754	3d ⁷ – 3d⁰(b³P)4p	$a^2 F - {}^4 D^\circ$	5-3		903
	60	477 395	43 8586 - 253 3262	$3d^7 = 3d^6(b^3P)4p$	$a^2 \mathbf{F} = {}^4 \mathbf{D}^6$	ź_ź		903
	60	477.375	45.8580 - 255.5202	$3d^{2} - 3d(0T)4p$	a P = D	2 2 2		903
	00	4//.4/5	18.1180 ~ 227.3494	3d - 3d (a D)4p	$a^{4}P - {}^{4}D^{2}$	2 - 2		903
	620	477.550	1.1897 - 210.5906	3d ² - 3d ² (a ² P)4p	ga F - D	2 - 2		903
	460	477.573	0. – 209.3914	3d ² – 3d ² (a ² H)4p	ga'F - 'G'	$\frac{1}{2} - \frac{2}{3}$		903
	100	477.623	24.6514 - 234.0195	3d' - 3d'(a'S)4p	a'P - 'P'	$\frac{1}{2} - \frac{1}{2}$		903
	170	477.897	23.6489 - 232.8970	3d ⁷ - 3d ⁶ (a ¹ D)4p	$a^2P - {}^2P^{\circ}$	$\frac{3}{2} - \frac{1}{2}$		903
	240	477.998	2.0425 - 211.2468	3d ⁷ – 3d ⁶ (a ³ F)4p	ga4F - 4D°	$\frac{5}{2} - \frac{3}{2}$		903
	20	478.162	0 209.1319	3d ⁷ – 3d ⁶ (a ³ H)4p	ga ⁴ F - ² G°	$\frac{9}{2} - \frac{9}{2}$	Q	903
	580	478.501	2.0425 - 211.0276	3d ⁷ - 3d ⁶ (a ³ P)4p	ga ⁴ F - ⁴ D°	$\frac{5}{2} - \frac{3}{2}$		903
	420	478.618	0 208.9336	$3d^7 - 3d^6(a^3F)4p$	$ga^4F - {}^4F^\circ$	$\frac{2}{2} - \frac{2}{2}$		903
	570	478.668	0. – 208.9121	3d ⁷ – 3d°(a ³ P)4p	$ga^4F - {}^4D^\circ$	$\frac{9}{2} - \frac{7}{2}$		903
	450	479 088	2 6211 - 211 3517	3d ⁷ – 3d⁰(a³F)4n	ga⁴F – ⁴D°	3_1		903
	580	479.175	10 8206 - 228 5185	$3d^{7} - 3d^{6}(a^{3}D)An$	$a^2 C = {}^2 F^{\circ}$	2 2		903
	320	479.221	2 6211 211 2469	$3d^{7} = 3d^{6}(a^{3}E)An$	a O = I	$\frac{2}{2}$ $\frac{2}{2}$		903
	320	479.331	2.0211 - 211.2408	3d - 3d(a F) + p $2d^7 - 2d^6(a^3 F) + p$	$ga \Gamma = D$	2 - 2 5 5		503 002
	200	479.304	2.0425 - 210.5906	$3d^2 - 3d^2(a^2P)4p$	ga F - D	$\frac{1}{2} - \frac{1}{2}$		903
	200	4/9.828	2.0211 - 211.02/6	3d" - 3d"(a'P)4p	ga F - D	2 - 2		903
	630	480.003	0 208.3307	3d° - 3d°(a°F)4p	ga'F - 'F'	2 - 2		903
	610	480.026	20.9476 – 229.2695	3d ⁷ - 3d ⁶ (a ³ D)4p	$a^2G - {}^2F^\circ$	$\frac{7}{2} - \frac{5}{2}$		903
	300	480.197	24.6514 - 232.8970	3d ⁷ – 3d ⁶ (a ¹ D)4p	$\mathbf{a}^{2}\mathbf{P} - {}^{2}\mathbf{P}^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		903
	310	480.908	1.1897 - 209.1319	3d ⁷ – 3d ⁶ (a ³ H)4p	ga⁴F - ² G°	$\frac{7}{2} - \frac{9}{2}$		903
	420	481.151	43.8586 - 251.6943	3d ⁷ – 3d ⁶ (b ³ F)4p	$a^2F - ^2D^\circ$	$\frac{7}{2} - \frac{5}{2}$		903
	460	481.359	1.1897 - 208.9336	3d ⁷ – 3d ⁶ (a ³ F)4p	ga ⁴ F - ⁴ F°	$\frac{7}{2} - \frac{9}{2}$		903
	40	481.410	1.1897 - 208.9121	3d ⁷ - 3d ⁶ (a ³ P)4p	$ga^4F - ^4D^\circ$	$\frac{7}{2} - \frac{7}{2}$		903
	390	481.485	2.6211 - 210.3133	3d ⁷ - 3d ⁶ (a ³ P)4p	ga⁴F - ⁴D°	$\frac{3}{2} - \frac{1}{2}$		903
	100	481.756	20.9476 - 228.5185	3d ⁷ - 3d ⁶ (a ³ D)4p	$a^2G - {}^2F^{\circ}$	3-3		903
	360	481.907	43,4375 - 250,9510	$3d^{7} - 3d^{6}(h^{3}F)4p$	$a^2F - ^2D^\circ$	3-3		903
	340	482.055	23.6489 - 231.0918	$3d^7 - 3d^6(a^1D)4p$	$a^2P - ^2D^\circ$	3-5		903
	160	482.123	1.1897 - 208.6057	$3d^{7} - 3d^{6}(a^{3}E)4n$	$ga^4F - {}^4F^\circ$	1 1		903
	300	482.279	2.0425 - 209.3914	3d ⁷ - 3d ⁶ (a ³ H)4p	$ga^4F - {}^2G^\circ$	$\frac{2}{2} - \frac{7}{2}$		903
	420	182 765	1 1907 200 2207	2.47 2.46(-315).4-	20 ⁴ E 4E ⁹	2 7		001
	220	402.705	1.1077 - 200.3307	3u - 3u (a r)4p	gar - r	2 - 2		7 03
	320	482.8//	24.0314 - 231.7420	30' - 30'(a'D)4p	a ⁻ P - ⁴ D ⁻	2 - 2		903
	330	483.043	18.1186 - 225.1369	3d' – 3d'(a'D)4p	a'P - 'D'	2 - 2		903
	220	483.276	27.0965 - 234.0195	3d' - 3d°(a'S)4p	a'D - 'P"	2 - 2		903
	70	483.388	19.8296 - 226.7025	3d ⁷ - 3d ⁶ (a ¹ I)4p	$a^2G - {}^2I^\circ$	$\frac{1}{2} - \frac{11}{2}$		903
	190	483.515	18.1186 - 224.9369	3d ⁷ - 3d ⁶ (a ³ D)4p	a ⁴ P – ² P°	$\frac{2}{2} - \frac{4}{2}$		903
	30	483.699	0. – 206.7407	3d ⁷ - 3d ⁶ (a ³ H)4p	ga⁴F - ⁴I°	$\frac{9}{2} - \frac{11}{2}$		903
	50	483.774	18.1186 - 224.8249	3d ⁷ – 3d ⁶ (a ³ D)4p	a ⁴ P - ⁴ F°	$\frac{5}{2} - \frac{7}{2}$		903
	40	484.020	20.9476 - 227.5494	3d ⁷ - 3d ⁶ (a ³ D)4p	$a^2G - {}^2D^\circ$	$\frac{1}{2} - \frac{5}{2}$		903
	300	484.114	2.0425 - 208.6057	$3d^{7} - 3d^{6}(a^{3}F)4p$	ga ⁴ F - ⁴ F°	3-3		903
	330	484,201	18.1186 - 224.6457	$3d^{2} - 3d^{6}(a^{3}D)4n$	a ⁴ P - ⁴ D ^o	1 4 4		903
	340	484,456	2.0425 - 208.4610	$3d^7 - 3d^6(a^3P)4n$	$ga^4F - {}^4P^4$	1 1 1		903
			2.0.25 200.4010		Barri	2 - 2		,05

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Multiplet Rel. In	t. λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
470	484.637	0. – 206.3409	3d ⁷ - 3d ⁶ (a ³ H)4p	ga⁴F - ⁴G°	$\frac{9}{2} - \frac{9}{2}$		903
270	484.759	2.0425 - 208.3307	$3d^{7} - 3d^{6}(a^{3}F)4p$	ga⁴F – ⁴F°	$\frac{2}{2} - \frac{1}{2}$		903
260	484.778	18.3668 - 224.6457	$3d^{7} - 3d^{6}(a^{3}D)4p$	$a^4P - {}^4D^\circ$	$\frac{2}{2} - \frac{2}{2}$		903
330	485.091	2.6211 - 208.7669	$3d^{7} - 3d^{6}(a^{3}F)4p$	ga⁴F – ⁴F°	$\frac{3}{2} - \frac{3}{2}$		903
190	485.310	18.1186 - 224.1740	$3d^{7} - 3d^{6}(a^{3}D)4p$	a ⁴ P - ⁴ D°	$\frac{2}{2} - \frac{3}{2}$		903
50	485.350	18.9584 - 224.9965	3d ⁷ - 3d ⁶ (a ³ D)4p	$a^4P - {}^2P^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
650	485.425	0 206.0053	3d ⁷ - 3d ⁶ (a ³ H)4p	ga⁴F - ⁴G°	$\frac{9}{2} - \frac{11}{2}$		903
360	485.472	2.6211 - 208.6057	3d ⁷ – 3d ⁶ (a ³ F)4p	ga⁴F – ⁴F°	$\frac{3}{2} - \frac{5}{2}$		903
310	485.536	18.1186 - 224.0753	3d ⁷ – 3d ⁶ (a ¹ G)4p	$a^4P - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		903
20	485.604	19.8296 - 225.7585	$3d^{7} - 3d^{6}(a^{1}G)4p$	a ² G - ² H°	$\frac{9}{2} - \frac{11}{2}$		903
100	485.670	18.1186 - 224.0213	$3d^7 - 3d^6(a^3D)4p$	a⁴P – ⁴F°	$\frac{5}{2} - \frac{5}{2}$		903
30	485.814	2.6211 - 208.4610	3d ⁷ - 3d ⁶ (a ³ P)4p	$ga^4F - {}^4P^\circ$	$\frac{3}{2} - \frac{3}{2}$		903
290	485.892	18.3668 - 224.1740	3d ⁷ – 3d ⁶ (a ³ D)4p	$a^4P - {}^4D^\circ$	$\frac{3}{2} - \frac{3}{2}$		903
20	486.117	1					903
100	486.204	1.1897 - 206.8655	3d ⁷ – 3d ⁶ (a ³ H)4p	ga⁴F – ⁴H°	$\frac{7}{2} - \frac{9}{2}$		903
80	486.254	18.3668 - 224.0213	$3d^7 - 3d^6(a^3D)4p$	a⁴P - ⁴F°	3-5		903
530	486.725	1.1897 - 206.6457	$3d^7 - 3d^6(a^3H)4p$	ga⁴F – ⁴G°	1 3 - 3		903
330	486.758	27.0965 - 232.5395	3d ⁷ - 3d ⁶ (a ¹ D)4p	$a^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		903
330	486 812	18 3668 - 223 7854	$3d^{7} - 3d^{6}(a^{3}D)4n$	a ⁴ P – ⁴ D°	3_1		903
480	487.014	1 1897 - 206 5232	$3d^{7} - 3d^{6}(a^{3}P)4p$	$a^4F = {}^4P^6$	2 2		903
480	487.014	10 8296 - 225 1369	$3d^{7} - 3d^{6}(a^{3}D)4p$	$a^2G = {}^4D^9$	$\frac{2}{9}$ $\frac{2}{7}$		903
250	487.071	19.8296 225.1509	$3d^{7} - 3d^{6}(a^{3}D)Ap$	$a^2G = {}^4F^\circ$	2^{-2}_{2-2}		903
250	487.170	19.8290 - 223.0904	3d - 3d (a D) + p $3d^{7} - 3d^{6}(a^{1}S) + p$	a O - F $a^2 D - ^2 P^{\circ}$	$\frac{2}{3}$ $\frac{2}{3}$		903
90	487.234	2.6211 - 207.8462	$3d^{7} - 3d^{6}(a^{3}P)4p$	a D - P $ga^4F - ^4P^\circ$	2 - 2 $\frac{3}{2} - \frac{1}{2}$		903 903
				20 200			
380	487.396	27.0965 - 232.2727	$3d^2 - 3d^2(a^2D)4p$	$a^2D - F^2$	$\frac{1}{2} - \frac{1}{2}$		903
600	487.446	1.1897 - 206.3409	3d' - 3d'(a'H)4p	ga F - G	$\frac{1}{2} - \frac{1}{2}$		903
100	487.584	2.0425 - 207.1360	3d' - 3d'(a'H)4p	ga'F - 'H'	2 - 2		903
80	487.819	19.8296 - 224.8249	3d' - 3d'(a'D)4p	$a^{2}G - F^{2}$	$\frac{2}{7} - \frac{1}{2}$		903
400	487.910	20.9476 - 225.9037	3d' - 3d'(a'1)4p 3d' - 3d'(a'G)4p	$a^2G - {}^2H^2$	$\frac{1}{2} - \frac{1}{2}$		903
590	407.907	19.8290 - 224.7015	3u - 3u (a C)Ap	a 0 - 0	2 - 2		<i>)</i> 03
270	488.141	18.3668 - 223.2254	3d ⁷ – 3d ⁶ (a ³ D)4p	a ⁴ P - ⁴ P°	$\frac{3}{2} - \frac{1}{2}$		903
380	488.274	2.0425 - 206.8470	$3d^7 - 3d^6(a^3H)4p$	ga⁴F – ⁴G°	$\frac{5}{2} - \frac{5}{2}$		903
290	488.653	27.0965 - 231.7420	3d ⁷ – 3d ⁶ (a'D)4p	$a^2D - {}^2D^\circ$	$\frac{5}{2} - \frac{3}{2}$		903
570	488.754	2.0425 - 206.6457	3d ⁷ - 3d ⁶ (a ³ H)4p	ga⁴F - ⁴G°	$\frac{5}{2} - \frac{7}{2}$		903
340	488.842	23.6489 - 228.2142	$3d^7 - 3d^6(a^1D)4p$	$a^2P - {}^2P^\circ$	$\frac{3}{2} - \frac{3}{2}$		903
410	488.892	18.1186 - 222.6629	3d ⁷ - 3d ⁶ (a ³ D)4p	$a^4P - {}^4P^\circ$	$\frac{5}{2} - \frac{3}{2}$		903
470	489.036	20.9476 - 225.4316	$3d^7 - 3d^6(a^1G)4p$	$a^2G - {}^2F^\circ$	7 - 5		903
30	489.486	18.3668 - 222.6629	$3d^7 - 3d^6(a^3D)4p$	$a^4P - {}^4P^\circ$	3-3		903
250	489.558	18.9584 - 223.2254	$3d^7 - 3d^6(a^3D)4p$	$a^4P - {}^4P^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
350	489.608	19.8296 - 224.0753	$3d^7 - 3d^6(a^1G)4p$	$a^2G - {}^2F^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		903
590	489.658	2.6211 - 206.8470	$3d^7 - 3d^6(a^3H)4p$	ga ⁴ F - ⁴ G°	$\frac{3}{2} - \frac{5}{2}$		903
580	489.682	18.1186 - 222.3333	3d ⁷ - 3d ⁶ (a ³ D)4p	a ⁴ P – ⁴ P°	$\frac{5}{2} - \frac{5}{2}$		903
20	489 915	28 7777 - 232 8970	3d ⁷ - 3d⁰(a¹D)4p	$a^2D - {}^2P^{\circ}$	3-1		903
30	490 213	27 0965 - 231 0918	$3d^7 - 3d^6(a^1D)4p$	$a^2D - {}^2D^\circ$	\$ _ \$		903
420	490 275	18 3668 - 222 3333	$3d^7 - 3d^6(a^3D)4p$	$a^4P - {}^4P^\circ$	3 - 5		903
160	490.275	23 6489 - 227 5494	$3d^{7} - 3d^{6}(a^{3}D)4p$	$a^2 P - {}^2 D^\circ$	3_5		903
280	490 494	20.9476 - 224.8249	$3d^7 = 3d^6(a^3D)4r$	$a^2G - {}^4F^\circ$	1 _ 1		903
430	490.906	18.9584 - 222.6629	$3d^{7} - 3d^{6}(a^{3}D)4p$	$a^4P - {}^4P^\circ$	$\frac{1}{2} - \frac{3}{2}$		903
200	401 353	24 6514 229 2142	247 2466-1534-	2 D 2 D °	1 2		003
320	491.253	24.0314 - 228.2142	$3d^{2} - 3d^{2}(a^{2}D)4p$	$a^2 P = P^2$	$\frac{2}{3}$ $\frac{-2}{3}$		903
300	491.328	23.0489 - 227.1811	30" - 30"(a"D)4p	$a^2 P - D^2$	$\frac{1}{2} - \frac{1}{2}$		903
590	491.364	20.9476 - 224.4636	3d' - 3d'(a'G)4p		$\frac{2}{3} - \frac{1}{2}$		903
280	491.422	28.7777 - 232.2727	3d' – 3d°(a'D)4p	a D - F	2 - 2		903
550	492.216	19.8296 - 222.9933	3d' – 3d'(a'l)4p	a G - H	2 - 2		903
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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	1 - 1	Notes	References
	160	492.441	2.0425 - 205.1141	3d ⁷ - 3d ⁶ (a ³ P)4p	ga ⁴ F - ⁴ S°	1-1		903
	170	492.705	28.7777 - 231.7420	$3d^{7} - 3d^{6}(a^{1}D)4p$	$a^2D - ^2D^\circ$	3-3		903
	360	492.917	19.8296 - 222.7055	$3d^7 - 3d^6(a^1G)4p$	$a^2G - {}^2H^\circ$	2 2		903
	40	493,756	24.6514 - 227.1811	$3d^{7} - 3d^{6}(a^{3}D)4p$	$a^2P - ^2D^\circ$	1_1		903
	220	494,286	28 7777 - 231 0918	$3d^7 - 3d^6(a^1D)4n$	$a^2D - ^2D^4$	1 1		903
	20	494 565	19 8296 - 222 0293	$3d^7 - 3d^6(a^3G)4p$	$a^2G - {}^2G^{\circ}$	2 1		903
	20	474.505	17.8290 - 222.0293	50 - 50 (a C) , p	a 0 - 0	2 - 2		505
	120	494.658	19 8296 - 221,9910	$3d^{7} - 3d^{6}(a^{3}G)4n$	$a^2G - {}^2G^\circ$	2 - 2		903
	30	494 871				2 2		903
	50	495 584	23 6489 - 225 4316	$3d^7 - 3d^6(a^1G)An$	$a^2 P - {}^2 F^{\circ}$	1 1		903
	520	495 648	25.0407 - 225.4510	$3d^{7} - 3d^{6}(a^{1}G)Ap$	$a^2G - {}^2H^\circ$	2 2 2 2 2 2		903
	100	496 470	20.9470 - 222.7035	$3d^{2} - 3d^{2}(a^{3}D)4p$	aO = H $a^2D = {}^2F^{\circ}$	2 - 2 5 - 1		903
	80	496 660	27.0909 - 220.9109	$3d^{7} - 3d^{6}(a^{3}D)4p$	$aD = 1^{\circ}$ $a^2D = ^2D^{\circ}$	2^{-2} 3^{-1}		903
		470.000	23.0407 - 224.7703	50 - 50 (a D)Ap		2 - 2		705
	170	406 906	23 6480 - 224 9369	$3d^{7} - 3d^{6}(a^{3}D)Mp$	$p^2 \mathbf{D} = {}^2 \mathbf{D}^{o}$	3 3		903
	410	407 222	23.0469 - 224.9309	$3d^{7} - 3d^{6}(a^{1}D)An$	$a \Gamma = \Gamma$ $a^2 D 2 P^2$	2^{-2}		903
	200	497.235	27.0905 - 228.2142	$3d^7 - 3d^6(a^3G)Am$	aD - T			903
	400	497.313	20.7470 - 222.0293	2d7 2d6(alS)4m	a G - G	2 2 2		903
	400	498.700	28.7777 229.2973	247 - 246(-3D)4p	$a^2D - P$	$\frac{1}{2} - \frac{1}{2}$		903
	200	498.783	28.7777 - 229.2095	30' - 30'(a'D)4p	$a^2D - F^2$	2 - 2		903
	390	498.873	27.0965 - 227.5494	3d' - 3d'(a'D)4p	$a^{2}D - b^{2}$	$\bar{2} - \bar{2}$		903
	1.50			217 216(37)4	20 200	1 1		
	150	499.141	24.6514 - 224.9965	3d' - 3d°(a'D)4p	$a^2P - ^2P^2$	2 - 2		903
	470	499.805	43.4375 - 243.5201	3d' - 3d°(a'F)4p	a ² F - ² F°	2 - 2	1	903
	620	499.840	19.8296 - 219.8960	3d' - 3d°(a'G)4p	$a^2G - {}^2F^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
	550	499.873	26.6491 - 226.7025	3d' - 3d°(a'I)4p	$a^2H - {}^2I^\circ$	2 - 2		903
	600	499.915	26.6491 - 226.6850	3d' - 3d°(a'I)4p	$a^2H - {}^2I^\circ$	2 - 2		903
	410	500.165	19.8296 - 219.7650	3d ⁷ - 3d ⁶ (a ³ G)4p	$a^2G - {}^2H^\circ$	$\frac{y}{2} - \frac{y}{2}$		903
	350	500.799	43.8586 - 243.5420	3d ⁷ − 3d ⁶ (a ¹ F)4p	$a^2F - {}^2F^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
	70	500.856	43.8586 - 243.5201	3d ⁷ - 3d ⁶ (a ¹ F)4p	$a^2F - {}^2F^\circ$	$\frac{1}{2} - \frac{5}{2}$		903
	120	501.065	18.3668 - 217.9397	3d ⁷ - 3d ⁶ (a ³ F)4p	$a^4P - ^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$		903
	120	502.179	24.6514 - 223.7854	3d ⁷ – 3d ⁶ (a ³ D)4p	$a^2P - {}^4D^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
	540	502.243	26.6491 - 225.7585	3d ⁷ - 3d ⁶ (a ¹ G)4p	a ² H - ² H°	$\frac{11}{2} - \frac{11}{2}$		903
	90	502.391	18.3668 - 217.4143	3d ⁷ - 3d ⁶ (a ³ F)4p	$a^4P - ^2D^\circ$	$\frac{3}{2} - \frac{5}{2}$		903
	600	502.447	19.8296 - 218.8606	3d ⁷ - 3d ⁶ (a ³ H)4p	$a^2G - {}^2H^\circ$	$\begin{vmatrix} 2 \\ 2 \\ - \frac{11}{2} \end{vmatrix}$		903
	290	502.978	20.9476 - 219.7650	3d ⁷ – 3d ⁶ (a ³ G)4p	$a^2G - {}^2H^\circ$	$\frac{7}{2} - \frac{9}{2}$	1	903
	130	503.089	28.7777 – 227.5494	3d ⁷ – 3d ⁶ (a ³ D)4p	$a^2D - ^2D^\circ$	$\frac{1}{2} - \frac{5}{2}$		903
	480	503.512	20.9476 - 219.5534	3d ⁷ – 3d ⁶ (a ³ G)4p	$a^2G - {}^2F^\circ$	$\frac{7}{2} - \frac{5}{2}$		903
	90	503.931	26.6491 - 225.0964	3d ⁷ – 3d ⁶ (a ³ D)4p	a ² H - ⁴ F°	$\frac{11}{2} - \frac{9}{2}$		903
	250	504.032	28.7777 - 227.1811	3d ⁷ - 3d ⁶ (a ³ D)4p	$a^2D - ^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$		903
	610	504.477	27.6776 - 225.9037	3d ⁷ – 3d ⁶ (a ¹ I)4p	a ² H – ² H°	$\frac{9}{2} - \frac{9}{2}$		903
	210	504.770	26.6491 - 224.7615	3d ⁷ - 3d ⁶ (a ¹ G)4p	$a^{2}H - {}^{2}G^{\circ}$	$\frac{11}{2} - \frac{9}{2}$		903
	360	504.847	27.6776 - 225.7585	3d ⁷ - 3d ⁶ (a ¹ G)4p	$a^2H - {}^2H^\circ$	$\frac{9}{2} - \frac{11}{2}$		903
	320	504.951	27.0965 - 225.1369	3d ⁷ – 3d ⁶ (a ³ D)4p	$a^2D - {}^4D^\circ$	$\frac{5}{2} - \frac{7}{2}$		903
	220	505.467	27.0965 - 224.9369	3d ⁷ - 3d ⁶ (a ³ D)4p	$a^2D - {}^2P^\circ$	$\frac{5}{2} - \frac{3}{2}$		903
	190	505.750	27.0965 - 224.8249	3d ⁷ – 3d ⁶ (a ³ D)4p	$a^2D - {}^4F^\circ$	$\frac{5}{2} - \frac{7}{2}$		903
	120	506.434	27.6776 - 225.1369	3d ⁷ - 3d ⁶ (a ³ D)4p	a²H - ⁴D°	$\frac{9}{2} - \frac{7}{2}$		903
	60	506.539	27.6776 - 225.0964	3d ⁷ - 3d ⁶ (a ³ D)4p	a ² H - ⁴ F°	$\frac{9}{2} - \frac{9}{2}$		903
	60	506.675	27.0965 - 224.4636	3d ⁷ - 3d ⁶ (a ¹ G)4p	a ² D - ² G°	$\frac{5}{2} - \frac{7}{2}$		903
	120	507.207	18.3668 - 215.5310	3d ⁷ - 3d ⁶ (a ³ P)4p	$a^4P - {}^2S^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
	480	507.400	27.6776 - 224.7615	3d ⁷ - 3d ⁶ (a ¹ G)4p	$a^2H - {}^2G^\circ$	2 - 2		903
	590	508.179	27.6776 - 224.4636	$3d^7 - 3d^6(a^1G)4p$	$a^{2}H - {}^{2}G^{\circ}$	2 - 7		903
						1		
	330	508.510	28.7777 - 225.4316	3d ⁷ - 3d ⁶ (a ¹ G)4p	$a^2D - {}^2F^\circ$	3-5		903
	200	509,170	27.6776 - 224.0753	$3d^7 - 3d^6(a^1G)4p$	$a^2H - {}^2F^{\circ}$	2 1		903
	610	509.313	26.6491 - 222.9933	$3d^7 - 3d^6(a^1)A_D$	$a^2H - {}^2H^\circ$	ų_1		903
	40	509.796	28.7777 - 224.9369	$3d^7 - 3d^6(a^3D)4n$	$a^2D - {}^2P^\circ$	$\frac{2}{3}$		903
	50	510.061	26.6491 - 222.7055	$3d^7 - 3d^6(a^1G)4n$	$a^2H - {}^2H^\circ$	11 2		903
	70	510.449	19.8296 - 215.7361	$3d^{7} - 3d^{6}(a^{3}G)4n$	a ² G - ⁴ H°	2 2		903
						2 2		

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NI IV — Continued

ultiplet Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm 1)	Configurations	Terms	J - J	Notes	Reference
310	510.584	19.8296 - 215.6845	3d ⁷ - 3d ⁶ (a ³ G)4p	$a^2G - {}^4H^\circ$	$\frac{9}{2} - \frac{11}{2}$		903
30	511.025	18.3668 - 214.0558	$3d^{7} - 3d^{6}(a^{3}P)4p$	$a^4P - {}^2P^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
80	511.339	27.0965 - 222.6629	3d ⁷ - 3d ⁶ (a ³ D)4p	$a^2D - {}^4P^\circ$	$\frac{5}{2} - \frac{3}{2}$		903
580	511.925	26.6491 - 221.9910	3d ⁷ - 3d ⁶ (a ³ G)4p	$a^2H - {}^2G^\circ$	$\frac{11}{2} - \frac{9}{2}$		903
130	512.432	43.8586 - 239.0087	$3d^{7} - 3d^{6}(a^{1}F)4p$	$a^2F - ^2D^\circ$	$\frac{1}{2} - \frac{5}{2}$		903
70	512.568	43.8586 - 238.9578	$3d^{7} - 3d^{6}(a^{1}F)4p$	$a^2F - {}^2G^\circ$	$\frac{1}{2} - \frac{9}{2}$		903
200	512.747	27.6776 - 222.7055	3d ⁷ - 3d ⁶ (a ¹ G)4p	a ² H - ² H °	$\frac{9}{2} - \frac{9}{2}$		903
60	512.786	18.1186 - 213.1311	$3d^7 - 3d^6(a^3F)4p$	$a^4P - {}^2F^\circ$	$\frac{5}{2} - \frac{1}{2}$		903
80	512.999	27.0965 - 222.0293	3d ⁷ - 3d ⁶ (a ³ G)4p	$a^2D - {}^2G^\circ$	$\frac{5}{2} - \frac{7}{2}$		903
230	513.371	19.8296 - 214.6228	$3d^{7} - 3d^{6}(a^{3}F)4p$	$a^2G - {}^2G^\circ$	$\frac{9}{2} - \frac{7}{2}$		903
90	513.458	19.8296 - 214.5874	$3d^{7} - 3d^{6}(a^{3}H)4p$	$a^2G - {}^2H^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
150	514.023	67.9898 - 262.5387	$3d^{7} - 3d^{6}(b^{1}G)4p$	$b^2D - {}^2G^\circ$	$\frac{5}{2} - \frac{7}{2}$		903
290	514.173	19.8296 - 214.3168	3d ⁷ - 3d ⁶ (a ³ G)4p	a²G - ⁴G°	$\frac{9}{2} - \frac{11}{2}$		903
510	514.525	27.6776 - 222.0293	$3d^{7} - 3d^{6}(a^{3}G)4p$	$a^2H - {}^2G^\circ$	$\frac{9}{2} - \frac{7}{2}$		903
90	514.628	27.6776 - 221.9910	$3d^7 - 3d^6(a^3G)4p$	$a^2H - {}^2G^\circ$	$\frac{9}{2} - \frac{9}{2}$		903
260	514.684	23.6489 - 217.9397	$3d^7 - 3d^6(a^3F)4p$	$a^2P - {}^2D^\circ$	$\frac{3}{3} - \frac{3}{3}$		903
90	515,164	26.6491 - 220.7626	$3d^7 - 3d^6(a^1I)4p$	$a^2H - {}^2K^\circ$	<u><u> </u></u>		903
120	515.358	43.4375 237.4803	$3d^7 - 3d^{\circ}(a^1F)4p$	$a^2F - {}^2G^\circ$	$\frac{5}{2} - \frac{7}{2}$		903
230	515 560	20 9476 - 214 9105	3d ⁷ – 3d⁵(a³G)4n	$a^2G - {}^4G^\circ$	7 - 9		903
550	515 701	19 8296 - 213 7397	$3d^7 - 3d^6(a^3E)4n$	$a^2G - C^{\circ}$	2 - 2		903
280	515 823	67 3600 - 261 2263	$3d^{7} - 3d^{6}(h^{1}G)4n$	$b^2D - F^{\circ}$	3_3		903
550	516.057	19 8296 - 213 6069	$3d^{7} - 3d^{6}(a^{3}G)4p$	$a^2G = {}^2H^\circ$	į 2 μ		903
570	516.070	236489 - 2174143	$3d^{7} - 3d^{6}(a^{3}E)4p$	$a^2 P - {}^2 D^\circ$	1 1 1		903
490	516.324	20.9476 - 214.6228	$3d^{7} - 3d^{6}(a^{3}F)4p$	$a^2G - {}^2G^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
140	\$16.420	20.0476 214 5974	2d ⁷ 2d ⁹ (a ³ U)4p	2G 2H	1 2		903
470	517 229	20.9470 - 214.3674	$3d^7 - 3d^6(a^3E)4p$	$a^2G = H$	2^{-2} 2^{-1}		903
470	517.328	19.8290 - 213.1311	$3d^7 = 3d(a^3F)4p$	$aU = P^{2}$	1 3		903 003
430	517.347	24.0514 - 217.9397	3d - 3d (a r)4p	$a \mathbf{r} = \mathbf{D}$	$\frac{2}{1}$		903 003
80	517.719	20.9476 - 214.1010	3d - 3d (a C)4p		2 - 2 3 1		903 002
190	518.175 518.449	18.3668 - 211.3317	$3d^{7} - 3d^{6}(a^{3}F)4p$	$a^{4}P - {}^{4}D^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		903 903
100	610 (02	10 1106 210 0426		4D 4D°	5 5		003
150	518.602	18.1180 - 210.9430	30 = 30 (a F)4p	$a \mathbf{r} - \mathbf{D}$	3 7		903
510	518.670	27.0965 - 219.8960	$3d^{2} - 3d^{2}(a^{2}G)4p$	$a^{-}D - F$	$\frac{1}{2} - \frac{1}{2}$		903
150	519.041	18.3668 - 211.0276	$3d^2 - 3d^2(a^2P)4p$	a'P - D'	3 - 5		903
190	519.265	18.3668 - 210.9436	$3d^{2} - 3d^{2}(a^{2}F)4p$	$a^{-}P - D^{-}$	2-2		903
290	519.556 519.572	18.1186 - 210.5906 20.9476 - 213.4121	$3d^{7} - 3d^{6}(a^{3}F)4p$ $3d^{7} - 3d^{6}(a^{3}F)4p$	$a^{2}P - {}^{2}D^{2}$ $a^{2}G - {}^{4}G^{2}$	<u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u>		903 903
				10 100			
200	519.605	19.8296 - 212.2818	3d' - 3d'(a'F)4p	$a^2G - {}^*G^*$	$\frac{1}{2} - \frac{1}{2}$		903
230	519.767	18.9584 - 211.3517	$3d^7 - 3d^{(0)}(a^3F)4p$	$a^{T}P - D^{T}$	2 - 2		903
340	519.848	67.9898 - 260.3555	3d ² - 3d ⁶ (b ² G)4p	6-D - F	2 - 2		903
330	519.959	19.8296 - 212.1509	$3d^2 - 3d^2(a^2F)4p$		$\frac{5}{1} = \frac{5}{3}$		903
410	520.042	18.9584 - 211.2468 18.3668 - 210.5906	$3d^{7} - 3d^{6}(a^{3}P)4p$ $3d^{7} - 3d^{6}(a^{3}P)4p$	$a^4P - D^6$ $a^4P - D^6$	$\begin{vmatrix} \frac{5}{2} - \frac{5}{2} \\ \frac{3}{2} - \frac{5}{2} \end{vmatrix}$		903 903
660	620.257	26 6401 219 8606	2.47 2.46(-31).4-	211 2110	1 п п		903
550	520.256	20.0471 - 218.8000	$3u - 3u^{2}(a^{2}H)4p$ $34^{7} - 34^{6}(a^{3}C)4-$	ann	2 2 2	ļ	903 002
430	520.587	27.6776 - 219.7650	3d - 3d (a' G) + p	$a \Pi - \Pi$	2^{-2}		903 003
80	520.038	18.9384 - 211.0276	3d - 3d (a F)4p $3d^{2} - 3d^{2}(a^{3}E)4p$	$a \mathbf{F} = \mathbf{D}$	$\frac{2}{5}$ $\frac{2}{1}$		903 003
390	520.817	18.1180 - 210.1218	3u - 3u (a r) + p $2d^7 - 2d^6(a^3 R) + p$	$a \mathbf{r} - \mathbf{D}$ $a^2 \mathbf{D} = 2\mathbf{S}^{\circ}$	2 - 2 3 - 1		903 002
260	521.156 522.646	23. 64 89 - 215.5310 20.9 47 6 - 212.2818	$3d^{7} - 3d^{6}(a^{3}F)4p$ $3d^{7} - 3d^{6}(a^{3}F)4p$	$a^2 F = 3$ $a^2 G = {}^4 G^\circ$	$\begin{array}{c} \frac{1}{2} - \frac{1}{2} \\ \frac{1}{2} - \frac{1}{2} \end{array}$		903 903
			1.17 - 216/ 3TD 4	-211 7110	9 11		007
60	523.051	27.6776 - 218.8606	30' - 30'(a'H)4p	a'H - 'H'	$\begin{bmatrix} 2 & -\frac{1}{2} \\ 1 & -\frac{1}{2} \end{bmatrix}$		903
180	523.892	24.6514 - 215.5310	3d' - 3d'(a'P)4p	a-r - 'S'	$\frac{1}{2}$		903
40	523.983	27.0965 - 217.9397	3d' - 3d°(a'F)4p	$a^{-}D - D^{-}D^{-}$	2-2		903
410	524.164	28.7777 - 219.5534	3d' – 3d°(a'G)4p	a'D - 'F"	2 2		903
50	524.956	18.1186 - 208.6057	3d' - 3d°(a'F)4p	a*P - *F*	$\frac{1}{2} - \frac{3}{2}$		903
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NI IV - Continued

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	70	525.362	18.1186 - 208.4610	3d ⁷ – 3d ⁶ (a ³ P)4p	a ⁴ P - ⁴ P°	$\frac{5}{2} - \frac{3}{2}$		903
	460	525.423	27.0965 - 217.4143	$3d^7 - 3d^6(a^3F)4p$	$a^2D - {}^2D^\circ$	3 - 5		903
	50	525.500	19.8296 - 210.1218	$3d^7 - 3d^6(a^3F)4p$	$a^2G - {}^4D^\circ$	<u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u>		903
	120	525.641	18.3668 - 208.6057	$3d^7 - 3d^6(a^3F)4p$	$a^4P - {}^4F^\circ$	3-5		903
	250	525.041	18 1186 - 208 3307	$3d^7 - 3d^6(a^3F)4p$	$a^4P - {}^4F^\circ$	1 <u>1</u>		903
	510	525.793	18.1180 - 200.5507	50 = 50 (a 1)+p		2 - 2		903
	510	525.175						705
	180	526.199	67.3600 - 257.4064	3d ⁷ – 3d ⁶ (b ³ F)4p	b ² D - ² F [•]	$\frac{3}{2} - \frac{5}{2}$		903
	250	526.341	23.6489 - 213.6402	3d ⁷ - 3d ⁶ (a ³ P)4p	$a^2P - {}^2P^\circ$	$\frac{3}{2} - \frac{1}{2}$		903
	490	528.248	19.8296 - 209.1319	3d ⁷ – 3d ⁶ (a ³ H)4p	a ² G - ² G°	$\frac{9}{2} - \frac{9}{2}$		903
	300	528.608	20.9476 - 210.1218	3d ⁷ – 3d ⁶ (a ³ F)4p	a ² G - ⁴ D°	$\frac{7}{2} - \frac{7}{2}$		903
	360	528.636	28.7777 - 217.9397	3d ⁷ – 3d ⁶ (a ³ F)4p	$a^2D - {}^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$		903
	210	528.804	43.4375 - 232.5395	3d ⁷ – 3d ⁶ (a ¹ D)4p	$a^2F - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		903
					2			
	350	528.994	26.6491 - 215.6845	3d' - 3d'(a'G)4p	$a^2H - H^2$	$\frac{1}{2} - \frac{1}{2}$		903
	270	529.022	67.9898 - 257.0180	3d' – 3d°(b'F)4p	$b^2D - {}^2F^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
	220	529.131	24.6514 - 213.6402	3d ⁷ - 3d ⁶ (a ³ P)4p	$a^2P - {}^2P^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
	200	529.341						903
	20	529.493	26.6491 - 215.5066	3d ⁷ − 3d ⁶ (a ³ G)4p	$a^2H - {}^4H^\circ$	$\frac{11}{2} - \frac{13}{2}$		903
	160	529.566	43.4375 - 232.2727	3d ⁷ – 3d ⁶ (a ¹ D)4p	$a^2F - {}^2F^\circ$	$\frac{5}{2} - \frac{5}{2}$		903
	450	520 002	42 8586 - 222 5205	$2d^7 - 2d^6(a^1D)(4n)$	$e^2 \mathbf{F} = {}^2 \mathbf{F}^{\circ}$	2 2		002
	40	529.992	43.8380 - 232.3393	$3d^{7} - 3d(a^{3}E)A_{7}$	$a^2D^2D^{\circ}$	2 2 2		903
	80	530.107	28.7777 - 217.4143	$3d^2 - 3d^2(a^2F)4p$	$a^{-}D - D^{-}D$	$\frac{1}{2} - \frac{1}{2}$		903
	120	530.133	23.0489 - 212.2739	30° – 30°(a°F)4p	a-P - F	$\overline{2} - \overline{2}$		903
	120	530.307	20.047(200.2014	247 246(-311)4-	20.20	7 7		903
	440	530.656	20.9476 - 209.3914	3d ² - 3d ² (a ² H)4p		$\frac{1}{2} - \frac{1}{2}$		903
	110	530.749	43.8386 - 232.2727	3d" - 3d"(a'D)4p	a-F - "F"	$\frac{1}{2} - \frac{1}{2}$		903
	390	531.293	19.8296 - 208.0468	$3d^7 - 3d^6(a^3H)4p$	a ² G - ⁴ I°	$\frac{2}{5} - \frac{2}{5}$		903
	120	531.386	20.9476 - 209.1319	$3d^7 - 3d^6(a^3H)4p$	$a^2G - C^{\circ}G^{\circ}$	<u>1</u> - 9	Į į	903
	180	531.697			-			903
	230	531,737	27.6776 - 215.7361	$3d^{7} - 3d^{6}(a^{3}G)4n$	$a^2H - {}^4H^\circ$	2 - 2		903
	110	532.008	20.9476 - 208.9121	$3d^{7} - 3d^{6}(a^{3}P)4p$	$a^2G - {}^4D^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
	170	532.754	67.3600 - 255.0640	$3d^7 - 3d^6(b^3P)4p$	$b^2D - {}^2D^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
	540	532.847	26.6491 - 214.3168	3d' - 3d°(a'G)4p	a ² H - *G*	$\frac{11}{2} - \frac{11}{2}$		903
	450	532.887	20.9476 - 208.6057	3d' - 3d°(a'F)4p	a ² G – *F *	$\frac{1}{2} - \frac{2}{2}$		903
	160	532.981	27.0965 - 214.7181	3d ⁷ - 3d ⁶ (a ³ G)4p	$a^2D - {}^4G^\circ$	$\frac{2}{2} - \frac{2}{2}$		903
	480	533.137	0 187.5703	$3d^{7} - 3d^{6}(a^{5}D)4p$	ga ⁴ F – ⁴ F°	$\frac{9}{2} - \frac{1}{2}$		903
	110	533.248	27.0965 - 214.6228	3d ⁷ – 3d ⁶ (a ³ F)4p	$a^2D - C^\circ$	$\frac{2}{2} - \frac{1}{2}$		903
	220	533.903	23.6489 - 210.9436	3d ⁷ – 3d ⁶ (a ³ F)4p	$a^2P - {}^4D^\circ$	$\frac{3}{2} - \frac{2}{2}$		903
	430	534.080	43.8586 - 231.0918	$3d^7 - 3d^6(a^1D)4n$	$a^2 F - {}^2 D^2$	7 - 5		903
	120	534.339						903
	460	534.388	1.1897 - 188.3201	3d ⁷ – 3d ⁶ (a ⁵ D)4p	ga ⁴ F - ⁴ F°	$\frac{7}{2} - \frac{5}{2}$		903
	270	534.491	26.6491 - 213.7397	$3d^7 - 3d^6(a^3F)4p$	$a^2H - CG^\circ$	<u>1</u> , - §		903
	210	534.648	19.8296 - 206.8655	$3d^7 - 3d^6(a^3H)4p$	a ² G - ⁴ H°	3-3		903
	170	534.742	27.0965 - 214.1010	3d ⁷ - 3d ⁶ (a ³ G)4p	$a^2D - {}^4F^\circ$	$\frac{5}{2} - \frac{7}{2}$		903
	170	624 760	10 1107 007 114	317 416 1 00 4	40.400	· , ,		
	1/0	534.759	18.1186 - 205.1141	3d' - 3d'(a'P)4p	a'P - 'S'	2 - 2		903
	640	534.874	27.0965 - 214.0558	3d' – 3d°(a ³ P)4p	$a^2D - {}^2P^\circ$	2 - 2		903
	400	534.905	27.6776 - 214.6228	3d ⁷ - 3d ⁶ (a ³ F)4p	$a^2H - {}^2G^{\circ}$	$\frac{9}{2} - \frac{1}{2}$	i	903
	540	535.003	19.8296 - 206.7407	3d ⁷ – 3d ⁶ (a ³ H)4p	a ² G – ⁴ I°	$\frac{9}{2} - \frac{11}{2}$		903
	200	535.131						903
	370	535.386	2.0425 - 188.8242	3d ⁷ – 3d⁵(a⁵D)4p	$ga^4F - {}^4F^\circ$	$\frac{5}{2} - \frac{3}{2}$		903
	140	535 441	28 7777 - 215 5413	3d7 - 2d6(a3G)4-	a ² D - ⁴ E ⁹	3 3		002
	290	535 472	18 3669 - 205 1141	$3u - 3u^{2}(a^{2}U)^{4}p$	a D - F	$\frac{1}{2} - \frac{1}{2}$		903
	160	535.4/2	16.3006 - 203.1141	30° - 30°(a°P)4p	a'r - 5	$\frac{1}{2} - \frac{1}{2}$		903
	100	535.903	24.0314 - 211.2468	30° – 30°(a°F)4p	a-P - 'D'	2 - 2		903
	80	535.986			1			903
	/0	536.084	A 100 ((m. (903
	000	536.282	0 186.4701	3d' – 3d°(a'D)4p	ga"F - "F"	$\frac{1}{2} - \frac{1}{2}$		903

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NI IV - Continued

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	590	536.535	1.1897 - 187.5703	3d ⁷ - 3d ⁶ (a ⁵ D)4p	ga ⁴ F - ⁴ F°	$\frac{7}{2} - \frac{7}{2}$		903
	20	536.659	23.6489 - 209.9851	$3d^7 - 3d^6(a^3P)4p$	$a^2P - {}^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$		903
	20	536.754						903
	540	536.832	2.0425 - 188.3201	$3d^{7} - 3d^{6}(a^{5}D)4p$	ga ⁴ F - ⁴ F°	$\frac{5}{2} - \frac{5}{2}$		903
	20	536.927			0	1		903
	560	537.048	2.6211 - 188.8242	$3d^{7} - 3d^{6}(a^{5}D)4p$	ga⁴F - ⁴F°	$\frac{3}{2} - \frac{3}{2}$		903
	430	537.080	20.9476 - 207.1360	3d ⁷ - 3d ⁶ (a ³ H)4p	a ² G - ⁴ H°	7 - 7		903
	330	537.441	27 6776 - 213 7397	$3d^7 - 3d^6(a^3F)4p$	$a^2H - {}^2G^\circ$	2 - 2		903
	370	537 522	27.0965 - 213.1311	$3d^7 - 3d^6(a^3F)4p$	$a^2D - {}^2F^\circ$	<u>5</u> - 7		903
	290	537.825	27 6776 - 213 6069	$3d^7 - 3d^6(a^3G)4p$	$a^2H - {}^2H^\circ$	<u><u><u></u></u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u>		903
	670	537.955	0 = 185,8900	$3d^7 - 3d^6(a^5D)4n$	$ga^4F - {}^4D^\circ$	3 - 1		903
	90	538.051			8	· ·		903
	370	538 257						903
	90	538 312						903
	50	538.004	27 6776 - 213 4086	$3d^7 = 3d^6(a^3G)4n$	$a^{2}H - {}^{4}F^{9}$	2 2	0	903
	240	538 503	26211 188 3201	$3d^7 = 3d^6(a^5D)4p$	$\sigma a^4 F = {}^4 F^\circ$	3 5	×	903
	70	538.505	2.0211 - 100.0201	$3d^7 - 3d^6(a^3\mathbf{P})Ap$	$a^2 P = {}^4 D^\circ$			903
	370	538.590	2.0425 - 187.5703	$3d^{2} - 3d^{2}(a^{2}D)4p$	$a^{4}F - {}^{4}F^{\circ}$	$\frac{2}{2} - \frac{2}{2}$		903
		630 0 72	24 (401 - 212 1500	247 246/-3534-	-211 40%	11 9		007
	200	539.072	26.6491 - 212.1509	$3d^{2} - 3d^{2}(a^{3}F)4p$	$a^2H = G$	$\frac{1}{2} - \frac{1}{2}$		903
	20	539.339	43.8586 - 229.2695	30° – 30°(a°D)4p	a-rr	$\overline{2} - \overline{2}$		903
	30	539.476		2.17 2.10(37) 4.	20 200	1 3		903
	490	539.558	24.6514 - 209.9851	3d' - 3d'(a'P)4p	$a^2P - ^2D^2$	$\frac{2}{7} - \frac{1}{2}$		903
	640	539.590	1.1897 – 186.5161	3d' - 3d'(a'D)4p	$ga^{4}F - {}^{4}D^{2}$	$\frac{1}{2} - \frac{1}{2}$		903
	370	539.727	1.1897 – 186.4701	3d' – 3d°(a'D)4p	ga"F – "F"	$\frac{1}{2} - \frac{1}{2}$		903
	50	539.849						903
	220	539.989	27.0965 - 212.2818	3d ⁷ – 3d ⁶ (a ³ F)4p	a²D – ⁴G°	$\frac{2}{2} - \frac{1}{2}$		903
	20	540.450						903
	590	540.792	2.0425 - 186.9572	3d ⁷ - 3d ⁶ (a ⁵ D)4p	ga⁴F – ⁴D°	$\frac{5}{2} - \frac{3}{2}$		903
	200	540.947	28.7777 - 213.6402	3d ⁷ – 3d ⁶ (a ³ P)4p	$a^2D - {}^2P^\circ$	$\frac{4}{2} - \frac{1}{2}$		903
	20	541.193	43.4375 - 228.2142	3d ⁷ - 3d ⁶ (a ¹ D)4p	$a^2 F - {}^2 P^\circ$	$\frac{2}{2} - \frac{3}{2}$		903
	20	541.342						903
	460	541.421	1.1897 - 185.8900	3d ⁷ – 3d ⁶ (a ⁵ D)4p	$ga^4F - {}^4D^\circ$	$\frac{7}{2} - \frac{7}{2}$		903
	80	541.521	43.8586 - 228.5185	$3d^{7} - 3d^{6}(a^{3}D)4p$	$a^2F - {}^2F^\circ$	$\frac{2}{2} - \frac{7}{2}$		903
	140	541.600	28.7777 - 213.4121	3d ⁷ - 3d ⁶ (a ³ F)4p	$a^2D - {}^4G^\circ$	$\frac{3}{2} - \frac{5}{2}$		903
	550	541.697	2.6211 - 187.2257	$3d^7 - 3d^6(a^5D)4p$	ga⁴F – ⁴D°	$\frac{3}{2} - \frac{1}{2}$		903
	40	541.908	27.6776 - 212.2070	3d ⁷ - 3d ⁶ (a ³ F)4p	a²H - ⁴G°	$\frac{9}{2} - \frac{11}{2}$		903
	490	542.088	2.0425 - 186.5161	$3d^{7} - 3d^{6}(a^{5}D)4p$	ga⁴F – ⁴D°	$\frac{5}{2} - \frac{5}{2}$		903
	280	542.305	2.0425 - 186.4414	$3d^7 - 3d^6(a^5D)4p$	ga⁴F – °P°	$\frac{5}{2} - \frac{3}{2}$		903
	410	542.405	23.6489 - 208.0091	$3d^{7} - 3d^{6}(a^{3}P)4p$	$a^2 P - {}^2 D^\circ$	$\frac{3}{2} - \frac{5}{2}$		903
	470	542.488	2.6211 - 186.9572	$3d^{7} - 3d^{6}(a^{5}D)4p$	$ga^{4}F - {}^{4}D^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		903
	450	542.549	1.1897 - 185.5053	$3d^7 - 3d^6(a^5D)4p$	ga ⁴ F - ⁶ P°	$\frac{7}{2} - \frac{5}{2}$		903
	20	543.024	27.0965 - 211.2468	3d ⁷ - 3d ⁶ (a ³ F)4p	$a^2D - {}^4D^\circ$	$\frac{5}{2} - \frac{3}{2}$		903
	500	543.189	0. – 184.0991	$3d^7 - 3d^6(a^5D)4p$	ga⁴F - ⁶ P°	$\frac{9}{2} - \frac{7}{2}$		903
	20	543.676	27.0965 - 211.0276	$3d^7 - 3d^6(a^3P)4p$	$a^2D - {}^4D^\circ$	$\frac{5}{2} - \frac{3}{2}$		903
	70	543,789	2.6211 - 186.5161	$3d^{7} - 3d^{6}(a^{5}D)4p$	$ga^4F - {}^4D^\circ$	$\frac{3}{2} - \frac{5}{2}$		903
	110	543.928	2.0425 - 185.8900	$3d^{7} - 3d^{6}(a^{5}D)4p$	$ga^4F - {}^4D^\circ$	$\frac{5}{2} - \frac{7}{2}$		903
	150	544.013	2.6211 - 186.4414	$3d^7 - 3d^6(a^5D)4p$	ga⁴F – ⁶ P°	$\frac{3}{2} - \frac{3}{2}$		903
	210	544.232	43.4375 - 227.1811	3d ⁷ – 3d ⁶ (a ³ D)4p	$a^2F - {}^2D^\circ$	$\frac{5}{2} - \frac{3}{2}$		903
	470	544 351	67 9898 - 251 6943	$3d^7 - 3d^6(h^3F)4n$	$b^2D - {}^2D^\circ$	5 _ 5		903
	400	544 375	43 8586 - 227 5494	$3d^{7} - 3d^{6}(a^{3}D)4n$	$a^2 F - {}^2 D^2$	<u><u><u></u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		903
	320	544 695	67 3600 - 250 9510	$3d^{7} = 3d^{6}(h^{3}F)4n$	$h^2D - D^2$	2 2		903
	500	544.095	26 6401 - 210 1770	$3d^{7} = 3d^{6}(a^{3}H)Aa$	$a^{2}H = 2I^{\circ}$	1		903
	170	544.80/	20.0491 - 210.1770	$3d - 3d (a \pi)^4p$ $3d^7 - 3d^{6/a^3}E^{3/a}$	$a^2D^2E^{\circ}$	2 2 2		903
	1 1/0	544.950	28.1111 - 212.2/39	50 - 50 (a r)4p	aD-r	2 - 2	1	705
	220	EAEOCC	2 0425 105 5052	247 246(-513)4-	204E 6D	5 5		903

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NI IV - Continued

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lultiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	Reference
-	450	545.509	27.6776 - 210.9875	3d ⁷ - 3d ⁶ (a ³ H)4p	$a^2H - {}^2I^\circ$	$\frac{9}{2} - \frac{11}{2}$		903
	20	545.652			1			903
	40	546.565	67.9898 - 250.9510	3d ⁷ – 3d ⁶ (b ³ F)4p	$b^2D - {}^2D^\circ$	$\frac{2}{2} - \frac{3}{2}$		903
	150	546.717	1.1897 - 184.0991	$3d^{7} - 3d^{6}(a^{5}D)4p$	ga⁴F – ⁶ P°	$\frac{1}{2} - \frac{1}{2}$		903
	60	546.804	2.6211 - 185.5053	3d ⁷ – 3d ⁶ (a ⁵ D)4p	ga⁴F – °P°	$\frac{3}{2} - \frac{5}{2}$		903
	20	546.866						903
	20	546.974						903
	20	547.256						903
	20	547.330						903
	20	547.426						903
I	40	547.669						903
	50	547.897						903
	240	547.984	26.6491 - 209.1319	3d ⁷ – 3d ⁶ (a ³ H)4p	$a^2H - {}^2G^{\circ}$	$\frac{11}{2} - \frac{9}{2}$		903
	90	548.101	27.6776 - 210.1218	$3d^7 - 3d^6(a^3F)4p$	$a^2H - {}^4D^\circ$	$\frac{9}{2} - \frac{7}{2}$		903
1	70	548.155		. , .				903
	60	548.294						903
	90	548.546	27.0965 - 209.3914	$3d^{7} - 3d^{6}(a^{3}H)4p$	$a^2D - C^{\circ}G^{\circ}$	5-7		903
	70	549.013						903
	290	549.073	0 182.1256	$3d^{7} - 3d^{6}(a^{5}D)4p$	ga ⁴ F - ⁶ F°	2 - 7		903
	70	549,161			8	22		903
	270	549.315	0. – 182.0449	$3d^{7} - 3d^{6}(a^{5}D)4p$	$ga^4F - {}^6F^\circ$	2 - 2		903
	70	549.366		50 50 (a 2),p	Bur I	1 2 2		903
	270	549 457	43 4375 - 225 4316	$3d^7 = 3d^6(a^1G)4n$	$a^2 \mathbf{F} - {}^2 \mathbf{F}^\circ$	5 5		903
	180	549.496	26.6491 - 208.6313	$3d^{7} - 3d^{6}(a^{3}H)4p$	$a^2H - {}^4H^\circ$	$\frac{11}{2} - \frac{13}{2}$	Q	903
	140	550 303	27 6776 - 209 3914	3d ⁷ - 3d ⁶ (a ³ H)An	$a^2H = {}^2G^{\circ}$	9 Z		903
	70	551.089	27.6776 - 209.1319	$3d^7 - 3d^6(a^3H)4p$	$a^{2}H - 2G^{\circ}$	2 2 2 2 2		903
	100	551 268	27.0770 = 203.1313 26 6491 = 208 0468	$3d^{7} = 3d^{6}(a^{3}H)Ap$	$a^{2}H = 4I^{\circ}$	2 - 2 11 9		903
	150	551.200	20.0491 - 206.0408	3d - 3d (a H) + p $3d^7 - 3d^6(a^3D) + n$	$a \Pi = I$ $a^2 E = 4 D^{\circ}$	2 - 2 2 - 2 2 - 2		903
	110	551.027	43.8380 - 223.1309	$3d^7 - 3d^6(a^3D)4p$	$a \Gamma - D$	2 2 2		903
	260	552.401	43.4375 - 224.4636	$3d^{7} - 3d^{6}(a^{1}G)4p$	$a^2F - {}^2G^\circ$	$\frac{2}{2} - \frac{2}{7}$		903
	270	552 427	1 1907 192 2069	2d7 2d%(5))/m	an ⁴ E ⁶ E°	2 5		002
	120	552.457	1.1897 - 182.2008	$3d^{7} - 3d^{8}(a^{5}D)4p$	ga F - F	$\frac{1}{2} - \frac{1}{2}$		903
	120	552.065	1.1697 - 182,1230	3d = 3d (a D)4p	ga F - F	$\frac{1}{2} - \frac{1}{2}$		903
	260	554 270	43.8386 - 224.7615	30° - 30°(a°G)4p	a'r - 'G'	2 - 2		903
	250	554.579	43 8586 234 0753	2d ⁷ 2d%a ¹ C)4p	2E 2E°	1 1 1		903
	100	555.062	2.0425 - 182.2068	$3d^{7} - 3d^{6}(a^{5}D)4p$	a F - F $ga^4F - F^{\circ}$	2 - 2	o	903 903
	20	556.604	2.6211 - 182.2884	3d' – 3d°(a°D)4p	ga ⁴ F – ^e F ^e	$\frac{1}{2} - \frac{1}{2}$		903
	30	557.243	27.6776 - 207.1360	3d' - 3d'(a'H)4p	a-H - "H"	2 - 2	·	903
	10	557.401					1 1	903
	10	557.566	26.6491 - 206.0053	3d' – 3d°(a'H)4p	a²H – ⁴G°	1		903
	10 10	557.949 558.469	28.7777 - 208.0091 27.6776 - 206.7407	3d′ – 3d°(a³P)4p 3d ⁷ – 3d°(a³H)4p	$a^2D - {}^2D^\circ$ $a^2H - {}^4I^\circ$	$\frac{1}{2} - \frac{1}{2}$ $\frac{2}{3} - \frac{11}{3}$		903 903
	250	559.935	43.4375 - 222.0293	3d' - 3d°(a'G)4p	a'F – 'G°	2 - 2		903
	300	561.378	43.8586 - 221.9910	3d' - 3d ⁶ (a ³ G)4p	$a^2F - {}^2G^\circ$	$\frac{1}{2} - \frac{9}{2}$		903
	40	566.714	43.4375 - 219.8960	$3d^{7} - 3d^{6}(a^{3}G)4p$	$a^2F - {}^2F^\circ$	$\frac{2}{2} - \frac{7}{2}$		903
	100	567.811	43.4375 - 219.5534	$3d^{7} - 3d^{6}(a^{3}G)4p$	$a^2F - {}^2F^\circ$	$\frac{5}{2} - \frac{5}{2}$		903
	150	568.056	43.8586 - 219.8960	$3d^{7} - 3d^{6}(a^{3}G)4p$	$a^2F - {}^2F^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
	20	568.489	43.8586 - 219.7650	$3d^7 - 3d^6(a^3G)4p$	$a^2F - {}^2H^\circ$	$\frac{7}{2} - \frac{9}{2}$		903
	10	568.621	0 175.8691	3d ⁷ - 3d ⁶ (a ⁵ D)4p	$ga^4F - {}^6D^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		903
	20	569.165	43.8586 - 219.5534	$3d^{7} - 3d^{6}(a^{3}G)4p$	$a^2F - {}^2F^\circ$	$\frac{7}{2} - \frac{5}{2}$		903
	20	569.564	0. – 175.5695	$3d^{7} - 3d^{6}(a^{5}D)4p$	$ga^4F - {}^6D^\circ$	$\frac{9}{2} - \frac{9}{2}$		903
	10	571.262	1.1897 - 176.2471	$3d^{7} - 3d^{6}(a^{5}D)4p$	ga⁴F - ⁰D°	2, - 5		903
1	60	573.063	43.4375 - 217.9397	$3d^{7} - 3d^{6}(a^{3}F)4p$	$a^2F - ^2D^\circ$	$\frac{5}{5} - \frac{3}{5}$		903

NI IV - Continued

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lultiplet Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	Reference
30	574.799	43.4375 - 217.4143	3d ⁷ - 3d ⁶ (a ³ F)4p	$a^2F - {}^2D^\circ$	$\frac{5}{2} - \frac{5}{2}$		903
250	575.818	18.3668 - 192.0335	3d ⁷ – 3d ⁶ (a ⁵ D)4p	a ⁴ P – ⁴ P°	$\frac{3}{2} - \frac{1}{2}$		903
70	576.180	43.8586 - 217.4143	3d ⁷ – 3d ⁶ (a ³ F)4p	$a^2F - ^2D^\circ$	$\frac{7}{2} - \frac{5}{2}$		903
250	576.376	18.1186 - 191.6182	3d ⁷ - 3d ⁶ (a ⁵ D)4p	a ⁴ P – ⁴ P °	$\frac{5}{2} - \frac{3}{2}$		903
100	577 201	18.3668 - 191.6182	$3d^{7} - 3d^{6}(a^{5}D)4p$	a ⁴ P – ⁴ P°	3-3		903
80	577.788	18.9584 - 192.0335	3d ⁷ - 3d ⁶ (a ⁵ D)4p	$a^4P - {}^4P^\circ$	$\frac{1}{2} - \frac{1}{2}$		903
400	579.009	18 1186 - 190 8303	3d ⁷ - 3d ⁶ (a ⁵ D)4p	a ⁴ P – ⁴ P°	5-5		903
300	570 183	18 9584 - 191 6182	$3d^{7} - 3d^{6}(a^{5}D)4p$	$a^4P - {}^4P^\circ$	1, 1,		903
20	570 227	10.7504 - 171.0102	54 54 (4 D).p				903
20	579.337	18 2668 100 8202	2d7 2d6(05D)4m	4D 4D°	3 5		003
300	579.835	18.3008 - 190.8303	$3d^{7} - 3d(a D) + p$	a = 1 $a^2 E = 4 U^\circ$			003
100	580.423	43.4375 - 215.7245	3d - 3d (a C)4p	$a^{2}F - H$	$\frac{2}{7}$ $\frac{2}{9}$		903
20	581.818	43.8586 - 215.7361	3d' - 3d'(a'G)4p	a'F - 'H'	2 - 3		903
10	582.167						903
10	582.544	43.8586 - 215.5168	3d ⁷ - 3d ⁶ (a ³ G)4p	a ² F – ⁴ F°	$\frac{1}{2} - \frac{2}{2}$	Q	903
30	584.167	43.4375 - 214.6228	3d ⁷ - 3d ⁶ (a ³ F)4p	a ² F - ² G°	$\frac{5}{2} - \frac{7}{2}$		903
10	584.559						903
10	584.741	67.9898 - 239.0087	3d ⁷ - 3d ⁶ (a ¹ F)4p	$b^2D - {}^2D^\circ$	5-5		903
20	588.426						903
20	599 654	43 8586 - 213 7307	3d ⁷ - 3d ⁶ (a ³ F)4n	$a^2 \mathbf{F} = {}^2 \mathbf{G}^2$	7 9		903
20	588.034	43.8380 - 213.7377	$3d^7 - 3d^3(a^3F)/m$	$a^2 \mathbf{E}^2 \mathbf{E}^2$	2 2		002
30	589.299	43.4373 - 213.1311	$3d^{2} - 3d(a^{2})^{4}p$	$a \Gamma = \Gamma$			003
10	589.803	43.8586 - 213.4086	3d' – 3d'(a'G)4p	a-F - F	2 - 2		903
10	590.152	18.1186 - 187.5703	3d' – 3d''(a'D)4p	a'P – 'F'	2 - 2		903
10	590.943				1		903
30	592.224	18.3668 - 187.2257	3d ⁷ – 3d*(a ⁵ D)4p	a'P - 'D°	$\frac{3}{2} - \frac{1}{2}$		903
20	592.280	43.4375 - 212.2759	3d' - 3d*(a³F)4p	$a^2F - {}^2F^\circ$	$\frac{5}{2} - \frac{5}{2}$		903
60	593,148	18.3668 - 186.9572	$3d^{7} - 3d^{6}(a^{5}D)4p$	a ⁴ P - ⁴ D°	3-3		903
60	593 842	18 1186 - 186 5161	$3d^{7} - 3d^{6}(a^{5}D)4p$	$a^4P - {}^4D^\circ$	3 - 3		903
60	594 294	18 9584 - 187 2257	$3d^{7} - 3d^{6}(a^{5}D)4n$	$a^4P - {}^4D^\circ$	ĺ į_į	1	903
150	504 707	19 3669 196 5161	$3d^{7} - 3d^{6}(a^{5}D)Ap$	$a^{4}P - {}^{4}D^{\circ}$	3 5		903
20	595.008	18.5008 - 180.5101	50 - 50 (a D)+p				903
	505.240	10 0594 10(057)	24/C 24%	at P 4D°	1 3		003
80	595.249	18.9584 - 186.9572	30 - 30 (a D)4p	a P - D	2^{-2}_{3}		903
20	595.327	23.6489 - 191.6182	3d" - 3d"(a"D)4p	a-P - 'P'	5 - 5		903
30	595.447						903
20	595.621						903
300	596.058	18.1186 - 185.8900	3d ⁷ - 3d ⁶ (a ⁵ D)4p	a⁴P – ⁴D°	$\frac{5}{2} - \frac{1}{2}$		903
10	596.338						903
10	597.083	18.9584 - 186.4414	3d ⁷ - 3d ⁶ (a ⁵ D)4p	a⁴P – "P°	1, - 3	0	903
30	597.436	24.6514 - 192.0335	$3d^7 - 3d^6(a^5D)4p$	$a^2P - {}^4P^\circ$	Į į į		903
30	598 154	23.6489 - 190.8303	$3d^{7} - 3d^{5}(a^{5}D)4p$	$a^2P - {}^4P^\circ$	3_5		903
30	508 210	18 3669 195 5053	$3d^{7} - 3d^{6}(a^{5}D)An$	$a^{4}P = {}^{h}P^{o}$	1 1 1		903
30	590.319	18,5008 - 185,5055	$3d^{7} - 3d^{6}(a^{5}D)/4p$	$a^2 D = 4 D^\circ$			903
30	598.932 599.197	24.0314 - 191.0182	50 - 50 (a D)+p		2 - 2		903
					7 4		003
20	599.761	43.8580 - 210.5906	3a - 3d (a P)4p	a-r - D'	1 2 - 2	V V	903
20	599.930	43.4375 - 210.1218	3d' 3d°(a'F)4p	a-F - *D*	2 - 2		903
10	601.063				1		903
20	602.323	67.9898 - 234.0195	3d ⁷ – 3d ⁶ (a ¹ S)4p	$b^2D - {}^2P^\circ$	2-2		903
100	602.482	18.1186 - 184.0991	3d ⁷ - 3d ⁶ (a ⁵ D)4p	a ⁴ P – "P"	$\frac{2}{2} - \frac{1}{2}$		903
100	602.573	43.4375 - 209.3914	3d ⁷ - 3d ⁶ (a ³ H)4p	$a^2F - {}^2G^\circ$	$\frac{5}{2} - \frac{7}{2}$		903
10	603,770						903
20	604 106	43 8586 - 200 3014	$3d^7 = 3d^6(a^3H)4n$	$a^2 \mathbf{F} - {}^2 \mathbf{G}^\circ$	1 - 1		903
20	604 719	+3.0300 - 207.3714	50 - 50 (a 1174)		2 - 2		903
10	004./38	42.0506	247 2466-3174		7 9		003
150	605.045	43.8580 - 209.1319	30° - 30°(a°H)4p		7 9		903
30	605.785	43.8586 - 208.9336	50 - 50 (a r)+p	a-F - F	2 - 2		903

NI IV - Continued

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	10	606.597						903
	10	606.811			3- 4-0	1 1		903
	20	607.260	23.6489 - 188.3201	3d' – 3d°(a'D)4p	a ² P – *F*	2 - 2		903
	10	607.781						903
	10	608.709	67.9898 - 232.2727	3d' - 3d''(a'D)4p	$b^2D - F^{\circ}$	2 - 2		903
	50	609.058	43.8586 - 208.0468	3d' – 3d°(a'H)4p	a²F – ⁴I°	$\frac{1}{2} - \frac{3}{2}$		903
	50	609.448	18.1186 - 182.2068	3d ⁷ - 3d ⁶ (a ⁵ D)4p	a⁴P – °F°	$\frac{5}{2} - \frac{5}{2}$		903
	10	609.593						903
	250	610.043	18.3668 - 182.2884	3d' – 3d°(a°D)4p	a⁴P ~ °F°	$\frac{2}{2} - \frac{1}{2}$	Q	903
	10	610.255						903
	10	610.366	18.3668 - 182.2068	3d ⁷ - 3d ⁶ (a ⁵ D)4p	a⁴P – °F°	$\frac{2}{2} - \frac{2}{2}$		903
	20	612.351	18.9584 – 182.2599	$3d^7 - 3d^6(a^5D)4p$	a ⁴ P – "F"	$\frac{1}{2} - \frac{2}{2}$		903
	10	613.474	43.8586 - 206.8655	3d ⁷ – 3d⁰(a³H)4p	a ² F - ⁴ H°	$\frac{7}{2} - \frac{9}{2}$		903
	20	614.005	23.6489 - 186.5161	3d ⁷ – 3d ⁶ (a ⁵ D)4p	$a^2P - {}^4D^\circ$	$\frac{3}{2} - \frac{5}{2}$		903
	20	617.635	67.3600 - 229.2695	$3d^7 - 3d^6(a^3D)4p$	$b^2D - {}^2F^\circ$	$\frac{3}{2} - \frac{5}{2}$		903
	10	621.238					. 1	903
	10	621.690	67.3600 - 228.2142	$3d^7 - 3d^6(a^1D)4p$	$b^2D - {}^2P^\circ$	$\frac{3}{2} - \frac{3}{2}$		903
	20	622.940	67.9898 - 228.5185	$3d^{7} - 3d^{6}(a^{3}D)4p$	$b^2D - {}^2F^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		903
	10	624,130	67 9898 - 228 2142	$3d^7 - 3d^6(a^1D)4p$	$b^2D - {}^2P^\circ$	5-3		903
	10	624 243	67 3600 - 227 5494	$3d^{7} - 3d^{6}(a^{3}D)4p$	$b^2D - {}^2D^\circ$	3 5		903
	30	626.712	67 9898 - 227 5494	$3d^7 - 3d^6(a^3D)4p$	$b^2D - {}^2D^\circ$	\$ _ \$		903
	10	631 158	18 1186 - 176 5544	$3d^{2} - 3d^{6}(a^{5}D)4n$	$a^4P - D^\circ$	ž_3		903
	30	631 421		50 50 (a 2), p		2 2		903
	30	632.415	18.1186 - 176.2471	3d ⁷ – 3d ⁶ (a ⁵ D)4p	a⁴P – ⁰D°	$\frac{5}{2} - \frac{5}{2}$		903
	50	632 615	67 3600 - 225 4316	3d ⁷ - 3d ⁶ (a ¹ G)4p	$b^2D = {}^2F^{\circ}$	3_2		903
	10	622.015	07.3000 - 223.4310	5 u - 5 u (a C)+p	0 D - 1	2 - 2		903
	10	622.033						903
	10	632.923	10 1106 175 0601	2d ⁷ 2d%(a ⁵ D)4p	a ⁴ ₽ ⁰₽°	5 2		903
	10	633.910	18.1180 - 175.8091	$3d^{7} - 3d(a^{7}D)4p$	$a \mathbf{r} - \mathbf{D}$ $a^2 \mathbf{D} \mathbf{o} \mathbf{P}^{0}$	2 2 2	0	903
	20	634.377	67.3600 - 224.9965	$3d^{2} - 3d(a^{2}D)4p$ $3d^{7} - 3d^{6}(a^{3}D)4p$	$\mathbf{a} \mathbf{D} = \mathbf{I}$ $\mathbf{b}^2 \mathbf{D} - {}^2 \mathbf{P}^\circ$	$\frac{2}{2} - \frac{2}{2}$	Y	903
	20	(2(242	(7.0900 225.12(0	247 2466-3034-	12D 4D	5 7		001
	30	636.343	67.9898 ~ 225.1369	$3d^{7} - 3d^{8}(a^{3}D)4p$	$D^{2}D - D^{2}$	$\frac{2}{5} - \frac{2}{3}$		903
	20	637.158	67.9898 - 224.9369	$3d^{2} - 3d^{2}(a^{2}D)4p$	$D^{-}D^{-}P^{-}$	$\begin{bmatrix} 2 & -2 \\ 3 & 5 \end{bmatrix}$		903
	20	638.329	67.3600 - 224.0213	$3d^2 - 3d^2(a^2D)4p$	$\mathbf{D}^{2}\mathbf{D} - \mathbf{F}^{2}$			903
	20	639.080	07.9898 - 224.4030	$3d^2 - 3d^2(a^2G)4p$	$b^{-}D - G$	$\frac{1}{2} - \frac{1}{2}$		903
	30	640.008	67.9898 - 224.0753	30° – 30°(a°G)4p	0-DF	2 - 2		903
	20	049.870						505
		651.32	0 153.5336	$3d^7 - 3d^6(a^3D)4s$	ga ⁴ F - ⁴ D	$\frac{9}{2} - \frac{7}{2}$	F,P	375,903
		652.15	0 153.3388	3d ⁷ - 3d ⁶ (a ³ D)4s	ga⁴F – ⁴D	$\frac{9}{2} - \frac{5}{2}$	F,P	375,903
		656.41	1.1897 - 153.5336	3d ⁷ – 3d ⁶ (a ³ D)4s	ga⁴F – ⁴D	$\frac{7}{2} - \frac{7}{2}$	F,P	375,903
	100	657.043	67.3600 - 219.5534	3d ⁷ – 3d°(a ³ G)4p	$b^2D - {}^2F^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		903
		657.25	1.1897 - 153.3388	3d ⁷ – 3d ⁶ (a ³ D)4s	ga⁴F – ⁴D	$\frac{7}{2} - \frac{5}{2}$	F,P	375,903
		657.36	1.1897 - 153.3138	$3d^7 - 3d^6(a^3D)4s$	ga⁴F - ⁴D	$\frac{7}{2} - \frac{3}{2}$	F,P	375,903
	150	658.285	67.9898 - 219.8960	3d ⁷ - 3d ⁶ (a ³ G)4p	$b^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		903
		659.73	19.8296 - 171.4060	3d ⁷ - 3d ⁶ (a ¹ F)4s	$a^2G - {}^2F$	3 - 7	F,P	375,903
	30	659.783	67.9898 - 219.5534	$3d^{7} - 3d^{6}(a^{3}G)4p$	$b^2D - {}^2F^\circ$	3-5		903
		660.91	2.0425 - 153.3494	$3d^7 - 3d^6(a^3D)4s$	ga ⁴ F - ⁴ D	<u>\$</u> _;	F,P	375,903
		660.95	2.0425 - 153.3388	$3d^7 - 3d^6(a^3D)4s$	ga ⁴ F - ⁴ D	3-3	F.P	375,903
		661.06	2.0425 - 153.3138	$3d^{7} - 3d^{6}(a^{3}D)4s$	ga⁴F - ⁴D	$\frac{5}{2} - \frac{3}{2}$	F,P	375,903
		663.45	2.6211 - 153 3494	3d ⁷ - 3d ⁶ (a ³ D)4s	αa ⁴ F - ⁴ D	7-1	FP	375.903
		663.60	2.6211 - 153.3138	3d ⁷ - 3d ⁶ (a ³ D)4e	$ga^4F - {}^4D$	$\frac{2}{3}$ $\frac{2}{3}$	FP	375,903
	30	664 086	67 3600 - 217 9397	$3d^{7} = 3d^{6}(a^{3}E)An$	$h^2D = 2D^2$	2 2 2 3	1,1	903
	30	664 63	20 9476 - 171 4080	$3d^{7} = 3d(a^{1}F)4p$	$a^2G - {}^2F$	2 2 2	FP	375 903
	40	669 222	67 9898 - 217 4143	$3d^{7} = 3d(a^{1})^{48}$	$h^2 D = 2 D^2$	2 2 2 5 5	1,1	903
	150	672 957	07.7070 - 217.4143	50 – 50 (a r)+p	00-0	2 2		903
	1.50	012.751						,05

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Multiplet Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	References
20	678.122	28.7777 - 176.2471	3d ⁷ - 3d ⁶ (a ⁵ D)4p	$a^2D - {}^6D^\circ$	$\frac{3}{2} - \frac{5}{2}$	Q	903
10	683.321						903
30	683.639	67.3600 - 213.6402	3d ⁷ – 3d ⁶ (a ³ P)4p	$b^2D - {}^2P^\circ$	$\frac{3}{2} - \frac{1}{2}$	Q	903
40	684.631	67.9898 - 214.0558	3d ⁷ – 3d ⁶ (a ³ P)4p	$b^2D - {}^2P^\circ$	$\frac{5}{2} - \frac{3}{2}$		903
	686.33	0 145.7022	3d ⁷ – 3d ⁶ (a ³ G)4s	ga⁴F – ⁴G	$\frac{9}{2} - \frac{9}{2}$	F,P	375,903
100	688.947						903
10	689.741						903
	690.27	1.1897 - 146.0615	3d ⁷ - 3d ⁶ (a ³ G)4s	ga⁴F – ⁴G	$\frac{7}{2} - \frac{7}{2}$	F,P	375,903
	690.54	0 144.8151	3d ⁷ - 3d ⁶ (a ³ G)4s	ga⁴F – ⁴G	$\frac{9}{2} - \frac{11}{2}$	F,P	375,903
50	690.689			-			903
10	690.851						903
	691.98	1.1897 - 145.7022	3d7 - 3d6(a3G)4s	$ga^4F - {}^4G$	$\frac{7}{2} - \frac{9}{2}$	F,P	375,903
	692.96	27.0965 - 171.4060	3d7 - 3d6(a1F)4s	$a^2D - {}^2F$	$\frac{5}{2} - \frac{7}{2}$	F,P	375,903
	693.91	2.0425 - 146.1538	3d ⁷ - 3d ⁶ (a ³ G)4s	ga⁴F - ⁴G	5-5	F.P	375,903
	694.35	2.0425 - 146.0615	$3d^7 - 3d^6(a^3G)4s$	ga ⁴ F – ⁴ G	\$ _ 7	F.P	375,903
	696.09	2.0425 - 145.7022	$3d^7 - 3d^6(a^3G)4s$	$ga^4F - {}^4G$	5-9	F.P	375,903
	696.26	1 1897 - 144 8151	$3d^7 - 3d^6(a^3G)4s$	$ga^4F - {}^4G$	1 <u>1</u> <u>1</u>	F.P	375.903
	696.71	2.6211 - 146.1538	3d ⁷ - 3d ⁶ (a ³ G)4s	ga ⁴ F - ⁴ G	$\frac{3}{2} - \frac{5}{2}$	F,P	375,903
	607.15	2 6211 146 0615	3d ⁷ - 3d ⁶ (a ³ G)4s	$m^4 F = {}^4 G$	3 1	FP	375 903
20	697.15	2.0211 - 140.0015	50 - 50 (a C)+s	ga I = O	2 - 2	1,1	903
50	608.244						903
10	701 11	28 7777 - 171 4080	$3d^7 - 3d^6(a^1F)4s$	$a^2D - {}^2F$	3_1	FP	375 903
	701.11	28.7777 - 171.4080	$3d^{7} = 3d^{6}e^{3}E^{4$	aD = 1 $a^4E = {}^4E$	2 2 2 2 2 2	EP	375 903
	705.00	0 141.5772	3d ⁷ - 3d ⁶ (a ³ F)4s	$ga^4F - {}^4F$	$\frac{2}{2} - \frac{2}{2}$	F,P	375,903
10	707 770						903
10	708.11	0 - 141 2203	$3d^7 - 3d^6(a^3F)4s$	$\sigma a^4 F - {}^4 F$	2 2	F.P	375.903
10	708.195	0 141.2205	5u - 5u (a 1)+3	gal - I	2 2	1,1	903
10	708.183						903
10	708.307	1 1907 142 0225	$2d^7 - 3d^6(a^3 E)Ac$	$ga^4E = {}^4E$	Z_3	FP	375 903
	710.00	1.1897 - 142.0233	$3d^7 = 3d^6(a^3E)/a$	$ga^4F = {}^4F$	$\frac{2}{2} - \frac{2}{2}$	FP	375 903
	/11.02	1.1677 - 141.8520	50 - 50 (a 1)43	ga I - I	2 - 2	1,1	575,705
	712.31	1.1897 - 141.5772	3d ⁷ – 3d ⁶ (a ³ F)4s	ga⁴F - ⁴F	$\frac{1}{2} - \frac{1}{2}$	F,P	375,903
	714.13	1.1897 - 141.2203	3d ⁷ – 3d ⁶ (a ³ F)4s	ga4F - 4F	$\frac{7}{2} - \frac{9}{2}$	F,P	375,903
	714.38	2.0425 - 142.0235	3d ⁷ - 3d ⁶ (a ³ F)4s	ga4F - 4F	$\frac{5}{2} - \frac{3}{2}$	F,P	375,903
	715.36	2.0425 - 141.8320	3d ⁷ - 3d ⁶ (a ³ F)4s	ga⁴F - ⁴F	$\frac{5}{2} - \frac{5}{2}$	F,P	375,903
	716.67	2.0425 - 141.5772	3d ⁷ - 3d ⁶ (a ³ F)4s	$ga^4F - {}^4F$	$\frac{5}{2} - \frac{7}{2}$	F,P	375,903
	717.35	2.6211 - 142.0235	3d ⁷ - 3d ⁶ (a ³ F)4s	ga ⁴ F - ⁴ F	$\frac{3}{2} - \frac{3}{2}$	F,P	375,903
	718.33	2.6211 - 141.8320	3d7 - 3d6(a3F)4s	ga⁴F - ⁴F	$\frac{1}{2} - \frac{5}{2}$	F,P	375,903
	718.51	2.0425 - 141.2203	3d ⁷ - 3d ⁶ (a ³ F)4s	$ga^4F - {}^4F$	$\frac{5}{2} - \frac{9}{2}$	F,P	375,903
	719.65	2.6211 - 141.5772	3d ⁷ - 3d ⁶ (a ³ F)4s	$ga^4F - {}^4F$	$\frac{3}{2} - \frac{7}{2}$	F,P	375,903
	732.48	19.8296 - 156.3512	3d7 - 3d6(a1G)4s	$a^2G - C^2G$	$\frac{9}{2} - \frac{7}{2}$	F,P	375,903
	732.79	19.8296 - 156.2940	$3d^7 - 3d^6(a^1G)4s$	$a^2G - {}^2G$	$\frac{9}{2} - \frac{9}{2}$	F,P	375,903
	734.38	23.6489 - 159.8184	3d ⁷ - 3d ⁶ (a ³ D)4s	$a^2P - {}^2D$	$\frac{3}{2} - \frac{5}{2}$	F,P	375,903
	736.11	23.6489 - 159.4985	3d7 - 3d6(a3D)4s	$a^2P - {}^2D$	$\frac{3}{2} - \frac{3}{2}$	F,P	375,903
	738.47	18.1186 - 153.5336	3d ⁷ - 3d ⁶ (a ³ D)4s	a ⁴ P - ⁴ D	$\frac{5}{2} - \frac{7}{2}$	F,P	375,903
	738.53	20.9476 - 156.3512	3d ⁷ - 3d ⁶ (a ¹ G)4s	$a^2G - {}^2G$	$\frac{1}{2} - \frac{1}{2}$	F,P	375,903
	738.84	20.9476 - 156.2940	$3d^7 - 3d^6(a^1G)4s$	$a^2G - {}^2G$	$\frac{7}{2} - \frac{9}{2}$	F,P	375,903
	739.53	18.1186 - 153.3388	$3d^7 - 3d^6(a^3D)4s$	a ⁴ P – ⁴ D	5 - 5	F,P	375,903
	739.83	18.3668 - 153.5336	3d ⁷ - 3d ⁶ (a ³ D)4s	a ⁴ P - ⁴ D	$\frac{3}{2} - \frac{7}{2}$	F,P	375,903
	740.89	18 3668 - 153 3388	$3d^{7} - 3d^{6}(a^{3}D)4s$	a ⁴ P - ⁴ D	3-5	F.P	375,903
	741.03	18.3668 - 153.3138	$3d^7 - 3d^6(a^3D)4s$	$a^4P - {}^4D$	3 - 3	F.P	375,903
	741.59	24 6514 - 159 4985	$3d^7 = 3d^6(a^3D)4e$	$a^2P - ^2D$	1 - 3	E.P.	375,903
	744 10	18 9584 - 153 3494	$3d^{7} = 3d^{6}(a^{3}D)Ac$	$a^4P - {}^4D$	$\frac{1}{1}$	FP	375.903
	744.10	10.7504 - 155.5474	$3d^{2} = 3d^{6}(a^{3}D)Aa$	$a^4P = 4D$	1 1	FP	375,903
	744.10	10.7504 - 155.5500 18 9584 - 152 2129	$3d^{2} = 3d(a D) + 3$ $3d^{2} = 3d^{6}(a^{3}D) 4a$	$a^4P - {}^4D$	$\frac{2}{1} - \frac{2}{3}$	FP	375,903
	144.29	10.7304 - 133.3130	Ju – Ju (a D)45	a1 - D	2 - 2	•,•	5,5,505
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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	References
		753.46	27.0965 - 159.8184	3d ⁷ - 3d ⁶ (a ³ D)4s	$a^2D - ^2D$	$\frac{5}{2} - \frac{5}{2}$	F,P	375,903
		754.64	19.8296 - 152.3437	$3d^7 - 3d^6(a^3G)4s$	$a^2G - {}^2G$	$\frac{9}{2} - \frac{7}{2}$	F,P	375,903
		755.28	27.0965 - 159.4985	$3d^7 - 3d^6(a^3D)4s$	$a^2D - {}^2D$	5-3	F.P	375,903
		759.04	19.8296 - 151.5747	$3d^7 - 3d^6(a^3G)4s$	$a^2G - {}^2G$	2 - 2	F.P	375,903
		761.06	20.9476 - 152.3437	$3d^7 - 3d^6(a^3G)4s$	$a^2G - {}^2G$	1 1	F.P	375,903
		763.12	28.7777 - 159.8184	$3d^7 - 3d^6(a^3D)4s$	$a^2D - {}^2D$	1 1 - 1	F.P	375,903
						2 2	- ,	0,00,000
		764.99	28.7777 - 159.4985	$3d^{7} - 3d^{6}(a^{3}D)4s$	$a^2D - {}^2D$	$\frac{3}{2} - \frac{3}{2}$	F,P	375,903
		771.00	26.6491 - 156.3512	$3d^7 - 3d^6(a^1G)4s$	$a^2H - {}^2G$	$\frac{11}{2} - \frac{7}{2}$	F,P	375,903
		771.34	26.6491 - 156.2940	3d ⁷ - 3d ⁶ (a ¹ G)4s	$a^2H - {}^2G$	11 - 2 2 - 2	F,P	375,903
		777.16	27.6776 - 156.3512	3d ⁷ – 3d ⁶ (a ¹ G)4s	$a^{2}H - {}^{2}G$	$\frac{9}{2} - \frac{7}{2}$	F,P	375,903
		777.25	26.6491 - 155.3087	3d ⁷ – 3d ⁶ (a ¹ I)4s	$a^{2}H - {}^{2}I$	44	F,P	375,903
		777.51	27.6776 – 156.2940	$3d^7 - 3d^6(a^1G)4s$	$a^2H - {}^2G$	$\frac{9}{2} - \frac{9}{2}$	F,P	375,903
		777.58	26.6491 - 155.2537	3d ⁷ - 3d ⁶ (a ¹ I)4s	$a^2H - {}^2I$	កំ-កំ	F.P	375,903
		778.04	19.8296 - 148.3582	$3d^7 - 3d^6(a^3F)4s$	$a^2G - {}^2F$	9_5	FP	375 903
		781.43	434375 - 1714080	$3d^7 - 3d^6(a^1F)4s$	$a^2 E = {}^2 E$	5 5	E P	375 903
		783 51	27 6776 - 155 3087	$3d^7 - 3d^6(a^3I)Ac$	a^2H^2I	2 - 2 9 11	ED.	375 903
		783.85	27.6776 155.5007	$3d^{7} = 3d(a^{1})4s$	$a^{2}H^{-1}$	2 - 2 9 - 13	F,F	375,903
		784.02	42 9596 171 4060	3d - 3d (a 1)4s	$a^{-}H = -1$	$\frac{1}{2} - \frac{1}{2}$	Г,Р	375,903
		784.02	45.8580 - 171.4000	3d - 3d (a F)4s	a-F – -F	$\bar{2} - \bar{2}$	F,P	375,903
		784.86	20.9476 - 148.3582	3d ⁷ – 3d ⁶ (a ³ F)4s	$a^2G - {}^2F$	7-5	F.P	375.903
		789.34	20.9476 - 147.6359	$3d^7 - 3d^6(a^3F)4s$	$a^2G - {}^2F$	$\frac{1}{3} - \frac{1}{3}$	F.P	375.903
		791.36	19.8296 - 146.1943	$3d^{7} - 3d^{6}(a^{3}H)4s$	$a^2G - {}^2H$	<u><u><u><u></u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u>	F.P	375,903
		792.81	19.8296 - 145.9625	$3d^7 - 3d^6(a^3H)4s$	$a^2G - {}^2H$	2 <u>1</u>	FP	375 903
		795 58	26 6491 - 152 3437	$3d^7 - 3d^6(a^3G)As$	$a^2H - {}^2G$	$\frac{1}{1}$ $\frac{1}{1}$	EP	375 903
		798.42	20.9476 - 146.1943	$3d^7 - 3d^6(a^3H)4s$	$a^2G - {}^2H$	$\frac{2}{2} - \frac{2}{2}$	F,P	375,903
		799 90	20 9476 - 145 9625	2d ⁷ 3d ⁶ /a ³ H)4c	a ² G ² H	2 11	ED	275 002
		800.48	26.9470 = 143.9023 26.6491 = 151.5747	$3d^7 - 3d^6(a^3G)/a$	$a \mathbf{U} = \mathbf{\Pi}$	1 2 - 2 11 9	F,F	375,903
		810.09	18 1186 141 5612	$3d^7 - 3d^6(a^3P)Aa$	aH = G	2 - 2 2 1	г,r	375,903
		811.72	18.1180 - 141.5012	$3d^{2} - 3d^{2}(a^{2}P)4s$	a'P - P	$\frac{5}{2} - \frac{5}{2}$	F,P	375,903
		011.75	18.3008 - 141.5012	$3d^{2} - 3d^{2}(a^{2}P)4s$	$\mathbf{a}^{T}\mathbf{P} - \mathbf{P}$	$\frac{1}{2} - \frac{1}{2}$	F,P	375,903
		818.17	18.9384 - 141.3612	$3d^{7} - 3d^{6}(a^{3}P)4s$ $3d^{7} - 3d^{6}(a^{3}P)4s$	$a^{4}P - {}^{4}P$	$\frac{1}{2} - \frac{1}{2}$	F,P F,P	375,903
						2 2	- ,-	575,765
		819.83	18.3668 - 140.3430	3d ⁷ – 3d ⁶ (a ³ P)4s	$a^4P - {}^4P$	$\frac{3}{2} - \frac{3}{2}$	F,P	375,903
		822.75	23.6489 - 145.1921	$3d^7 - 3d^6(a^3P)4s$	$a^2P - {}^2P$	$\frac{3}{2} - \frac{3}{2}$	F,P	375,903
		823.83	18.9584 - 140.3430	3d ⁷ – 3d ⁶ (a ³ P)4s	a ⁴ P – ⁴ P	$\frac{1}{2} - \frac{3}{2}$	F,P	375,903
		825.11	1.1897 – 122.3861	$3d^7 - 3d^6(a^5D)4s$	ga⁴F – ⁴D	$\frac{2}{2} - \frac{3}{2}$	F,P	375,903
		827.06	0 120.9095	$3d^{7} - 3d^{6}(a^{5}D)4s$	$ga^4F - {}^4D$	$\frac{9}{2} - \frac{7}{2}$	F,P	375,903
		828.67	2.0425 - 122.7174	$3d^7 - 3d^6(a^5D)4s$	$ga^4F - {}^4D$	$\frac{5}{2} - \frac{1}{2}$	F,P	375,903
		829.06	1.1897 - 121.8077	3d ⁷ – 3d ⁶ (a ⁵ D)4s	ga ⁴ F – ⁴ D	$\frac{7}{2} - \frac{5}{2}$	F,P	375,903
		829.60	27.0965 - 147.6359	3d ⁷ - 3d ⁶ (a ³ F)4s	$a^2D - {}^2F$	$\frac{5}{2} - \frac{7}{2}$	F,P	375,903
		830.95	2.0425 - 122.3861	$3d^7 - 3d^6(a^5D)4s$	ga⁴F – ⁴D	$\frac{5}{2} - \frac{3}{2}$	F.P	375,903
		831.06	18.1186 - 138.4462	$3d^7 - 3d^6(a^3P)4s$	a ⁴ P - ⁴ P	\$ - 5	F.P	375,903
		832.67	2.6211 - 122.7174	$3d^7 - 3d^6(a^5D)4s$	$ga^4F - {}^4D$	3 - 1	F.P	375,903
		832.78	18.3668 - 138.4462	$3d^{7} - 3d^{6}(a^{3}P)4s$	$a^4P - {}^4P$	$\frac{3}{2} - \frac{5}{2}$	F,P	375,903
		834.97	2.0425 - 121.8077	3d ⁷ - 3d ⁶ (2 ⁵ D)4e	ga ⁴ F - ⁴ D	5_5	FP	375 003
		835.28	1 1897 - 120 9095	$3d^7 = 3d^6(a^5D)4s$	ga^4F 4D	2 2 2	ED	375,903
		836.26	28 7777 - 148 3592	$3d^{7} - 3d^{6}(a^{3}E)Aa$	gar - D	2 2 2	F,F	375,903
		836.50	26.777 - 146.3362	$3u - 3u^{2}(a^{2}r) 4s$		1 - 2 - 2 11 - 4	r,P	375,903
		836.00	18 0584 128 4462	30° - 30°(a°H)4s	a'H - 'H	$\frac{1}{2} - \frac{1}{2}$	F,P	375,903
		838.13	26.6491 - 145.9625	$3d^{7} - 3d^{6}(a^{3}H)4s$ $3d^{7} - 3d^{6}(a^{3}H)4s$	$a^{7}P - {}^{7}P$ $a^{2}H - {}^{2}H$	<u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u>	F,P F,P	375,903 375,903
		941.24		a 17 a 167 3-00 4				
		841.34	28./// - 14/.6359	3d' – 3d'(a'F)4s	a D – F	2 - 2	F,P	375,903
		843.76	27.6776 - 146.1943	3d' – 3d°(a'H)4s	$a^2H - {}^2H$	$\frac{2}{2} - \frac{9}{2}$	F,P	375,903
		845.42	27.6776 - 145.9625	$3d^{7} - 3d^{6}(a^{3}H)4s$	$a^2H - {}^2H$	$\frac{9}{2} - \frac{11}{2}$	F,P	375,903
		846.77	27.0965 - 145.1921	$3d^7 - 3d^6(a^3P)4s$	$a^2D - {}^2P$	$\frac{5}{2} - \frac{3}{2}$	F,P	375,903
		859.00	28.7777 - 145.1921	$3d^{7} - 3d^{6}(a^{3}P)4s$	$a^2D - {}^2P$	$\frac{3}{2} - \frac{3}{2}$	F,P	375,903
		859.25	43.4375 - 159.8184	$3d^7 - 3d^6(a^3D)4s$	$a^2F - {}^2D$	$\frac{5}{2} - \frac{5}{2}$	F,P	375,903

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Multiplet	Rel. Int.	$\lambda_{\rm vac}$ (in Å)	Levels (in 10^3 cm 3)	Configurations	Terms	J - J	Notes	References
		861.62	43.4375 - 159.4985	3d ⁷ - 3d ⁶ (a ³ D)4s	$a^2F - ^2D$	$\frac{5}{2} - \frac{3}{2}$	F,P	375,903
		862.37	43.8586 - 159.8184	$3d^{7} - 3d^{6}(a^{3}D)4s$	$a^2F - ^2D$	$\frac{1}{2} - \frac{2}{2}$	F,P	375,903
		864.75	43.8586 - 159.4985	3d ⁷ - 3d ⁶ (a ³ D)4s	$a^2F - ^2D$	$\frac{7}{2} - \frac{3}{2}$	F,P	375,903
		885.63	43.4375 - 156.3512	3d ⁷ - 3d ⁶ (a ¹ G)4s	a ² F - ² G	$\frac{5}{2} - \frac{7}{2}$	F,P	375,903
		886.08	43.4375 - 156.2940	3d ⁷ - 3d ⁶ (a ¹ G)4s	$a^2F - {}^2G$	$\frac{5}{2} - \frac{9}{2}$	F,P	375,903
		888.95	43.8586 - 156.3512	3d ⁷ - 3d ⁶ (a ¹ G)4s	$a^2F - {}^2G$	$\frac{7}{2} - \frac{7}{2}$	F,P	375,903
		889.40	43.8586 - 156.2940	3d7 - 3d6(a1G)4s	$a^2F - C^2G$	$\frac{7}{2} - \frac{9}{2}$	F,P	375,903
		894.75	0 111.7633	$3d^7 - 3d^6(a^5D)4s$	ga ⁴ F - ⁶ D	$\frac{9}{2} - \frac{5}{2}$	F,P	375,903
		899.31	0 111.1958	$3d^7 - 3d^6(a^5D)4s$	ga⁴F - ⁰D	3 - 7	F,P	375,903
		901.21	1.1897 - 112.1519	$3d^7 - 3d^6(a^5D)4s$	ga⁴F - ⁶ D	$\frac{1}{7} - \frac{3}{7}$	F.P	375,903
		904 38	1,1897 - 111,7633	$3d^7 - 3d^6(a^5D)4s$	ga⁴F – °D	7 - 5	F.P	375,903
		905.71	0 110.4106	$3d^7 - 3d^6(a^5D)4s$	ga⁴F - °D	$\frac{2}{2} - \frac{2}{2}$	F,P	- 375,903
		906 32	2 0425 - 112 3793	$3d^7 - 3d^6(a^5D)4s$	ga⁴F - °D	5-1	F.P	375,903
		908 19	2.0425 - 112.1519	$3d^7 - 3d^6(a^5D)4s$	ga⁴F - "D	5 - 3	F.P	375,903
		909.04	1 1897 - 111 1958	$3d^7 - 3d^6(a^5D)4s$	ga ⁴ F - ⁶ D	1 1 1	F.P	375,903
		911.09	2 6211 - 112 3793	$3d^7 - 3d^6(a^5D)4s$	ga ⁴ F - ⁶ D	3_1	F.P	375,903
		011.40	2.0211 - 112.5775	$3d^{7} - 3d^{6}(a^{5}D)4s$	$ga^4F = ^{\circ}D$	5_5	FP	375.903
		912.99	2.6211 - 112.1519	$3d^{7} - 3d^{6}(a^{5}D)4s$	ga⁴F – °D	$\frac{3}{2} - \frac{3}{2}$	F,P	375,903
		018 22	42 4275 152 2427	2d7 2d%=3GMs	$a^2 E^2 G$	5 2	EP	375 903
		918.22	43.4375 - 152.3437	3d - 3d (a G)4s	$a \Gamma = O$	2 2 2	F,F	375,903
		921.79	43.8586 - 152.3437	$3d^{2} - 3d^{2}(a^{2}G)4s$	$a^2F = C$	2 - 2	F,F	375,903
		924.75	43.43/5 - 151.5/4/	$3d^2 - 3d^2(a^2G)4s$	$a^2F = C$	$\frac{1}{2} - \frac{1}{2}$	F,P	375,903
		928.37	43.8586 - 151.5747	$3d^2 - 3d^2(a^2G)4s$	a'F - 'G	$\frac{1}{2} - \frac{1}{2}$	F,P	375,903
		953.10	43.4375 - 148.3582 43.8586 - 148.3582	$3d^2 - 3d^2(a^2F)4s$ $3d^2 - 3d^6(a^3F)4s$	$a^2F - {}^2F$	2 - 2 7 - 5	F,P F,P	375,903
		959.71	43.4375 - 147.6359	3d ⁷ - 3d ⁶ (a ³ F)4s	$a^2F - F$	$\frac{1}{2} - \frac{1}{2}$	F,P	375,903
		961.09	67.3600 - 171.4080	3d' – 3d'(a'F)4s	6°D - °F	2 - 2	F,P	375,903
		961.11	67.3600 - 171.4060	3d' – 3d°(a'F)4s	b ² D - ² F	2 - 2	F,P	375,903
		961.36	18.3668 - 122.3861	3d' – 3d°(a'D)4s	a*P - *D	2 - 2	F,P	375,903
		963.60	43.8586 - 147.6359	$3d' - 3d^{\circ}(a^{\circ}F)4s$ $3d^{7} - 3d^{\circ}(a^{\circ}D)4c$	$a^{4}F - {}^{4}F$		F,P	375,903
		903.77	10.7304 - 122.7174	50 - 50 (a D)+s		2 - 2	1,1	575,905
		964.42	18.1186 - 121.8077	3d ⁷ - 3d ⁶ (a ⁵ D)4s	a⁴P – ⁴D	2 - 2	F,P	375,903
		966.74	18.3668 - 121.8077	3d ⁷ – 3d ⁶ (a ⁵ D)4s	a ⁴ P – ⁴ D	$\frac{3}{2} - \frac{5}{2}$	F,P	375,903
		966.86	18.9584 - 122.3861	3d ⁷ - 3d ⁶ (a ⁵ D)4s	a ⁴ P - ⁴ D	$\frac{1}{2} - \frac{3}{2}$	F,P	375,903
		966.97	67.9898 - 171.4060	3d ⁷ - 3d ⁶ (a ¹ F)4s	b ² D - ² F	$\frac{5}{2} - \frac{7}{2}$	F,P	375,903
		972.30	18.9584 - 121.8077	3d ⁷ - 3d ⁶ (a ⁵ D)4s	a ⁴ P – ⁴ D	$\frac{1}{2} - \frac{5}{2}$	F,P	375,903
		972.85	18.1186 - 120.9095	3d ⁷ - 3d ⁶ (a ⁵ D)4s	a⁴P – ⁴D	$\frac{5}{2} - \frac{7}{2}$	F,P	375,903
		975.20	18.3668 - 120.9095	3d ⁷ – 3d ⁶ (a ⁵ D)4s	a ⁴ P - ⁴ D	$\frac{3}{2} - \frac{7}{2}$	F,P	375,903
	1	1081.6	67.3600 - 159.8184	3d ⁷ - 3d ⁶ (a ³ D)4s	$b^2D - {}^2D$	$\frac{3}{2} - \frac{5}{2}$	F,P	375,903
		1085.3	67.3600 - 159.4985	3d ⁷ - 3d ⁶ (a ³ D)4s	$b^2D - ^2D$	$\frac{3}{2} - \frac{3}{2}$	F,P	375,903
		1089.0	67.9898 - 159.8184	3d ⁷ - 3d ⁶ (a ³ D)4s	$b^2D - {}^2D$	$\frac{5}{2} - \frac{5}{2}$	F,P	375,903
		1092.8	67.9898 - 159.4985	3d ⁷ - 3d ⁶ (a ³ D)4s	$b^2D - {}^2D$	$\frac{5}{2} - \frac{3}{2}$	F,P	375,903
	0	1210.116						903
		1234.6	67.3600 - 148.3582	3d ⁷ - 3d ⁶ (a ³ F)4s	$b^2D - {}^2F$	$\frac{3}{2} - \frac{5}{2}$	F,P	375,903
		1244.3	67.9898 - 148.3582	3d ⁷ - 3d ⁶ (a ³ F)4s	$b^2D - {}^2F$	3-3	F,P	375,903
	60	1245.631	144.8151 - 225.0964	$3d^{\circ}(a^{3}G)4s - 3d^{\circ}(a^{3}D)4p$	⁴G - ⁴F°	4 - 3		903
		1245.7	67.3600 - 147.6359	3d ⁷ - 3d ⁶ (a ³ F)4s	$b^2D - {}^2F$	$\frac{3}{2} - \frac{7}{2}$	F,P	375,903
		1255.5	67.9898 - 147.6359	$3d^{7} - 3d^{6}(a^{3}F)4s$	$b^2D - {}^2F$	5-7	F,P	375,903
	10	1263.863	145.7022 - 224.8249	3d ⁶ (a ³ G)4s - 3d ⁶ (a ³ D)4p	⁴ G - ⁴ F°	$\frac{9}{2} - \frac{7}{2}$		903
	10	1269.056	145 9625 - 224 7615	$3d^{b}(a^{3}H)4s = 3d^{b}(a^{1}G)4n$	² H - ² G°	Ц_2		903
	60	1209.050	145.7025 - 224.7015	50 (a 11/15 - 50 (a C)/1p		2 2 2		903
	00	1282.700						903
	20	1287.400						903
	0	1288.310	67.0909 146.1031	247 246(=30)4=	h2D 2D	5 3	ED	375 001
	10	1295.3	0/.9898 - 143.1921	3u = 3u (a + r) + s $3d^{6}(a^{3}G)Aa = 3d^{6}(a^{3}G)Aa$	4G 2G	2 2 11 2	1,1	903
	10	1295.730	144.8151 - 221.9910	50 (a C)+s - 50 (a C)+p	0-0	2 - 2		,05

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0 1335.030 220 1335.623 179.7920 - 254.6634 $3d^{\circ}(b^{3}F)4s - 3d^{\circ}(b^{3}P)4p$ $4F - 4D^{\circ}$ $\frac{2}{3} - \frac{2}{3}$	903	,
220 1335.623 179.7920 - 254.6634 $3d^{\circ}(b^{3}F)4s - 3d^{\circ}(b^{3}P)4p$ ${}^{4}F - {}^{4}D^{\circ}$ $\frac{7}{2} - \frac{7}{2}$	903	3
	903	,
170 1336.164	903	3
30 1336.805 112.1519 - 186.9572 $3d^{6}(a^{5}D)4s - 3d^{6}(a^{5}D)4p$ $b^{-1}D^{-1}D^{-1}$	903	3
100 1337.751 111.7633 - 186.5161 $3d^{\circ}(a^{\circ}D)4s - 3d^{\circ}(a^{\circ}D)4p$ $b^{\circ}D - b^{\circ}D^{\circ}(\frac{1}{2} - \frac{1}{2})$	903	3
40 1337.973 156.3512 - 231.0918 $3d^{\circ}(a^{\dagger}G)4s - 3d^{\circ}(a^{\dagger}D)4p$ $^{2}G - ^{2}D^{\circ}$ $\frac{7}{2} - \frac{5}{2}$	903	ļ.
70 1338 796 111 1958 - 185 8900 $3d^{6}(a^{5}D)4s - 3d^{6}(a^{5}D)4p$ $b^{-4}D^{-2} - \frac{2}{2}$	901	1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	903	, ,
350 1350.674 171.655 - 164.2000 246(4)E ($\mathbf{x} = \mathbf{y} = \mathbf{z} = \mathbf{z}$	903	, ,
$330 1320 \text{ for } 177.0330 - 234.3000 \qquad 30 \ (0 \text{ for } 48 - 30 \ (0 \text{ for } 49 \ (0 \ (0 \text{ for } 49 \ (0 \ (0 \ for) 49 \ (0 \ (0 \ for) 49 \ ($	903	,
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580 1345.718 111.1958 - 185.5053 3d ⁶ (a ⁵ D)4s - 3d ⁶ (a ⁵ D)4p $^{6}D - ^{6}P^{\circ} = \frac{7}{2} - \frac{5}{2}$	903	3
470 1346.083 112.1519 - 186.4414 3d ⁶ (a ⁵ D)4s - 3d ⁶ (a ⁵ D)4p b ⁶ D - b ⁶ P ⁶ $\frac{3}{2} - \frac{3}{2}$	903	3
0 1347.447 139.8867 - 214.1010 3d ⁶ (a ³ H)4s - 3d ⁶ (a ³ G)4p ${}^{4}H - {}^{4}F^{\circ} = \frac{9}{2} - \frac{7}{2}$	903	3
20 1349.151 139.6192 - 213.7397 $3d^{\circ}(a^{3}H)4s - 3d^{\circ}(a^{3}F)4p$ $^{4}H - ^{2}G^{\circ} = \frac{11}{2} - \frac{9}{2}$	903	3
510 1350.218 112.3793 - 186.4414 $3d^{\circ}(a^{\circ}D)4p = {}^{\circ}D - {}^{\circ}P^{\circ} = \frac{1}{2} - \frac{3}{2}$	903	3
90 1350.515 144.8151 - 218.8606 $3d^{6}(a^{3}G)4s - 3d^{6}(a^{3}H)4p$ ${}^{4}G - {}^{2}H^{\circ}$ $\frac{11}{2} - \frac{11}{2}$	903	3
170 1351.419 179 5830 - 253 5793 $3d^6(h^3F)4s = 3d^6(h^3F)4n$ $4F = 4F^6 = \frac{3}{2} - \frac{3}{2}$	903	1
20 1351.574 139.6192 - 213.6069 $3d^{6}(a^{3}H)ds = 3d^{6}(a^{3}G)dp$ $^{4}H = {}^{2}H^{4}$ $\frac{1}{2} = \frac{1}{2}$	903	2
50 1351733 141 5612 - 215 5413 34 $(a_3^{1}P)$ 34 $(a_3^{1}P)$ 47 $(a_3^{1}P)$ 47 $(a_3^{1}P)$	903	,
40 136140 170 7070 253 6301 2466 $EVA = 4E^{-2}$	903	, ,
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$2v$ 1350.500 141.57/2 - 215.2929 $3d^{\circ}(a^{\circ}F)4s - 3d^{\circ}(a^{\circ}G)4p$ $^{4}F - {}^{4}G^{\circ}$ $\frac{1}{2} - \frac{1}{2}$	Q 903	3
U 1356.813 146.1943 - 219.8960 $3d^{\circ}(a^{3}H)4s - 3d^{\circ}(a^{3}G)4p$ $^{2}H - ^{2}F^{\circ}$ $\frac{9}{2} - \frac{7}{2}$	903	\$
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	903	3
60 1357.679	903	3
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	903	3
40 1359.442 152.3437 - 225.9037 $3d^{6}(a^{3}G)4s - 3d^{6}(a^{1}I)4p$ $^{2}G - ^{2}H^{6}$ $\frac{7}{2} - \frac{9}{2}$	903	3
60 1359.911 179.7920 - 253.3262 $3d^{6}(b^{3}F)4s - 3d^{6}(b^{3}P)4p$ $^{4}F - ^{4}D^{\circ}$ $\frac{7}{2} - \frac{5}{2}$	907	3
0 1362.426 159.4985 - 232.8970 $3d^{4}(a^{1})Ma = 3d^{4}(a^{1})Ma = 3d^{2}(a^{2})Ma	001	1
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450 1363 267 112 1510 195 5052 236/ 5704 336/ 5704	903	,
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NI IV -- Continued

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ultiplet Rel. Int	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
200	1364.795	140.1409 - 213.4121	3d6(a3H)4s - 3d6(a3F)4p	⁴ H – ⁴ G°	$\frac{7}{2} - \frac{5}{2}$		903
70	1365,162	179.7240 - 252.9754	$3d^{6}(b^{3}F)4s - 3d^{6}(b^{3}P)4p$	⁴ F – ⁴ D°	5-3		903
30	1365.283	139.8867 - 213.1311	$3d^{6}(a^{3}H)4s - 3d^{6}(a^{3}F)4p$	${}^{4}H - {}^{2}F^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		903
0	1366 895	145 7022 - 218 8606	$3d^{6}(a^{3}G)4s - 3d^{6}(a^{3}H)4p$	${}^{4}G - {}^{2}H^{\circ}$	1 2 _ 1		903
40	1368 208	152 3437 - 225 4316	$3d^{6}(a^{3}G)4s = 3d^{6}(a^{1}G)4n$	${}^{2}\mathbf{G} - {}^{2}\mathbf{F}^{\circ}$	1 - 5		903
10	1368 987	141 5772 - 214 6228	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}F)4p$	${}^{4}F - {}^{2}G^{\circ}$	1 - 1	0	903
	1500.507	141.5772 - 214.0220					,
0	1369.212	141 5770 014 5074	2-16/-3724- 2-16/-3424-	412 2119	7 9		903
0	1369.690	141.5//2 - 214.58/4	3d (a F)45 - 3d (a F)4p	$\Gamma - \Pi$	2 - 2	Q	903
10	1370.062	140.1409 - 213.1311	$3d^{\circ}(a^{\circ}H)4s - 3d^{\circ}(a^{\circ}F)4p$	H - F	$\frac{1}{2} - \frac{1}{2}$	Q	903
240	1371.411	139.2894 - 212.2070	$3d^{\circ}(a^{\circ}H)4s - 3d^{\circ}(a^{\circ}F)4p$	H - G	$\frac{1}{2} - \frac{1}{2}$		903
600	1371.697	111.1958 – 184.0991	$3d^{\circ}(a^{\circ}D)4s = 3d^{\circ}(a^{\circ}D)4p$	$^{\circ}D - ^{\circ}P$	$\frac{1}{2} - \frac{1}{2}$		903
540	1371.780	145.9625 - 218.8606	3d°(a°H)4s – 3d°(a°H)4p	.HH.	$\frac{1}{2} - \frac{1}{2}$		903
10	1372.006	141.8320 - 214.7181	3d6(a3F)4s - 3d6(a3G)4p	⁴ F − ⁴ G°	$\frac{5}{2} - \frac{5}{2}$		903
20	1373.774	152.3437 - 225.1369	3d6(a3G)4s - 3d6(a3D)4p	$^{2}G - ^{4}D^{\circ}$	$\frac{7}{2} - \frac{7}{2}$		903
20	1377.644	139.6192 - 212.2070	3d6(a3H)4s - 3d6(a3F)4p	⁴ H − ⁴ G°	$\frac{11}{2} - \frac{11}{2}$		903
160	1378,708	139.6192 - 212.1509	$3d^{6}(a^{3}H)4s - 3d^{6}(a^{3}F)4p$	⁴ H – ⁴ G°	$\frac{11}{2} - \frac{9}{7}$		903
0	1379.337	138.4462 - 210.9436	$3d^{6}(a^{3}P)4s - 3d^{6}(a^{3}F)4p$	${}^{4}P - {}^{4}D^{\circ}$	5-5		903
10	1381.051						903
150	1201 207	120 9967 212 2919	2d%(a31)4a 2d%(a3E)4a	4H 4G°	2 1		003
150	1381.307	139.8807 - 212.2818	5u (a 11)45 - 5u (a 1)4p	n- u	2 - 2		903
20	1381.905						903
30	1382.290	111 5(33 101 0001	246(-50)4-246(-50)4-	60 600	5 7		903
400	1382.459	111.7633 - 184.0991	$3d^{\circ}(a^{\circ}D)4s = 3d^{\circ}(a^{\circ}D)4p$	$^{1}D - ^{1}P$	$\frac{1}{2} - \frac{1}{2}$		903
10	1382.745	139.8867 - 212.2070	$3d^{\circ}(a^{\circ}H)4s - 3d^{\circ}(a^{\circ}F)4p$	H - G	$\frac{1}{2} - \frac{1}{2}$		903
20	1383.727	141.8320 - 214.1010	3d°(a°F)4s – 3d°(a°G)4p	"F - "F"	2 - 2		903
50	1383.805	139.8867 - 212.1509	3d ⁶ (a ³ H)4s - 3d ⁶ (a ³ F)4p	⁴ H - ⁴ G°	$\frac{9}{2} - \frac{9}{2}$		903
20	1383.899	147.6359 - 219.8960	3d6(a3F)4s - 3d6(a3G)4p	${}^{2}F - {}^{2}F^{\circ}$	$\frac{7}{2} - \frac{7}{2}$		903
50	1384.574	156.2940 - 228.5185	3d ⁶ (a ¹ G)4s - 3d ⁶ (a ³ D)4p	${}^{2}G - {}^{2}F^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		903
20	1385.274	141.2203 - 213.4086	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}G)4p$	⁴ F – ⁴ F°	$\frac{9}{2} - \frac{9}{2}$		903
20	1385.763	141.5772 - 213.7397	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}F)4p$	${}^{4}\mathbf{F} - {}^{2}\mathbf{G}^{\circ}$	$\frac{7}{2} - \frac{9}{2}$		903
470	1386.230						903
290	1386 711	171 4060 - 243 5201	$3d^{6}(a^{1}E)4s = 3d^{6}(a^{1}E)4n$	${}^{2}\mathbf{F} - {}^{2}\mathbf{F}^{\circ}$	1-5		903
70	1386 001	171.4000 - 245.5201	50 (01) / 5 50 (01) / p	• •			903
20	1389 702	140 1409 - 212 1509	$3d^{6}(a^{3}H)As = 3d^{6}(a^{3}F)An$	4H - 4G°	2 9		903
20	1300.702	141 2203 213 1311	$3d^{6}(a^{3}E)4s = 3d^{6}(a^{3}E)4p$	${}^{4}\mathbf{F} = {}^{2}\mathbf{F}^{\circ}$	2 1		903
20	1390.014	141.2203 - 213.1311	$3d(a^{1})+s = 3d(a^{1})+p$	$^{2}G - ^{2}F^{\circ}$	2^{-2}_{2}		903
00	1394.103	132.3437 - 224.0733	3d(a O) + s = 3d(a O) + p $3d(a^{3}U) + a = 3d(a^{3}U) + p$	411 210	<u>13</u> Ц		903
30	1394.739	139.2894 - 210.9873	5u (a H)+s - 5u (a H)+p	11-1	2 - 2		705
10	1395.031	153.3138 - 224.9965	3d6(a3D)4s - 3d6(a3D)4p	${}^{4}\mathbf{D} - {}^{2}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{1}{2}$		903
30	1395.190	138.4462 - 210.1218	3d°(a'P)4s – 3d°(a'F)4p	$^{4}P - ^{4}D^{\circ}$	$\frac{2}{2} - \frac{7}{2}$	1	903
20	1395.734	153.3494 - 224.9965	3d ⁶ (a ³ D)4s - 3d ⁶ (a ³ D)4p	$^{4}D - {}^{2}P^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		903
450	1395.993	110.4106 - 182.0449	3d°(a°D)4s - 3d°(a°D)4p	°D - °F°	$\frac{4}{2} - \frac{4}{2}$		903
400	1396.560	153.5336 - 225.1369	$3d^{6}(a^{3}D)4s - 3d^{6}(a^{3}D)4p$	$^{4}D - ^{4}D^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		903
620	1397.364	153.5336 - 225.0964	3d ⁶ (a ³ D)4s - 3d ⁶ (a ³ D)4p	⁴ D - ⁴ F°	$\frac{1}{2} - \frac{9}{2}$		903
760	1398.193	110.4106 - 181.9315	3d6(a5D)4s - 3d6(a5D)4p	°D – °F°	$\frac{9}{2} - \frac{11}{2}$		903
450	1398.838		}				903
30	1399.604	155.2537 - 226.7025	$3d^{6}(a^{1}I)4s - 3d^{6}(a^{1}I)4p$	${}^{2}I - {}^{2}I^{\circ}$	$\frac{13}{2} - \frac{11}{2}$		903
660	1399.947	155.2537 - 226.6850	$3d^{6}(a^{1}I)4s - 3d^{6}(a^{1}I)4p$	${}^{2}\mathbf{I} - {}^{2}\mathbf{I}^{\circ}$	$\frac{13}{2} - \frac{13}{2}$		903
100	1400.211	151.5747 - 222.9933	$3d^{6}(a^{3}G)4s - 3d^{6}(a^{1}I)4p$	$^{2}G - ^{2}H^{\circ}$	$\frac{9}{2} - \frac{11}{2}$		903
270	1400.376	185.9970 - 257.4064	3d ⁶ (b ³ F)4s - 3d ⁶ (b ³ F)4p	${}^{2}\mathbf{F} - {}^{2}\mathbf{F}^{\bullet}$	$\frac{5}{2} - \frac{5}{2}$		903
110	1400 570						903
310	1400.570	155 3097 226 7025	2d6(a)1)4a 2d6(a)1)4a	21, 210	ц п		903
630	1400.678	155.3087 - 220.7025	$30^{1}(a^{-}1)48 = 30^{1}(a^{-}1)4p$ $346(a^{3}E)4a = 346(-^{3}E)4m$	4E 40°	2 - 2 3 5		903
290	1400.782	142.0235 - 213.4121	$30^{+}(a^{-}F)48 = 30^{+}(a^{-}F)4p$	21 210	2 ⁻² 11 13		903
20	1401.027	155.3087 - 226.6850	30°(a°1)45 - 30°(a°1)4p	40 40	$\frac{2}{3} - \frac{1}{2}$		903
360	1401.895	155.5138 - 224.6457	30°(a°D)4s - 30°(a°D)4p	- D - D'	2 - 2		903
30	1402.133						903
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NI IV - Continued

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	References
	120	1402.391	153.3388 - 224.6457	$3d^{6}(a^{3}D)4s - 3d^{6}(a^{3}D)4p$	⁴ D - ⁴ D°	5-5		903
	150	1402.542	141,8320 - 213,1311	$3d^{6}(a^{3}F)4s = 3d^{6}(a^{3}F)4n$	${}^{4}\mathbf{F} - {}^{2}\mathbf{F}^{\circ}$	1 1 1		903
	30	1403.944	153.5336 - 224.7615	$3d^{6}(a^{3}D)4s = 3d^{6}(a^{1}G)4p$	${}^{4}\mathbf{D} = {}^{2}\mathbf{G}^{\circ}$	1 2 2		903
	30	1404 084	155.5550 - 224.7615	50 (a D)43 - 50 (a O)4p	D-0	2 2 2		903
	20	1404.609	148 3582 210 5534	3d%(a ³ E)4a 3d%(a ³ C)4a	2E 2E°	5 5		903
	30	1405 940	148.3382 - 217.3334	50 (a 1)45 - 50 (a 0)4p	- F - F	2 - 2		903
	30	1403.940						903
	40	1406.058						003
	90	1406.050	139 8867 - 210 9875	3d%a3H)4e 3d%a3H)4e	41.7 210	2 11		903
	180	1407.440	195.0670 257.0180	3d(a H) + s = 3d(a H) + p $2d(b^3E) 4a = 2d(b^3E) 4a$	1 - 1 $2E 2E^{9}$	2 2 2		903
	20	1409 221	111 1058 192 2068	3d(0F)4s = 3d(0F)4p $3d(c^{5}D)4c = 3d(c^{5}D)4c$		2 - 2		903
	620	1408.231	111.1938 - 182.2008	$3d^{2}(a^{2}D)4s = 3d^{2}(a^{2}D)4p$	D - F	$\frac{7}{2} - \frac{7}{2}$		903
	640	1400.711	141.2203 - 212.2070	$30^{-}(a^{-}F)4s = 30^{-}(a^{-}F)4p$	F - G	$\frac{1}{2} - \frac{1}{2}$		903
	040	1409.847	111.1938 - 182.1236	3d (a ² D)4s - 3d ² (a ² D)4p	°D - °F	2 - 2		903
	30	1410.953				1		003
	20	1410.933	152 2128 224 1740	240(a3D)4a 240(-3D)4a	40 400	3 3		903
	740	1411.229	155.5158 - 224.1740	$3d^{2}(a^{2}D)4s = 3d^{2}(a^{2}D)4p$		$\frac{5}{7} - \frac{5}{9}$		903
	110	1411.455	111.1958 - 182.0449	$3d^{\circ}(a^{\circ}D)4s = 3d^{\circ}(a^{\circ}D)4p$	$^{\circ}D \sim ^{\circ}F^{\circ}$	$\frac{2}{2} - \frac{2}{3}$		903
	110	1411.941	155.5494 - 224.1740	3d'(a'D)4s - 3d'(a'D)4p	- D - D	2 - 2		903
	20	1413.124	152 2200 224 0752		45 350	5 7		903
	20	1413.073	153.3388 - 224.0753	3d°(a°D)4s – 3d°(a°G)4p	*D - *F*	2 - 2		903
	00	1414 270	152 2128 224 0212	246(-3D)4- 746(-3D)4-	4D 4D	3 5	1	002
	90	1414.279	155.5158 - 224.0215	$3d^{2}(a^{2}D)4s - 3d^{2}(a^{2}D)4p$	D - F	2 - 2		903
	200	1414.003	144.8151 - 215.5000	3d°(a°G)4s - 3d°(a°G)4p	G - H	$\frac{1}{2} - \frac{1}{2}$		903
	390	1414.773	153.3388 - 224.0213	3d°(a°D)4s - 3d°(a°D)4p	*D - *F*	2 - 2		903
	190	1414.899			4.5.4.5.4	1		903
	390	1416.403	140.3430 - 210.9436	$3d^{\circ}(a^{\circ}P)4s - 3d^{\circ}(a^{\circ}F)4p$	$^{\circ}P - ^{\circ}D^{\circ}$	2 - 2		903
	430	1410.535	155.3087 - 225.9037	3d°(a'1)4s - 3d°(a'1)4p	1 - 'H'	$\frac{11}{2} - \frac{3}{2}$		903
	500	1416 060	141 5772 212 1500	240(-35)4-240(-35)4-	45 400	7 9		003
	290	1410.900	141.5772 - 212.1509	$3d^{2}(a^{2}F)4s = 3d^{2}(a^{2}F)4p$	F - G	$\frac{1}{2} - \frac{1}{2}$		903
	410	1417.282	159.6192 - 210.1770	$3d^{2}(a^{2}H)4s = 3d^{2}(a^{2}H)4p$	H - T	$\frac{1}{2} - \frac{1}{2}$		903
	410	1417.587	153.5336 - 224.0753	$3d^{\circ}(a^{\circ}D)4s - 3d^{\circ}(a^{\circ}G)4p$	*D - *F*	$\frac{1}{2} - \frac{1}{2}$		903
	290	1418.076	155 2527 225 7525	216/10/2016/10/2	27 27 70	13 11		903
	230	1418.557	155.2537 - 225.7585	$3d^{(a)}(a')4s - 3d^{(a)}(a'G)4p$	$^{-1} - ^{-1}H^{-1}$	17 - 7		903
	130	1416.308	111.7633 - 182.2399	3d"(a"D)4s - 3d"(a"D)4p	"D - "F"	2 - 2		903
	60	1419 786						
	610	1410.700	128 4462 208 0121	2-10(-3D)4- 2-10(-3D)4-	4D 4D°	5 7		903
	590	1419.124	138.4402 - 208.9121	$3d^{2}(a^{2}F)4s = 3d^{2}(a^{2}F)4p$	P - D	1 - 2		903
	690	1419.430	141.0520 - 212.2818	$3d^{2}(a^{2}F)4s = 3d^{2}(a^{2}F)4p$ $3d^{2}(a^{2}D)4a = 3d^{2}(a^{2}D)4p$	F - G	2 - 2		903
	130	1419.577	153 3404 223 7854	$3d^{0}(a^{3}D)(a^{2}-3d^{0}(a^{3}D))(a^{2}-3d^{0}(a^{3}-3D))(a^{2}$		1 2 - 2		903
	540	1470 136	153.3494 - 223.7834 151.5747 221.0010	3d(a D)4s - 3d(a D)4p $3d^{b}(a^{3}C)4a - 3d^{b}(a^{3}C)4r$	2C - 2C	2 - 2		903
	540	1420.150	191.9747 - 221.9910	50 (a C)45 - 50 (a C)4p	0-0	2 - 2		903
	80	1420.281	156,2940 - 226 7025	$3d^{0}(a^{1}G)4s = 3d^{0}(a^{1}I)4n$	$^{2}G = ^{2}I^{\circ}$	5 Π		903
	740	1421.218	111.7633 - 182 1256	$3d^{6}(a^{5}D)4s = 3d^{6}(a^{5}D)4r$	°D-°E°	2 2 2		903
	0	1421.806	111.7055 - 102.1250	50 (a D)+s = 50 (a D)+p	D-1	2 - 2		903
	160	1422.607	190 9328 - 261 2263	$3d^{6}(h^{1}G)4s = 3d^{6}(h^{1}G)4n$	${}^{2}G = {}^{2}F^{\circ}$	Z 2		903
	220	1423 437	$142\ 0235 = 212\ 2759$	$3d^{6}(a^{3}E)4a = 3d^{6}(a^{3}E)4a$	$4\mathbf{E} = {}^{2}\mathbf{E}^{\circ}$	3 5		903
	190	1423.524	140.3430 - 210.5906	$3d^{6}(a^{3}P)4s = 3d^{6}(a^{3}P)4p$	4P - 4D°	2 2 2		903
			1100000	54 (a 1) 15 54 (a 1) 1p	1 - 2	2 - 2	1	
	230	1425.791	112.1519 - 182.2884	3d ⁶ (a ⁵ D)4s - 3d ⁶ (a ⁵ D)4n	°D - °F°	3 - 1		903
	660	1426.369	112,1519 - 182,2599	$3d^{6}(a^{5}D)4s = 3d^{6}(a^{5}D)4n$	"D – "F"	3 3		903
	80	1426 505		50 (a D)15 50 (a D)1p	D = 1	2 - 2		903
	390	1426.794						903
	30	1426.941						903
	700	1427.450	112,1519 - 182 2068	$3d^{6}(a^{5}D)4s = 3d^{6}(a^{5}D)4n$	6D - 6E	3 5		903
			112.12.17 102.2000	ο (« Δ)το - ου (α Δ)τρ	0-1	2 2		903
	50	1427,906						903
	670	1428,929	145.7022 - 215.6845	$3d^{6}(a^{3}G)4s = 3d^{6}(a^{3}G)4n$	4G - 4H°	2 LL		903
	660	1430,188	120.9095 - 190.8303	$3d^{6}(a^{5}D)4s = 3d^{6}(a^{5}D)4n$	4D 4P	2 2 Z 5		903
	630	1430.431	112.3793 - 182.2884	$3d^{6}(a^{5}D)4s = 3d^{6}(a^{5}D)4n$	0- F	2 - 2 1 1		903
	520	1430.935	138.4462 - 208.3307	$3d^{6}(a^{3}P)4s = 3d^{6}(a^{3}F)4p$	$4P + 4F^{\circ}$	2 2 2		903
	600	1431 016	112.3793 - 182.2599	$3d^6(a^5D)Ae = 3d^6(a^5D)A=$	6D 6E	1 3		903
			11210190 10212999		D-F	2 - 2		905

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Multiplet Rel.	. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	Reference
1	20	1431.818		· · · · · · · · · · · · · · · · · · ·				903
1	10	1432.283						903
5	20	1432.453	121.8077 - 191.6182	3d*(a5D)4s - 3d*(a5D)4p	⁴ D - ⁴ P°	2 - 2		903
4	40	1433.088	147.6359 - 217.4143	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}F)4p$	${}^{2}\mathbf{F} - {}^{2}\mathbf{D}^{\circ}$	$\frac{1}{2} - \frac{2}{2}$		903
1	80	1433.260	159.4985 - 229.2695	3d ⁶ (a ³ D)4s - 3d ⁶ (a ³ D)4p	${}^{2}D - {}^{2}F^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		903
	80	1433.338	141.2203 - 210.9875	3d ⁶ (a ³ F)4s - 3d ⁶ (a ³ H)4p	⁴ F − ² I °	$\frac{9}{2} - \frac{11}{2}$		903
	10	1434.665						903
2	30	1434.953						903
4	80	1435.031	152.3437 – 222.0293	3d ⁶ (a ³ G)4s - 3d ⁶ (a ³ G)4p	${}^{2}G - {}^{2}G^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		903
6	70	1435.235	146.0615 - 215.7361	3d°(a ³ G)4s - 3d°(a ³ G)4p	⁴G – ⁴H°	$\frac{7}{2} - \frac{9}{2}$		903
1	70	1435.385						903
24	40	1435.793	152.3437 - 221.9910	3d*(a3G)4s - 3d*(a3G)4p	$^{2}G - ^{2}G^{\circ}$	$\frac{1}{2} - \frac{9}{2}$	-	903
1	70	1436.984	145.7022 - 215.2929	3d6(a3G)4s - 3d6(a3G)4p	⁴G - ⁴G°	$\frac{9}{2} - \frac{7}{2}$		903
4	70	1437.168	148.3582 - 217.9397	3d*(a3F)4s - 3d*(a3F)4p	${}^{2}\mathbf{F} - {}^{2}\mathbf{D}^{\circ}$	$\frac{5}{2} - \frac{3}{2}$		903
6	10	1437.393	146.1538 - 215.7245	3d*(a ³ G)4s - 3d*(a ³ G)4p	⁴G – ⁴H°	$\frac{5}{2} - \frac{7}{2}$		903
20	00	1437.552	138.4462 - 208.0091	3d°(a3P)4s - 3d°(a3P)4p	${}^{4}\mathbf{P} - {}^{2}\mathbf{D}^{\circ}$	$\frac{5}{2} - \frac{5}{2}$		903
1	80	1437.761	156.3512 - 225.9037	$3d^{\circ}(a^{\dagger}G)4s - 3d^{\circ}(a^{\dagger}I)4p$	${}^{2}\mathbf{G} - {}^{2}\mathbf{H}^{\circ}$	$\frac{7}{2} - \frac{9}{2}$		903
6	60	1437.943	145.9625 - 215.5066	3d°(a3H)4s - 3d°(a3G)4p	² H – ⁴ H°	$\frac{11}{2} - \frac{13}{2}$		903
	20	1438.590	139.6192 - 209.1319	3d°(a3H)4s - 3d°(a3H)4p	⁴ H - ² G°	$\frac{11}{2} - \frac{9}{2}$		903
70	00	1438.816	144.8151 - 214.3168	3d°(a3G)4s - 3d°(a3G)4p	⁴G – ⁴G°	$\frac{11}{2} - \frac{11}{2}$		903
5	60	1439.060	146.1943 - 215.6845	3d°(a ³ H)4s - 3d°(a ³ G)4p	² H – ⁴ H°	$\frac{9}{2} - \frac{11}{2}$		903
20	60	1439.497						903
5	80	1439.584	156.2940 - 225.7585	3d6(a1G)4s - 3d6(a1G)4p	${}^{2}G - {}^{2}H^{\circ}$	$\frac{9}{2} - \frac{11}{2}$		903
29	90	1439.773	146.0615 - 215.5168	$3d^{6}(a^{3}G)4s - 3d^{6}(a^{3}G)4p$	⁺G – ⁺F°	$\frac{7}{2} - \frac{5}{2}$		903
2	30	1440.617	141.8320 - 211.2468	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}F)4p$	⁴ F - ⁴ D°	$\frac{5}{2} - \frac{3}{2}$		903
2	90	1441.269						903
4	80	1441.620	141.5772 - 210.9436	3d°(a ³ F)4s - 3d°(a ³ F)4p	${}^{4}F - {}^{4}D^{\circ}$	$\frac{1}{2} - \frac{5}{2}$	Р	903
6	40	1442.134	139.2894 - 208.6313	$3d^{6}(a^{3}H)4s - 3d^{6}(a^{3}H)4p$	⁴ H – ⁴ H*	13 - 13		903
20	00 Ì	1442.414	142.0235 - 211.3517	3d ⁶ (a ³ F)4s - 3d ⁶ (a ³ F)4p	⁴ F – ⁴ D°	$\frac{3}{2} - \frac{1}{2}$	Р	903
2	70	1442.500	153.3388 - 222.6629	$3d^{6}(a^{3}D)4s - 3d^{6}(a^{3}D)4p$	⁴ D - ⁴ P°	$\frac{5}{2} - \frac{3}{2}$	Р	903
3	70	1442.675	122.7174 - 192.0335	3d*(a5D)4s - 3d*(a5D)4p	4D - 4P°	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		903
	90	1444.043	140.1409 - 209.3914	$3d^{6}(a^{3}H)4s - 3d^{6}(a^{3}H)4p$	${}^{4}H - {}^{2}G^{\circ}$	<u>1</u> _ <u>7</u>		903
2	20	1444.137	139.8867 - 209.1319	$3d^{6}(a^{3}H)4s - 3d^{6}(a^{3}H)4p$	⁺H - ² G°	2 - 2		903
6	20	1444.425	146.0615 - 215.2929	$3d^{6}(a^{3}G)4s - 3d^{6}(a^{3}G)4p$	⁺G - ⁺G°	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		903
1	10	1444 604	142.0235 - 211.2468	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}F)4p$	⁴ F - ⁴ D°	3-3		903
6	60	1444.899	145.7022 - 214.9105	3d°(a'G)4s - 3d°(a'G)4p	⁺G – ⁺G°	$\frac{1}{2} - \frac{1}{2}$		903
5.	40	1445 078	179 6550 - 248 8554	$3d^{6}(h^{3}F)4s = 3d^{6}(h^{3}F)4n$	⁴ F - ⁴ G°	<u></u> ξ_μ		903
2	10	1446 376	146 1538 - 215 2929	$3d^{6}(a^{3}G)4s = 3d^{6}(a^{3}G)4p$	⁴ G - ⁴ G°	3-1		903
2	60	1446 935	141 8320 - 210 9436	$3d^{6}(a^{3}F)4s = 3d^{6}(a^{3}F)4n$	⁴ F - ⁴ D°	3-3		903
	20	1447 193	1461943 = 2152929	$3d^{(a+1)}s = 3d^{(a+1)}p$ $3d^{(a+1)}s = 3d^{(a+1)}p$	² H - ⁴ G ⁹	2 _ 1		903
2	40	1447.576	156 3512 = 225 4316	$3d^{6}(a^{1}G)4s = 3d^{6}(a^{1}G)4n$	${}^{2}G - {}^{2}F^{*}$	1 2 5		903
3	20	1448.805	121.8077 - 190.8303	3d ⁶ (a ⁵ D)4s - 3d ⁶ (a ⁵ D)4p	⁴ D - ⁴ P°	$\frac{5}{2} - \frac{5}{2}$		903
7	30	1449 011	139 6192 - 208 6313	3d°(a3H)4s - 3d°(a3H)4n	⁴H – ⁴H°	<u>1</u> – 1		903
	90	1449 193	142 0235 - 211 0276	$3d^{6}(a^{3}F)4s = 3d^{6}(a^{3}P)4n$	4F - 4D*	$\begin{vmatrix} 2 & 2 \\ 3 & -\frac{3}{2} \end{vmatrix}$		903
2	30	1449 464	140 1409 - 209 1319	$3d^{6}(a^{3}H)4s = 3d^{6}(a^{3}H)4n$	4H - 2G*	$\frac{1}{2} - \frac{2}{2}$		903
5	50	1449.782	139,6192 - 208 5953	$3d^{6}(a^{3}H)4s = 3d^{6}(a^{3}H)4n$	4H - 4H°	ų́ _ ų́		903
	40	1450.366	145.9625 - 214.9105	$3d^{6}(a^{3}H)4s - 3d^{6}(a^{3}G)4n$	² H - ⁴ G°	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		903
	20	1450.926	145.7022 - 214.6228	3d ⁶ (a ³ G)4s - 3d ⁶ (a ³ F)4p	⁴ G - ² G°	$\frac{2}{2} - \frac{2}{2}$	Q	903
1	70	1451 347	141 2203 - 210 1218	3d6(a3F)4s - 3d6(a3F)4n	4F - 4D°	2 _ 7		903
4	60	1452 220	139 2894 _ 208 1495	$3d^{6}(a^{3}H)4s = 3d^{6}(a^{3}H)4n$	4H - 41°	11 22		903
1	30	1452 549	200.1475	56 (a 11)76 - 56 (a 11)7p				903
	70	1453 495	153 5336 - 222 3333	$3d^{6}(a^{3}D)4s = 3d^{6}(a^{3}D)4n$	⁴ D - ⁴ P°	² - ⁵		903
4	50	1453 653	144 8151 - 213 6069	$3d^{6}(a^{3}G)4s = 3d^{6}(a^{3}G)4n$	${}^4G - {}^2H^{\circ}$	ļ ų́ _ ų́		903
	20	1454 374	141 8320 - 210 5006	$3d^{6}(a^{3}E)Ae = 3d^{6}(a^{3}D)Ae$	4F_4D*	2 - 2 5 - 5		903
	211	1 - 14 1/0					. 1	141

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NI IV - Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	310	1454 501	141 5612 - 210 3133	$3d^{6}(a^{3}P)4s - 3d^{6}(a^{3}P)4p$	$^{4}P - ^{4}D^{\circ}$	1-1		903
	700	1455 434	120 8867 208 6053	$\frac{3}{2}d^{2}(a^{3}H)Aa = \frac{3}{2}d^{2}(a^{3}H)Aa$	40 400	2 11		003
	/00	1455.424	159.8807 - 208.5955	3d(a H)4s = 3d(a H)4p	$^{2}D^{2}E^{\circ}$	2^{-2}		903
	410	1455.602	159.8184 - 228.5185	$3d^{\circ}(a^{\circ}D)4s - 3d^{\circ}(a^{\circ}D)4p$	$^{2}D - ^{2}F$	$\frac{1}{2} - \frac{1}{2}$		903
	140	1455.897	171.4080 - 240.0942	$3d^{\circ}(a'F)4s - 3d^{\circ}(a'F)4p$	$^{2}\mathbf{F} - ^{2}\mathbf{D}^{2}$	2 - 2		903
	20	1456.314	185.9970 – 254.6634	3d ⁶ (b ³ F)4s - 3d ⁶ (b ³ P)4p	$^{2}\mathbf{F} - ^{4}\mathbf{D}^{\circ}$	$\frac{2}{2} - \frac{1}{2}$	Q	903
	380	1456.516	146.0615 - 214.7181	3d ⁶ (a ³ G)4s - 3d ⁶ (a ³ G)4p	⁴ G − ⁴ G°	$\frac{7}{2} - \frac{5}{2}$		903
	130	1456 862						903
	10	1457 165						903
	10	1457.105	145 5000 014 0160		40 400	9 11		003
	90	1457.422	145.7022 - 214.3168	3d°(a°G)4s - 3d°(a°G)4p		$\frac{1}{2} - \frac{1}{2}$		903
	500	1457.862	144.8151 - 213.4086	$3d^{\circ}(a^{\circ}G)4s - 3d^{\circ}(a^{\circ}G)4p$	"G – "F"	$\frac{1}{2} - \frac{1}{2}$		903
	80	1458.483	146.1538 - 214.7181	3d°(a'G)4s - 3d°(a'G)4p	⁴ G − ⁴ G°	$\frac{2}{2} - \frac{2}{2}$		903
	380	1458.904	141.5772 - 210.1218	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}F)4p$	⁴ F – ⁴ D°	$\frac{1}{2} - \frac{1}{2}$		903
	10	1459.211	156.2940 - 224.8249	$3d^{6}(a^{1}G)4s - 3d^{6}(a^{3}D)4p$	${}^{2}G - {}^{4}F^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		903
	400	1460 430	156 3512 - 224 8249	$3d^{6}(a^{1}G)4s - 3d^{6}(a^{3}D)4p$	${}^{2}G - {}^{4}F^{\circ}$	<u>1</u> <u>1</u>		903
	590	1460 543	1562940 - 2247615	$3d^{6}(a^{1}G)As = 3d^{6}(a^{1}G)Ap$	$^{2}G - ^{2}G^{\circ}$	2 2		903
	220	1461.069	120 8967 209 2207	$3d(a^{3}U)a = 3d(a^{3}U)a$	41 450	2 2 2	i i	003
	220	1401.008	139.8807 - 208.3307	30 (a H)48 - 30 (a F)4p		$\frac{1}{2} - \frac{1}{2}$		903
	460	1461.478	141.5612 - 209.9851	$3d^{\circ}(a^{\circ}P)4s - 3d^{\circ}(a^{\circ}P)4p$	·P - ·D·	$\frac{2}{2} - \frac{2}{2}$		903
	130	1461.762	156.3512 - 224.7615	3d°(a'G)4s – 3d°(a'G)4p	'G - 'G'	$\frac{1}{2} - \frac{1}{2}$		903
	460	1462.005	145.7022 - 214.1010	3d ⁶ (a ³ G)4s - 3d ⁶ (a ³ G)4p	⁴ G - ⁴ F°	$\frac{9}{2} - \frac{7}{2}$		903
	470	1462.144	146.1943 - 214.5874	$3d^{6}(a^{3}H)4s - 3d^{6}(a^{3}H)4p$	${}^{2}H - {}^{2}H^{\circ}$	$\frac{9}{2} - \frac{9}{2}$		903
	540	1463.248						903
	380	1463 683	151 5747 - 219 8960	$3d^{6}(a^{3}G)4s = 3d^{6}(a^{3}G)4n$	${}^{2}\mathbf{G} - {}^{2}\mathbf{F}^{\circ}$	2 _ 2		903
	50	1464 335	141 8320 210 1218	$3d^{6}(a^{3}E)As = 3d^{6}(a^{3}E)As$	4F 4D°	1 1 1 1 1		903
	0	1466 501	140.1400 208.2207	$3d(a^{3}H)/a = 3d(a^{3}E)/a$	44 450	2^{-2}_{2}		003
	80	1400.501	140.1409 - 208.3307	30 (a H)45 - 30 (a F)4p	n-r	$\overline{2} - \overline{2}$		903
	20	1466.932	156.2940 - 224.4636	3d6(a1G)4s - 3d6(a1G)4p	${}^{2}G - {}^{2}G^{\circ}$	$\frac{9}{2} - \frac{7}{2}$	-	903
	120	1467.140	139.8867 - 208.0468	3d ⁶ (a ³ H)4s - 3d ⁶ (a ³ H)4p	⁴ H − ⁴ I°	2 - 2		903
	90	1467.881						903
	570	1468.041	140.3430 - 208.4610	$3d^{6}(a^{3}P)4s - 3d^{6}(a^{3}P)4p$	${}^{4}P - {}^{4}P^{\circ}$	3-3		903
	400	1468.159	156.3512 - 224.4636	$3d^{6}(a^{1}G)4s - 3d^{6}(a^{1}G)4p$	${}^{2}G - {}^{2}G^{*}$	1 1		903
	130	1468.422	147.6359 - 215.7361	$3d^{\circ}(a^{3}F)4s - 3d^{\circ}(a^{3}G)4p$	${}^{2}\mathbf{F} - {}^{4}\mathbf{H}^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		903
	(20)	1469.026	128 4462 206 5222	2-10/-30-2-10/-30-4-	40 40	5 5		001
	620	1468.925	138.4462 - 206.5232	3d°(a°P)4s - 3d°(a°P)4p	$\mathbf{P} - \mathbf{P}^{*}$	$\frac{1}{2} - \frac{1}{2}$		903
	80	1469.737	146.0615 - 214.1010	3d°(a'G)4s – 3d°(a'G)4p	*G - *F*	2 - 2		903
	440	1470.422	179.7240 - 247.7317	3d ⁶ (b ³ F)4s - 3d ⁶ (b ³ F)4p	⁴ F − ⁴ G°	$\frac{3}{2} - \frac{7}{2}$		903
	30	1471.893	179.7920 - 247.7317	3d ⁶ (b ³ F)4s – 3d ⁶ (b ³ F)4p	⁴ F - ⁴ G°	$\frac{1}{2} - \frac{1}{2}$		903
	40	1472.500	141.2203 - 209.1319	3d ⁶ (a ³ F)4s - 3d ⁶ (a ³ H)4p	⁴ F - ² G °	$\frac{9}{2} - \frac{9}{2}$		903
	690	1472.633	140.1409 - 208.0468	3d6(a3H)4s - 3d6(a3H)4p	⁴ H − ⁴ I°	$\frac{7}{2} - \frac{9}{2}$		903
	220	1474.626	141.5772 - 209.3914	3d ⁶ (a ³ F)4s ~ 3d ⁶ (a ³ H)4n	${}^{4}\mathbf{F} - {}^{2}\mathbf{G}^{*}$	1_1_1		903
	150	1475 338	1562940 - 2240753	$\frac{3d^{6}(a^{\dagger}G)As}{3d^{6}(a^{\dagger}G)As} = \frac{3d^{6}(a^{\dagger}G)As}{3d^{6}(a^{\dagger}G)As}$	$^{2}\mathbf{G} = ^{2}\mathbf{F}^{\circ}$	2 1		903
	660	1476 233	155 2537 222 0033	$3d^{0}(a^{1}I)Aa = 3d^{0}(a^{1}I)Aa$	21 2110		ıl	003
	660	1476.233	133.2337 - 222.9933	3d (a 1)48 - 3d (a 1)4p	-1n	$\frac{1}{2} - \frac{1}{2}$		903
	000	14/0.290			1- 1-4			903
	490 680	1476.429	159.8184 - 227.5494 141.2203 - 208.9336	$3d^{\circ}(a^{3}D)4s - 3d^{\circ}(a^{3}D)4p$ $3d^{6}(a^{3}E)4s - 3d^{6}(a^{3}E)4p$	⁴ F - ⁴ F°	$\frac{5}{2} - \frac{5}{2}$		903
			2007000			2-2		
	80	1476.954	145.7022 - 213.4086	3d6(a3G)4s - 3d6(a3G)4p	⁴G - ⁴F°	$\frac{9}{2} - \frac{9}{2}$		903
	80	1477.284	141.2203 - 208.9121	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}P)4p$	⁴ F - ⁴ D°	3-1		903
	250	1477.485	159,4985 - 227,1811	$3d^{6}(a^{3}D)4s - 3d^{6}(a^{3}D)4n$	$^{2}D - ^{2}D^{\circ}$	11_1		903
	160	1477 576	146.0615 - 213 7397	$3d^{6}(a^{3}G)4s = 3d^{6}(a^{3}F)4n$	$4G - 2G^{2}$	1 2 2		903
	500	1477 939	140.3430 - 208.0001	$3d^{6}(a^{3}D)Aa = 3d^{6}(a^{3}D)Aa$	4p 2n°	3 5		903
	110	1478.041	147.6359 - 215.2929	$3d^{\circ}(a^{3}F)4s - 3d^{\circ}(a^{3}G)4p$	² F - ⁴ G ^e	$\frac{1}{2} - \frac{1}{2}$		903
	620	1478.323	145.9625 - 213.6069	3d°(a'H)4s - 3d°(a'G)4p	² H – ² H°	12 - 12	·	903
	20	1470.743	171 4060 200 0007	2-10/-112/4- 2-10/-122/4		7 .		503
	320	14/9.209	1/1.4000 - 239.008/	3d"(a'F)4s - 3d"(a'F)4p	-F - 'D'	2 - 2		903
	570	1480.345	171.4060 - 238.9578	3d°(a'F)4s - 3d°(a'F)4p	'F - 'G°	2-2		903
	260	1480.490	146.1943 - 213.7397	3d°(a ³ H)4s - 3d°(a ³ F)4p	² H – ² G°	2 - 2		903
	440	1481.411	140.3430 - 207.8462	3d°(a ³ P)4s - 3d°(a ³ P)4p	⁴ P − ⁴ P°	$\frac{3}{2} - \frac{1}{2}$		903
		1	1					

NI IV - Continued

Multiplet Rel. Int	$\lambda_{\rm vac}$ (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	Reference
730	1482.246	139.2894 - 206.7545	'3d6(a3H)4s - 3d6(a3H)4p	⁴ H - ⁴ I°	$\frac{13}{2} - \frac{13}{2}$		903
30	1482.556	139.2894 - 206.7407	3d ⁶ (a ³ H)4s - 3d ⁶ (a ³ H)4p	⁴H – ⁴I°	$\frac{13}{2} - \frac{11}{2}$		903
450	1482.670	145.9625 - 213.4086	3d6(a3H)4s - 3d6(a3G)4p	² H – ⁴ F°	$\frac{11}{2} - \frac{9}{2}$		903
510	1483.211	152.3437 - 219.7650	3d6(a3G)4s - 3d6(a3G)4p	² G – ² H°	$\frac{7}{2} - \frac{9}{2}$		903
30	1483.432	120.9095 - 188.3201	3d6(a5D)4s - 3d6(a5D)4p	⁴ D – ⁴ F°	$\frac{7}{2} - \frac{5}{2}$		299
180	1483.754	155.3087 - 222.7055	$3d^{6}(a^{1}I)4s - 3d^{6}(a^{1}G)4p$	² I – ² H°	$\frac{11}{2} - \frac{9}{2}$		903
110	1483.849	144.8151 - 212.2070	3d ⁶ (a ³ G)4s - 3d ⁶ (a ³ F)4p	⁴G - ⁴G°	<u><u><u></u></u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u>		903
230	1484.232	141.2203 - 208.5953	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}H)4p$	⁴ F – ⁴ H°	3 - 1		903
330	1484 442	148.3582 - 215.7245	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}G)4p$	² F - ⁴ H°	5 - 1		903
200	1484.640	141.5772 - 208.9336	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}F)4p$	⁴ F - ⁴ F°	Į - 2		903
60	1485 121	141 5772 - 208 9121	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}P)4p$	4F - 4D°	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		903
530	1486.204	151.5747 - 218.8606	3d ⁶ (a ³ G)4s - 3d ⁶ (a ³ H)4p	² G - ² H°	$\frac{9}{2} - \frac{11}{2}$		903
40	1486 461	147 6359 - 214 9105	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}G)4p$	² F - ⁴ G°	$\frac{7}{2} - \frac{9}{2}$		903
20	1486 805	1461538 = 2134121	$3d^{6}(a^{3}G)4s = 3d^{6}(a^{3}F)4n$	${}^{4}G - {}^{4}G^{\circ}$	<u>5</u> - 5		903
410	1487 011	139.8867 - 207.1360	$3d^{6}(a^{3}H)4s = 3d^{6}(a^{3}H)4p$	⁴ H - ⁴ H°	<u>9</u> 1		903
420	1487.064	139.6192 - 206.8655	$3d^{6}(a^{3}H)4s = 3d^{6}(a^{3}H)4n$	⁴ H – ⁴ H°	11 _ ž		903
300	1487 865	152 3437 - 219 5534	$3d^{6}(a^{3}G)4s = 3d^{6}(a^{3}G)4n$	${}^{2}G - {}^{2}F^{\circ}$	$\frac{1}{2} - \frac{2}{5}$		903
20	1487.805	148.3582 - 215.5168	3d6(a3F)4s - 3d6(a3G)4p	${}^{2}F - {}^{4}F^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		903
(70	1480 574	120 6102 206 7545	3d6(a3U)Ae 3d6(a3U)A-	4H 4Io	шв		903
6/0	1489.334	137.0172 - 200./343	$3u (a \Pi)^{+5} - 3u (a \Pi)^{+p}$	417 419			003
720	1489.833	139.6192 - 206.7407	$30^{\circ}(a^{\circ}H)4s = 30^{\circ}(a^{\circ}H)4p$		$\frac{1}{2} - \frac{1}{2}$ 9 1		903
390	1490.080	141.2203 - 208.3307	$30^{\circ}(a^{\circ}F)4s = 30^{\circ}(a^{\circ}F)4p$	$\mathbf{F} - \mathbf{F}$	2 - 2 5 7		903
20	1490.748	141.8320 - 208.9121	3d°(a°F)4s - 3d°(a°P)4p	$\mathbf{F} - \mathbf{D}$	$\frac{1}{2} - \frac{1}{2}$		903
20	1490.982	146.0615 - 213.1311	3d°(a°G)4s - 3d°(a°F)4p	G - F	$\frac{1}{2} - \frac{1}{2}$		903
430	1491.907	141.5772 - 208.6057	3d°(a'F)4s - 3d°(a'F)4p	'F - 'F'	$\frac{1}{2} - \frac{1}{2}$		903
0	1492.168	121.8077 - 188.8242	3d°(a5D)4s - 3d°(a5D)4p	⁴D - ⁴F°	$\frac{5}{2} - \frac{3}{2}$		903
610	1492.649	140.1409 - 207.1360	3d6(a3H)4s - 3d6(a3H)4p	⁴ H – ⁴ H°	$\frac{1}{2} - \frac{1}{2}$		903
690	1493.007	139.8867 - 206.8655	3d6(a3H)4s - 3d6(a3H)4p	⁴ H – ⁴ H°	$\frac{9}{2} - \frac{9}{2}$		903
740	1493.672	155.2537 - 222.2028	$3d^{6}(a^{1}I)4s - 3d^{6}(a^{1}I)4p$	² I – ² K °	$\frac{13}{2} - \frac{15}{2}$		903
290	1493.993	141.8320 - 208.7669	3d°(a3F)4s - 3d°(a3F)4p	⁴ F − ⁴ F°	$\frac{5}{2} - \frac{3}{2}$		903
640	1495.795	139.8867 - 206.7407	3d6(a3H)4s - 3d6(a3H)4p	⁴ H − ⁴ I°	$\frac{9}{2} - \frac{11}{2}$		903
60	1496.412	141.2203 - 208.0468	3d6(a3F)4s - 3d6(a3H)4p	⁴F – ⁴I°	$\frac{9}{2} - \frac{9}{2}$		903
0	1496.623	179.5830 - 246.4 + P	3d ⁶ (b ³ F)4s - 3d ⁶ (b ³ P)4p	${}^{4}F - {}^{2}S^{\circ}$	$\frac{1}{2} - \frac{1}{2}$	Q	903
380	1497.596	141.8320 - 208.6057	$3d^{\circ}(a^{3}F)4s - 3d^{\circ}(a^{3}F)4p$	⁴ F – ⁴ F°	5-5		903
530	1497.930	139.8867 - 206.6457	$3d^{\circ}(a^{3}H)4s - 3d^{\circ}(a^{3}H)4p$	⁴H - ⁴G°	<u>9</u> - 7		903
150	1498.051	141.5772 - 208.3307	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}F)4p$	⁴ F - ⁴ F°	1 - 1		903
490	1498.278	142.0235 - 208.7669	3d ⁶ (a ³ F)4s - 3d ⁶ (a ³ F)4p	⁴ F - ⁴ F°	$\frac{3}{2} - \frac{3}{2}$		903
680	1498 707	140 1409 - 206 8655	3d*(a ³ H)4s - 3d*(a ³ H)4p	⁴H – ⁴H°	7 - 2		903
710	1498.774	139.6192 - 206.3409	$3d^{6}(a^{3}H)4s - 3d^{6}(a^{3}H)4p$	⁴ H – ⁴ G°	11 - 2		903
720	1498.898	139.2894 - 206.0053	$3d^{6}(a^{3}H)4s - 3d^{6}(a^{3}H)4n$	⁴ H – ⁴ G°	بةً _ بْبًا		903
510	1499.136	140.1409 - 206.8470	$3d^{b}(a^{3}H)4s - 3d^{b}(a^{3}H)4p$	⁴ H - ⁴ G [*]	1 - 5		903
380	1499.248	156.2940 - 222 9933	$3d^{6}(a^{1}G)4s - 3d^{6}(a^{1}I)4p$	${}^{2}G - {}^{2}H^{\circ}$	<u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u>		903
0	1499.754				2		903
670	1499 977	138 4462 - 205 1141	$3d^{6}(a^{3}P)4s = 3d^{6}(a^{3}P)4n$	⁴ P – ⁴ S°	5 _ 3		903
350	1500 130	120 9095 - 187 5703	$3d^{6}(a^{5}D)4s = 3d^{6}(a^{5}D)4n$	⁴ D - ⁴ F°			903
110	1500.292	120.7075 - 107.5705			2 2		903
30	1501 204						903
100	1501.898	142 0235 - 208 6057	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}F)4n$	⁴ F - ⁴ F°	3-5		903
20	1502.867	.12.0205 200.0057			2 2		903
200	1503 172	185 9970 - 252 5230	$3d^6(h^3F)4s = 3d^6(h^3F)4r$	${}^{2}\mathbf{F} = {}^{2}\mathbf{G}^{\circ}$	5_1		903
290	1503.172	183.9970 - 232.3230	34(0 ⁵ D)40 34(0 ⁵ D)4-	40 450	2 2 2		903 002
430	1503.479	121.8077 - 188.3201	3u (a D) + 8 - 3u (a D) + p $3d^{6}(a^{3}U) A = 3d^{6}(a^{3}U) A =$				903
110	1503.653	140.1409 - 206.6457	$30^{\circ}(a^{\circ}H)48 = 30^{\circ}(a^{\circ}H)4p$ 240(-3E)4a = 240(-3E)4		2 - 2 2 7		903
20	1503.787	141.8320 - 208.3307	30"(a"F)4s - 30"(a"F)4p		$\frac{1}{2} - \frac{1}{2}$		903
10	1504.470	141.5772 - 208.0468	3d"(a'F)4s - 3d"(a'H)4p		$\frac{1}{2} - \frac{1}{2}$	<u>ע</u>	903
1 10	1504.544	147.6359 - 214.1010	3d°(a°F)4s - 3d°(a°G)4p	"F-"F"	1 5 - 5	1	903

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NI IV - Continued

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	References
<u> </u>	170	1504.800	139.8867 - 206.3409	3d6(a3H)4s - 3d6(a3H)4p	⁴ H - ⁴ G*	$\frac{9}{2} - \frac{9}{2}$		903
	20	1504.900	145.7022 - 212.1509	3d6(a3G)4s - 3d6(a3F)4p	⁴G - ⁴G°	$\frac{1}{2} - \frac{1}{2}$	o	903
	360	1505.170	122.3861 - 188.8242	$3d^{6}(a^{5}D)4s - 3d^{6}(a^{5}D)4p$	⁴ D – ⁴ F°	3-3		903
	180	1505.763	156.2940 - 222.7055	$3d^{6}(a^{1}G)4s - 3d^{6}(a^{1}G)4p$	$^{2}G - ^{2}H^{\circ}$	2 - 2		903
	220	1506 946	$148\ 3582 - 214\ 7181$	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}G)4p$	$^{2}\mathbf{F} - {}^{4}\mathbf{G}^{\circ}$	5_5		903
	500	1507.055	156 3512 - 222 7055	$3d^{6}(a^{1}G)As = 3d^{6}(a^{1}G)An$	² G ² H°	1 2		903
	500	1507.055	156.5512 - 222.7655	50 (a C)+s - 50 (a C)+p	0- n	2 - 2		903
	0	1507 338						903
	570	1509 108	148 3582 - 214 6228	$3d^{6}(a^{3}E)4e = 3d^{6}(a^{3}E)4e$	${}^{2}\mathbf{F} = {}^{2}\mathbf{G}^{\circ}$	5_2		903
	70	1510 106	146.0615	$3d^{6}(a^{3}G)Ac = 3d^{6}(a^{3}E)An$	4G 4G*	1 1		903
	10	1510.100	140.1409 206.3409	$3d(a^{3}U)a = 3d(a^{3}U)a$	41 40*	2 2 2	0	003
	10	1510.509	140.1409 - 200.3409	30 (a 11)45 – 30 (a 11)4p	п- 0	2 - 2	Ŷ	903
	100	1511.397	146 1528 212 2750	2d8(a3C)4a 2d8(a3E)4a	40 200	5 5		903
	190	1512.551	140.1338 - 212.2739	50 (a C)48 - 50 (a F)4p	GF	$\overline{2} - \overline{2}$		903
	350	1512 704	122 7174 - 188 8242	$3d^{6}(a^{5}D)Ae = 3d^{6}(a^{5}D)Ap$	4D 4E°	1 1	р	903
	250	1512.704	122.7174 - 108.0242	$24\%(a^{3}E)Aa = 24\%(a^{3}E)Aa$	D = T	2 2 2 2 2 2 2 2	n I	903
	330	1512.772	147.0339 - 213.7397	30(a F)4s - 30(a F)4p	$\mathbf{F} - \mathbf{G}$	$\frac{1}{2} - \frac{1}{2}$	r	903
	10	1513.132	146.1943 - 212.2818	3d ⁻ (a ⁻ H)4s - 3d ⁻ (a ⁻ F)4p	H-G	2 - 2		903
	530	1513.494	171.4080 - 237.4803	$3d^{\circ}(a'F)4s - 3d^{\circ}(a'F)4p$	$^{2}F - ^{2}G^{*}$	$\frac{1}{2} - \frac{1}{2}$	_	903
	90	1513.904	145.1921 – 211.2468	3d°(a'P)4s - 3d°(a'F)4p	² P - ⁴ D ^o	$\frac{3}{2} - \frac{3}{2}$	Q	903
	20	1514.862	146.1943 - 212.2070	3d ⁶ (a ³ H)4s - 3d ⁶ (a ³ F)4p	²H - ⁴G°	$\frac{9}{2} - \frac{11}{2}$		903
				and some and some	1- 1-1			
	700	1516.666	122.3861 - 188.3201	$3d^{\circ}(a'D)4s - 3d^{\circ}(a'D)4p$	*D – *F*	$\frac{1}{2} - \frac{1}{2}$		903
	20	1517.080	141.2203 - 207.1360	3d°(a'F)4s - 3d°(a'H)4p	*F – *H*	$\frac{2}{2} - \frac{1}{2}$	ł	903
	20	1518.951	145.1921 - 211.0276	3d ⁶ (a ³ P)4s - 3d ⁶ (a ³ P)4p	$^{2}P - ^{4}D^{\circ}$	$\frac{3}{2} - \frac{3}{2}$	•	903
	400	1519.604	185.9670 - 251.7736	3d6(b3F)4s - 3d6(b3F)4p	$^{2}\mathbf{F} - ^{2}\mathbf{G}^{\circ}$	$\frac{7}{2} - \frac{9}{2}$		903
	730	1520.626	121.8077 - 187.5703	3d ⁶ (a ⁵ D)4s - 3d ⁶ (a ⁵ D)4p	$^4D - ^4F^\circ$	$\frac{5}{2} - \frac{7}{2}$		903
	220	1520.864	145.1921 - 210.9436	$3d^{6}(a^{3}P)4s - 3d^{6}(a^{3}F)4p$	$^{2}\mathbf{P} - {}^{4}\mathbf{D}^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		903
					20.200	9 7		
	0	1521.250	156.2940 - 222.0293	3d°(a'G)4s - 3d°(a'G)4p	-G - G	2 - 2		903
	20	1521.438	185.9670 - 251.6943	3d°(b°F)4s – 3d°(b°F)4p	$^{2}F - ^{2}D^{2}$	$\frac{1}{2} - \frac{7}{2}$		903
	10	1522.209						903
	360	1524.239	120.9095 - 186.5161	$3d^{\circ}(a^{\circ}D)4s - 3d^{\circ}(a^{\circ}D)4p$	⁴ D – ⁴ D°	$\frac{1}{2} - \frac{2}{2}$	ļ	903
	10	1524.527						903
	10	1525.088						903
	750	1525 306	120 9095 186 4701	346(a ⁵ D)4c 346(a ⁵ D)4r	4D 4E°	1 9		903
	100	1525.500	120.9093 - 180.4701	3u(aD)+s - 3u(aD)+p		$\begin{vmatrix} 2 & -2 \\ 13 & 13 \end{vmatrix}$		903
	100	1320.303	155.2557 - 220.7626	30'(a'1)4s - 30'(a'1)4p	-1K	$\frac{1}{2} - \frac{1}{2}$	Ì I	903
	510	1526.764	159.4985 - 224.9965	$3d^{\circ}(a^{\circ}D)4s - 3d^{\circ}(a^{\circ}D)4p$	$^{2}D - ^{2}P^{2}$	$\frac{1}{2} - \frac{1}{2}$	ł	903
	520	1526.834	147.6359 - 213.1311	3d°(a°F)4s – 3d°(a°F)4p	"F ~ "F"	$\frac{1}{2} - \frac{1}{2}$		903
	740	1527.487	110 410(175 0(0)	2.16(5)) 4 2.16(5)) 4	10 10	97		903
	740	1327.083	110.4106 - 175.8691	30'(a'D)4\$ - 30'(a'D)4p	-DD	$\bar{2} - \bar{2}$		903
	740	1527.795	155.3087 - 220.7626	3d ⁶ (a ¹ I)4s - 3d ⁶ (a ¹ I)4p	² I – ² K°	<u>1</u> 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		903
	160	1527.933						903
	10	1528.138	159,4985 - 224,9369	$3d^{6}(a^{3}D)4s - 3d^{6}(a^{3}D)4n$	$^{2}D - ^{2}P^{\circ}$	3-3	0	903
	40	1528.454	141.2203 - 206.6457	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}H)4n$	⁴ F - ⁴ G°	<u>9</u> <u>1</u>	×	903
	20	1529.092	145 1921 - 210 5906	$3d^{6}(a^{3}P)4s - 3d^{6}(a^{3}P)4n$	$^{2}P - ^{4}D^{\circ}$	3_5		903
	0	1529.691				2 2		903
	660	1529.943	144.8151 - 210.1770	3d6(a3G)4s - 3d6(a3H)4p	${}^{4}G - {}^{2}I^{\circ}$	$\frac{11}{2} - \frac{13}{2}$		903
	10	1530.250						903
	10	1530.981	159.8184 - 225.1369	3d6(a3D)4s - 3d6(a3D)4p	$^{2}D - ^{4}D^{\circ}$	$\frac{5}{2} - \frac{7}{2}$	Q	903
	520	1531.734	145.7022 - 210.9875	$3d^{6}(a^{3}G)4s - 3d^{6}(a^{3}H)4p$	${}^{4}G - {}^{2}I^{\circ}$	3 - 11		903
	40	1532.086	141.5772 - 206.8470	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}H)4p$	⁴ F − ⁴ G°	1 3 - 5		903
	760	1534.710	110.4106 - 175.5695	3d6(a5D)4s - 3d6(a5D)4p	6D − 5D°	$\frac{1}{2} - \frac{2}{2}$		903
	460	1534.926	121.8077 - 186.9572	3d°(a ⁵ D)4s - 3d°(a ⁵ D)4p	⁴ D - ⁴ D°	$\frac{5}{2} - \frac{3}{2}$		903
	320	1535.612	141.2203 - 206.3409	3d6(a3F)4s - 3d6(a3H)4p	⁴ F – ⁴ G°	$\frac{9}{2} - \frac{9}{2}$		903
	300	1535.733			1			903
	310	1536.847	141.5772 - 206.6457	3d6(a3F)4s - 3d6(a3H)4p	⁴ F - ⁴ G°	$\frac{7}{2} - \frac{7}{2}$		903
	730	1537.246	111.1958 - 176.2471	3d ⁶ (a ⁵ D)4s - 3d ⁶ (a ⁵ D)4p	°D – °D°	$\frac{1}{2} - \frac{5}{2}$		903
	20	1537.875	145.9625 - 210.9875	3d6(a3H)4s - 3d6(a3H)4p	$^{2}\mathbf{H} - ^{2}\mathbf{I}^{\circ}$	$\frac{11}{2} - \frac{11}{2}$		903
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NI IV - Continued

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	190	1538.123	141.8320 - 206.8470	3d ⁶ (a ³ F)4s - 3d ⁶ (a ³ H)4p	⁴ F - ⁴ G°	$\frac{5}{2} - \frac{5}{2}$		903
	690	1538 933	120.9095 - 185.8900	$3d^{(a^{S}D)4s} - 3d^{(a^{S}D)4p}$	⁴ D - ⁴ D°	2 - 2		903
	20	1539 726	141.5772 - 206.5232	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}P)4p$	⁴ F − ⁴ P°	2 - 5	0	903
	20	1541 435	1461538 - 2110276	$3d^{6}(a^{3}G)4s - 3d^{6}(a^{3}P)4p$	⁴ G - ⁴ D°	5-3		903
	260	1542.263	122 3861 - 187 2257	$3d^{h}(a^{5}D)4s = 3d^{h}(a^{5}D)4n$	$^{4}D - ^{4}D^{\circ}$	3-1		903
	410	1542.205	122.3001 - 107.2237	$3d^{6}(a^{3}F)4s = 3d^{6}(a^{3}H)4n$	${}^{4}F - {}^{4}G^{\circ}$	$\frac{2}{3} - \frac{5}{3}$		903
	410	1542.002	142.0233 - 200.8470	50 (a r)45 - 50 (a r)74p	I'' U	2 - 2		705
	410	1542.886	141.8320 - 206.6457	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}H)4p$	⁴ F - ⁴ G°	$\frac{5}{2} - \frac{7}{2}$		903
	750	1543.412	111.7633 - 176.5544	3d°(a'D)4s - 3d°(a'D)4p	$^{\circ}\mathbf{D} - ^{\circ}\mathbf{D}^{\circ}$	2 - 2		903
	560	1543.562	141.2203 - 206.0053	3d°(a'F)4s - 3d°(a'H)4p	*F - *G*	$\frac{1}{2} - \frac{1}{2}$		903
	1 40	1544.082	141.5772 - 206.3409	3d°(a'F)4s - 3d°(a'H)4p	*F - *G*	$\frac{1}{2} - \frac{1}{2}$		903
	610	1545.402	121.8077 - 186.5161	3d°(a'D)4s - 3d°(a'D)4p	*D - *D*	$\frac{1}{2} - \frac{2}{2}$		903
	740	1546.231	111.1958 - 175.8691	3d°(a°D)4s - 3d°(a°D)4p	°D - °D°	$\frac{1}{2} - \frac{1}{2}$		903
	0	1546.695						903
	20	1546.889	147.6359 - 212.2818	3d°(a ³ F)4s - 3d°(a ³ F)4p	² F – ⁴ G°	$\frac{7}{2} - \frac{7}{2}$		903
	40	1547.121						903
	680	1548 043	112,1519 - 176,7490	3d°(a ⁵ D)4s - 3d°(a ⁵ D)4p	°D - °D°	3 - 1		903
	410	1548 680	122 3861 - 186 9572	$3d^{(a^{5}D)4s} - 3d^{(a^{5}D)4p}$	⁴ D - ⁴ D°	3-3		903
	20	1548.990	122.3001 100.3072					903
								007
	0	1549.275	1 17 (250 212 1500	216(35)4-246(-35)4-	215 400	2 9		903
i	100	1550.030	147.6359 - 212.1509	$3d^{(a+F)}4s - 3d^{(a+F)}4p$		2-2		903
	260	1550.191	122.7174 - 187.2257	3d°(a ⁻ D)4s - 3d°(a ⁻ D)4p	- D - D	2-2		903
	630	1550.779	111.7633 - 176.2471	3d°(a ³ D)4s - 3d°(a ³ D)4p	$^{\circ}D - ^{\circ}D^{\circ}$	5-5		903
	10	1551.419	155.3087 - 219.7650	3d°(a'1)4s - 3d°(a'G)4p	-1 H	2 - 2	}	903
	0	1552.002						903
	0	1552.065						903
	70	1552.306	145.7022 - 210.1218	3d6(a3G)4s - 3d6(a3F)4p	⁴ G - ⁴ D°	$\frac{9}{2} - \frac{7}{2}$		903
	10	1552.749	112.1519 - 176.5544	3d ^b (a ⁵ D)4s - 3d ^b (a ⁵ D)4p	"D – "D"	$\frac{3}{2} - \frac{3}{2}$		903
	620	1553.427	111.1958 - 175.5695	3d ^b (a ⁵ D)4s - 3d ^b (a ⁵ D)4p	°D – °D°	$\frac{7}{2} - \frac{9}{2}$		903
	520	1553.495					}	903
	20	1553.958						903
	470	1554 790	144 8151 200 1210	$3d^{6}(a^{3}G)4e = 3d^{6}(a^{3}H)4n$	$\frac{1}{2}$ G = $\frac{2}{2}$ G°	π_å		903
	4/0	1554.789	144.0151 - 207.1517	3d(a O) + s = 3d(a H) + p $3d^{6}(a^{3}D) A = 3d^{6}(a^{3}D) A = 3d$	² D - ⁴ D°	3 1	{	903
	10	1555.534	159.4965 - 225.7654	3d(aD)+s = 3d(aD)+p $3d^{0}(a^{3}D)/a = 3d^{0}(a^{3}G)/4p$	$^{2}D^{-2}E^{\circ}$	2 - 2 2 Z		903
	30	1556.277	139.8184 - 224.0733	3d(aD)4s - 3d(aC)4p	1 - U	1 3		903
	180	1556.675	122./1/4 - 186.95/2	3d(a D)48 - 3d(a D)4p	21 210	ц ц		903
	690	1557.276	145.9625 - 210.1770	$3d^{1}(a^{1}H)4s - 3d^{1}(a^{1}H)4p$		$\frac{1}{2} - \frac{1}{2}$		903
	610	1558.244	112.3793 - 176.5544	3d"(a D)4s - 3d"(a D)4p	D- D	2 - 2		903
	260	1559.340	122.3861 - 186.5161	3d°(a°D)4s - 3d°(a°D)4p	⁴D – ⁴D°	$\frac{3}{2} - \frac{5}{2}$		905
	660	1559.924	111.7633 - 175.8691	3d ⁶ (a ⁵ D)4s - 3d ⁶ (a ⁵ D)4p	⁶ D – ⁶ D °	$\frac{2}{2} - \frac{1}{2}$		903
	670	1560.177	112.1519 - 176.2471	$3d^{h}(a^{s}D)4s - 3d^{h}(a^{s}D)4p$	°D - °D°	$\frac{2}{2} - \frac{2}{2}$		903
	120	1560.501	121.8077 - 185.8900	3d°(a ^s D)4s - 3d°(a ^s D)4p	⁴ D - ⁴ D°	$\frac{2}{2} - \frac{7}{2}$	1	903
	30	1561.158	122.3861 - 186.4414	3d ^h (a ^s D)4s - 3d ^h (a ^s D)4p	⁴ D − ⁶ P°	$\frac{3}{2} - \frac{3}{2}$		903
	20	1564.277	146.1943 - 210.1218	3d°(a ³ H)4s - 3d°(a ³ F)4p	$^{2}H - ^{4}D^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		903
	0	1564 377	148 3582 - 212 2818	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}F)4p$	² F - ⁴G°	$\frac{5}{2} - \frac{7}{2}$		903
	70	1564 522	148.3582 - 212.2759	$3d^{\circ}(a^{3}F)4s - 3d^{\circ}(a^{3}F)4p$	${}^{2}F - {}^{2}F^{\circ}$	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		903
	20	1566 234	1005002 2120200					903
	460	1566.998	144.8151 - 208.6313	$3d^{6}(a^{3}G)4s - 3d^{6}(a^{3}H)4p$	⁴G - ⁴ H °	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		903
	0	1569 179	159 4985 - 223 2254	$3d^{\circ}(a^{3}D)4s - 3d^{\circ}(a^{3}D)4p$	${}^{2}D - {}^{4}P^{\circ}$	3-4	0	903
	0	1569.272	122.7174 - 186.4414	3d°(a ⁵ D)4s - 3d°(a ⁵ D)4p	⁴ D − ⁶ P °	1 - 2		903
					10 400	9 7		007
	0	1569.403	151.5747 - 215.2929	3d"(a'G)4s - 3d"(a'G)4p	-G - 'G'	2 - 2	Q	903
	260	1569.913	121.8077 - 185.5053	3d"(a'D)4s - 3d°(a'D)4p	D - "P"	2-3		903
	30	1570.108	145.7022 - 209.3914	3d°(a'G)4s - 3d°(a'H)4p	"G - 'G"	2-2		903
	10	1571.655						903
	0	1572.132	155.2537 - 218.8606	3d°(a'I)4s - 3d°(a'H)4p	$^{2}I - ^{2}H^{\circ}$	2 - 2	Q	903
	0	1572.260	156.2940 - 219.8960	3d°(a'G)4s - 3d°(a'G)4p	*G - *F*	2 - 2		903
					1	1	1	

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NI IV - Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	30	1575.662						903
	0	1576.539	145.7022 - 209.1319	3d*(a ³ G)4s - 3d*(a ³ H)4p	${}^{4}G - {}^{2}G^{\circ}$	$\frac{9}{2} - \frac{9}{2}$	Q	903
	20	1579.040	146.0615 - 209.3914	3d ⁶ (a ³ G)4s - 3d ⁶ (a ³ H)4p	⁴ G − ² G°	$\frac{7}{2} - \frac{7}{2}$	Q	903
	0	1579.220						903
	0	1579.584	147.6359 - 210.9436	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}F)4p$	${}^{2}F - {}^{4}D^{\circ}$	$\frac{7}{2} - \frac{5}{2}$	Q	903
	0	1580.695						903
	50	1601 242	146 1529 200 2014	2-16/-3/224- 2-16/-31124-	40.200	5 7		002
	270	1581.343	140.1538 - 209.3914	$3d^{2}(a^{2}G)4s = 3d^{2}(a^{2}H)4p$	40 40	$\frac{1}{2} - \frac{1}{2}$		903
	270	1581.483	145.7022 - 208.9336	3d°(a°G)4s – 3d°(a°F)4p	- 'F'	$\bar{2} - \bar{2}$		903
	50	1582.063			2	9 7		903
	440	1582.356	146.1943 - 209.3914	$3d^{(a'H)}4s - 3d^{(a'H)}4p$	² H - ² G ²	2 - 2		903
	410	1582.531	120.9095 - 184.0991	3d°(a'D)4s – 3d°(a'D)4p	$^{\circ}D - ^{\circ}P^{\circ}$	2-2		903
	420	1583.030	145.9625 - 209.1319	3d°(a'H)4s – 3d°(a'H)4p	'H – 'G"	$\frac{11}{2} - \frac{2}{2}$		903
	20	1584.299	122.3861 - 185.5053	3d6(a5D)4s - 3d6(a5D)4p	⁴ D – ⁶ P°	$\frac{3}{2} - \frac{5}{2}$		903
	70	1585.522	146.0615 - 209.1319	3d ⁶ (a ³ G)4s - 3d ⁶ (a ³ H)4p	⁴ G - ² G°	$\frac{1}{2} - \frac{9}{2}$		903
	120	1588.025	145.9625 - 208.9336	$3d^{\circ}(a^{3}H)4s - 3d^{\circ}(a^{3}F)4p$	² H – ⁴ F°	4-3		903
	20	1589.017				···		903
	320	1589.984	145.7022 - 208.5953	3d ⁶ (a ³ G)4s - 3d ⁶ (a ³ H)4p	⁴ G - ⁴ H°	3-4		903
	10	1590.126	148.3582 - 211.2468	$3d^{6}(a^{3}F)4s - 3d^{6}(a^{3}F)4p$	² F - ⁴ D°	$\frac{5}{2} - \frac{3}{2}$	Q	903
	0	1590.564			1	1 3 5		903
	490	1591.933	145.1921 - 208.0091	$3d^{\circ}(a^{\circ}P)4s - 3d^{\circ}(a^{\circ}P)4p$	² P - ² D°	2 - 5		903
	110	1593.836	151.5747 - 214.3168	3d°(a'G)4s - 3d°(a'G)4p	² G – *G*	$\frac{3}{2} - \frac{11}{2}$		903
	140	1597.898						903
	20	1598.274	152.3437 - 214.9105	3d°(a3G)4s - 3d°(a3G)4p	² G – ⁴ G°	$\frac{1}{2} - \frac{9}{2}$		903
	10	1605.345	121.8077 - 184.0991	3d°(a'D)4s - 3d°(a'D)4p	⁴D - ⁰P°	$\frac{2}{2} - \frac{1}{2}$		903
	280	1605.549	179.6550 - 241.9390	3d°(b ³ F)4s - 3d°(b ³ F)4p	⁴ F – ⁴ D°	3 - 7		903
	20	1606.415	185.9670 - 248.2180	3d ⁶ (b ³ F)4s - 3d ⁶ (b ³ F)4p	² F – ⁴ G °	2 - 3	0	903
	300	1606.575	152.3437 - 214.5874	$3d^{6}(a^{3}G)4s - 3d^{6}(a^{3}H)4p$	${}^{2}G - {}^{2}H^{\circ}$	3-3		903
	10	1607.505						903
	0	1607.926	153,3494 - 215,5413	$3d^{6}(a^{3}D)4s - 3d^{6}(a^{3}G)4p$	4D - 4F°	1-3		903
	0	1608.159				2 2		903
		1.000 605			20.20	9 9		000
	10	1608.625	151.5/47 - 213.7397	$3d^{\circ}(a^{\circ}G)4s - 3d^{\circ}(a^{\circ}F)4p$	-G - G	$\frac{1}{2} - \frac{1}{2}$		903
	20	1609.352	146.1943 - 208.3307	$3d^{\circ}(a^{3}H)4s - 3d^{\circ}(a^{3}F)4p$	2H - F	$\frac{1}{2} - \frac{1}{2}$	Q	903
	100	1610.711	145.9625 - 208.0468	3d°(a'H)4s - 3d°(a'H)4p	$^{2}H - ^{4}I^{\circ}$	$\frac{11}{2} - \frac{2}{2}$		903
	20	1611.570	144.8151 - 206.8655	3d°(a'G)4s - 3d°(a'H)4p	*G – *H*	$\frac{11}{2} - \frac{2}{2}$		903
	600	1612.071	151.5747 - 213.6069	3d°(a'G)4s - 3d°(a'G)4p	² G – ² H°	$\frac{2}{2} - \frac{11}{2}$		903
	230	1612.230	179.7920 – 241.8179	3d°(b°F)4s – 3d°(b°F)4p	*F - *D*	$\frac{1}{2} - \frac{1}{2}$		903
	10	1613.273	146.0615 - 208.0468	3d°(a ³ G)4s - 3d°(a ³ H)4p	⁴G - ⁴I°	$\frac{7}{2} - \frac{9}{2}$		903
	0	1613.476						903
	10	1614.119	153.3388 - 215.2929	3d°(a ³ D)4s - 3d°(a ³ G)4p	⁴ D - ⁴ G [•]	$\frac{5}{2} - \frac{7}{2}$		903
	10	1616.747	146.1943 - 208.0468	$3d^{6}(a^{3}H)4s - 3d^{6}(a^{3}H)4p$	${}^{2}H - {}^{4}I^{\circ}$	2 - 2		903
	30	1617.113				6 2		903
	20	1617.225	151.5747 - 213.4086	3d6(a3G)4s - 3d6(a3G)4p	² G − ⁴ F °	$\frac{9}{2} - \frac{9}{2}$	Q	903
	20	1617 (70						
	30	1017.078						903
	20	1617.924						903
	20	1619.297	147.6359 - 209.3914	3d°(a°F)4s - 3d°(a°H)4p	'F - 'G'	$\frac{1}{2} - \frac{1}{2}$		903
	10	1622.765						903
	10	1623.801						903
	150	1624.524	151.5747 - 213.1311	3d°(a'G)4s - 3d°(a'F)4p	² G – ² F°	$\frac{2}{2} - \frac{1}{2}$		903
	30	1628.757	152.3437 - 213.7397	3d°(a3G)4s - 3d°(a3F)4p	² G – ² G°	7 - 9		903
	120	1630.489	145.1921 - 206.5232	3d ⁶ (a ³ P)4s - 3d ⁶ (a ³ P)4p	$^{2}\mathbf{P} - {}^{4}\mathbf{P}^{\circ}$	3-5		903
	100	1631.376	120.9095 - 182.2068	$3d^{6}(a^{5}D)4s - 3d^{6}(a^{5}D)4n$	4D - 6F	1 1 1		299
	0	1633.555	120.9095 - 182.1256	$3d^{6}(a^{5}D)4s - 3d^{6}(a^{5}D)4n$	4D - 6F	1 1		903
	50	1634.246	144.8151 - 206.0053	$3d^6(a^3G)4s = 3d^6(a^3H)4n$	4G - 4G*	1 <u>1</u> <u>1</u>		903
	130	1635.703	120.9095 - 182.0449	$3d^{6}(a^{5}D)4s = 3d^{6}(a^{5}D)4n$	4D-6F	7 9		903
		10001100				2 2 2		,00

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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	References
	20	1637.511	152.3437 - 213.4121	3d6(a3G)4s - 3d6(a3F)4p	² G - ⁴ G°	$\frac{7}{2} - \frac{5}{2}$		903
	10	1637.717						903
	0	1638.482						903
	20	1639.820	146.1538 - 207.1360	3d*(a ³ G)4s - 3d*(a ³ H)4p	⁴G - ⁴H°	$\frac{5}{2} - \frac{7}{2}$		903
	210	1640.913	146.1943 - 207.1360	3d6(a3H)4s - 3d6(a3H)4p	${}^{2}H - {}^{4}H^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		903
	10	1641.961	145.9625 - 206.8655	$3d^{6}(a^{3}H)4s - 3d^{6}(a^{3}H)4p$	$^{2}\mathbf{H} - {}^{4}\mathbf{H}^{\bullet}$	$\frac{11}{2} - \frac{9}{2}$		903
	10	1642.953	171.4060 - 232.2727	3d°(a1F)4s - 3d°(a1D)4p	${}^{2}\mathbf{F} - {}^{2}\mathbf{F}^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		903
	20	1644.629	146.0615 - 206.8655	$3d^{6}(a^{3}G)4s - 3d^{6}(a^{3}H)4p$	⁴G - ⁴H°	$\frac{7}{2} - \frac{9}{2}$		903
	360	1644.951	145.9625 - 206.7545	$3d^{6}(a^{3}H)4s - 3d^{6}(a^{3}H)4p$	${}^{2}H - {}^{4}I^{\circ}$	$\frac{11}{2} - \frac{13}{2}$		903
	20	1647.251	151.5747 - 212.2818	$3d^{6}(a^{3}G)4s - 3d^{6}(a^{3}F)4p$	² G - ⁴ G°	3 - 7		903
	10	1649.112	145.7022 - 206.3409	$3d^{6}(a^{3}G)4s - 3d^{6}(a^{3}H)4p$	⁴ G - ⁴ G°	$\frac{1}{2} - \frac{1}{2}$		903
	0	1651.012						903
	140	1651.629	146.1943 - 206.7407	3d6(a3H)4s - 3d6(a3H)4p	² H – ⁴ I°	$\frac{9}{2} - \frac{11}{2}$		903
	10	1651.740						903
	30	1652.390						903
	0	1654.843						903
	0	1655.432						903
	0	1655.643	121.8077 - 182.2068	3d6(a5D)4s - 3d6(a5D)4p	⁴ D - ⁶ F°	$\frac{5}{2} - \frac{5}{2}$	Q	903
	60	1656.392						903
	80	1657.874	121.8077 - 182.1256	3d ⁶ (a ⁵ D)4s - 3d ⁶ (a ⁵ D)4p	⁴ D − ⁶ F°	$\frac{5}{2} - \frac{7}{2}$		903
	0	1658.292	145.7022 - 206.0053	$3d^{6}(a^{3}G)4s - 3d^{6}(a^{3}H)4p$	⁴ G – ⁴ G°	3 - 11		903
	0	1663.866						903
	40	1664.536	159.8184 - 219.8960	$3d^{6}(a^{3}D)4s - 3d^{6}(a^{3}G)4p$	$^{2}D - ^{2}F^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		903
	170	1665.040						903
	10	1668.549	152.3437 - 212.2759	3d6(a3G)4s - 3d6(a3F)4p	${}^{2}G - {}^{2}F^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		903
	10	1669.669						903
	100	1671.282						903
	20	1671.659	122.3861 - 182.2068	3d6(a5D)4s - 3d6(a5D)4p	⁴ D - ⁶ F°	3-5		903
	0	1672 632		50 (a 2) is to (a 2) ip		2 2		903
	Ő	1672.946						903
	0	1674.105						903
	0	1674 823						903
	0	1675.379						903
	10	1679 478	122 7174 - 182 2599	$3d^{6}(a^{5}D)4s = 3d^{6}(a^{5}D)4n$	⁴ D - ⁶ F°	1 3		903
	10	1680 678	147.6359 - 207.1360	$3d^6(a^3F)4s = 3d^6(a^3H)4n$	² F - ⁴ H°	1_1		903
	0	1684.338	141.0357 201.1500	54 (41) 15 54 (411) 1p				903
	10	1693.087	155.2537 - 214.3168	3d6(a1)4s - 3d6(a3G)4p	$^{2}I - {}^{4}G^{\circ}$	₩_ Ψ		903
	130	1713.687	155.2537 - 213.6069	$3d^{6}(a^{1}I)4s - 3d^{6}(a^{3}G)4p$	$^{2}I - ^{2}H^{\circ}$	ļ <u>Ļ</u> , <u>Ļ</u>] [903
	0	1727.113				l í í		903
	Ō	1737.206						903
	110	1737.420	151.5747 - 209.1319	3d ⁶ (a ³ G)4s - 3d ⁶ (a ³ H)4p	${}^{2}G - {}^{2}G^{\circ}$	$\frac{9}{5} - \frac{9}{5}$		903
	10	1743.427	151.5747 - 208.9336	$3d^{6}(a^{3}G)4s - 3d^{6}(a^{3}F)4p$	$^{2}G - {}^{4}F^{\circ}$	$\frac{\tilde{9}}{2} - \frac{\tilde{9}}{2}$		903
	0	1745.764						903
	0	1746.603						903
	10	1747.824						903
	40	1751.706						903
	10	1759.389						903
	20	1767.122	152.3437 - 208.9336	3d°(a3G)4s - 3d°(a3F)4p	² G - ⁴ F°	$\frac{7}{2} - \frac{9}{2}$		903
	20	1770.805	151.5747 - 208.0468	3d6(a3G)4s - 3d6(a3H)4p	² G - ⁴ I°	$\frac{9}{2} - \frac{9}{2}$		903
	0	1783.949		· · · · · · · · · · · · · · · ·				903
	20	1805.012						903
	10	1808.488						903
	10	1818.360						903
	10	1829 304						903

NI IV --- Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	20	1829.498	120.9095 - 175.5695	3d6(a5D)4s - 3d6(a5D)4p	⁴ D - ⁶ D°	$\frac{7}{2} - \frac{9}{2}$		903

NICKEL V (Ni ⁴⁺), Z = 28 Ground State $1s^22s^22p^63s^23p^63d^6(^5D_4)$ (24 electrons) Ionization Potential 613 500 cm⁻¹; 76.1 eV

Multiplet Re	l. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	410	199.154	0.0 - 502.124	3d ⁶ - 3d ⁵ (a ⁶ S)5f	ga ⁵ D - ⁵ F°	4 - 5		927
	370	199.504	0.8897 - 502.133	3d ⁶ – 3d ⁵ (a ⁶ S)5f	ga ⁵ D – ⁵ F°	3 - 4		927
	230	199.742	1.4899 - 502.137	3d ⁶ - 3d ⁵ (a ⁶ S)5f	ga ⁵ D – ⁵ F°	2 - 3		927
	120	199.890	1.8715 - 502.148	3d6 - 3d5(a6S)5f	ga ⁵ D – ⁵ F°	1 - 2		927
	250	199.966	2.0576 - 502.143	3d6 - 3d5(a6S)5f	ga ⁵ D – ⁵ F°	0-1		927
:	820	227.565	0.0 - 439.434	$3d^{6} - 3d^{5}(a^{6}S)4f$	ga ⁵ D - ⁵ F°	4 – 5		927
	780	228.031	0.8897 - 439.427	3d6 - 3d5(a6S)4f	ga ⁵ D - ⁵ F°	3 - 4		927
	660	228.346	1.4899 - 439.423	3d ⁶ - 3d ⁵ (a ⁶ S)4f	ga ⁵ D – ⁵ F°	2 - 3		927
	580	228.547	1.8715 - 439.419	3d ⁶ - 3d ⁵ (a ⁶ S)4f	ga ⁵ D - ⁵ F°	1 - 2		927
	300	228.644	2.0576 - 439.420	$3d^{6} - 3d^{5}(a^{6}S)4f$	$ga^{5}D - {}^{5}F^{\circ}$	0 - 1		927
	420	236.110	0.0 - 423.533	$3d^{6} - 3d^{5}(a^{6}S)5p$	ga ⁵ D - ⁵ P°	4 - 3		927
	290	236.467	0.8897 - 423.782	$3d^{6} - 3d^{5}(a^{6}S)5p$	ga ⁵ D - ⁵ P°	3 - 2		927
	200	236.606	0.8897 - 423.533	3d ⁶ - 3d ⁵ (a ⁶ S)5p	ga ⁵ D - ⁵ P°	3 - 3		927
	230	236.716	1.4899 - 423.935	$3d^{6} - 3d^{5}(a^{6}S)5p$	ga ⁵ D - ⁵ P°	2 - 1		927
	120	236.802	1.4899 - 423.782	$3d^{6} - 3d^{5}(a^{6}S)5p$	$ga^{5}D - {}^{5}P^{\circ}$	2 - 2		927
	100	236.932	1.8715 - 423.935	$3d^{6} - 3d^{5}(a^{6}S)5p$	$ga^{5}D - {}^{5}P^{\circ}$	1 - 1		927
	290	304.018	27.1112 - 356.0363	$3d^6 - 3d^5(h^2G)4p$	$a^{3}H - {}^{3}G^{\circ}$	6-5		922
	210	304.702	27.5782 - 355.7652	3d ⁶ – 3d ⁵ (b ² G)4p	$a^{3}H - {}^{3}G^{\circ}$	5 - 4		922
	20	304.854	41.6269 - 369.6491	$3d^6 - 3d^5(a^2P)4p$	$a^{3}D - {}^{3}P^{\circ}$	2 - 2		922
	130	304.991	27.1112 - 354.9896	$3d^{6} - 3d^{5}(b^{2}G)4p$	$a^{3}H - {}^{3}H^{\circ}$	6-6		922
1	100	305.129	41.9202 - 369.6491	$3d^6 - 3d^5(a^2P)4n$	$a^{3}D - {}^{3}P^{\circ}$	3-2		922
ļ	80	305.305	27.8588 - 355.3980	$3d^6 - 3d^5(b^2G)4p$	$a^{3}H = {}^{3}G^{\circ}$	4-3		922
	30	305 891	29 1237 - 356 0363	$3d^6 = 3d^5(b^2G)4p$	$a^3 F = {}^3 G^9$	4 - 5		922
	20	306.054	41.7011 - 368.4405	$3d^6 - 3d^5(a^2P)4p$	$a^3D - {}^3P^\circ$	1 - 0		922
	70	306.338	27.1112 - 353.5487	3d ⁶ - 3d ⁵ (h ² G)4n	$a^{3}H - {}^{3}H^{\circ}$	6-5		922
	20	306.488	29.1237 - 355.3980	$3d^{6} - 3d^{5}(b^{2}G)4p$	$a^{3}F - {}^{3}G^{\circ}$	4 - 3		922
	20	306.565	29.5708 - 355.7652	$3d^6 - 3d^5(b^2G)4p$	$a^{3}F - {}^{3}G^{\circ}$	3-4		922
	120	306.669	27.8588 - 353.9441	$3d^{6} - 3d^{5}(b^{2}G)4p$	$a^{3}H - {}^{3}F^{\circ}$	4 - 3		922
	160	306.776	27.5782 - 353.5487	$3d^{6} - 3d^{5}(b^{2}G)4p$	$a^{3}H - {}^{3}H^{\circ}$	5 - 5		922
	180	307.225	29.8992 - 355.3980	$3d^{6} - 3d^{5}(b^{2}G)4p$	$a^{3}F - {}^{3}G^{\circ}$	2 - 3		922
	130	307.492	27.8588 - 353.0716	3d ⁶ – 3d ⁵ (b ² G)4p	$a^{3}H - {}^{3}H^{\circ}$	4 - 4		922
	20	308.387						922
	80	308.994						922
	30	309.351	69.1561 - 392.4135	$3d^{6} - 3d^{5}(c^{2}D)4p$	$b^{3}P - {}^{3}P^{\circ}$	2 - 2		927
	20	309.769	0.0 - 322.8208	$3d^6 - 3d^5(a^4F)4p$	$ga^{5}D - F^{*}$	4 - 4		922
	210	309.811	33.2565 - 356.0363	3d ⁶ - 3d ⁵ (b ² G)4p	a'G - 'G°	5 - 5		922
	130	310.071	33.2565 - 355.7652	$3d^6 - 3d^5(b^2G)4p$	$a^{3}G - {}^{3}G^{\circ}$	5 - 4		922
	70	310.538	67.5479 - 389.5718	$3d^6 - 3d^5(c^2D)4p$	$b^{3}P - {}^{3}D^{\circ}$	1 - 2		922
	230	310.791	68.7187 - 390.4782	$3d^6 - 3d^5(c^2D)4p$	$h^3 F - {}^3 D^\circ$	4 - 3		922
	160	310.846	34.0617 - 355.7652	$3d^6 - 3d^5(h^2G)4n$	$a^3G - {}^3G^{\circ}$	4-4		922
	10	311.024	69.1561 - 390.6751	$3d^{6} - 3d^{5}(c^{2}D)4n$	$h^{3}P - D^{\circ}$	2-2		922
	240	311.201	34.0617 - 355.3980	$3d^{\circ} - 3d^{\circ}(h^{2}G)4n$	$a^3G - {}^3G^{\circ}$	4 - 3		922
1	- • •			54 54 (5 3)+p				,

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NI V -- Continued

ltiplet Rel.	. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm $^{-1}$)	Configurations	Terms	J - J	Notes	Reference
1	70	311.547	34.4164 - 355.3980	3d ⁶ – 3d ⁵ (b ² G)4p	$a^3G - {}^3G^\circ$	3 - 3		922
2	.60	311.788	34.4164 - 355.1500	3d ⁶ - 3d ⁵ (b ² G)4p	a'G - 'F°	3 - 2		922
2	50	311.800	68.8547 - 389.5718	3d ⁶ - 3d ⁵ (c ² D)4p	b ³ F – ³ D°	3 - 2		922
1	00	312.217	33.2565 - 353.5487	3d ⁶ – 3d ⁵ (b ² G)4p	a ³ G - ³ H°	5 - 5		922
2	20	312.388	68.6321 - 388.7461	$3d^6 - 3d^5(c^2D)4p$	$b^{3}F - {}^{3}D^{\circ}$	2 - 1		927
2.	40	312.412	33.2565 - 353.3471	3d ⁶ – 3d ⁵ (b ² G)4p	$a^{3}G - {}^{3}F^{\circ}$	5 - 4		922
	(0)	112 620	60 7107 200 6000	246 245(-20)4-	13E 3E*			077
1	00	312.520	08./18/ - 388.0989	$3d = 3d(c^2D)4p$		4-4	İ	927
	20	312.015	34.0617 - 353.9441	30° - 30° (0° (0) 4p		4-5		922
L.	30	312.680	33.2565 - 353.0716	3d° - 3d°(b°G)4p	a'G - H	5-4	Ē	922
	90	312.839	0.0 - 319.6527	3d° – 3d°(a°F)4p	ga D – G	4 - 5		922
1	70	312.962	34.4164 - 353.9441	3d° – 3d°(b²G)4p	a'G - 'F°	3 - 3		922
10	00	313.000	34.0617 - 353.5487	3d ⁶ – 3d ⁵ (b ² G)4p	a'G – 'H°	4 – 5		922
	80	313.059	67.5479 - 386.9688	3d ⁶ - 3d ⁵ (c ² D)4p	$b^{3}P - {}^{3}F^{\circ}$	1 - 2		922
1	20	313,993	68.8547 - 387.3334	$3d^6 - 3d^5(c^2D)4p$	$b^3F - {}^3F^\circ$	3-3		927
1	10	314 132	68 6321 - 386 9688	$3d^6 - 3d^5(c^2D)4p$	$b^3F - {}^3F^\circ$	2 - 2		927
1	30	315.082	0.0 - 317 3768	$3d^6 - 3d^5(9^2H)4n$	$G^{3}D = G^{2}$	4 - 3		922
	50	215 225	41 2522 358 4756	$3d^6 = 3d^5(h^2G)M_{\rm P}$		6 5		022
2	40	315.233	41.2322 - 338.4730 57 9241 - 374 8037	$3d^6 = 3d^5(a^2P)4p$	$a^{1}F - {}^{3}D^{\circ}$	3-2		927
		515.575	57.5241 - 574.0057	54 54 (a 1) (p				21
5	60	315.712	0.0 - 316.7440	3d ⁶ - 3d ⁵ (a ⁴ F)4p	ga ⁵ D - ⁵ D°	4 – 4		922
3	80	315.829	0.8897 - 317.5175	3d ⁶ - 3d ⁵ (a ⁴ F)4p	ga ⁵ D – ⁵ D°	3 - 2		922
2	10	315.905	42.2081 - 358.7600	$3d^6 - 3d^5(b^2G)4p$	a'G - 'G°	4 - 4		922
3	00	315 969	0.8897 - 317.3768	$3d^6 - 3d^5(a^2H)4p$	$ga^{5}D - {}^{3}G^{\circ}$	3 - 3		922
4	20	316 113	0.8897 - 317.2320	$3d^{6} - 3d^{5}(a^{4}E)4p$	$a^{5}D - {}^{5}D^{6}$	3-3		922
2	10	316.189	42.2081 - 358.4756	$3d^{6} - 3d^{5}(b^{2}G)4p$	$a^{\dagger}G - {}^{\dagger}H^{\circ}$	4 - 5		922
3	10	316.428	1.4899 - 317.5175	3d ⁶ - 3d ⁵ (a ⁴ F)4p	ga ^s D – ^s D°	2 – 2	1	922
3	30	316.468	1.4899 - 317.4779	3d ⁶ – 3d ⁵ (a ⁴ F)4p	ga`D - `D°	2 – 1	1	922
	60	316.569	1.4899 - 317.3768	3d ⁶ - 3d ⁵ (a ² H)4p	ga ⁵ D – ³ G°	2 – 3		922
	60	316.668	29.1237 - 344.9112	3d ⁶ – 3d ⁵ (b ² D)4p	a'F - 'F°	4 - 4		922
	90	316.714	1.4899 - 317.2320	3d ⁶ - 3d ⁵ (a ⁴ F)4p	ga ^s D – ^s D°	2 - 3		922
1	40	316.776	29.1237 - 344.8053	3d ⁶ - 3d ⁵ (b ² D)4p	a ³ F - ³ D°	4 - 3		922
,	10	316.810	1 8715 - 317 5175	$3d^{6} = 3d^{5}(a^{4}E)4n$	ma ⁵ D − ⁵ D°	1 - 2		922
1	40	216.052	1 8715 317 4770	$3d^6 - 3d^5(a^4E)Ap$	ga D = D	1 1		022
2	40	310.855	1.8715 - 317.4779	3d - 3d (a F) + p	ga D - D	1-1		922
2	:/0	316.800	1.8/15 - 31/.4623	3d" – 3d' (a'F)4p	ga D - D	1-0		922
1	.90	317.037	2.0576 - 317.4779	3d" – 3d (a*F)4p	ga D - D	0 - 1	•	922
4	10	317.291	0.0 - 315.1682	3d" – 3d'(a*F)4p	ga D - F°	4 - 5		922
2	90	317.402	77.8995 - 392.9571	3d° – 3d°(c ² D)4p	b'G - 'F"	4 – 3		922
1	60	317.865	0.0 - 314.5992	3d ⁶ - 3d ⁵ (a ⁴ F)4p	ga ⁵ D - ⁵ F°	4 - 4		922
	20	317.901	0.0 - 314.5628	$3d^{6} - 3d^{5}(a^{4}F)4p$	$ga^{5}D - {}^{5}F^{\circ}$	4 – 3		922
	80	318.260	0.0 - 314.2088	$3d^{6} - 3d^{5}(a^{2}F)4p$	ga'D - 'F°	4 - 4		922
	40	318.528	0.8897 - 314.8347	$3d^{6} - 3d^{5}(a^{4}F)4p$	ga ^s D - ^s F°	3 - 2		922
	20	318,703	41.6269 - 355.3980	$3d^{6} - 3d^{5}(b^{2}G)4p$	a'D - 'G'	2 – 3		922
3	90	318.766	0.8897 - 314.5992	$3d^{6} - 3d^{5}(a^{4}F)4p$	ga ⁵ D - ⁵ F°	3 – 4		922
			0.0007 014.6(00	2.16 2.15(+5).4	STO ST			022
	20	318.803	0.8897 - 314.5628	30° - 30°(a F)4p	ga D - F	3 - 3	1	922
	80	318.900	29.8992 - 343.4782	3d" - 3d"(b-D)4p	a F - D	2 - 1		922
1	10	319.015	0.0 - 313.4647	3d" - 3d"(a*F)4p	ga D - G	4 - 5		922
	90	319.031	41.7011 - 355.1500	3d" - 3d'(b'G)4p	a'D - 'F'	1 - 2		922
2	200	319.163	0.8897 - 314.2088	3d° - 3d°(a ² F)4p	ga`D - `F°	3 - 4		922
	20	319.202	1.8715 - 315.1528	3d ⁶ - 3d ⁵ (a ⁴ F)4p	ga'D - 'F°	1 – 1		922
	20	319.241	2.0576 - 315.3007	$3d^{6} - 3d^{5}(a^{2}F)4p$	$ga^{5}D - {}^{3}D^{\circ}$	0 - 1		922
1 1	60	319 392	2.0576 - 315 1528	$3d^{\circ} - 3d^{\circ}(a^{4}F)4n$	$a^{5}D - F^{\circ}$	0 - 1		922
	180	310 414	1 4899 - 314 5678	$3d^{6} = 3d^{5}(a^{4}F)An$	$a^{5}D - {}^{5}F^{\circ}$	2_1		922
4	140	317.414	1.4077 - 314.3020	2d ⁶ 2d ⁵ (a ⁴ E)/a	$a^{5}D^{5}E^{\circ}$	1 2 - 3		022
3	00	319.320	1.8/13 - 314.834/	50 - 50 (a r)4p	ga D - r	1-2	Í	744
	50	320.111	0.8897 - 313.2813	30" - 30"(a"F)4p	ga D - 'G'	3-4		921

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NI V - Continued

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm 1)	Configurations	Terms	J - J	Notes	References
	110	320.208	41.2522 - 353.5487	3d ^h - 3d ⁵ (b ² G)4p	a'I – ³ H°	6 - 5		922
	20	320.351						922
	30	320.702	66.7378 - 378.5550	$3d^6 - 3d^5(a^2P)4p$	b ³ P - ³ S°	0 - 1		922
	20	320.815	1.8715 - 313.5773	$3d^6 - 3d^5(a^2D)4p$	$ga^{5}D - {}^{3}P^{\circ}$	1-0		922
	290	320 868	33 2565 - 344 9112	$3d^6 - 3d^5(b^2D)4p$	$a^{3}G - {}^{3}F^{\circ}$	5 - 4		922
	170	321 102	A1 0202 353 3471	$3d^6 - 3d^5(b^2G)4p$	$a^{3}D = {}^{3}F^{\circ}$	3-4		922
	170	321.102	41.7202 - 555.5471	50 - 50 (0 C)+p		5-4		,22
	80	321.385	41.9202 - 353.0716	3d ⁶ - 3d ⁵ (b ² G)4p	$a^{3}D - {}^{3}H^{\circ}$	3 - 4		922
	60	321.535	67.5479 - 378.5550	3d° - 3d³(a²P)4p	b' P – 'S°	1 - 1		922
	100	321.809	34.0617 - 344.8053	3d ⁶ – 3d ⁵ (b ² D)4p	a ³ G - ³ D°	4 – 3		922
	50	323.113	34.4164 - 343.9057	3d ⁶ – 3d ⁵ (b ² D)4p	a ³ G - ³ D°	3 - 2		922
	40	323.168	77.8995 - 387.3334	$3d^6 - 3d^5(c^2D)4p$	b ¹ G - ³ F°	4 – 3		927
	180	323.208	69.1561 - 378.5550	3d ⁶ - 3d ⁵ (a ² P)4p	b ³ P – ³ S °	2 - 1		922
					10.100			
	160	323.394	34.0617 - 343.2810	3d° – 3d°(b²D)4p	a'G - 'F'	4 - 3		922
	130	324.172	34.4164 - 342.8946	3d° - 3d°(b²D)4p	a'G - 'F°	3 – 2		922
	120	324.460	68.8547 - 377.0591	$3d^6 - 3d^5(a^2P)4p$	b ³ F - ¹ D°	3 – 2		922
	340	324.936	68.7187 - 376.4716	$3d^{6} - 3d^{5}(a^{2}P)4p$	$b^{3}F - {}^{3}D^{\circ}$	4 - 3		922
	20	325.082	68.8547 - 376.4716	$3d^6 - 3d^5(a^2P)4p$	b ³ F - ³ D°	3 - 3	ļ	922
	280	326.588	68.6321 - 374.8281	$3d^6 - 3d^5(a^2P)4p$	$b^{3}F - {}^{3}D^{\circ}$	2 - 1		927
	10	326.614	68.6321 - 374.8037	$3d^6 - 3d^5(a^2P)4p$	b ³ F - ³ D°	2 – 2		927
	220	326.852	68.8547 - 374.8037	$3d^{6} - 3d^{5}(a^{2}P)4p$	b ³ F - ³ D °	3 - 2		927
	20	327.510	41.6269 - 346.9595	$3d^{6} - 3d^{5}(b^{2}D)4p$	$a^{3}D - {}^{3}P^{\circ}$	2 - 1		922
	20	327,876	41.9202 - 346.9124	$3d^{6} - 3d^{5}(b^{2}D)4p$	$a^{3}D - {}^{3}P^{\circ}$	3 - 2		922
	40	328 613	41 6269 - 345 9361	$3d^{6} - 3d^{5}(b^{2}D)4p$	$a^{3}D - {}^{1}F^{\circ}$	2 - 3		927
	20	329.251	26.1530 - 329.8729	$3d^{\circ} - 3d^{\circ}(b^{2}F)4p$	$a^{3}P - {}^{3}D^{\circ}$	2 - 3		922
	180	330.043	41.9202 - 344.9112	3d ⁶ - 3d ⁵ (b ² D)4p	a ³ D - ³ F°	3 – 4		922
	210	330.158	41.9202 - 344.8053	$3d^{6} - 3d^{5}(b^{2}D)4p$	$a^{3}D - {}^{3}D^{\circ}$	3 - 3	1	922
	160	330.820	41.6269 - 343.9057	$3d^{6} - 3d^{5}(b^{2}D)4p$	$a^{3}D - {}^{3}D^{\circ}$	2 - 2		922
	150	331.017	67.5479 - 369.6491	$3d^{\circ} - 3d^{\circ}(a^{2}P)4p$	$b^{3}P - {}^{3}P^{\circ}$	1-2		922
	120	331 113	66 7378 - 368 7497	$3d^6 - 3d^5(a^2P)4p$	$h^{3}P - {}^{3}P^{\circ}$	0 - 1		922
	40	331.141	41.9202 - 343.9057	$3d^6 - 3d^5(b^2D)4p$	$a^{3}D - {}^{3}D^{\circ}$	3 - 2		922
	110	331.370	41.7011 - 343.4782	3d ⁶ - 3d ⁵ (b ² D)4p	$a^{3}D - {}^{5}D^{\circ}$	1 - 1		922
	200	331.507	41.6269 - 343.2810	3d ⁶ – 3d ⁵ (b ² D)4p	a ³ D - ³ F°	2 - 3		922
	160	331.571	29.1237 - 330.7181	3d ⁶ – 3d ⁵ (b ² F)4p	a ³ F - ³ G°	4 - 5		922
	200	332.012	41.7011 - 342.8946	3d ⁶ – 3d ⁵ (b ² D)4p	$a^{3}D - {}^{3}F^{\circ}$	1 - 2		922
	40	332.140	28.6976 - 329.7763	3d ⁶ – 3d ⁵ (b ² F)4p	$a^{3}P - {}^{3}D^{\circ}$	1 - 2		922
	230	332.293	48.6070 - 349.5460	3d ⁶ – 3d ⁵ (b ² D)4p	$a^{1}D - {}^{1}D^{\circ}$	2 - 2		922
	200	222.216	0.0 200.0181	246 245/64D)4-	n ⁵ D ³ E ^o			922
	200	332.310	67 5470 269 4405	3d - 3d (a D) + p	5 ³ D ³ D ⁹	1 0		022
	70	332.345	07.3479 - 308.4403	30 - 30 (a r)4p		1-0		922
	20	332.410	57.9241 - 358.7600	3d" – 3d"(b*G)4p	a'F - 'G'	3-4		922
	220	332.471	47.6997 - 348.4779	3d° – 3d°(b²D)4p	a'S - 'P'	0-1		922
	150	332.504	29.1237 - 329.8729	3d° - 3d³(b²F)4p	a'F - 'D'	4-3		922
	220	332.528	29.5708 - 330.2976	3d° - 3d3(b2F)4p	a'F - 'G'	3 - 4		922
	60	332.689	0.8897 - 301.4702	3d ⁶ - 3d ⁵ (a ⁴ D)4p	ga ⁵ D - ³ F°	3 - 3		922
	290	332,788	69,1561 - 369,6491	$3d^{6} - 3d^{5}(a^{2}P)4p$	$b^{3}P - {}^{3}P^{\circ}$	2 - 2		922
	330	333,109	0.0 - 300 2010	$3d^6 - 3d^5(a^4D)4n$	ga ⁵ D - ⁵ P°	4 - 3		922
	110	333 302	0 8897 - 300 0181	$3d^6 = 3d^5(a^4D)An$	$a^{5}D = {}^{3}F^{9}$	3_4		922
	160	122 260	1 4900 201 4703	2.46 2.45(-4T))4-		2 2		922
	40	333.475	48.6070 - 348.4779	3d ⁶ - 3d ⁵ (b ² D)4p	$a^{1}D - P^{\circ}$	2-3		922
	140	333.651	29.8992 - 329.6143	3d ⁶ - 3d ⁵ (b ² F)4p	$a^{3}F - {}^{3}G^{\circ}$	2 - 3		922
	180	334.116	27.5782 - 326.8763	3d° - 3d³(b²F)4p	a 'H – 'F°	5-4		922
	20	334.429	27.8588 - 326.8763	3d ⁶ - 3d ⁵ (b ² F)4p	a ³ H - ³ F°	4 - 4		922
	150	334.479	0.0 - 298.9723	3d ⁶ − 3d ⁵ (a ⁴ D)4p	ga ⁵ D - ³ D°	4 - 3		922
	420	335.382	27.8588 - 326.0299	3d° - 3d5(b2F)4p	a ³ H - ³ F°	4 - 3		922
	420	335.395	0.8897 - 299.0456	3d° - 3d ⁵ (a ⁴ D)4p	ga ⁵ D - ⁵ P°	3 - 2		922
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NI V --- Continued

ultiplet Rel. Int.	$\lambda_{\rm vac}$ (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	Reference
390	335.478	0.8897 - 298.9723	3d ⁶ - 3d ⁵ (a ⁴ D)4p	ga ⁵ D - ³ D°	3 - 3		922
240	335 529	27 1112 - 325 1484	$3d^6 - 3d^5(a^2G)4p$	$a^{3}H - {}^{3}H^{\circ}$	6-6		922
240	335 503	27 5782 - 325 5586	$3d^6 - 3d^5(b^2E)4p$	$a^{3}H - {}^{1}G^{\circ}$	5-4		922
240	335.575	27.3782 - 323.3380	$3d^6 - 3d^5(a^2G)Ap$	all G	6 5		022
570	335.718	27.1112 - 324.9802	$50^{\circ} = 50^{\circ}(a + C)^{4}p$		0-5		722
220	335.851	29.1237 - 326.8763	3d° – 3d°(b°F)4p	a F - F	4-4		922
90	335.911	26.1530 - 323.8531	3d° - 3d°(a*F)4p	a'P - 'F'	2 - 2		922
510	335.971	27.5782 - 325.2229	$3d^6 - 3d^5(a^2G)4p$	a ³ H - ³ G°	5 - 4		922
160	336.072	1.4899 - 299.0456	3d ⁶ - 3d ⁵ (a ⁴ D)4p	ga ⁵ D - ⁵ P°	2 - 2		922
280	336,154	1.4899 - 298.9723	$3d^6 - 3d^5(a^4D)4p$	$ga^{5}D - {}^{3}D^{\circ}$	2 - 3		922
460	336 301	27.8588 - 325.2119	$3d^6 - 3d^5(a^2G)4p$	$a^{3}H - {}^{3}G^{\circ}$	4 - 3		922
+00	226 446	27.0500 - 525.2115	$3d^6 - 3d^5(b^2E)Ap$	$a^3 \mathbf{F} = {}^1 \mathbf{D}^2$	2_2		922
90	330.440	29.6792 - 327.1227	3d - 3d (01) + p		1 2 2		022
290	336.504	1.8715 - 299.0456	3d° - 3d°(a°D)4p	ga D - P	1 - 2		922
360	336.575	1.4899 - 298.6006	3d ⁶ - 3d ⁵ (a ⁴ P)4p	ga ⁵ D - ³ D°	2 – 1		922
630	336.792	0.0 - 296.9193	3d ⁶ - 3d ⁵ (a ⁴ D)4p	ga ⁵ D - ⁵ D°	4 – 4		922
570	336.818	0.0 - 296.8970	$3d^6 - 3d^5(a^4G)4p$	$ga^{5}D - {}^{3}G^{\circ}$	4 - 4		927
320	336 930	27 1112 - 323 9086	$3d^6 - 3d^5(a^2G)4p$	$a^{3}H - {}^{3}H^{\circ}$	6-5		922
320	337 184	0.0 296 5740	$3d^6 - 3d^5(a^4D)4p$	$\sigma^{5}D = {}^{5}D^{\circ}$	4 - 3		922
380	337.184	0.9907 207 4191	$2d^{5} - 2d^{5}(a^{4}\mathbf{D})Am$	$a^{3}D^{-3}D^{2}$	2 2		022
230	337.230	0.8897 - 297.4181	30 - 30 (a r)4p	ga D - D	3-3		922
250	337.276	1.4899 - 297.9828	3d ⁶ - 3d ⁵ (a ⁴ D)4p	ga ⁵ D - ⁵ P°	2 - 1		922
220	337.315	29.5708 - 326.0299	3d ⁶ – 3d ⁵ (b ² F)4p	$a^{3}F - {}^{3}F^{\circ}$	3 - 3		922
100	337.340	29.1237 - 325.5586	$3d^{6} - 3d^{5}(b^{2}F)4p$	$a^{3}F - {}^{1}G^{\circ}$	4 - 4		922
230	337 441	27 5782 - 323 9263	$3d^6 - 3d^5(a^2H)4n$	$a^{3}H - {}^{3}H^{\circ}$	5-4		922
250	227 461	27.5782 323.9265	$3d^6 - 3d^5(m^2G)An$	$a^3H - {}^3H^{\circ}$	5-5		922
340	337.401	27.3782 - 323.9080	246 245(-4D)4-		1 0		027
310	337.623	1.8715 - 298.0600	3d° – 3d°(a D)4p	ga D - D	1-0		921
360	337.696	0.8897 - 297.0139	3d ⁶ - 3d ⁵ (a ⁴ D)4p	ga ⁵ D - ⁵ D°	3 - 2		922
240	337.726	29.1237 - 325.2229	$3d^{6} - 3d^{5}(a^{2}G)4p$	a ³ F - ³ G°	4 – 4		922
330	337.743	29.8992 - 325.9822	$3d^{6} - 3d^{5}(b^{2}F)4p$	$a^{3}F - {}^{3}F^{\circ}$	2 - 2		922
350	337 761	27 8588 - 323 9263	$3d^6 - 3d^5(a^2H)4p$	$a^3H - {}^3H^\circ$	4 - 4		922
350	227 904	0 8807 206 0103	$3d^{6} - 3d^{5}(a^{4}D)4p$	$m^5D - 5D^9$	3_4		922
160	337.830	0.8897 - 296.8970 0.8897 - 296.8970	$3d^{\circ} - 3d(a^{\circ}D)$	ga ⁵ D - ³ G°	3-4		922
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250	337.920	1.4899 – 297.4179	3d ⁶ - 3d ⁵ (a ⁴ D)4p	ga'D – 'D°	2 - 1		922
20	337.978	34.4164 - 330.2976	3d ⁶ – 3d ⁵ (b ² F)4p	a ³ G - ³ G°	3 – 4		922
490	338.198	0.8897 - 296.5740	3d ⁶ - 3d ⁵ (a ⁴ D)4p	ga ⁵ D - ⁵ D°	3 - 3		922
230	338 357	1 8715 - 297 4179	$3d^6 - 3d^5(a^4D)4n$	$\tilde{g}a^{5}D - {}^{5}D^{\circ}$	1 - 1		922
250	338 383	1 4899 297 0139	$3d^{6} - 3d^{5}(a^{4}D)4p$	$G^{3}D = {}^{3}D^{2}$	2.2		922
550	338.473	0.0 - 295.4443	$3d^{6} - 3d^{5}(a^{4}D)4p$	ga ⁵ D - ⁵ F°	4 - 5		922
300	338.569	2.0576 - 297.4179	3d° - 3d°(a4D)4p	ga'D – 'D°	0 - 1		922
90	338.738	27.1112 - 322.3242	$3d^{6} - 3d^{5}(a^{2}H)4p$	$a^{3}H - {}^{1}I^{\circ}$	6 - 6		922
410	338.819	1.8715 - 297.0139	3d ⁶ - 3d ⁵ (a ⁴ D)4p	$ga^{5}D - {}^{5}D^{\circ}$	1 - 2		922
440	338.886	1.4899 - 296.5740	$3d^{6} - 3d^{5}(a^{4}D)4p$	$ga^{5}D - {}^{5}D^{\circ}$	2 - 3		922
220	339.052	0.0 - 294.9396	$3d^{6} - 3d^{5}(a^{4}D)4p$	ga ⁵ D - ⁵ F°	4 - 4		922
40	339.213	29.1237 - 323.9263	$3d^{6} - 3d^{5}(a^{2}H)4p$	a'F - 'H°	4 – 4		922
40	220 277	27 5782 222 2242	246 2472	-311 119			022
40	339.277	21.5/82 - 322.3242	30° - 30°(a°H)4p		5-0	1	922
60	339.674	29.1237 - 323.5232	30° - 30°(a°F)4p	a F - F	4-3		922
20	339.716	26.1530 - 320.5138	3d° - 3d°(a ² G)4p	a'P - 'F°	2 – 3		922
60	339.810	29.5708 - 323.8531	3d ⁶ - 3d ⁵ (a ⁴ F)4p	a 'F - 'F°	3 – 2		922
490	340.079	0.8897 - 294.9396	3d ⁶ - 3d ⁵ (a ⁴ D)4p	ga ^s D - ^s F°	3 – 4		922
160	340.189	29.8992 - 323.8531	3d ⁶ - 3d ⁵ (a ⁴ F)4p	$a^{3}F - {}^{3}F^{\circ}$	2 – 2		922
200	340 497	20 1237 - 322 8208	3d6 - 3d5(a4F)4-	$a^3 \mathbf{F} = {}^3 \mathbf{F}^{\circ}$	4_4		922
290	340.48/	27.1237 - 322.8208	5u - 5u (a F)4p 2d6 - 2d5(-2TT)4	a1' - 1'	6 7		022
460	340.316	27.1112 - 320.7831	30" - 30'(a'H)4p		0-/		722
90	340.577	33.2565 - 326.8763	3d° – 3d°(b ² F)4p	a G - 'F'	5-4		922
360	340.653	0.8897 – 294.4433	3d ⁶ - 3d ⁵ (a ⁴ D)4p	ga`D - `F°	3 - 3		922
	340 742	27.5782 - 321.0564	3d ⁶ - 3d ⁵ (a ² G)4p	a ³ H - ³ F°	5 – 4		922
140	340.742						

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NI V - Continued

			11.1.1. AT ALL					
Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	60	341.039	27.8588 - 321.0819	3d ⁶ - 3d ⁵ (a ² F)4p	a ³ H - ¹ F°	4 - 3		922
	90	341.068	0.8897 - 294.0860	$3d^6 - 3d^5(a^4D)4p$	ga ⁵ D - ⁵ F°	3 - 2		922
	30	341,242	29.5708 - 322.6176	$3d^6 - 3d^5(a^4F)4p$	$\int a^{3}F - {}^{3}D^{\circ}$	3 - 3		922
	430	341 351	1 4899 - 294 4433	$3d^6 - 3d^5(a^4D)4n$	ea ⁵ D − ⁵ F°	2 - 3		922
	270	341 589	27 1112 - 319 8604	$3d^6 = 3d^5(a^2H)4n$	$a^{3}H - {}^{3}I^{\circ}$	6-6		922
	180	341.509	27.1112 - 519.8004	$3d^6 - 3d^5(a^2G)Ap$	$a^{3}G = {}^{1}F^{\circ}$	4 3		922
	180	341.0/4	34.0017 - 320.7390	50 - 50 (a O)4p	a0-1	4-3		722
	380	341.701	27.8588 - 320.5138	3d ⁶ - 3d ⁵ (a ² G)4p	$a^{3}H - {}^{3}F^{\circ}$	4 - 3		922
	360	341.768	1.4899 - 294.0860	3d° - 3d ⁵ (a ⁴ D)4p	ga'D - 'F°	2 - 2		922
	500	341.832	27.1112 - 319.6527	3d ⁶ – 3d ⁵ (a ⁴ F)4p	a'H - 'G°	6 - 5		922
	320	341.858	42.2081 - 334.7276	3d ⁶ – 3d ⁵ (b ² F)4p	$a^{1}G - {}^{1}F^{\circ}$	4 – 3		922
	440	342.090	27.5782 - 319.8991	3d ⁶ – 3d ⁵ (a ⁴ F)4p	a ³ H - ³ G°	5-4		922
	350	342.135	27.5782 - 319.8604	3d ⁶ - 3d ⁵ (a ² H)4p	a ³ H - ³ I°	5 - 6		922
			1.0515 201.00/0	246 245 40.4-	5D 5E*			022
	370	342.215	1.8715 - 294.0860	$3d^{\circ} - 3d^{\circ}(a^{*}D)4p$	ga ⁵ D - F	1-2		922
	100	342.355	0.8897 – 292.9830	3d° – 3d ³ (a*P)4p	ga'D - 'P'	3 – 2		922
	220	342.379	27.5782 - 319.6527	3d° - 3d³(a4F)4p	a'H – 'G°	5 - 5		922
	180	342.418	27.8588 - 319.8991	3d ⁶ - 3d ⁵ (a ⁴ F)4p	a ³ H - ³ G°	4 - 4		922
	110	342.472	1.8715 - 293.8670	3d ⁶ – 3d ⁵ (a ⁴ P)4p	$ga^{5}D - {}^{3}P^{\circ}$	1-0		922
	500	342.506	27.1112 - 319.0762	3d ⁶ – 3d ⁵ (a ² H)4p	$a^{3}H - {}^{3}I^{\circ}$	6 - 5		927
	360	242 545	1 4899 293 4200	3d ⁶ - 3d ⁵ (s ⁴ P)4p	$m^5D = {}^3P^{\circ}$	2_1		977
	500	342.545	1.4677 - 275.4200	$3d^6 - 3d^5(a^2G)4n$	a D - I	5 6		022
	500	342.592	33.2505 - 325.1484	3d - 3d (a C) 4p		0 1		027
	340	342.728	2.0576 - 293.8338	$3d^{\circ} - 3d^{\circ}(a^{\circ}D)4p$	ga ^D - F	0-1		927
	200	342.747	27.8588 - 319.6202	3d° – 3d'(a*F)4p	a'H - 'G'	4-3		922
	400	342.790	33.2565 - 324.9802	3d° - 3d'(a2G)4p	a'G - 'G°	5 - 5		922
	420	342.910	57.9241 - 349.5460	3d° – 3d°(b²D)4p	a'F – 'D°	3 - 2		922
	420	342.976	34.4164 - 325.9822	3d ⁶ – 3d ⁵ (b ² F)4p	a ³ G - ³ F°	3 - 2		922
	350	342.996	1.8715 - 293.4200	$3d^{6} - 3d^{5}(a^{4}P)4p$	$ga^{5}D - {}^{3}P^{\circ}$	1-1		922
	440	343.044	29.5708 - 321.0819	$3d^{6} - 3d^{5}(a^{2}F)4p$	a ³ F - ³ F°	3 - 3		922
	510	343.057	27.5782 - 319.0762	$3d^{6} - 3d^{5}(a^{2}H)4p$	$a^{3}H - {}^{3}I^{\circ}$	5 - 5		922
	90	343 182	29 1237 - 320 5138	$3d^6 - 3d^5(a^2G)4n$	$a^3 \mathbf{F} - {}^3 \mathbf{F}^\circ$	4 - 3		922
	140	343.215	2.0576 - 293.4200	$3d^6 - 3d^5(a^4P)4p$	$ga^5D - {}^3P^\circ$	0 - 1		922
	180	343.256	0.0 - 291.3285	$3d^{\circ} - 3d^{\circ}(a^{4}G)4p$	ga'D – 'F°	4 – 3		922
	340	343.385	27.8588 - 319.0762	3d ⁶ - 3d ⁵ (a ² H)4p	a ³ H – ³ I°	4 - 5		922
	140	343.427	29.8992 - 321.0819	3d ⁶ – 3d ⁵ (a ² F)4p	a ³ F - ¹ F°	2 - 3		922
	460	343.454	34.0617 - 325.2229	3d ⁶ - 3d ⁵ (a ² G)4p	a ³ G - ³ G°	4 - 4		922
	430	343.464	34.0617 - 325.2119	3d ⁶ - 3d ⁵ (a ² G)4p	a ³ G - ³ G°	4 - 3	1	922
	390	343.503	29.8992 - 321.0183	3d ⁶ - 3d ⁵ (a ² G)4p	$a^{3}F - {}^{3}F^{\circ}$	2 - 2		922
	380	343 711	29 5708 - 320 5138	$3d^{6} = 3d^{5}(a^{2}G)4n$	$a^3 \mathbf{F} = {}^3 \mathbf{F}^\circ$	3-3		922
	310	343 730	34 0617 - 324 9802	$3d^6 - 3d^5(a^2G)4n$	*G - G	4-5		922
	360	343.960	34,4164 325 2220	$3d^6 = 3d^5(a^2G)Ap$	a ³ G = ³ G°	3_4		922
	450	242.007	34.4164 - 325.2227	$3d^6 - 3d^5(a^2G)Ap$	*G *G*	3 - 4		922
	430	343.003	54.4104 - 525.2119	3d - 3d (a C) + p		1 2 2		022
	220	343.930	0.0 - 290.7570	$3d^{2} - 3d(a^{2}P)^{4}P$	$ga^{*}D - F$	4-5		922
	320	344.038	0.8897 - 291.5546	3d" - 3d"(a"G)4p	ga D - F	3-4		922
	370	344.053	33.2565 - 323.9086	3d ⁶ - 3d ⁵ (a ² G)4p	a ³ G - ³ H°	5 - 5		922
	360	344.200	29.1237 - 319.6527	3d ⁶ – 3d ⁵ (a ⁴ F)4p	a ³ F - ³ G°	4 - 5		922
	590	344.234	0.8897 - 291.3900	$3d^6 - 3d^5(a^4P)4p$	$ga^{5}D - {}^{5}P^{\circ}$	3 - 2		922
	250	344.438	29.5708 - 319.8991	$3d^6 - 3d^5(a^4F)4p$	a ³ F - ³ G°	3 - 4		922
	60	344.516	0.0 - 290.2620	3d ⁶ - 3d ⁵ (a ⁴ P)4p	$ga^5D - {}^5D^\circ$	4 - 4		922
	600	344.571	27.1112 - 317.3273	3d ⁶ - 3d ⁵ (a ² H)4p	a ³ H - ³ H°	6 - 6		922
	(0)	244 676	26 1520 216 2002	2.46 2.45(-217).4-	alD in			022
	60	344.070	20.1330 - 310.2803	30° - 30°(a°F')4p	ar-r	2-3		922
	530	344.767	1.4899 - 291.5417	30° - 30°(a'P)4p	ga D - P	2-1		922
	330	344.810	29.1237 - 319.1387	3d" – 3d'(a'G)4p	a'F - 'G'	4-4		922
	130	344.881	29.1237 - 319.0762	3d° - 3d'(a²H)4p	a F - 'I°	4 - 5		922
	490	344.947	1.4899 - 291.3900	3d ⁶ - 3d ⁵ (a ⁴ P)4p	ga'D – 'P°	2 - 2		922
	500	344.986	0.8897 - 290.7570	3d ⁶ - 3d ⁵ (a ⁴ P)4p	ga ⁵ D – ⁵ P°	3 - 3		\$?2
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NI V -- Continued

ultiplet Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	1 - 1	Notes	References
460	345.011	34.0617 - 323.9086	3d° - 3d ⁵ (a ² G)4p	a ³ G - ³ H°	4 - 5		922
540	345.120	27.5782 - 317.3273	3d ⁶ – 3d ⁵ (a ² H)4p	$a^{3}H - {}^{3}H^{\circ}$	5 - 6		922
280	345.160	29.8992 - 319.6202	3d* – 3d ⁵ (a⁴F)4p	a ³ F – ³ G°	2 - 3		922
460	345.219	1.8715 - 291.5417	3d° – 3d⁵(a⁴P)4p	ga ^s D - ^s P°	1 - 1		922
330	345.287	27.1112 - 316.7266	$3d^{6} - 3d^{5}(a^{2}H)4p$	a ³ H – ³ G°	6 - 5		922
500	345.345	33.2565 - 322.8208	3d ⁶ - 3d ⁵ (a ⁴ F)4p	$a^{3}G - {}^{3}F^{\circ}$	5 - 4		922
550	345.406	34.4164 - 323.9263	3d° - 3d ⁵ (a ² H)4p	a ³ G - ³ H°	3 - 4		922
360	345,442	2.0576 - 291.5417	$3d^6 - 3d^5(a^4P)4p$	ga ⁵ D - ⁵ P°	0 - 1		922
380	345,469	34.0617 - 323.5232	3d ⁶ - 3d ⁵ (a ⁴ F)4p	a ³ G - ³ F°	4 - 3		922
380	345.500	34.4164 - 323.8531	3d ⁶ - 3d ⁵ (a ⁴ F)4p	$a^{3}G - {}^{3}F^{\circ}$	3 - 2		922
590	345 576	0.8897 - 290.2620	$3d^{6} - 3d^{5}(a^{4}P)4p$	ga ⁵ D - ⁵ D°	3-4		922
520	345.652	27.5782 - 316.8878	3d° - 3d ^s (a ² H)4p	a ³ H - ³ G°	5 - 4		922
510	345 662	27 5782 - 316 8878	3d ⁶ - 3d ⁵ (a ² H)4n	$a^{3}H - {}^{3}G^{\circ}$	5-4		922
340	345 701	1 4899 - 290 7570	$3d^6 = 3d^5(a^4P)4p$	$ga^{5}D - {}^{5}P^{\circ}$	2-3		922
340	345 821	275782 - 3167440	$3d^6 - 3d^5(a^4F)4p$	$a^3H - 5D^{\circ}$	5-4		922
290	343.621	27.5782 - 510.7440	$3d^6 = 3d^5(a^2H)4p$	$a^{3}H = {}^{3}G^{\circ}$	5-5		922
260	245.043	27.5782 - 510.7200	$3d^{\circ} = 3d^{\circ}(a^{4}F)4p$	$a^3G = F^{\circ}$	1 3 - 3	1	922
200	345.892	34.4164 - 323.3232 33.2565 - 322.3242	$3d^{\circ} - 3d^{\circ}(a^{2}H)4p$	$a^{3}G - I^{\circ}$	5-6		922
90	345.987	27.8588 - 316.8878	$3d^{\circ} - 3d^{\circ}(a^{2}H)4p$	a H - G	4-4	1	922
80	346.036	57.9241 - 346.9124	3d° - 3d°(b²D)4p	a'F - 'P'	3-2		922
320	346.165	27.1112 - 315.9905	$3d^\circ - 3d^3(a^2H)4p$	a'H - 'H'	6-5		922
160	346.239	28.6976 - 317.5175	3d° - 3d ³ (a ⁴ F)4p	a P - D	1 - 2		922
300	346.309	34.0617 - 322.8208	3d° - 3d³(a⁴F)4p	a'G - 'F°	4 - 4		922
250	346.327	41.6269 - 330.3707	3d [°] - 3d [°] (a ² S)4p	a'D - 'P°	2 - 1		922
340	346.417	41.7011 - 330.3707	3d ⁶ - 3d ⁵ (a ² S)4p	$a^{3}D - {}^{3}P^{\circ}$	1 - 1		922
240	346.553	34.0617 - 322.6176	3d ⁶ - 3d ⁵ (a ⁴ F)4p	a'G - 'D°	4 - 3		922
130	346.577	104.4205 - 392.9571	$3d^{6} - 3d^{5}(c^{2}D)4p$	b'D – 'F°	2 - 3		922
130	346.632	27.5782 - 316.0688	$3d^{6} - 3d^{5}(a^{2}F)4p$	a ³ H - ³ G°	5-4		922
630	346.730	0.8897 - 289.2980	$3d^{6} - 3d^{5}(a^{4}P)4p$	ga ⁵ D – ⁵ D°	3 - 3		922
110	346.925	41.6269 - 329.8729	3d" - 3d ^s (b ² F)4p	$a^{3}D - {}^{3}D^{\circ}$	2 - 3		922
270	346.970	27.8588 - 316.0688	$3d^{6} - 3d^{5}(a^{2}F)4p$	a'H - 'G°	4 - 4		922
600	347 028	0.0 - 288.1616	3d ⁶ - 3d ⁵ (a ⁴ G)4p	ga ⁵ D - ⁵ F°	4 - 4		922
400	347.020	27 8588 - 315 9905	$3d^6 - 3d^5(a^2H)4p$	$a^{3}H - {}^{3}H^{\circ}$	4 - 5	ŀ	922
260	347 134	41 7011 - 329 7763	$3d^6 - 3d^5(b^2F)4p$	$a^{3}D - {}^{3}D^{\circ}$	1-2		922
410	347 156	27 1112 - 315 1682	3d ⁶ - 3d ⁵ (a ⁴ F)4p	a'H - 'F'	6 - 5		922
190	347.200	34.4164 - 322.4364	3d ⁶ - 3d ⁵ (a ⁴ F)4p	a ³ G - ³ D°	3 - 2		927
240	247 226	0 8807 288 8770	2d ⁶ 2d ⁵ (a ⁴ D)4n	°2 ³ – ¹ €°	3_2		927
240	347.230	0.8897 - 200.8779	$3d^{6} - 3d^{5}(b^{2}E)Ap$	$a^3D - 3D^6$	3-2		922
740	347.275	41.9202 - 329.8729	$3d^{\circ} = 3d^{\circ}(a^{4}G)4p$	$a^{5}D = 5^{6}$	4-5		927
/40	347.335	41 0202 220 7762	$3d^6 - 3d^5(b^2E)Ap$	$a^3D = 1$	3_2		922
410	347.397	41.9202 - 329.7703	$3d^6 = 3d^5(b^2E)4p$	$a^{3}D = D^{2}$	3 = 2 2 = 1	1	922
700	347.422	1.4899 - 289.2980	$3d^{6} - 3d^{5}(a^{4}P)4p$	ga ⁵ D - ⁵ D°	2 - 3		922
		ac 1520 - 212 0100	246 245(-20)4-	-3D 3D*			077
630	347.505	26.1530 - 313.9198	3d ^o - 3d ^o (a ² D)4p	$a^{T} - D^{T}$	2-3		922
610	347.515	1.4899 - 289.2471	3d ² – 3d ² (a ² G)4p	ga D - F	2-2		922
450	347.592	41.9202 - 329.6143	3d" - 3d (b-F)4p	a D - G	3-3	1	922
640	347.702	29.1237 - 316.7266	3d" - 3d"(a-H)4p		4-5		922
670 460	347.716	27.1112 - 314.7022 26.1530 - 313.6866	$3d^{\circ} - 3d^{\circ}(a^{2}F)4p$ $3d^{\circ} - 3d^{5}(a^{2}D)4p$	$a^{3}H - {}^{3}O^{\circ}$	2-2		922 922
400							
630	347.811	27.8588 - 315.3701	$3d^6 - 3d^5(a^2G)4p$	$a^{3}H - {}^{3}H^{\circ}$	4 - 4		922
	347.865	28.6976 - 316.1654	3d" – 3d'(a'F)4p	a P - F	1-2		922
530	1		$3d^{\circ} = 3d^{\circ}(a^{4}G)4n$	(a)) - 'F°	1 1 - 2	1	922
530 610	347.977	1.8715 - 289.2471	50 - 50 (a C)+p				
530 610 610	347.977 348.047	1.8715 - 289.2471 68.7187 - 356.0363	$3d^{\circ} - 3d^{\circ}(b^{2}G)4p$	b'F - 'G'	4 - 5		922
530 610 610 630	347.977 348.047 348.080	1.8715 - 289.2471 68.7187 - 356.0363 1.8715 - 289.1630	3d ⁶ - 3d ⁵ (b ² G)4p 3d ⁶ - 3d ⁵ (a ⁴ G)4p 3d ⁶ - 3d ⁵ (a ⁴ G)4p	b ³ F - ³ G ⁹ ga ⁵ D - ⁵ F ⁹	4 - 5 1 - 1		922 922

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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm $^{-1}$)	Configurations	Terms	J - J	Notes	References
	220	348.226	29.5708 - 316.7440	3d ⁶ - 3d ⁵ (a ⁴ F)4p	a ³ F - ⁵ D°	3 - 4		922
	230	348.245	29.1237 - 316.2803	$3d^6 - 3d^5(a^2F)4p$	$a^{3}F - {}^{3}F^{\circ}$	4 - 3		922
	620	348.278	0.0 - 287.1280	$3d^{6} - 3d^{5}(a^{4}G)4p$	$ga^{5}D - {}^{5}H^{\circ}$	4 - 5		922
	530	348 303	2 0576 - 289 1630	$3d^6 - 3d^5(a^4G)4p$	$ga^5D - F^{\circ}$	0 - 1		922
	420	348 347	0 8897 - 287 9600	$3d^6 - 3d^5(a^4G)Ap$	$a^{5}D = {}^{5}F^{6}$	3_3		922
	310	348 375	69 7197 355 7652	$3d^6 - 3d^5(h^2G)4n$	$h^3 F^{-3} G^{\circ}$	4.4		022
	510	340.373	08.7187 - 333.7032	30 – 30 (0 C)4p	01-0	4-4		922
	410	348.409	34.0617 - 321.0819	$3d^6 - 3d^5(a^2F)4p$	$a^3G - {}^1F^\circ$	4 - 3		922
	370	348.422	1.8715 - 288.8779	3d" – 3d'(a*P)4p	ga D – S	1 - 2	Į	927
	450	348.498	29.1237 - 316.0688	$3d^{6} - 3d^{5}(a^{2}F)4p$	a'F - 'G°	4 – 4	1	922
	330	348.541	68.8547 - 355.7652	3d° – 3d5(b2G)4p	b ³ F – ³ G°	3 – 4		922
	400	348.563	0.8897 - 287.7821	3d° - 3d ⁵ (a ⁴ P)4p	ga ⁵ D - ⁵ D°	3 - 2]	922
	140	348.594	29.1237 - 315.9905	3d° - 3d ^s (a ² H)4p	$a^{3}F - {}^{3}H^{\circ}$	4 - 5		922
	50	348.623	27.8588 - 314.7022	$3d^{6} - 3d^{5}(a^{2}F)4p$	$a^{3}H - {}^{3}G^{\circ}$	4 - 5		922
	500	348 674	26 1530 - 312 9536	$3d^{6} - 3d^{5}(a^{2}F)4n$	$a^{3}P - {}^{3}D^{\circ}$	2 - 3		922
	70	348 716	68 6321 - 355 3980	$3d^{6} - 3d^{5}(h^{2}G)4n$	$h^3 E = 3G^2$	2 3		922
	200	348.750	26 1520 212 9904	$3d^{6} - 3d^{5}(a^{4}E)Ap$	a ³ P 5G ^o	2-5	ł	027
	200	340.732	20.1330 - 312.8874	240 245(-27)4-		2-3		927
	320	348.780	29.5708 - 516.2805	30" - 30"(a"F)4p		3-3		927
	410	348.830	28.09/0 - 315.3001	30° - 30°(a°F)4p	a'P - 'D	1 - 2		922
	310	348.883	27.5782 - 314.2088	3d ⁶ - 3d ⁵ (a ² F)4p	$a^{3}H - {}^{3}F^{\circ}$	5 - 4		927
	410	348.915	34.4164 - 321.0183	3d ⁶ - 3d ⁵ (a ² G)4p	$a^{3}G - {}^{3}F^{\circ}$	3 – 2		922
	320	348.987	68.8547 - 355.3980	3d* – 3d*(b2G)4p	b ³ F - ³ G°	3 - 3		922
	380	349.019	68.6321 - 355.1500	$3d^{6} - 3d^{5}(b^{2}G)4p$	b'F - 'F°	2 - 2		922
	340	349.043	29.5708 - 316.0688	$3d^{6} - 3d^{5}(a^{2}F)4p$	$a^{3}F - {}^{3}G^{\circ}$	3-4		922
	550	349.076	1.4899 - 287.9600	3d° - 3d ⁵ (a ⁴ G)4p	ga ⁵ D – ⁵ F°	2 - 3		922
	100	340.004	24.0617 220.5129	2d9 2d5(c2C)4=	30 350			011
	160	345.050	10 8002 216 2803	3d - 3d (a O) + p				922
	100	349.104	29.8992 - 310.2803	30 - 30 (a r)4p		2-3		922
	00	349.220	27.1112 - 313.4647	$3d^{*} - 3d^{*}(a^{*}F)4p$	a'H - 'G'	0-5		922
	180	349.293	1.4899 - 287.7821	3d" - 3d"(a"P)4p	ga D - D	2-2		922
	360	349.326	1.4899 - 287.7555	3d" – 3d'(a*P)4p	ga D – D	2 - 1		927
	330	349.339	104.4205 - 390.6751	3d° - 3d°(c²D)4p	β'D – 'D°	2 – 2		922
	120	349.403	29.1237 - 315.3262	3d ⁶ - 3d ⁵ (a ² D)4p	a ³ F - ¹ F*	4 - 3		922
	210	349.485	28.6976 - 314.8347	$3d^{6} - 3d^{5}(a^{4}F)4p$	$a^{3}P - {}^{5}F^{\circ}$	1 – 2		922
	230	349.500	48.6070 - 334.7276	$3d^{6} - 3d^{5}(b^{2}F)4p$	$a^{1}D - {}^{1}F^{\circ}$	2 - 3		922
	240	349.522	41.2522 - 327.3566	$3d^{6} - 3d^{5}(a^{2}H)4p$	a ¹ I - ¹ H°	6 - 5		922
	40	349.576	27.8588 - 313.9198	$3d^{6} - 3d^{5}(a^{2}D)4p$	$a^{3}H - {}^{3}D^{\circ}$	4-3		922
	310	349.759	1.8715 - 287.7821	$3d^{\circ} - 3d^{\circ}(a^{4}P)4p$	$ga^{5}D - {}^{5}D^{\circ}$	1 - 2		922
	400	340 704	1 9715 107 7555	2-10 2-15/-4014-	5D 5D9			027
	490	349.794	1.8/13 - 28/./333	3d = 3d(a P)4p		1-1		927
	490	349.809	48.0070 - 334.4772	30" - 30" (a*S)4p	$a^{1}D - P^{2}$	2-1		922
	370	349.879	20.1530 - 311.9005	$3d^{\circ} = 3d^{\circ}(a^{2}D)4p$	$a^{2}P - P^{2}$	2-2		927
	270	349.900	29.5708 - 315.3661	$3d^{\circ} - 3d^{\circ}(a^{2}F)4p$	$a^{2}F - D^{*}$	3 - 2	1	922
	190 240	349.950	29.5708 - 315.3262	$3d^{0} - 3d^{3}(a^{2}D)4p$ $3d^{6} - 3d^{5}(a^{4}P)4p$	$a^{5}D - {}^{5}D^{\circ}$	3-3 0-1		922 927
			2.0010 2000000	50 50 (01)10				21
	310	350.065	29.6400 - 315.3007	3d° - 3d5(a2F)4p	a ³ P - ³ D°	0 - 1		922
	80	350.133	27.8588 - 313.4647	3d ⁶ - 3d ⁵ (a ⁴ F)4p	a ³ H - ⁵ G°	4 - 5		922
	290	350.166	29.1237 - 314.7022	$3d^{6} - 3d^{5}(a^{2}F)4p$	$a^{3}F - {}^{3}G^{\circ}$	4 - 5		922
	160	350.191	34.0617 - 319.6202	3d° - 3d ⁵ (a4F)4p	$a^3G - {}^3G^\circ$	4 - 3		922
	260	350.249	34.4164 - 319.9265	$3d^{6} - 3d^{5}(a^{2}F)4p$	$a^{3}G - {}^{1}D^{\circ}$	3-2	1	922
	470	350.302	29.8992 - 315.3661	3d ⁶ - 3d ⁵ (a ² F)4p	a ³ F - ³ D°	2 - 2		922
	350	350 353	77 8588 313 3013	2,46 2,454-4554-	JU 500			007
	330	350.332	27.0300 - 313.2013 57.0341 - 343.3910	30° - 30°(a°F)4p 246 - 256-2004-		4-4		927
	20	350.437	57.7241 - 343.201U	30 - 30 (0 ⁻ D)4p		3-3		922
	420	330.493	08.0321 - 353.9441	30° - 30°(b°G)4p	D'F - 'F"	2-3		922
	430	350.357	29.5/08 - 314.8347	3d" – 3d'(a'F)4p	a F - 'F'	3 - 2		922
	390	350.566	29.8992 - 315.1528	3d° – 3d°(a*F)4p	a'F - 'F'	2 – 1		922

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Iultiplet Rel. Int	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	Reference
150	350.626	34.4164 - 319.6202	3d ⁶ – 3d ⁵ (a ⁴ F)4p	a ³ G - ³ G°	3 - 3		922
460	350.694	42.2081 - 327.3566	3d ⁶ – 3d ⁵ (a ² H)4p	a'G 'H°	4 - 5		922
690	350.773	41.2522 - 326.3371	3d° – 3d ⁵ (a²G)4p	a'I – 'H°	6 - 5		922
310	350.841	27.8588 - 3.12.8894	$3d^6 - 3d^5(a^4F)4p$	a ³ H - ⁵ G°	4 - 3		927
320	350.900	28.6976 - 313.6866	$3d^{6} - 3d^{5}(a^{2}D)4p$	$a^{3}P - {}^{3}D^{\circ}$	1 - 2		922
220	350.931	41.9202 - 326.8763	$3d^{6} - 3d^{5}(b^{2}F)4p$	$a^{3}D - {}^{3}F^{\circ}$	3 - 4		922
270	351.026	28.6976 - 313.5773	$3d^6 - 3d^5(a^2D)4p$	$a^{3}P - {}^{3}P^{\circ}$	1-0		922
220	351.085	68.7187 - 353.5487	$3d^6 - 3d^5(b^2G)4p$	b ³ F - ³ H°	4 - 5		922
350	351,128	29.1237 - 313.9198	$3d^6 - 3d^5(a^2D)4p$	$a^{3}F - {}^{3}D^{\circ}$	4 - 3	. 1	927
320	351,286	42.2081 - 326.8763	$3d^6 - 3d^5(b^2F)4p$	$a^1G - {}^3F^{\circ}$	4-4		922
430	351,335	68 7187 - 353 3471	$3d^6 - 3d^5(b^2G)4p$	$b^3 E - {}^3 E^{\circ}$	4-4		922
400	351.365	27.8588 - 312.4633	$3d^{\circ} - 3d^{\circ}(a^{2}F)4p$	$a^{3}H - {}^{3}G^{\circ}$	4 - 3		922
450	351.455	42.2081 - 326.7390	3d ⁶ - 3d ⁵ (a ² G)4p	a'G - 'F°	4 - 3		922
60	351.503	68.8547 - 353.3471	$3d^6 - 3d^5(b^2G)4p$	$b^3F - {}^3F^\circ$	3-4		922
60	351.581	27 5782 - 312 0083	$3d^6 - 3d^5(a^2F)4p$	$a^3H - G^{\circ}$	5-4		922
300	351.613	0.0 - 2844025	$3d^6 = 3d^5(a^4G)4n$	$ra^5D - G^{\circ}$	4-5		927
330	351.677	29 5708 - 313 9198	$3d^6 = 3d^5(a^2D)4n$	$a^{3}F - {}^{3}D^{\circ}$	3-3		922
200	351.691	29.1237 - 313.4647	$3d^6 - 3d^5(a^4F)4p$	$a^{3}F - {}^{5}G^{\circ}$	4 - 5		922
40	351 730	0.0 284 3089	3d ⁶ - 3d ⁵ (a ⁴ G)4n	°°D – 5G°	4_4		977
120	351.750	$41\ 7011 = 325\ 9822$	$3d^{\circ} = 3d^{\circ}(a^{\circ}C)^{+}P$ $3d^{\circ} = 3d^{\circ}(b^{2}E)4n$	$a^{3}D = C$	1 - 2		927
200	351.944	41.7011 = 323.7822	$3d^6 = 3d^5(b^2G)4p$	$h^3 E = {}^3 H^6$	3 - 4		922
200	351.044	27 9599 212 0092	$3d^6 - 3d^5(c^2E)Ap$	³ H G°			922
500	351.920	27.8388 - 312.0083	$3d^{\circ} = 3d^{\circ}(a, 1)^{4}p^{\circ}$	aH = O	2 2		922
130	352.241	41.2522 - 325.1484	$3d^6 - 3d^5(a^2G)4p$	$a^{\dagger}I - {}^{3}H^{\circ}$	6-6		922
520	352 324	20 1227 212 0526	$3d^6 - 3d^5(a^2E)An$	a ³ E - ³ D ^o	4 3		977
380	352.324	29.1257 - 512.9550	$3d^{6} = 3d^{5}(a^{2}D)/a^{2}$	$a^{3}F = ^{3}D^{\circ}$	2 - 1		022
60	352.500	41 2522 - 324 9802	$3d^{6} = 3d^{5}(a^{2}G)/4p$	$a^{1} - D$	6-5		922
140	352.451	41.2522 - 524.7602	$3d^{6} = 3d^{5}(b^{2}E)A_{P}$	$a^{3}D = {}^{1}G^{\circ}$	3 4		022
140	252.501	41.5202 ~ 525.5580	$3d^{9} - 3d^{5}(a^{2}D)/a$	a D = O	1 1		022
570	352.769	33.2565 - 316.7266	$3d^6 - 3d^5(a^2H)4p$	$a^{3}G - {}^{3}G^{\circ}$	5 - 5		922
210	352 834	0 8897 - 284 3089	3d ⁶ - 3d ⁵ (a ⁴ G)4p	es ⁵ D – ⁵ G°	3_4		927
70	352.879	295708 - 3129536	$3d^6 = 3d^5(a^2E)An$	$a^3F = 3D^2$	3_3		927
400	352.019	42 2081 225 5586	3d = 3d (a T) + p $2d^{5} = 2d^{5} (b^{2} E) A =$				922
400	352.919	42.2081 - 323.3380	3d = 3d (0 P) + p $3d^{5} = 2d^{5} (a^{4}E) A p$				922
120	352.900	29.5708 - 312.8894	3d = 3d (a F) + p	aF = G	3-3		927
160	353.099	29.8992 - 312.8894	3d ⁶ - 3d ⁵ (a ⁴ F)4p	$a^{3}F - {}^{5}G^{\circ}$	3-2 2-3		927
410	262.607		2.16 2.15(-277).4				
410	353.407	34.4164 - 317.3768	3d° – 3d°(a-H)4p	a'G - 'G'	3-3		922
330	353.492	29.5708 - 312.4633	$3d^{\circ} - 3d^{\circ}(a^{-}F)4p$	$a^{T}F - G^{T}$	3 - 3		922
200	353.507	29.8992 - 312.7782	$3d^{2} - 3d^{2}(a^{2}F)4p$	a'F - 'G			927
620	353.573	34.0617 - 316.8878	$3d^{2} - 3d^{2}(a^{2}H)4p$	a'G - 'G'	4-4		922
280	353.588	26.1530 - 308.9430	3d ⁶ - 3d ⁵ (a ² D)4p	$a^3\mathbf{P} - {}^1\mathbf{D}^9$	3-4 2-2		922 922
170	353 655	1 4800 284 2400	240 245/4014-	m ⁵ D 5C*	2.2		027
1/0	333.033	1.4077 - 284.2490	30° - 30° (a°G)4P		2-3		927
230	353.089	33.2303 - 313.9903	3u = 3u (a - 1)4p	a G - H	0 1		922
1/0	353.734	41.2522 222.0094	$30^{-} - 30^{-}(a^{-}5)4p$	a 5 - P	6 6		922
410	353.788	41.2322 - 323.9080	246 245(a ² D)4-		5 4		922
30	353.901	29.8992 - 312.4633	$3d^6 - 3d^5(a^2F)4p$	$a^{3}F - {}^{3}G^{\circ}$	2 - 3		922
20	254 012	24 4164 216 0070	2.46 2.45/~27.7.4-	-3G 3G*	2 4		072
20	354.013	34.4104 - 310.8878	30° - 30°(a°H)4P		3-4		922
220	354.061	29.5708 - 312.0083	30° - 30°(a°F)4p	a'F - 'G'	3-4		922
440	354.118	29.8992 - 312.2910	3d" – 3d'(a²D)4p	a'F - 'P'	2-1		922
400	354.140	27.5782 - 309.9525	3d° – 3d'(a²I)4p	a'H – 'H°	5-4		922
				1			
720	354.181	1.8715 - 284.2155	$3d^{\circ} - 3d^{\circ}(a^{\circ}G)4p$	ga D - G	1-2		927

NI V - Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	760	354.418	27.1112 - 309.2640	3d ⁶ - 3d ⁵ (a ² I)4p	a ³ H - ³ H°	6-6		922
	360	354.467	33,2565 - 315,3701	$3d^6 - 3d^5(a^2G)4p$	a ³ G - ³ H°	5-4		922
	680	354.493	27.8588 - 309.9525	$3d^6 - 3d^5(a^2I)4p$	a ³ H ~ ³ H°	4 - 4		922
	180	354.533	27.8588 - 309.9195	$3d^6 - 3d^5(a^2I)4p$	$a^{3}H - {}^{3}H^{\circ}$	4 - 5		922
	370	354 721	33,2565 - 315,1682	$3d^6 - 3d^5(a^4F)4p$	$a^{3}G - {}^{5}F^{\circ}$	5-5		922
	290	354 780	344164 - 3162803	$3d^6 - 3d^5(a^2F)4p$	$a^3G - {}^3F^\circ$	3-3		922
	290	334.780	54.4104 - 510.2805	50 - 50 (a 1)+p		J = J		/22
	250	354.925	34.4164 - 316.1654	3d ⁶ - 3d ⁵ (a ² F)4p	$a^{3}G - {}^{3}F^{\circ}$	3 - 2		922
	350	354.964	42.2081 - 323.9263	3d ⁶ – 3d ⁵ (a ² H)4p	a'G - ³ H°	4 – 4		922
	0	354.994	27.1112 - 308.8041	3d ⁶ – 3d ⁵ (a ² I)4p	a ³ H – ¹ H°	6 - 5		922
	70	355.046	34.4164 - 316.0688	$3d^{6} - 3d^{5}(a^{2}F)4p$	a ³ G - ³ G°	3-4		922
	250	355.140	26.1530 - 307.7311	$3d^6 - 3d^5(a^2D)4p$	$a^{3}P - {}^{3}F^{\circ}$	2 – 2		922
	120	355.240	33.2565 - 314.7564	3d ⁶ – 3d ⁵ (a ⁴ F)4p	a3G - 5G°	5 - 6		922
				a. 16 a. 154	10.100			000
	220	355.309	33.2565 - 314.7022	3d° - 3d [°] (a ² F)4p	a'G - 'G'	5-5		922
	90	355.439	33.2565 - 314.5992	3d° – 3d°(a⁴F)4p	a'G - 'F°	5-4		922
	50	355.471	42.2081 - 323.5232	3d ⁶ - 3d ⁵ (a ⁴ F)4p	$a^{1}G - {}^{3}F^{\circ}$	4 – 3		922
	420	355.537	34.0617 - 315.3262	$3d^6 - 3d^5(a^2D)4p$	$a^{3}G - {}^{1}F^{\circ}$	4 – 3		922
	400	355.586	27.5782 - 308.8041	$3d^{6} - 3d^{5}(a^{2}I)4p$	a ³ H - ¹ H°	5-5		922
	680	355.611	27.1112 - 308.3173	$3d^{6} - 3d^{5}(a^{2}I)4p$	a ³ H – ³ I°	6 - 7		922
				a. 16 . a. 15 / June 4	1. 1.			
	700	355.780	41.2522 - 322.3242	$3d^{\circ} - 3d^{\circ}(a^{2}H)4p$	a'l - 'l'	6-6		922
	580	355.935	33.2565 - 314.2088	$3d^{6} - 3d^{3}(a^{2}F)4p$	a'G - 'F°	5 - 4	1	922
	140	355.986	34.4164 - 315.3262	3d ⁶ - 3d ⁵ (a ² D)4p	$a^{3}G - {}^{1}F^{\circ}$	3 – 3		922
	580	356.047	77.8995 - 358.7600	3d ⁶ – 3d ⁵ (b ² G)4p	$b^{1}G - {}^{1}G^{\circ}$	4 - 4		922
	160	356.090	29.1237 - 309.9525	3d ⁶ – 3d ⁵ (a ² I)4p	$a^{3}F - {}^{3}H^{\circ}$	4 - 4		922
	20	356.134	29.1237 - 309.9195	$3d^{6} - 3d^{5}(a^{2}I)4p$	$a^{3}F - {}^{3}H^{\circ}$	4 - 5		922
	120	356 208	27 8588 308 5920	$3d^6 - 3d^5(a^2D)4p$	a ³ H – ³ F°	4 - 3		977
	40	356 253	41 9202 - 322 6176	$3d^6 - 3d^5(a^4E)4p$	$a^3D = {}^3D^\circ$	1 2 3		922
	110	350.255	41.9202 - 322.01/0	3d - 3d (a T) + p	aD - D	3-3		022
	220	330.328	34.0017 - 314.7022	$3d^2 - 3d(aF)4p$		4-5		922
	20	356.359	42.2081 - 322.8208	3d° – 3d°(a°F)4p	a'G - 'F	4-4		922
	250	356.410	77.8995 - 358.4756	3d° – 3d°(b°G)4p	b'G - 'H'	4-5		922
	60	356.460	34.0617 - 314.5992	3d° – 3d'(a*F)4p	a'G - 'F'	4-4		922
	70	356.506	34.0617 - 314.5628	3d ⁶ - 3d ⁵ (a ⁴ F)4p	a ³ G - ⁵ F°	4-3		922
	390	356.621	42.2081 - 322.6176	$3d^6 - 3d^5(a^4F)4p$	a'G - 'D°	4 - 3		922
	490	356.775	27.1112 - 307.3997	$3d^6 - 3d^5(a^2I)4p$	$a^{3}H - {}^{3}I^{\circ}$	6-6		922
	70	356 831	28 6976 - 308 9430	$3d^6 - 3d^5(a^2D)4p$	$a^{3}P - {}^{1}D^{\circ}$	1 - 2		922
	170	356 860	26 1530 - 306 3778	$3d^6 - 3d^5(a^4D)4n$	$a^{3}\mathbf{P} = {}^{3}\mathbf{P}^{\circ}$	2_2		922
	330	356 876	33 2565 - 313 4647	$3d^6 - 3d^5(a^4F)4n$	$a^3G - {}^5G^{\circ}$	5-5		922
	550	550.070	33.2303 - 313.4047	54 - 54 (41),p				
	30	356.957	34.4164 - 314.5628	3d ⁶ – 3d ⁵ (a ⁴ F)4p	a ³ G – ⁵ F°	3 - 3		922
	650	357.371	27.5782 - 307.3997	$3d^{6} - 3d^{5}(a^{2}I)4p$	$a^{3}H - {}^{3}I^{\circ}$	5-6		922
	230	357.550	26.1530 - 305.8381	$3d^{6} - 3d^{5}(a^{4}D)4p$	$a^{3}P - {}^{3}P^{\circ}$	2 - 1		922
	20	357.743	41.2522 - 320.7831	3d ⁶ – 3d ⁵ (a ² H)4p	$a^{1}I - {}^{3}I^{\circ}$	6 - 7		922
	400	357.822	29.1237 - 308.5920	$3d^{6} - 3d^{5}(a^{2}D)4p$	$a^{3}F - {}^{3}F^{\circ}$	4 - 3		922
	110	357.897	34.0617 - 313.4647	3d ⁶ – 3d ⁵ (a ⁴ F)4p	a ³ G - ⁵ G°	4 - 5		922
	110	167.021	41 6360 331 0103	246 246	30 300			022
	130	357.921	41.0209 - 321.0183	30° – 30° (a°G)4p	a D - F	2 - 2	1	922
	160	357.946	29.5708 - 308.9430	$3d^{\circ} - 3d^{3}(a^{2}D)4p$	a ^s F – 'D'	3 - 2		927
	360	358.014	41.7011 - 321.0183	3d ⁶ – 3d ⁵ (a ² G)4p	a'D - 'F°	1 – 2		922
	50	358.142	34.0617 - 313.2813	3d ⁶ - 3d ⁵ (a ⁴ F)4p	a ³ G - ⁵ G°	4 - 4		927
	370	358.248	41.9202 - 321.0564	3d ⁶ - 3d ⁵ (a ² G)4p	$a^{3}D - {}^{3}F^{\circ}$	3 - 4		922
	100	358.368	29.8992 - 308.9430	3d ⁶ - 3d ⁵ (a ² D)4p	a ³ F - ¹ D°	2 – 2		922
	140	358 206	29 5708 - 308 5920	3d ⁶ - 3d ⁵ (a ² D)4n	a ³ E, ³ E ^o	3 2		922
	70	358 502	27.1112 204.0400	$3d^6 = 3d^5(a^{2}I)A_{\pi}$	a1 - F	6 4		922
	600	336.303	27.1112 - 300.0490	50 - 50 (a-1)4p		6-5		922
	690	358.570	27.1112 - 305.9963	30" - 30"(a*1)4p	aH-K	0-7		927
	680	358.583	42.2081 - 321.0819	30° – 30°(a°F)4p	a'G - 'F'	4-3		922
	530	358.618	42.2081 - 321.0564	3d° - 3d3(a2G)4p	a'G - 'F'	4-4		922
	260	358.742	33.2565 - 312.0083	3d" - 3d'(a'F)4p	a'G - 'G'	5-4		922
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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	60	358.819	29.8992 - 308.5920	3d° - 3d°(a2D)4p	a ³ F - ³ F°	2 - 3		922
	260	358.927	41.2522 - 319.8604	$3d^{6} - 3d^{5}(a^{2}H)4p$	$a^{1}I - {}^{3}I^{\circ}$	6-6		922
	120	358.944	41.9202 - 320.5138	$3d^6 - 3d^5(a^2G)4p$	a ³ D - ³ F°	3 - 3		922
	240	359.020	34.4164 - 312.9536	$3d^{6} - 3d^{5}(a^{2}F)4p$	$a^{3}G - {}^{3}D^{\circ}$	3 - 3		922
	380	359 047	48.6070 - 327.1227	$3d^{6} - 3d^{5}(b^{2}F)4p$	$a^{1}D - {}^{1}D^{\circ}$	2 - 2		922
	190	359,101	34.4164 - 312.8894	3d ⁶ – 3d ⁵ (a ⁴ F)4p	a ³ G - ⁵ G°	3 - 3		927
	150	359.194	34.0617 - 312.4633	$3d^{6} - 3d^{5}(a^{2}F)4p$	a'G - 'G°	4 - 3		922
	150	359.316	42.2081 - 320.5138	3d° - 3d°(a ² G)4p	a'G - 'F'	4 - 3		922
	70	359.420	41.7011 - 319.9265	3d° - 3d³(a²F)4p	a'D - 'D'	1 - 2		922
	660	359.467	27.8588 - 306.0490	$3d^{\circ} - 3d^{\circ}(a^{2}I)4p$	a'H - 'I'	4 - 5		922
	330	359.505	29.5708 - 307.7311	$3d^{6} - 3d^{5}(a^{2}D)4p$	a'F - 'F°	3 - 2		922
	330	359.542	48.6070 - 326.7390	3d° - 3d ⁵ (a²G)4p	a'D - 'F°	2 - 3		922
	580	359.696	27.5782 - 305.5908	3d ⁶ - 3d ⁵ (a ² I)4p	a ³ H - ³ K°	5-6		922
	260	359.720	41.6269 - 319.6202	$3d^{6} - 3d^{5}(a^{4}F)4p$	a ³ D - ³ G°	2 - 3		922
	170	359.737	41.9202 - 319.8991	3d ⁶ - 3d ⁵ (a ⁴ F)4p	a ³ D - ³ G°	3 - 4		922
	350	359 781	34 0617 - 312 0083	$3d^6 - 3d^5(a^2F)4p$	a ³ G - ¹ G°	4-4		922
	140	359 967	69 1561 - 346 9595	$3d^6 - 3d^5(b^2D)4p$	$b^{3}P - {}^{3}P^{\circ}$	2 - 1		922
	350	360.028	69.1561 - 346.9124	$3d^6 - 3d^5(b^2D)4p$	$b^{3}P - {}^{3}P^{\circ}$	2 - 2		922
					10.100			
	220	360.112	42.2081 - 319.8991	3d° - 3d°(a'F)4p	a'G - 'G'	4-4		922
	60	360.242	34.4164 - 312.0083	3d° – 3d'(a ⁻ F)4p	a'G - 'G'	3-4		922
	410	360.474	42.2081 - 319.6202	3d° - 3d³(a³F)4p	a'G - 'G"	4 – 3		922
	270	360.726	41.9202 - 319.1387	3d° - 3d ⁵ (a ² G)4p	$a^{3}D - {}^{1}G^{\circ}$	3 - 4		927
	90	360.827	28.6976 - 305.8381	3d° - 3d ⁵ (a4D)4p	a ³ P - ³ P°	1 - 1		922
	550	360.886	26.1530 - 303.2495	3d° - 3d ⁵ (a ⁴ P)4p	a ³ P - ³ S°	2 - 1		922
	550	361,101	42.2081 - 319.1387	3d ⁶ – 3d ⁵ (a ² G)4p	a'G - 'G°	4 - 4		922
	580	361.266	57.9241 - 334.7276	$3d^{6} - 3d^{5}(b^{2}F)4p$	a'F - 'F"	3-3		922
	80	361 349	66.7378 - 343.4782	$3d^6 - 3d^5(b^2D)4p$	$b^{3}P - {}^{3}D^{\circ}$	0 - 1		922
	70	361 416	28 6976 - 305 3869	$3d^{\circ} - 3d^{\circ}(a^{\circ}D)4p$	$a^{3}P - {}^{3}P^{\circ}$	1-0		927
	140	361.450	33 2565 - 309 9195	$3d^{\circ} - 3d^{\circ}(a^{2})4p$	$a^{3}G - {}^{3}H^{\circ}$	5-5		922
	110	361.526	48.6070 - 325.2119	3d ⁶ – 3d ⁵ (a ² G)4p	a'D - ³ G°	2 - 3		922
			(7.5.170, 3.13.0057	2.15 - 2.15/1.2014-		1		022
	170	361.851	67.5479 - 343.9057	3d" - 3d'(b'D)4p	$\mathbf{D}^{\mathbf{P}} - \mathbf{D}^{\mathbf{r}}$	1-2		922
	70	362.058	29.6400 - 305.8381	3d" - 3d'(a'D)4p	$a^{3}P - P^{3}$	0-1		922
	130	362.120	34.0617 - 310.2126	3d" – 3d (a-D)4p		4-4		922
	550	362.219	68.7187 - 344.8053	3d" - 3d'(b ² D)4p	$\mathbf{b}\mathbf{F} - \mathbf{D}^{*}$	4-3		922
	590	362.309	33.2565 - 309.2640	3d" - 3d'(a-1)4p	a'G - 'H'	5-0		922
	560	362.506	34.0617 - 309.9195	3d" - 3d (a-1)4p	a'G - 'H'	4-5		922
	280	362.654	104.4205 - 380.1656	3d [*] - 3d ⁵ (a ² P)4p	$\mathbf{b}^{T}\mathbf{D} - {}^{T}\mathbf{P}^{*}$	2 - 1		922
	220	362.779	69.1561 - 344.8053	3d ⁶ – 3d ⁵ (b ² D)4p	b'P - 'D°	2 - 3		922
	530	362.928	34.4164 - 309.9525	3d ⁶ - 3d ⁵ (a ² I)4p	a ³ G - ³ H°	3 - 4		922
	40	363.043	77.8995 - 353.3471	3d ⁶ – 3d ⁵ (b ² G)4p	b ¹ G - ³ F [•]	4 – 4		922
	20	363.182	67.5479 - 342.8946	3d ⁶ - 3d ⁵ (b ² D)4p	b ³ P - ³ F °	1 - 2		922
	50	363.309	48.6070 - 323.8531	3d* - 3d ⁵ (a*F)4p	$a^1D - {}^3F^\circ$	2 - 2		922
	340	363 541	57 9241 - 332 0056	$3d^{6} - 3d^{5}(a^{2}H)4n$	a'F-'G'	3-4		922
	60	363 569	68 8547 - 343 9057	$3d^{6} = 3d^{5}(h^{2}D)4n$	$b^3F - ^3D^2$	3_2		922
	20	363.900	68 6321 - 343 4792	$3d^{6} = 3d^{5}(h^{2}D)4h$	$h^3 F = ^3 D^2$	2 - 1		922
	20	263.039	34 0617 - 308 2041	$3d^6 = 3d^5(a^2I)4n$	a ³ G - ¹ H°	4_5		922
	00	364.050	42 2081 - 216 9979	$3d^{6} = 3d^{5}(a^{2}H)4n$	a'G - 'G'	4_4		922
	20	364.094	41.6269 - 316.2803	$3d^{\circ} - 3d^{\circ}(a^{2}F)4p$	$a^{3}D - {}^{3}F^{\circ}$	2 - 3		922
					in ice			000
	360	364.229	28.6976 - 303.2495	3d° – 3d'(a*P)4p	a'P - 'S'	1-1		922
	160	364.262	34.0617 - 308.5920	3d" - 3d'(a ² D)4p	a G - F	4-3		922
	20	364.345	41.7011 - 316.1654	3d° - 3d'(a ² F)4p	a'D - 'F°	1 - 2		922
	50	364.485	41.9202 - 316.2803	$3d^{\circ} - 3d^{\circ}(a^{2}F)4p$	a 'D - 'F°	3 - 3		922
	240	364.773	33.2565 - 307.3997	$3d^{\circ} - 3d^{\circ}(a^{2}I)4p$	a 'G - 'I°	5-6		922
	120	364.797	69.1561 - 343.2810	3d ⁶ – 3d ⁵ (b ² D)4p	b'P - 'F°	2 - 3		922
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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	110	364.867	26.1530 - 300.2249	3d° - 3d ⁵ (a ⁴ D)4p	$a^{3}P - {}^{3}D^{\circ}$	2 - 2		922
	340	364.899	26.1530 - 300.2010	$3d^6 - 3d^5(a^4D)4p$	$a^{3}P - {}^{5}P^{\circ}$	2-3		922
	50	365,148	42.2081 - 316.0688	$3d^6 - 3d^5(a^2F)4p$	a'G - 'G°	4 - 4		922
	100	365.189	48.6070 - 322.4364	$3d^{6} - 3d^{5}(a^{4}F)4p$	$a^{1}D - {}^{3}D^{\circ}$	2 - 2		922
	60	365 363	41 6269 - 315 3262	$3d^6 - 3d^5(a^2D)4n$	$a^{3}D - {}^{1}F^{\circ}$	2 - 3		922
	80	365 410	41.3269 - 315.3262 41.7011 - 315.3661	$3d^6 - 3d^5(a^2E)4n$	$a^3D - {}^3D^\circ$	1-2		922
		305.410	41.7011 - 515.5001	54 54 (41)49				,
	190	365.485	29.6400 - 303.2495	3d ⁶ - 3d ⁵ (a ⁴ P)4p	$a^{3}P - {}^{3}S^{\circ}$	0 – 1		922
	180	366.085	42.2081 - 315.3701	3d° - 3d ⁵ (a ² G)4p	a'G - 'H°	4 - 4		922
	620	366.113	41.2522 - 314.3920	3d ⁶ - 3d ⁵ (a ² I)4p	a'I – 'I°	6 - 6		922
	80	366.386	41.6269 - 314.5628	3d ⁶ - 3d ⁵ (a ⁴ F)4p	a ³ D - ⁵ F°	2 – 3		922
	140	366.541	26.1530 - 298.9723	3d ⁶ − 3d ⁵ (a ⁴ D)4p	a'P - 'D°	2 – 3		922
	410	367.005	48.6070 - 321.0819	$3d^{6} - 3d^{5}(a^{2}F)4p$	$a^{1}D - {}^{1}F^{\circ}$	2 - 3		922
	30	367.093	48.6070 - 321.0183	$3d^6 - 3d^5(a^2G)4p$	$a^{1}D - {}^{3}F^{\circ}$	2 - 2		922
	150	367 182	291237 = 3014702	$3d^6 - 3d^5(a^4D)4n$	$a^3 \mathbf{F} - {}^3 \mathbf{F}^\circ$	4 - 3		922
	280	367 258	419202 - 3142088	$3d^6 - 3d^5(a^2E)4n$	$a^{3}D - {}^{3}F^{\circ}$	3-4		922
	110	367 567	41.5262 - 313.6866	$3d^{6} - 3d^{5}(a^{2}D)4n$	$a^3D - {}^3D^\circ$	2_2		922
	130	367 648	41.0209 = 313.0000	$3d^6 = 3d^5(a^2D)4p$	$a^{3}D = D^{2}$	3_3		922
	130	307.040	41.9202 - 313.9198	$3d^{0} - 3d^{2}(a^{2}I)An$		1 5		022
	120	307.004	54.0017 - 500.0490	50 – 50 (a 1) 4 p	a 0 - 1	4-5		922
	90	367.778	29.5708 - 301.4702	$3d^{6} - 3d^{5}(a^{4}D)4p$	$a^{3}F - {}^{3}F^{\circ}$	3 - 3		922
	50	367.826	28.6976 - 300.5633	3d ⁶ - 3d ⁵ (a ⁴ D)4p	$a^{3}P - {}^{3}D^{\circ}$	1 – 1		922
	130	367.923	29.1237 - 300.9181	$3d^{6} - 3d^{5}(a^{4}D)4p$	$a^{3}F - {}^{3}F^{\circ}$	4 - 4		922
	50	368.037	42.2081 - 313.9198	$3d^{6} - 3d^{5}(a^{2}D)4p$	$a^{1}G - {}^{3}D^{\circ}$	4 – 3		922
	20	368.115	29.8992 - 301.5530	$3d^{6} - 3d^{5}(a^{4}D)4p$	$a^{3}F - {}^{3}F^{\circ}$	2 - 2		922
	320	368.286	28.6976 - 300.2249	$3d^6 - 3d^5(a^4D)4p$	a ³ P - ³ D°	1 - 2		922
	420	260.406	47 (007 210 0724		ale inº			011
	420	308.490	47.0997 - 319.0734	3d - 3d (a D) + p				922
	580	308.309	48.6070 - 319.9265	30" - 30"(a"F)4p		2-2		922
	40	368.641	26.1530 - 297.4181	3d" - 3d"(a*P)4p	$a^{3}P - D^{2}$	2-3		922
	510	368.898	29.1237 - 300.2010	$3d^{\circ} - 3d^{\circ}(a^{*}D)4p$	$a^{3}F - P^{2}$	4-3		927
	90	368.958	41.9202 - 312.9536	3d" – 3d"(a²F)4p	$a^{\prime}D - D^{\prime}$	3-3		922
	230	368.986	48.6070 - 319.6202	3d° - 3d°(a°F)4p	a'D - 'G'	2 - 3		922
	150	369.108	29.6400 - 300.5633	3d ⁶ - 3d ⁵ (a ⁴ D)4p	$a^{3}P - {}^{3}D^{\circ}$	0 - 1		922
	80	369.192	26.1530 - 297.0139	$3d^{6} - 3d^{5}(a^{4}D)4p$	$a^{3}P - {}^{5}D^{\circ}$	2 – 2		922
	150	369.226	41.6269 - 312.4633	$3d^6 - 3d^5(a^2F)4p$	$a^{3}D - G^{\circ}$	2 – 3		922
	210	369.475	29.5708 - 300.2249	3d° - 3d ⁵ (a ⁴ D)4p	$a^{3}F - {}^{3}D^{\circ}$	3 - 2		922
	120	369.508	29.5708 - 300.2010	$3d^{6} - 3d^{5}(a^{4}D)4p$	a ³ F - ⁵ P°	3 – 3		922
	80	369.562	41.7011 - 312.2910	$3d^{6} - 3d^{5}(a^{2}D)4p$	$a^{3}D - {}^{3}P^{\circ}$	1 – 1		922
	120	369 733	48 6070 - 319 0734	$3d^6 = 3d^5(s^2D)4p$	a ¹ D - ¹ P°	2_1		922
	70	369 906	41 6269 - 311 9665	$3d^6 = 3d^5(a^2D)4n$	$a^3D = {}^3P^{\circ}$	2 . 2		922
	40	369 925	29 8992 - 300 2249	$3d^{6} = 3d^{5}(a^{4}D)4p$	$a^{3}E = {}^{3}D^{\circ}$	2 2		922
	60	370 021	42 2081 - 312 4633	$3d^6 = 3d^5(a^2E)4n$	2 ¹ G - ³ G*	4 - 3		922
	700	370.616	27 1112 - 296 9329	$3d^6 - 3d^5(e^4G)4n$	2H-G	6-5		922
	220	370.975	27.8588 - 297.4181	$3d^6 - 3d^5(a^4P)4p$	$a^{3}H - {}^{3}D^{\circ}$	4 - 3		922
)			
	290	371.091	29.5708 - 299.0456	3d° - 3d3(a*D)4p	a'F - 'P'	3 - 2		922
	590	371.275	27.5782 – 296.9193	3d° - 3d°(a4D)4p	a'H - 'D'	5 – 4		927
	670	371.306	27.5782 - 296.8970	3d° - 3d5(a4G)4p	a'H - 'G'	5 - 4	1	922
	330	371.473	57.9241 - 327.1227	3d ⁶ - 3d ⁵ (b ² F)4p	$a^{1}F \sim D^{\circ}$	3 - 2		922
	100	371.543	29.8992 - 299.0456	$3d^{6} - 3d^{5}(a^{4}D)4p$	a ³ F - ⁵ P°	2 – 2		922
	120	371.643	29.8992 - 298.9723	3d° - 3d ⁵ (a ⁴ D)4p	a ³ F - ³ D°	2 – 3		922
	680	371.763	27.8588 ~ 296.8471	3d° - 3d ⁵ (a4G)4p	a ³ H - ³ G°	4-3		922
	250	371.812	29,6400 - 298,6006	$3d^{6} - 3d^{5}(a^{4}P)4n$	$a^{3}P - {}^{3}D^{\circ}$	0-1		922
	430	372,002	57.9241 - 326.7390	$3d^{6} - 3d^{5}(a^{2}G)4n$	a ¹ F - ¹ F°	3-3		922
	390	372,159	29.8992 - 298.6006	$3d^6 = 3d^5(a^4P)4n$	$a^3 \mathbf{F} - {}^3 \mathbf{D}^\circ$	2 - 1		922
	610	372 451	41 2522 - 309 7436	$3d^{6} - 3d^{5}(a^{2}I)\Delta n$	a ¹ I - ¹ K°	6-7		922
	620	372 774	29 1237 . 297 4181	$3d^{6} - 3d^{5}(a^{4}D)An$	$a^{3}F = {}^{3}D^{\circ}$	4_1		922
	020	512.127	27.1257 277.4101	50 - 50 (a r)+p		3		766

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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	Reference
	560	372.756	29.5708 - 297.8425	3d ⁶ - 3d ⁵ (a ⁴ P)4p	$a^{3}F - {}^{3}D^{\circ}$	3 - 2		922
	300	372.987	57.9241 - 326.0299	3d ⁶ – 3d ⁵ (b ² F)4p	$a^{1}F - {}^{3}F^{\circ}$	3 – 3		922
	410	373.018	29.8992 - 297.9828	3d ⁶ - 3d ⁵ (a ⁴ D)4p	a ³ F - ⁵ P°	2 – 1		922
	230	373.083	77.8995 - 345.9361	3d ⁶ – 3d ⁵ (b ² D)4p	b ¹ G - ¹ F°	4 – 3		927
	170	373.213	29.8992 - 297.8425	3d ⁶ - 3d ⁵ (a ⁴ P)4p	$a^{3}F - {}^{3}D^{\circ}$	2 - 2		922
	140	373.347	29.5708 - 297.4181	3d ⁶ - 3d ⁵ (a ⁴ P)4p	a ³ F - ³ D°	3 – 3		922
	540	373.401	29.1237 - 296.9329	3d ⁶ - 3d ⁵ (a ⁴ G)4p	a ³ F - ³ G°	4 - 5		922
	270	373.418	29.1237 - 296.9193	3d ⁶ - 3d ⁵ (a ⁴ D)4p	a ³ F - ⁵ D°	4 - 4		927
	140	373.449	29.1237 - 296.8970	3d ⁶ – 3d ⁵ (a ⁴ G)4p	a ³ F - ³ G°	4 – 4		922
	220	373.521	234.4127 - 502.137	3d5(a4F)4s - 3d5(abS)5f	5 F – 5 F °	2 - 3		922
	230	373.536	42.2081 - 309.9195	$3d^6 - 3d^5(a^2I)4p$	a'G – ³ H°	4 - 5		922
	670	373.605	33.2565 - 300.9181	3d ⁶ - 3d ⁵ (a ⁴ D)4p	a ³ G - ³ F°	5 – 4		922
	400	373.644	57.9241 - 325.5586	3d° - 3d ⁵ (b²F)4p	$a^{1}F - {}^{1}G^{\circ}$	3 - 4		922
	180	373,690	47.6997 - 315.3007	$3d^{6} - 3d^{5}(a^{2}F)4p$	$a^{i}S - {}^{3}D^{\circ}$	0-1		922
	390	373,760	41.2522 - 308.8041	$3d^{6} - 3d^{5}(a^{2}I)4p$	a'I – 'H°	6 - 5		922
	400	373,804	29.8992 - 297.4179	$3d^{6} - 3d^{5}(a^{4}D)4p$	a ³ F - ⁵ D°	2 - 1		922
	370	373,903	29.1237 - 296.5740	$3d^{6} - 3d^{5}(a^{4}D)4p$	a ³ F - ⁵ D°	4 - 3		922
	640	373.960	34.0617 - 301.4702	3d ⁶ - 3d ⁵ (a ⁴ D)4p	a ³ G - ³ F°	4 – 3		922
	300	374 045	29 5708 - 296 9193	3d⁵ – 3d⁵(a⁴D)4n	$a^{3}F - {}^{5}D^{\circ}$	3-4		927
	640	374.075	29 5708 - 296 8970	3d ⁶ - 3d ⁵ (a ⁴ G)4n	$a^{3}F - {}^{3}G^{\circ}$	3-4		922
	500	374 159	261530 - 2934200	$3d^6 - 3d^5(a^4P)4p$	$a^{3}P - {}^{3}P^{\circ}$	2 - 1		922
	620	374 340	344164 - 3015530	$3d^6 - 3d^5(a^4D)4p$	$a^{3}G - {}^{3}F^{\circ}$	3-2		922
	210	374.540	34,4164 = 301,6550	$3d^{6} - 3d^{5}(a^{4}D)4p$	$a^3G - {}^3F^\circ$	3-3		922
	240	374.581	41.6269 - 308.5920	$3d^{6} - 3d^{5}(a^{2}D)4p$	$a^{3}D - {}^{3}F^{\circ}$	2 - 3		922
	480	374 604	29 8992 - 296 8471	3d ⁶ - 3d ⁵ (a ⁴ G)4n	$a^{3}F - {}^{3}G^{\circ}$	2-3	}	922
	130	374.004	34 0617 - 300 9181	$3d^6 = 3d^5(a^4D)4p$	$a^3G - {}^3F^\circ$	4 - 4		922
	500	374.770	26 1530 - 292 9830	$3d^6 = 3d^5(a^4P)4p$	$a^{3}P - {}^{3}P^{\circ}$	2 - 2		922
	50	374.770	48 6070 - 315 3007	$3d^{\circ} = 3d^{\circ}(a^{2}F)4p$	$a^{\dagger}D = {}^{3}D^{\circ}$	2 - 1		922
	10	374.903	41,0202 308 5020	$3d^6 - 3d^5(a^2D)4p$	$a^{3}D - {}^{3}F^{\circ}$	3_3		922
	580	375.100	42.2081 - 308.8041	$3d^{\circ} - 3d^{\circ}(a^{2}I)4p$	$a^{1}G - {}^{1}H^{\circ}$	4 - 5		922
	20	375 733	41 2522 - 307 3997	3d ⁶ – 3d ⁵ (a ² I)4p	a'I - ³ I°	6-6		922
	160	375 898	41.2522 = 307.3577 41.7011 = 307.7311	$3d^6 - 3d^5(a^2D)4p$	$a^{3}D - {}^{3}F^{\circ}$	1-2		922
	20	376 119	68 8547 - 334 7276	$3d^6 = 3d^5(h^2 E) 4n$	$\mathbf{b}^{3}\mathbf{F} - \mathbf{F}^{\circ}$	3-3		922
	70	376 211	34 4164 300 2249	$3d^{6} = 3d^{5}(a^{4}D)4p$	a ³ G - ³ D°	3-2		922
	20	376 500	57 0241 223 5232	$3d^6 - 3d^5(a^4F)4p$	$a^{\dagger}F = {}^{3}F^{\circ}$	3_3		922
	110	376.810	28.6976 - 294.0860	$3d^{\circ} - 3d^{\circ}(a^{4}D)4p$	a ³ P – ⁵ F°	1 - 2		922
	110	377 015	27 1112 - 292 3534	3d ⁶ - 3d ⁵ (a ⁴ G)4n	a ³ H - ³ H°	6-5		922
	240	377 117	28 6976 - 293 8670	$3d^6 - 3d^5(a^4P)4p$	$a^{3}P - {}^{3}P^{\circ}$	1-0		922
	20	377 251	48 6070 - 313 6866	$3d^6 - 3d^5(a^2D)4p$	$a^1D - {}^3D^\circ$	2 - 2		922
	60	377 283	27 5782 - 292 6310	$3d^6 - 3d^5(a^4G)4p$	$a^{3}H - {}^{3}H^{\circ}$	5-4		922
	100	377 486	34 0617 - 298 9723	$3d^6 - 3d^5(a^4D)4p$	$a^{3}G - {}^{3}D^{\circ}$	4 - 3		922
	290	377.646	41.2522 - 306.0490	$3d^{\circ} - 3d^{\circ}(a^{2}I)4p$	$a^{3}I - {}^{3}I^{\circ}$	6 - 5		922
	720	377 676	27 1112 - 291 8914	3d ⁶ - 3d ⁵ (a⁴G)4n	a ³ H – ³ H°	6-6		922
	320	377 713	41 6269 - 306 3778	$3d^6 - 3d^5(a^4D)4n$	$a^{3}D - {}^{3}P^{\circ}$	2 - 2		927
	220	377 754	28 6976 - 293 4200	$3d^6 - 3d^5(a^4P)4p$	$a^{3}P - {}^{3}P^{\circ}$	1-1		922
	50	377.794	57 9241 - 322 6176	$3d^{6} - 3d^{5}(a^{4}F)4p$	$a^{1}F - {}^{3}D^{\circ}$	3-3		922
	70	378 054	57 9241 - 322 4364	$3d^{6} = 3d^{5}(a^{4}F)4n$	$a^{1}F - {}^{3}D^{\circ}$	3-2		922
	520	378.133	41.9202 - 306.3778	$3d^{\circ} - 3d^{\circ}(a^{\circ}D)4p$	$a^{3}D - {}^{3}P^{\circ}$	3 - 2		922
	100	278 270	28 6076 . 202 0820	3d6 - 3d5(24D)4r	$a^{3}P = {}^{3}P^{\circ}$	1-2		922
	190	378.379	20.09/0 - 292.9830	3d - 3d (a r)4p	a ³ D ³ P ⁰	1 - 2 2 - 1		922
	3/0	378.483	41.0209 - 303.8381	3d - 3d(a D) + p $3d^{6} - 2d^{5}(a^{4}D) + d^{-1}$	aD - F	1 1		922
	150	378.591	41./011 - 303.8381	3u - 3u (a D) + p		5 4		022
	40	378.820	27.5782 - 291.5546	$30^{\circ} - 30^{\circ}(a^{\circ}C)4p$		1 4		022
	310	379.018	42.2081 - 306.0490	$30^{\circ} - 30^{\circ}(a^{-1})4p$	a G - T	4-5		922
	160	379.104	29.6400 - 293.4200	30° - 30°(a*P)4p	ar-r	0-1		922
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$\mathbf{NI} \; \mathbf{V} - \mathbf{Continued}$

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	190	379.225	27.8588 – 291.5546	3d ⁶ - 3d ⁵ (a ⁴ G)4p	a ³ H - ³ F°	4 - 4		922
	560	379.252	33.2565 - 296.9329	$3d^6 - 3d^5(a^4G)4p$	a ³ G - ³ G°	5-5		927
	80	379.497	29.1237 - 292.6310	$3d^6 - 3d^5(a^4G)4p$	$a^{3}F - {}^{3}H^{\circ}$	4 - 4		922
	70	379.550	27.8588 - 291.3285	$3d^6 - 3d^5(a^4G)4p$	$a^{3}H - {}^{3}F^{\circ}$	4 - 3		922
	40	379.895	29.1237 - 292.3534	$3d^6 - 3d^5(a^4G)4p$	$a^{3}F - {}^{3}H^{\circ}$	4 - 5		922
	30	380.037	57 9241 - 321 0564	$3d^6 - 3d^5(a^2G)4p$	$a^{1}F - {}^{3}F^{\circ}$	3-4	1	922
	50	560.057	57.5241 - 521.0504	50 - 50 (a C)+p		5-4)11
	20	380.141	29.5708 - 292.6310	3d ⁶ - 3d ⁵ (a ⁴ G)4p	a ³ F - ³ H°	3 – 4		922
	270	380.417	34.0617 – 296.9329	3d° - 3d°(a⁺G)4p	a'G - 'G°	4 - 5		922
	330	380.433	34.0617 - 296.9193	3d ⁶ - 3d ⁵ (a ⁴ D)4p	a ³ G - ⁵ D°	4 - 4		927
	370	380.467	34.0617 - 296.8970	3d ⁶ - 3d ⁵ (a ⁴ G)4p	a ³ G - ³ G°	4 - 4	}	922
	220	380.626	66.7378 - 329.4623	3d ⁶ - 3d ⁵ (b ² F)4p	$b^{3}P - {}^{3}D^{\circ}$	0 - 1	ļ	927
	140	380.920	69.1561 - 331.6782	$3d^{6} - 3d^{5}(a^{2}S)4p$	$b^{3}P - {}^{3}P^{\circ}$	2 – 2		922
	60	380 048	34 4164 - 296 9193	$3d^{6} = 3d^{5}(a^{4}D)4p$	aiG - ⁱ D°	3_4		927
		200.001	24 4164 206 9070	3d = 3d (a D) + p		2 4		027
	60	360.981	34.4104 - 290.8970	50 - 50 (a C)4p		3-4]	922
	620	381.052	29.1237 - 291.5546	3d° - 3d°(a°G)4p	a [°] F - [°] F	4-4		922
	210	381.346	67.5479 - 329.7763	3d ^a – 3d ^a (b ^a F)4p	$\mathbf{b} \mathbf{P} - \mathbf{D}^{*}$	1 - 2		922
	130	381.380	29.1237 - 291.3285	3d° - 3d°(a⁴G)4p	a'F - 'F°	4 – 3		922
	20	381.577	67.5479 - 329.6185	$3d^6 - 3d^5(a^2S)4p$	$b^{3}P - {}^{3}P^{\circ}$	1 - 0		927
	400	381.678	68.7187 - 330.7181	$3d^6 - 3d^5(b^2F)4p$	$b^{3}F - {}^{3}G^{\circ}$	4 - 5		922
	130	381 702	29 5708 - 291 5546	$3d^6 - 3d^5(a^4G)4n$	$a^{3}E - {}^{3}E^{\circ}$	3-4		922
	500	382 032	29.5708 291.3340	$3d^6 - 3d^5(a^4G)Ap$	$a^3 F = {}^3 F^{\circ}$	3_3		022
	20	382.032	22.5708 - 221.5285	$3d^6 - 3d^8(a^4D)4\pi$	al - I	5 1		922
	30	382.142	53.2303 - 294.9390	$3d^2 - 3d^2(a^2D)4p$	a'G-F	5-4		922
	20	382.294	68./18/ - 330.29/6	3d° – 3d°(b°F)4p	b'F - 'G'	4-4		922
	170	382.370	29.5708 - 291.0977	3d° – 3d°(a*G)4p	$a^{3}F - {}^{3}F^{3}$	3 – 2		922
	310	382.493	68.8547 - 330.2976	$3d^{6} - 3d^{5}(b^{2}F)4p$	$b^{3}F - {}^{3}G^{\circ}$	3 - 4		922
	160	382.509	29.8992 - 291.3285	3d ⁶ – 3d ⁵ (a ⁴ G)4p	$a^{3}F - {}^{3}F^{\circ}$	2 - 3		922
	120	382.788	68.6321 - 329.8729	$3d^{6} - 3d^{5}(b^{2}F)4p$	$b^{3}F - {}^{3}D^{\circ}$	2 - 3		922
	240	382.827	57.9241 - 319.1387	$3d^6 - 3d^5(a^2G)4p$	$a^{\dagger}F - {}^{\dagger}G^{\circ}$	3-4		922
	480	382.849	29.8992 - 291.0977	$3d^6 - 3d^5(a^4G)4p$	$a^{3}F - {}^{3}F^{\circ}$	2 - 2		922
	90	382.914	68.7187 - 329.8729	$3d^{6} - 3d^{5}(b^{2}F)4p$	b ³ F - ³ D°	4 - 3		922
	80	202 147	69 6221 220 6142	2.46 2.45(1.275).4-	LID 3C*			000
	80	383.107	08.0321 - 329.0143	3d" - 3d'(b"F)4p	0'F - 'G	2-3		922
	30	383.255	68.8547 - 329.7763	3d° – 3d°(b°F)4p	b'F - 'D'	3 - 2		922
	50	383.293	68.7187 – 329.6143	$3d^{\circ} - 3d^{\circ}(b^{2}F)4p$	b'F - 'G"	4 - 3		922
	20	383.496	68.8547 – 329.6143	3d° – 3d°(b²F)4p	b'F – 'G°	3 – 3		922
	230	383.557	69.1561 – 329.8729	3d ⁶ – 3d ⁵ (b ² F)4p	$b^{3}P - {}^{3}D^{\circ}$	2 – 3		922
	70	383.826	27.1112 – 287.6459	$3d^{6} - 3d^{5}(a^{4}G)4p$	a'H – ⁵ H°	6 - 6		927
	220	383.938	69.1561 - 329.6143	3d ⁶ – 3d ⁵ (b ² F)4p	$b^{3}P - {}^{3}G^{\circ}$	2 - 3		922
	70	384,594	27.1112 - 287.1280	$3d^6 - 3d^5(a^4G)4n$	$a^{3}H - {}^{5}H^{\circ}$	6-5		972
	20	385 245	67 5479 - 327 1227	$3d^6 - 3d^5(h^2 E)4n$	$h^3P - D^{\circ}$	1_2		922
	70	385 283	97 5782 - 287 1280	$3d^6 - 3d^5(a^4G)An$	3H 5H	5 5		022
	20	385 010	27.5782 286.7066	$3d^6 - 3d^5(a^4G)4p$		5 1		017
	20	386.044	29.1237 - 288.1616	$3d^6 - 3d^5(a^4G)4p$	$a^{3}F - {}^{5}F^{\circ}$	4-4		927
	20	386.106	41.9202 - 300.9181	3d ⁶ – 3d ⁵ (a ⁴ D)4p	$a^{3}D - {}^{3}F^{\circ}$	3 – 4		922
	90	386.196	41.6269 - 300.5633	$3d^{6} - 3d^{5}(a^{4}D)4p$	$a^{3}D - {}^{3}D^{\circ}$	2 – 1		922
	230	386.306	41.7011 - 300.5633	3d ⁶ - 3d ⁵ (a ⁴ D)4p	a'D - 'D°	1 - 1		922
	480	386.645	33.2565 - 291.8914	$3d^6 - 3d^5(a^4G)4p$	a ³ G - ³ H°	5-6		922
	400	386.702	41.6269 - 300.2249	$3d^6 - 3d^5(a^4D)4p$	$a^{3}D - {}^{3}D^{\circ}$	2 - 2		922
	120	386.738	34.0617 - 292.6310	$3d^{6} - 3d^{5}(a^{4}G)4p$	a ³ G - ³ H°	4 - 4		922
	00	396.045	77 0500 204 2024	2.46 2.45(-400)4-	-311 5110			027
	90	300.943	27.8388 - 280.2930	30° - 30°(a°G)4p	a.H - "H"	4-3		927
	60	387.074	5/.9241 - 316.2803	3d° – 3d'(a°F)4p	a'F - 'F"	3-3		922
	580	387.154	34.0617 - 292.3534	3d° - 3d°(a*G)4p	a'G - 'H°	4 – 5		922
	530	387.176	41.9202 - 300.2010	3d° - 3d ⁵ (a4D)4p	a3D - 5P°	3 - 3		922
	340	387.274	34.4164 - 292.6310	3d ⁶ - 3d ⁵ (a ⁴ G)4p	a ³ G - ³ H°	3 – 4		922
	310	387.360	68.7187 - 326.8763	$3d^{6} - 3d^{5}(b^{2}F)4p$	$b^{3}F - {}^{3}F^{\circ}$	4 - 4		922
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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	130	387.563	68.7187 - 326.7390	3d ⁶ - 3d ⁵ (a ² G)4p	b ³ F – ¹ F °	4 - 3		922
	160	387.771	68.8547 - 326.7390	3d ⁶ – 3d ⁵ (a ² G)4p	$b^{3}F - {}^{1}F^{\circ}$	3 – 3		922
	20	388.224	29.1237 - 286.7066	3d ⁶ - 3d ⁵ (a ⁴ G)4p	a ³ F – ⁵ H°	4 – 4		927
	130	388.360	34.0617 - 291.5546	$3d^{6} - 3d^{5}(a^{4}G)4p$	a'G - 'F°	4 – 4		922
	60	388.398	27.1112 - 284.5795	3d ⁶ - 3d ⁵ (a ⁴ G)4p	a ³ H – ⁵ G°	6-6		927
	120	388.503	68.6321 - 326.0299	$3d^{6} - 3d^{5}(b^{2}F)4p$	b ³ F - ³ F°	2 - 3		922
	360	200 576	68 6321 325 0822	$3d^{6} = 3d^{5}(h^{2}E)4n$	$h^3 F = {}^3 F^{\circ}$	2_2		977
	360	366.370	06.0521 - 525.9622	$3d^{6} = 3d^{5}(a^{4}G)Ap$	$a^3G = F^{\circ}$	4 - 3		922
	280	300.702	54.0017 - 291.3265	$3d^6 = 3d^8(h^2E)/(h^$		2 2		922
	210	388.841	08.8347 - 320.0299	3d = 3d (0 T) + p $3d^{6} = 3d^{5}(a^{4}D) + p$	$D = D^{\circ}$	3-3		922
	240	389.026	41.9202 - 298.9723	3d = 3d (a D)4p		3-3		922
	100	389.239	34.4164 - 291.3285	3d = 3d (a C)/4p		3 - 3		922
	80	389.239	41.7011 - 298.0000	30" - 30'(a P)4p	aD-D	1-1		922
	230	389.350	68.7187 - 325.5586	3d ⁶ - 3d ⁵ (b ² F)4p	$b^{3}F - {}^{1}G^{\circ}$	4 – 4		922
	260	389.365	77.8995 - 334.7276	3d ⁶ - 3d ⁵ (b ² F)4p	b'G – 'F°	4 – 3		927
	60	389.554	68.8547 - 325.5586	3d ⁶ – 3d ⁵ (b ² F)4p	b ³ F - ¹ G°	3 – 4		922
	250	389.588	34.4164 - 291.0977	3d ⁶ - 3d ⁵ (a ⁴ G)4p	a'G - 'F°	3 – 2		922
	160	389.855	68.7187 - 325.2229	3d ⁶ - 3d ⁵ (a ² G)4p	b'F - 'G°	4 - 4		922
	130	390.082	68.8547 - 325.2119	3d ⁶ - 3d ⁵ (a ² G)4p	b ³ F – ³ G°	3 - 3		922
		200 158	67 5470 323 8531	3d ⁶ – 3d ⁵ (a ⁴ E)4n	$h^{3}P = {}^{3}F^{\circ}$	1-2		922
	90	390.138	41 7011 207 9828	$3d^{6} = 3d^{5}(a^{4}D)4p$	$a^3D = {}^5P^{\circ}$	1 _ 1		922
	90	390.197	41.7011 - 277.9828	$3d^{0} = 3d(a^{-}D)^{4}p$		4.5		922
	180	390.220	66.7187 - 324.9802	$3d^{6} - 3d^{5}(a^{4}E)Ar$	$b^3 \mathbf{P} = {}^3 \mathbf{D}^2$	0 1		922
	150	390.249	00.7378 - 322.9843	$3d^{6} = 3d(ar)/4p$	$a^3D - {}^3D^\circ$	2 2 2		922
	90	390.296	41.0209 - 297.8423	$3d^{+} = 3d(a^{+}r)^{+}p$	aD = D $a^{3}D = {}^{3}D^{\circ}$	1 - 2		922
	30	390.410	41.7011 - 297.8425	30 - 30 (a r)4p	aD-D	1-2		922
	50	390.744	41.9202 - 297.8425	3d ⁶ - 3d ⁵ (a ⁴ P)4p	$a^{3}D - {}^{3}D^{\circ}$	3 - 2		922
	30	390.943	41.6269 - 297.4181	$3d^{6} - 3d^{5}(a^{4}P)4p$	a 'D - 'D°	2 - 3		922
	300	391.177	104.4205 - 360.0597	3d ⁶ – 3d ⁵ (b ² G)4p	b'D – 'F°	2 – 3		922
	120	391.394	41.9202 - 297.4181	3d ⁶ – 3d ⁵ (a ⁴ P)4p	$a^{3}D - {}^{3}D^{\circ}$	3 - 3		922
	130	391.487	67.5479 - 322.9845	3d ⁶ - 3d ⁵ (a ⁴ F)4p	b'P – 'D°	1 – 1		922
	230	391.816	68.6321 - 323.8531	$3d^{6} - 3d^{5}(a^{4}F)4p$	b'F – 'F°	2 – 2		922
	480	392.010	77.8995 - 332.9956	3d ⁶ - 3d ⁵ (a ² H)4p	b ¹ G – ¹ G°	4 – 4		922
	250	392,159	68.8547 - 323.8531	$3d^6 - 3d^5(a^4F)4p$	b'F - 'F°	3-2		922
	250	392.328	68.6321 - 323.5232	$3d^{\circ} - 3d^{\circ}(a^{4}F)4p$	$b^{3}F - {}^{3}F^{\circ}$	2 - 3		922
	310	392.458	68.7187 - 323.5232	$3d^6 - 3d^5(a^4F)4p$	b ³ F - ³ F °	4 - 3		922
	80	392.623	69.1561 - 323.8531	$3d^{4} - 3d^{5}(a^{4}F)4p$	$b^{3}P - {}^{3}F^{\circ}$	2 - 2		922
	370	392.659	68.8547 - 323.5232	3d ⁶ - 3d ⁵ (a ⁴ F)4p	b'F - 'F°	3 - 3		922
	100	202.124	60 1661 202 5222	246 245(a ⁴ E)4a	L'D E	2 2		022
	190	393.134	09.1501 - 325.5252	3d = 3d (a F) + p	or - r	2-3		922
	250	393.155	29.8992 - 284.2490	$3d^{0} = 3d(a^{2}G)4p$	aF = O	2-3	1	922
	100	393.211	29.8992 - 284.2133	$3d^{6} = 3d(a^{2}G)^{4}F$	$a \Gamma = 0$			927
	440	393.343	68./18/- 322.8208	3d - 3d (a r) + p		3 4		922
	240	393.373	68.7187 - 322.6176	$3d^{\circ} - 3d^{\circ}(a^{+}F)4p$ $3d^{\circ} - 3d^{\circ}(a^{+}F)4p$	a F = O $b^3 F = ^3 D^\circ$	4-3		922
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	700	393.914	0.0 - 253.8627	3d" - 3d ⁵ (a"S)4p	gaʿD - ʿP°	4 - 3		922
	130	394.005	68.6321 - 322.4364	3d ⁵ - 3d ⁵ (a ⁴ F)4p	b'F - 'D°	2 - 2	ļ	922
	180	394.070	68.8547 - 322.6176	3d° - 3d ⁵ (a ⁴ F)4p	b'F – 'D°	3 - 3		922
	660	394.313	0.8897 - 254.4956	3d° - 3d ⁵ (a°S)4p	ga'D – ^s P°	3 - 2		922
	260	394.350	68.8547 - 322.4364	3d ⁶ - 3d ⁵ (a ⁴ F)4p	b'F - 'D°	3 – 2		922
	270	394.537	69.1561 - 322.6176	$3d^{\circ} - 3d^{\circ}(a^{4}F)4p$	b ³ P - ³ D°	2 - 3		922
	520	394 641	1 4899 - 254 8850	3d ⁶ - 3d ⁵ (a ⁶ S)4p	ga ⁵ D - ⁵ P°	2 - 1		922
	920	304.910	69 1561 - 322 4364	$3d^{6} = 3d^{5}(a^{4}F)4n$	$h^{3}P - {}^{3}D^{9}$	2_2		922
	640	305 343	1 4800 - 354 4056	3d ⁶ - 3d ⁵ (a ⁶ S)4n	ea ⁵ D - ⁵ P°	2 _ 2		922
	600	375.242	0 8907 352 9437	$3d^{6} = 3d^{5}(a^{6}E)A_{2}$	$ga^{5}D = {}^{5}P^{6}$	3_2	1	922
	580	393.299	0.007/ - 200.002/	246 245(262)4-	ga D - F	0 1		922
	420	393.52/	2.0570 - 254.8850	30 - 30 (a 3)4p	ga D - F	1 1		922
	340	395.845	1.8/15 - 254.4956	30° - 30°(a°S)4p	ga D - P	1-2		922

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Multiplet	Rel. Int.	$\lambda_{\rm vac}$ (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	210	396.239	1.4899 - 253.8627	3d° - 3d ⁵ (a°S)4p	ga ⁵ D - ⁵ P°	2 - 3	1	922
	70	396.256	68.7187 - 321.0819	$3d^{6} - 3d^{5}(a^{2}F)4p$	$\mathbf{b}^{3}\mathbf{F} - \mathbf{F}^{\circ}$	4 – 3		922
	30	397.015	68.6321 - 320.5138	$3d^{6} - 3d^{5}(a^{2}G)4p$	$b^{3}F - {}^{3}F^{\circ}$	2 - 3		922
	230	398.336	68.8547 - 319.8991	$3d^6 - 3d^5(a^4F)4p$	b ³ F - ³ G°	3 - 4		922
	310	398.514	68.7187 - 319.6527	$3d^{6} - 3d^{5}(a^{4}F)4p$	$h^3F - {}^3G^\circ$	4 - 5	1	922
	410	400.588	41.9202 - 291.5546	$3d^6 - 3d^5(a^4G)4n$	$a^{3}D - {}^{3}F^{\circ}$	3-4		922
		100.200	11.7202 271.5510	50 - 50 (a C),1p	".D=1	5-4)22
	250	400.871	77.8995 - 327.3566	$3d^6 - 3d^8(a^2H)4p$	b'G - 'H°	4 - 5		922
	120	400.952	41.9202 - 291.3285	3d° – 3d°(a*G)4p	a D - F	3 - 3		922
	260	400.969	41.7011 - 291.0977	3d° – 3d`(a⁺G)4p	a'D - 'F°	1 – 2		922
	20	401.644	77.8995 – 326.8763	3d° – 3d°(b²F)4p	b'G – 'F°	4 – 4		922
	20	402.024	68.6321 - 317.3768	3d ⁶ – 3d ⁵ (a ² H)4p	$b^{3}F - {}^{3}G^{\circ}$	2 – 3		922
	210	402.515	77.8995 - 326.3371	3d ⁶ – 3d ⁵ (a ² G)4p	b'G – 'H°	4 – 5		922
	60	403.172	68.8547 - 316.8878	3d ⁶ – 3d ⁵ (a ² H)4p	b ³ F - ³ G°	3 - 4		922
	50	403.211	68.7187 - 316.7266	$3d^6 - 3d^5(a^2H)4p$	$b^3F - {}^3G^\circ$	4 - 5		922
	60	403,781	77,8995 - 325,5586	$3d^6 - 3d^5(b^2E)4p$	$h'G = G^{\circ}$	4-4		922
	20	404 954	66 7378 - 313 6790	$3d^{6} = 3d^{5}(a^{2}D)4p$	$h^3P = {}^3D^2$	0-1		922
	110	407.953	104 4205 - 349 5460	$3d^{\circ} = 3d^{\circ}(h^{2}D)4p$	מי תיא	10^{-1}		022
	80	408 443	68 8547 313 6866	$3d^{\circ} - 3d^{\circ}(0^{\circ}D)4p$	b D = D	2 - 2		922
	00	400.443	08.8547 - 515.0800	50 - 50 (a D)+p	Dr-D	3-2		922
	20	409.127	67.5479 - 311.9665	3d ⁶ – 3d ⁵ (a ² D)4p	$b^{3}P - {}^{3}P^{\circ}$	1 - 2		922
	80	409.451	68.7187 - 312.9536	$3d^{6} - 3d^{5}(a^{2}F)4p$	$b^{3}F - {}^{3}D^{\circ}$	4 - 3		922
	180	410.495	0.0 - 243.6085	$3d^{\circ} - 3d^{\circ}(a^{\circ}S)4p$	$ga^5D - P^\circ$	4 - 3		927
	220	413.321	0.8897 - 242.8370	$3d^{6} - 3d^{5}(a^{6}S)4p$	$ga^{5}D - {}^{7}P^{\circ}$	3 - 2		927
	20	414 344	14899 - 2428370	$3d^6 - 3d^5(a^6S)4n$	$ga^5D = {}^7P^\circ$	2 - 2		927
	70	418.237	68.6321 - 307.7311	3d ⁶ - 3d ⁵ (a ² D)4p	$b^{3}F - {}^{3}F^{\circ}$	2 - 2		922
		410 704	(7.5.70, 00(0770)					
	120	418.704	67.5479 - 306.3778	$3d^{\circ} - 3d^{\circ}(a^{*}D)4p$	b ³ P - ³ P ²	1 - 2		922
	50	420.456	67.5479 - 305.3869	$3d^{\circ} - 3d^{\circ}(a^{\circ}D)4p$	b ³ P - ³ P ⁶	1-0		927
	120	421.547	69.1561 - 306.3778	3d° - 3d°(a*D)4p	b'P - 'P°	2 – 2		922
	50	422.510	69.1561 - 305.8381	3d° – 3d°(a*D)4p	b 'P – 'P°	2 – 1		922
	20	424.273	67.5479 - 303.2495	3d° – 3d`(a ⁴ P)4p	b 'P – 'S°	1 – 1		922
		461.69	0.0 - 216.5960	3d [°] – 3d ⁵ (a⁴D)4s	$ga^{s}D - {}^{s}D$	4 – 3	F,P	375,927
		462.56	0.0 - 216.1899	3d ⁶ - 3d ⁵ (a ⁴ D)4s	ga ⁵ D - ⁵ D	4 - 4	F.P	375,927
		463.59	0.8897 - 216.5960	$3d^{6} - 3d^{5}(a^{4}D)4s$	$ga^{5}D - {}^{5}D$	3 - 3	F.P	375.927
		463.61	0.8897 - 216.5905	$3d^6 - 3d^5(a^4D)4s$	$ga^{5}D - {}^{5}D$	3 - 2	F.P	375.927
		463.94	0.8897 - 216.4347	3d ⁶ - 3d ⁵ (a ⁴ D)4s	$ga^{5}D - {}^{5}D$	3 - 1	E.P	375.927
		464.27	27.1112 - 242.5043	$3d^6 - 3d^5(a^2G)4s$	$a^{3}H - {}^{3}G$	6-4	F.P	375,927
		464.47	0.8897 - 216.1899	3d [*] - 3d ⁵ (a ⁴ D)4s	ga ⁵ D - ⁵ D	3 - 4	F,P	375,927
		161.80	1 4800 216 5060	240 245(-40)4-	in in			275.027
		465 24	1 4809 - 216 4247	$3d^{6} = 3d^{6}(a^{2}D)4s$		2-3	F,P	375,927
		465.52	1.400 214 2064	$3d = 3d^{2}(a^{2}D)4s$	ga D – D	2-1	F,P	375,927
		403.32	1.4699 - 210.3034	$3d^{\circ} - 3d^{\circ}(a^{\circ}D)4s$	$ga^{\circ}D = D$	2-0	F,P	375,927
		403.72	1.8/15 - 210.5905	$3d^{\circ} - 3d^{\circ}(a^{*}D)4s$	ga D - D	1 - 2	F,P	375,927
		465.77	1.4699 - 210.1899 1.8715 - 216.4347	$3d^{\circ} - 3d^{\circ}(a^{\circ}D)4s$ $3d^{\circ} - 3d^{\circ}(a^{4}D)4s$	$ga^{*}D - D$	2-4	F,P	375,927
		400.00	1.0715 - 210.4547	50 - 50 (a D)45	ga D - D	1-1	F,F	373,927
		466.13	2.0576 - 216.5905	3d* - 3d ⁵ (a ⁴ D)4s	ga ⁵ D - ⁵ D	0 – 2	F,P	375,927
		466.34	1.8715 - 216.3054	3d ⁶ – 3d ⁵ (a ⁴ D)4s	ga ⁵ D – ⁵ D	1 - 0	F,P	375,927
		466.47	2.0576 - 216.4347	3d ⁶ – 3d ⁵ (a ⁴ D)4s	ga ⁵ D - ⁵ D	0 - 1	F,P	375,927
		471.14	0.0 - 212.2534	3d ⁶ – 3d ⁵ (a ⁴ P)4s	ga ⁵ D - ⁵ P	4 – 2	F,P	375,927
		471.49	0.0 - 212.0958	3d° - 3d ⁵ (a ⁴ P)4s	ga ^s D – ^s P	4 - 3	F,P	375,927
		472.67	0.8897 – 212.4557	3d° - 3d ⁵ (a ⁴ P)4s	ga ⁵ D - ⁵ P	3 – 1	F,P	375,927
		473.12	0 8897 - 212 2534	3d ⁶ - 3d ⁵ /a ⁴ D\4a	60 ⁵ D 5B	2 2	ED	375 037
		473 47	0.8897 - 212.2554	$3d^6 = 3d^5(a^4D)Aa$		3-2	F,P	375,927
		474.01	1 4900 212 4557	30° - 30°(a°P)4s	ga D - P	3-3	F,P	375,927
		474.01	1.400 212.400/	30" - 30"(a'P)4s	ga D - P	2 - 1	F,P	375,927
		4/4.4/	1.4699 - 212.2034	30° - 30°(a°P)4s	ga D - P	2 - 2	F,P	375,927
		4/4.8/	1.8/15 - 212.4557	30" – 30" (a*P)4s	ga D - 'P	1-1	F,P	375,927
		480.39	0.0 - 208.1637	3d" - 3d"(a*G)4s	ga'D - 'G	4 - 4	F,P	375,927
	1				1	1	1	

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NI V -- Continued

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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
		480.47	0.0 - 208.1310	3d ⁶ - 3d ⁵ (a ⁴ G)4s	ga ⁵ D - ⁵ G	4 - 5	F,P	375,927
		480.66	0.0 - 208.0464	3d ⁶ – 3d ⁵ (a ⁴ G)4s	ga ⁵ D – ⁵ G	4 - 6	F,P	375,927
		482.45	0.8897 - 208.1637	3d ⁶ - 3d ⁵ (a ⁴ G)4s	$ga^{5}D - {}^{5}G$	3-4	F,P	375,927
		482.53	0.8897 - 208.1310	$3d^6 - 3d^5(a^4G)4s$	$\tilde{g}a^{5}D - {}^{5}G$	3 – 5	F,P	375,927
		483.85	1.4899 - 208.1646	3d ⁶ - 3d ⁵ (a ⁴ G)4s	ga ⁵ D - ⁵ G	2 – 3	F.P	375,927
		483.88	1.4899 - 208.1515	$3d^6 - 3d^5(a^4G)4s$	ga ⁵ D - ⁵ G	2 – 2	F,P	375,927
		100100			5		- ,-	
		484.75	1.8715 - 208.1646	$3d^6 - 3d^5(a^4G)4s$	ga ⁵ D – ⁵ G	1 - 3	F,P	375,927
	ļ	484.78	1.8715 - 208.1515	$3d^6 - 3d^5(a^4G)4s$	ga'D - 'G	1 – 2	F,P	375,927
		485.22	2.0576 - 208.1515	3d ⁶ – 3d ⁵ (a ⁴ G)4s	ga ⁵ D – ⁵ G	0 – 2	F,P	375,927
		607.81	0.0 - 164.5259	3d ⁶ – 3d ⁵ (a ⁶ S)4s	ga ⁵ D - ⁷ S	4 – 3	F,P	375,927
		611.11	0.8897 - 164.5259	3d ⁶ - 3d ⁵ (a ⁶ S)4s	$ga^{5}D - {}^{7}S$	3 – 3	F,P	375,927
	30	990.816	216.5905 - 317.5175	3d⁵(a⁴D)4s – 3d⁵(a⁴F)4p	⁵ D - ⁵ D°	2 – 2		927
	90	990.867	216 5960 - 317 5175	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ F)4p	⁵ D - ⁵ D°	3 - 2		927
	110	993 676	2165960 - 3172320	$3d^{5}(a^{4}D)4s = 3d^{5}(a^{4}F)4n$	${}^{5}D - {}^{5}D^{\circ}$	3-3		927
	180	1002 410	217 1291 - 316 8878	$3d^{5}(a^{4}G)4s = 3d^{5}(a^{2}H)4p$	³ G - ³ G°	4-4	1	927
	270	1003 233	217.0487 - 316.7266	$3d^{5}(a^{4}G)4s = 3d^{5}(a^{2}H)4n$	³ G - ³ G ^o	5-5		927
	140	1008 269	217.1010 - 316.2803	$3d^{5}(a^{4}G)4s = 3d^{5}(a^{2}F)4p$	$^{3}G = ^{3}F^{\circ}$	3_3		927
	540	1010 338	217.1010 - 510.2005	$3d^{5}(a^{4}D)As = 3d^{5}(a^{4}E)Ap$	5D - 5F°	4-5		927
	540	1010.558	210.1899 - 515.1082	50 (a D)45 - 50 (a 1)4p	D = 1	4-5		921
	340	1020.382	208.0464 - 306.0490	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ² I)4p	⁵ G - ³ I°	6 – 5		927
	320	1020.707	216.5905 - 314.5628	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}F)4p$	${}^{5}D - {}^{5}F^{\circ}$	2 – 3		927
	140	1021.536	251.6549 - 349.5460	$3d^{5}(b^{2}F)4s - 3d^{5}(b^{2}D)4p$	${}^{1}F - {}^{1}D^{\circ}$	3 – 2		927
	50	1024.462	216.5960 - 314.2088	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{2}F)4p$	⁵ D - ³ F°	3 - 4		927
	280	1026.306						927
	220	1026.504	225.2007 - 322.6176	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ F)4p	${}^{3}D - {}^{3}D^{\circ}$	3 - 3		927
	160	1042 220	225 2007 221 0564	245(-50)4-245(-20)4-	30 350	2.4		017
	150	1043.230	225.2007 - 321.0504	$3d^{2}(a^{2}D)4s - 3d^{2}(a^{2}C)4p$	D - F	3-4		927
	20	1044.633	247.1030 - 342.8940	$3d(0^{-}r) + s = 3d(0^{-}D) + p$	$\mathbf{F} - \mathbf{F}$	2-2		927
	550	1047.429	223.3431 - 321.0183	$3d^{2}(a^{2}D) + 8 = 3d^{2}(a^{2}C) + p$	D - F			927
	110	1058.190	229.4088 - 323.9086	$3d^{2}(a^{-1})4s = 3d^{2}(a^{-2}G)4p$		0-5		927
	100	1064.534	221.4290 - 315.3001	$3d^{2}(a^{2}F)4s = 3d^{2}(a^{2}F)4p$ $2d^{2}(a^{2}F)4s = 2d^{2}(b^{2}F)4r$	$\mathbf{P} = \mathbf{D}$	1 - 2		927
	150	10/4.040	253.9052 - 346.9595	30'(a-S)4s - 30'(b-D)4p	r	1-1		927
	300	1075.182	253.9052 - 346.9124	3d ⁵ (a ² S)4s - 3d ⁵ (b ² D)4p	${}^{3}\mathbf{S} - {}^{3}\mathbf{P}^{\circ}$	1 – 2		927
	640	1081.097	233.8392 - 326.3371	3d ⁵ (a ² I)4s - 3d ⁵ (a ² G)4p	'I – 'H°	6 – 5		927
	170	1089.481	268.2739 - 360.0597	3d ⁵ (b ² D)4s - 3d ⁵ (b ² G)4p	$^{1}D - ^{1}F^{\circ}$	2 – 3		927
	230	1094.767	229.4406 - 320.7831	$3d^{5}(a^{2}I)4s - 3d^{5}(a^{2}H)4p$	³ I - ³ I°	7 – 7		927
	600	1105.561	229.4088 - 319.8604	3d ⁵ (a ² I)4s - 3d ⁵ (a ² H)4p	${}^{3}I - {}^{3}I^{\circ}$	6 - 6		927
	420	1115.298	229.4130 - 319.0762	$3d^{5}(a^{2}I)4s - 3d^{5}(a^{2}H)4p$	${}^{3}\mathbf{I} - {}^{3}\mathbf{I}^{\circ}$	5 - 5		927
	580	1119 345	164 5259 - 253 8627	3d5(a*S)4s - 3d5(a*S)4p	⁷ S _ ⁵ P°	3_3		927
	820	1120.894	241.0822 - 330.2976	$3d^{5}(a^{2}H)4s - 3d^{5}(b^{2}F)4p$	³ H - ³ G°	5-4		927
	820	1124.311	241 7736 - 330 7181	$3d^{5}(a^{2}H)4s - 3d^{5}(b^{2}F)4p$	$^{3}H - ^{3}G^{\circ}$	6 - 5		927
	540	1125.053	208 0464 - 296 9329	$3d^{5}(a^{4}G)4s = 3d^{5}(a^{4}G)4p$	5G - ³ G°	6-5		927
	440	1135.020	212.0958 = 300.2010	$3d^{5}(a^{4}P)4s - 3d^{5}(a^{4}D)4p$	⁵ P - ⁵ P°	3 - 3		927
	180	1137.829	229.4406 - 317.3273	$3d^{5}(a^{2}I)4s - 3d^{5}(a^{2}H)4p$	${}^{3}I - {}^{3}H^{\circ}$	7 - 6		927
	530	1139.055	242.5043 - 330.2976	3d ³ (a ² G)4s - 3d ³ (b ² F)4p	G - G*	4 - 4		927
	90	1141.140	239.1077 - 326.7390	$3d^{3}(a^{2}D)4s - 3d^{3}(a^{2}G)4p$	$^{\prime}D - ^{\prime}F^{\circ}$	2 - 3		927
	20	1141.758	242.2904 - 329.8729	$3d^{\circ}(a^{2}G)4s - 3d^{\circ}(b^{2}F)4p$	'G - 'D°	3 - 3		927
	50	1143.576	247.2818 - 334.7276	$3d^{3}(b^{2}F)4s - 3d^{3}(b^{2}F)4p$	`F - 'F°	4 – 3		927
	690	1144.197	208.0464 - 295.4443	3d ⁵ (a ⁴ G)4s – 3d ⁵ (a ⁴ D)4p	`G − `F°	6 – 5		927
	450	1144.602						927
	450	1145,318	208.1310 - 295.4443	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ D)4p	⁵ G - ⁵ F°	5-5		927
	310	1149,889	243.3315 - 330.2976	$3d^{5}(a^{4}F)4s - 3d^{5}(b^{2}F)4p$	³ F - ³ G°	4-4		927
	540	1150 096	212 0958 - 299 0456	$3d^{5}(a^{4}P)4s = 3d^{5}(a^{4}D)4n$	⁵ P - ⁵ P°	3-2		927
	170	1150 482	21210/00 2//10100					927
	690	1151.066	212 0958 - 298 9723	$3d^{5}(a^{4}P)4s = 3d^{5}(a^{4}D)4n$	⁵ P - ³ D ^o	3 - 3		927
	660	1151 972	208 1310 - 294 9396	$3d^{5}(a^{4}G)4s = 3d^{5}(a^{4}D)4n$	⁵ G - ⁵ F°	5_4		927
	000	1151.572	200.1310 - 274.7370		.	5 = 4		, <u>,</u>

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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	References
	310	1152.179	212.2534 - 299.0456	3d ⁵ (a ⁴ P)4s - 3d ⁵ (a ⁴ D)4p	⁵ P – ⁵ P°	2 – 2		927
	460	1152.403	208.1637 - 294.9396	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ D)4p	⁵ G - ⁵ F°	4 – 4		927
	490	1152.533	225.2007 - 311.9665	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{2}D)4p$	${}^{3}D - {}^{3}P^{\circ}$	3 - 2	1	927
	780	1152.687	246.2409 - 332.9956	$3d^{5}(a^{2}H)4s - 3d^{5}(a^{2}H)4p$	¹ H – ¹ G°	5 - 4		927
	70	1153.994	229.4130 - 316.0688	$3d^{5}(a^{2}I)4s - 3d^{5}(a^{2}F)4p$	${}^{3}I - {}^{3}G^{\circ}$	5 - 4		927
	280	1154.888	212.4557 – 299.0456	$3d^{5}(a^{4}P)4s - 3d^{5}(a^{4}D)4p$	⁵ P - ⁵ P°	1 - 2		927
	40	1155.471	240.1938 - 326.7390	$3d^{5}(a^{2}F)4s - 3d^{5}(a^{2}G)4p$	'F – 'F°	3 – 3		927
	30	1155.929	243.2662 - 329.7763	$3d^{5}(a^{4}F)4s - 3d^{5}(b^{2}F)4p$	$^{3}F - ^{3}D^{\circ}$	2 - 2		927
	150	1157.343	243.3705 - 329.7763	$3d^{5}(a^{4}F)4s - 3d^{5}(b^{2}F)4p$	${}^{3}F - {}^{3}D^{\circ}$	3 - 2		927
	260	1157.450	240.9596 - 327.3566	3d ⁵ (a ² H)4s – 3d ⁵ (a ² H)4p	${}^{3}H - {}^{1}H^{\circ}$	4 - 5		927
	420	1158.127	212.2534 - 298.6006	$3d^{5}(a^{4}P)4s - 3d^{5}(a^{4}P)4p$	${}^{5}\mathbf{P} - {}^{3}\mathbf{D}^{\circ}$	2 - 1		927
	790	1159.021	208.1637 - 294.4433	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ D)4p	⁵ G – ⁵ F°	4 - 3		927
	190	1159.521	243.3705 - 329.6143	$3d^{5}(a^{4}F)4s - 3d^{5}(b^{2}F)4p$	${}^{3}F - {}^{3}G^{\circ}$	3 - 3		927
	320	1160.120				1		927
	130	1163.362	229.4130 - 315.3701	$3d^{5}(a^{2}I)4s = 3d^{5}(a^{2}G)4p$	³ I – ³ H°	5-4		927
	450	1163 523	247.0491 - 332.9956	$3d^{5}(a^{2}G)4s = 3d^{5}(a^{2}H)4n$		4 4		927
	260	1163 688	208 1515 - 294 0860	$3d^{5}(a^{4}G)/a = 3d^{5}(a^{4}D)/a$	5G 5F	2 2 2		027
	620	1163.000	208.1515 - 254.0800	3d(a C) + s = 3d(a D) + p $2dS(a^4C) + a = 2dS(a^4D) + p$			1	927
	030	1105.805	208.1040 - 294.0800	3d (a G)4s - 3d (a D)4p	-G-'F	3-2		927
	70	1165.596	241.0822 - 326.8763	3d ⁵ (a ² H)4s - 3d ⁵ (b ² F)4p	${}^{3}H - {}^{3}F^{\circ}$	5 – 4		927
	180	1165.861	234.1254 - 319.8991	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{4}F)4p$	⁵ F – ³ G°	4 - 4		927
	240	1166.226	212.0958 - 297.8425	$3d^{5}(a^{4}P)4s - 3d^{5}(a^{4}P)4p$	${}^{5}\mathbf{P} - {}^{3}\mathbf{D}^{\circ}$	3 - 2		927
	320	1166.475	212.2534 - 297.9828	$3d^{5}(a^{4}P)4s - 3d^{5}(a^{4}D)4p$	⁵ P - ⁵ P°	2 - 1		927
	370	1166.683	247.2818 - 332.9956	$3d^{5}(b^{2}F)4s - 3d^{5}(a^{2}H)4p$	${}^{3}\mathbf{F} = {}^{1}\mathbf{G}^{\circ}$	4 _ 4		927
	650	1167.113	208.1515 - 293.8338	$3d^{5}(a^{4}G)4s - 3d^{5}(a^{4}D)4p$	⁵ G - ⁵ F°	2 - 1		927
	20	1167 802	224 2752 210 0001	245(-45)4-245(-45)4-	ST 300			0.27
	20	1167.893	234.2752 - 319.8991	$3d^{2}(a^{2}F)4s = 3d^{2}(a^{2}F)4p$	F - 'G'	3-4		927
	200	1168.166	212.4557 - 298.0600	$3d^{(a^{2}P)4s} - 3d^{(a^{2}D)4p}$	$P - D^{2}$	1-0	'	927
	390	1168.626	234.0821 - 319.6527	3d ³ (a ⁺ F)4s - 3d ³ (a ⁺ F)4p	F - G°	5 – 5		927
	290	1170.254	306.9629 - 392.4135	$3d^{3}(c^{2}D)4s - 3d^{3}(c^{2}D)4p$	⁵ D – ⁵ P °	3 – 2		927
	450	1171.138	212.4557 - 297.8425	3d°(a*P)4s – 3d°(a*P)4p	$^{\circ}\mathbf{P} - ^{\circ}\mathbf{D}^{\circ}$	1 – 2		927
	350	1171.450	240.1938 - 325.5586	3d ⁵ (a ² F)4s - 3d ⁵ (b ² F)4p	'F - 'G°	3 - 4		927
	240	1171.712	234.2752 - 319.6202	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{4}F)4p$	⁵ F - ³ G°	3 – 3		927
	150	1172.128	229.4406 - 314.7564	$3d^{5}(a^{2}I)4s - 3d^{5}(a^{4}F)4p$	${}^{3}I - {}^{5}G^{\circ}$	7-6		927
	420	1172.468	221.0876 - 306.3778	$3d^{5}(a^{4}P)4s = 3d^{5}(a^{4}D)4p$	$^{3}\mathbf{P} = ^{3}\mathbf{P}^{\circ}$	2.2		927
	800	1174.202	212.2534 - 297.4181	$3d^{5}(a^{4}P)4s = 3d^{5}(a^{4}P)4n$	⁵ P - ³ D°	2 - 2		927
	760	1176 986	212 4557 - 297 4179	$3d^{5}(a^{4}P)4s = 3d^{5}(a^{4}D)4p$	5P 5D°		1	027
	180	1177.178	221.4290 - 306.3778	$3d^{5}(a^{4}P)4s - 3d^{5}(a^{4}D)4p$	$^{3}\mathbf{P} - ^{3}\mathbf{P}^{\circ}$	1 - 1		927
	160	1177 (01	212.0059 207.0120		50 500			
	100	1177.601	212.0958 - 297.0139	$3d^{(a^{+}P)4s} - 3d^{(a^{+}D)4p}$	$\mathbf{P} - \mathbf{D}^{*}$	3 - 2		927
	610	11/8.22/	216.5960 - 301.4702	$3d^{(a^{+}D)}4s - 3d^{(a^{+}D)}4p$	$D - F^*$	3 - 3		927
	1/0	1178.382	234.2752 - 319.1387	$3d^{(a^{+}F)}4s - 3d^{(a^{-}G)}4p$	"F - 'G"	3 - 4		927
	20	1178.806	232.5459 - 317.3768	$3d^{(a^2D)4s} - 3d^{(a^2H)4p}$	[°] D – [°] G°	3 ~ 3		927
	710	1178.914	212.0958 - 296.9193	$3d^{(a^{+}P)4s} - 3d^{(a^{+}D)4p}$	$^{\circ}P - ^{\circ}D^{\circ}$	3 – 4	·	927
	560	1179.234	212.0958 - 296.8970	3d ³ (a ⁺ P)4s - 3d ³ (a ⁺ G)4p	°P – 'G°	3 - 4		927
	700	1179.970						927
	570	1180.256	216.1899 - 300.9181	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}D)4p$	${}^{5}D \rightarrow {}^{3}F^{\circ}$	4 – 4		927
	70	1182.506	232.9108 - 317.4779	$3d^{5}(a^{2}D)4s - 3d^{5}(a^{4}F)4p$	${}^{3}D - {}^{5}D^{\circ}$	1-1		927
	620	1182.615	212.4557 - 297.0139	$3d^{5}(a^{4}P)4s - 3d^{5}(a^{4}D)4p$	⁵ P - ⁵ D°	1 - 2		927
	20	1182,724	232.9108 - 317.4623	$3d^{5}(a^{2}D)4s - 3d^{5}(a^{4}F)4n$	$^{3}D = ^{5}D^{2}$	1_0		927
	260	1183.767	241.0822 - 325.5586	$3d^{5}(a^{2}H)4s - 3d^{5}(b^{2}F)4p$	³ H - ¹ G°	5-4		927
	20	1105 336	242 5042 226 9762	2456-20124-2456-20124-				0.27
	30	1185.236	242.5043 - 326.8763	3d (a G)4s - 3d (b F)4p	'G - 'F'	4 – 4	·	927
	770	1185.948	212.2534 - 296.5740	3d'(a*P)4s - 3d'(a*D)4p	°P - °D°	2 - 3		927
	20	1187.197	235.4206 - 319.6527	$3d^{3}(a^{2}F)4s - 3d^{5}(a^{4}F)4p$	'F - 'G°	4 - 5		927
	200	1187.321	208.1310 - 292.3534	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	⁵ G - ³ H°	5 - 5		927
	350	1187.781	235.7365 - 319.9265	3d ⁵ (a ² F)4s - 3d ⁵ (a ² F)4p	${}^{3}\mathbf{F} - {}^{1}\mathbf{D}^{\circ}$	2 - 2		927
	550	1189.544	241.0822 - 325.1484	$3d^{5}(a^{2}H)4s - 3d^{5}(a^{2}G)4p$	${}^{3}H - {}^{3}H^{\circ}$	5 - 6		927

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tiplet Rel. Int.	$\lambda_{\rm vac}$ (in Å)	Levels (in 10^3 cm 3)	Configurations	Terms	J - J	Notes	Reference
20	1189.687	229.4088 - 313.4647	3d ⁵ (a ² I)4s - 3d ⁵ (a ⁴ F)4p	³ I – ⁵ G°	6 – 5		927
550	1190.334	216.1899 - 300.2010	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ D)4p	⁵ D - ⁵ P°	4 – 3		927
220	1191.082	221.4290 - 305.3869	3d ⁵ (a ⁴ P)4s - 3d ⁵ (a ⁴ D)4p	$^{3}\mathbf{P} - ^{3}\mathbf{P}^{\circ}$	1 – 0		927
330	1192.687	208.0464 - 291.8914	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	⁵ G - ³ H°	6 - 6		927
20	1192.849	242.5043 - 326.3371	3d ⁵ (a ² G)4s - 3d ⁵ (a ² G)4p	³ G – ¹ H°	4 - 5		927
90	1193.612	274.6954 - 358.4756	$3d^{5}(b^{2}G)4s - 3d^{5}(b^{2}G)4p$	³ G - ¹ H°	5 – 5		927
440	1193.887	208.1310 - 291.8914	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	⁵ G - ³ H°	5 - 6		927
550	1194.282	240.1938 - 323.9263	$3d^{5}(a^{2}F)4s - 3d^{5}(a^{2}H)4p$	¹ F - ³ H°	3-4		927
30	1194.498	235.4206 - 319.1387	$3d^{5}(a^{2}F)4s - 3d^{5}(a^{2}G)4p$	³ F - ¹ G°	4 - 4		927
20	1194 576	306 9629 - 390 6751	$3d^{5}(c^{2}D)4s - 3d^{5}(c^{2}D)4p$	${}^{3}\mathbf{D} - {}^{1}\mathbf{D}^{\circ}$	3-2		927
390	1194 862	242,2904 = 325,9822	$3d^{5}(a^{2}G)4s = 3d^{5}(h^{2}F)4n$	$^{3}G - ^{3}F^{\circ}$	3 - 2		927
710	1195.192	247.0491 - 330.7181	$3d^{5}(a^{2}G)4s - 3d^{5}(b^{2}F)4p$	¹ G – ³ G°	4 - 5		927
120	1105 825	232 6556 - 316 2803	$3d^{5}(a^{2}D)4s = 3d^{5}(a^{2}E)4n$	³ D - ³ F°	2 - 3		927
120	1106.036	216 5905 300 2010	$3d^{5}(a^{4}D)4s = 3d^{5}(a^{4}D)4n$	⁵ D - ⁵ P°	2 3		927
620	1190.030	216.5965 - 300.2010	$3d^{5}(a^{4}D)4a^{-3}d^{5}(a^{4}D)4n$	50 5P°	2 - 5		027
200	1190.110	210.3700 - 300.2010	$3d^{2}(a^{4}E)4a = 3d^{2}(a^{2}E)4p$	D-I	3-3		927
300	1190.973	243.3313 - 320.8703	3d(a P)4s = 3d(0 P)4p $2d^{2}(a^{2}D)4a = 2d^{2}(a^{2}E)4m$		2 4		027
370	1197.274	232.3439 - 310.0088	3d(a D)4s = 3d(a P)4p $3d^{5}(c^{2}D)4s = 3d^{5}(c^{2}D)4p$	³ D ² - 0 ⁴	3-4		927
570	1197.576	500.7027 - 570.4702	54 (c D)+5 - 54 (c D)+p		5 5		21
230	1197.975	242.8626 - 326.3371	3d ⁵ (a ² G)4s - 3d ⁵ (a ² G)4p	³ G - ¹ H°	5-5		927
230	1197.998	236.4541 - 319.9265	3d ⁵ (a ² F)4s - 3d ⁵ (a ² F)4p	${}^{3}\mathbf{F} - {}^{1}\mathbf{D}^{\circ}$	3 – 2		927
410	1198.278	307.0252 - 390.4782	3d ⁵ (c ² D)4s - 3d ⁵ (c ² D)4p	$^{3}D - ^{3}D^{\circ}$	2 – 3		927
710	1198.525	247.2818 - 330.7181	3d ⁵ (b ² F)4s - 3d ⁵ (b ² F)4p	³ F – ³ G°	4 - 5		927
210	1198.699	208.1310 - 291.5546	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	⁵ G - ³ F°	5 - 4		927
270	1198.898						927
800	1199.402	241.7736 - 325.1484	3d ⁵ (a ² H)4s - 3d ⁵ (a ² G)4p	³ H – ³ H°	6 - 6		927
230	1200.947	242.2904 - 325.5586	$3d^{5}(a^{2}G)4s - 3d^{5}(b^{2}F)4p$	³ G – ¹ G°	3 - 4		927
290	1201.087	263.7009 - 346.9595	$3d^{5}(b^{2}D)4s - 3d^{5}(b^{2}D)4p$	${}^{3}\mathbf{D} - {}^{3}\mathbf{P}^{\circ}$	1-1	ļ l	927
440	1201.197	234.1254 - 317.3768	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{2}H)4p$	⁵ F – ³ G°	4 - 3		927
460	1201.324	234.2752 - 317.5175	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{4}F)4p$	${}^{5}\mathbf{F} - {}^{5}\mathbf{D}^{\circ}$	3 - 2		927
340	1201.594	263.7357 - 346.9595	$3d^{5}(b^{2}D)4s - 3d^{5}(b^{2}D)4p$	${}^{3}D - {}^{3}P^{\circ}$	2 - 1		927
240	1201 644	263 7009 - 346 9202	$3d^{5}(h^{2}D)4s = 3d^{5}(h^{2}D)4n$	$^{3}D = ^{3}P^{\circ}$	1-0		927
240	1201.044	263.7009 - 346.9202	3d(0D)4s = 3d(0D)4p $3d^{5}(b^{2}D)4s = 3d^{5}(b^{2}D)4p$	$^{3}D - ^{3}P^{2}$	1 - 0		927
460	1201.700	203.7009 - 340.9124	$3d^{5}(e^{2}H)4e^{-3d^{5}(e^{2}G)4p}$	JH G	6 5		927
300	1201.654	241.7730 - 324.7802	$3d^{5}(h^{2}E)4s = 3d^{5}(h^{2}S)4n$	3E 3P	2 - 1		927
290	1201.857	247.1040 230.3707	3d(0F)4s - 3d(aS)4p $2d^{5}(h^{2}E)4n - 2d^{5}(h^{2}E)4n$	F C°	2-1		927
380	1202.040	263.7357 - 346.9124	$3d^{5}(b^{2}D)4s - 3d^{5}(b^{2}D)4p$	³ D - ³ P°	2 - 2		927 927
		200 1/27 201 2005					0.27
290	1202.427	208.1637 - 291.3285	3d (a*G)4s - 3d (a*G)4p	G - F	4-3		927
780	1203.285	263.8058 - 346.9124	$3d^{2}(b^{2}D)4s = 3d^{2}(b^{2}D)4p$		3-2		927
/90	1203.314	234.4127 - 317.5175	$3d^{2}(a^{2}F)4s = 3d^{2}(a^{2}F)4p$	$\mathbf{F} - \mathbf{D}$	2-2		927
630	1203.361	217.1010 - 300.2010	$3d^{-}(a^{+}G)4s = 3d^{-}(a^{+}D)4p$	G = P	3-3		927
740	1203.776	234.4127 - 317.4779	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{4}F)4p$ $3d^{5}(a^{4}F)4s - 3d^{5}(a^{4}F)4p$	'F - 'D'	4-3 2-1		927
	1004			300 1000			027
120	1204.738	243.3315 - 326.3371	$3d^{(a^{+}F)}4s = 3d^{(a^{+}G)}4p$	$\mathbf{F} = \mathbf{H}^{2}$	4-5		927
600	1205.310	240.9596 - 323.9263	$3d^{2}(a^{2}H)4s - 3d^{2}(a^{2}H)4p$	"H - "H"	4-4		927
640	1205.453	234.2752 - 317.2320	$3d^{2}(a^{+}F)4s - 3d^{2}(a^{+}F)4p$	$\mathbf{F} - \mathbf{D}$	3-3		927
640	1205.559	240.9596 - 323.9086	$3d^{2}(a^{2}H)4s = 3d^{2}(a^{2}G)4p$	H - H	4-5		927
210	1205.794	242.2904 - 325.2229 242.2904 - 325.2119	$3d^{5}(a^{2}G)4s - 3d^{5}(a^{2}G)4p$ $3d^{5}(a^{2}G)4s - 3d^{5}(a^{2}G)4p$	G - G' G - 'G'	3 - 4 3 - 3		927 927
)			
800	1207.345	241.0822 - 323.9086	3d ³ (a ² H)4s - 3d ³ (a ² G)4p	'H - 'H°	5 - 5		927
670	1207.394	247.0491 - 329.8729	3d ³ (a ² G)4s - 3d ⁵ (b ² F)4p	'G - 'D°	4 – 3		927
490	1207.452	234.4127 - 317.2320	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{4}F)4p$	`F - `D°	2 - 3		927
90	1207.636	234.0821 - 316.8878	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ² H)4p	⁵ F - ³ G°	5 – 4		927
210	1207.989	216.1899 - 298.9723	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ D)4p	⁵ D - ³ D°	4 – 3		927
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NI V -- Continued

Multiplet	Rel. Int.	$\lambda_{\rm vac}$ (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	20	1208.266	234.1254 - 316.8878	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{2}H)4p$	⁵ F - ³ G°	4 - 4		927
	650	1208.908	242 5043 - 325 2229	$3d^{5}(a^{2}G)4s - 3d^{5}(a^{2}G)4n$	³ G - ³ G [*]	4 - 4		927
	480	1208.966	243.2667 = 325.2223	$3d^{5}(a^{4}E)4s = 3d^{5}(h^{2}E)4n$	$^{3}\mathbf{F} = {}^{3}\mathbf{F}^{\circ}$	2_2		927
	530	1208.900	247.1650 329.8729	$d^{5}(h^{2}E)4s = 3d^{5}(h^{2}E)4p$	$^{3}\mathbf{F} = ^{3}\mathbf{D}^{9}$	2 2		927
	200	1209.099	247.1030 - 329.8729	3d(0F)4s - 3d(0F)4p $2d^{5}(r^{4}E)4r = 2d^{5}(h^{2}E)4r$	F = D			927
	300	1209.225	243.3315 - 326.0299	$3d^{2}(a^{2}F)48 - 3d^{2}(b^{2}F)4p$	F - F	4-5		927
	220	1209.431	236.4541 - 319.1387	3d ⁻ (a ⁻ F)4s – 3d ⁻ (a ⁻ G)4p	"F – 'G*	3-4		927
	700	1209.607	247.1049 - 329.7763	3d ⁵ (b ² F)4s - 3d ⁵ (b ² F)4p	${}^{3}\mathbf{F} - {}^{3}\mathbf{D}^{\circ}$	3 - 2		927
	790	1209.771	234.0821 - 316.7440	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{4}F)4p$	⁵ F – ⁵ D°	5 – 4		927
	810	1210.399	234.1254 - 316.7440	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{4}F)4p$	⁵ F – ⁵ D°	4 - 4		927
	850	1210.509	247.1650 - 329.7763	$3d^{5}(b^{2}F)4s - 3d^{5}(b^{2}F)4p$	${}^{3}F - {}^{3}D^{\circ}$	2 - 2		927
	190	1210.638	234.1254 - 316.7266	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{2}H)4p$	${}^{5}F - {}^{3}G^{\circ}$	4 - 5		927
	480	1210.736	229.4130 - 312.0083	$3d^{5}(a^{2}I)4s - 3d^{5}(a^{2}F)4p$	³ I – ¹ G°	5 - 4		927
	420	1210.799	247.2818 - 329.8729	3d ⁵ (b ² F)4s - 3d ⁵ (b ² F)4p	${}^{3}\mathbf{F} - {}^{3}\mathbf{D}^{\circ}$	4 - 3		927
	240	1211 424	307 0252 - 389 5718	$3d^{5}(c^{2}D)4s = 3d^{5}(c^{2}D)4n$	$^{3}\mathbf{D} - ^{3}\mathbf{D}^{\circ}$	2-2		927
	210	1211.424	247 1049 - 329 6143	$3d^{5}(b^{2}E)4s = 3d^{5}(b^{2}E)4n$	5-0°	3_3		927
	150	1211.999	247.1049 - 329.0143	3d(0T)4s = 3d(0T)4p $3d^{2}(a^{2}C)4a = 3d^{2}(a^{2}C)4a$		3-3		927
	150	1212.474	242.3043 - 324.9802	3d(a O) + s - 3d(a O) + p	0-0 '0'-0'	4-5		927
	590	1212.592	307.1051 - 389.5718	3d ⁻ (c ⁻ D)4s - 3d ⁻ (c ⁻ D)4p	D - D	1 - 2		927
	780	1212.780	216.5905 - 299.0456	$3d^{(a^*D)4s} - 3d^{(a^*D)4p}$	³ D - ³ P ³	2 – 2		927
	460	1212.889	247.1650 - 329.6143	3d ⁵ (b ² F)4s - 3d ⁵ (b ² F)4p	${}^{3}F - {}^{3}G^{\circ}$	2 - 3		927
	200	1213.237	240.1938 - 322.6176	$3d^{5}(a^{2}F)4s - 3d^{5}(a^{4}F)4p$	$^{1}F - ^{3}D^{\circ}$	3 - 3		927
	520	1213.589	235.1165 - 317.5175	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ⁴ F)4p	⁵ F – ⁵ D°	1 – 2		927
	660	1213.859	216.5905 - 298.9723	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ D)4p	${}^{5}\mathbf{D} - {}^{3}\mathbf{D}^{\circ}$	2 – 3		927
	780	1213.943	216.5960 - 298.9723	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}D)4p$	${}^{5}\mathbf{D} - {}^{3}\mathbf{D}^{\circ}$	3 - 3		927
	710	1214.174	242.8626 - 325.2229	$3d^{5}(a^{2}G)4s - 3d^{5}(a^{2}G)4p$	${}^{3}\mathbf{G} - {}^{3}\mathbf{G}^{\circ}$	5 – 4		927
	700	1214 410	235 1165 - 317 4623	$3d^{5}(a^{4}F)4s = 3d^{5}(a^{4}F)4n$	5F - 5D°	1 - 0		927
	630	1214 595	2472818 - 3296143	$3d^{5}(b^{2}E)4s = 3d^{5}(b^{2}E)4n$	F-G	4 3		927
	600	1214.575	216 3054 - 298 6006	$3d^{5}(a^{4}D)Aa = 3d^{5}(a^{4}P)Aa$	5D 3D°	0 1		927
	750	1215.155	210.3034 - 238.0000	3d(aD)+s = 3d(aP)+p $3d^{2}(a^{2}C)Aa = 3d^{2}(a^{2}C)Aa$		5 6		927
	670	1213.272	242.8020 - 325.1484	3d(a G) + s = 3d(a G) + p	U-H	5-0		927
	280	1216.131	243.3313 - 323.3380 263 7357 - 345 9361	$3d^{5}(h^{2}D)4s = 3d^{5}(h^{2}D)4p$	$^{3}\mathbf{D} = {}^{1}\mathbf{F}^{0}$	2-3		927
	200	1210.000	20011001 0101001	54 (6 2)46 54 (6 2)49		1		21
	640	1217.062	216.4347 - 298.6006	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ P)4p	⁵ D - ³ D°	1 - 1		927
	740	1217.112	221.0876 - 303.2495	$3d^{5}(a^{4}P)4s - 3d^{5}(a^{4}P)4p$	³ P – ³ S°	2 - 1	1	927
	320	1217.502	241.7736 - 323.9086	$3d^{5}(a^{2}H)4s - 3d^{5}(a^{2}G)4p$	${}^{3}H - {}^{3}H^{\circ}$	6 - 5		927
	750	1217.576	208.1310 - 290.2620	$3d^{5}(a^{4}G)4s - 3d^{5}(a^{4}P)4p$	⁵ G - ⁵ D°	5 - 4		927
	810	1217.761	242.8626 - 324.9802	$3d^{5}(a^{2}G)4s - 3d^{5}(a^{2}G)4p$	³ G - ³ G°	5 - 5		927
	410	1218.061	208.1637 - 290.2620	$3d^{5}(a^{4}G)4s - 3d^{5}(a^{4}P)4p$	⁵ G – ⁵ D°	4 - 4		927
	160	1218 726	232 5459 - 314 5992	$3d^{5}(a^{2}D)4s = 3d^{5}(a^{4}F)4p$	³ D - ⁵ F°	3_4		927
	250	1219.886	232.3437 = 314.3772	$3d^{5}(a^{2}D)As = 3d^{5}(a^{2}E)Ap$		3 - 4		927
	360	1219.000	233.1077 = 321.0013	$3d^{5}(a^{4}E)As = 3d^{5}(a^{2}C)Ap$	JE JC	2-3		927
	250	1220.317	245.2002 - 325.2119	3d(a r) + s = 3d(a G) + p $3d(a^2 G) A = 3d(a^2 G) A = $		2-3		927
	200	1220.830	239.1077 - 321.0185	$3d^{2}(a^{2}D)A_{2} = 3d^{2}(a^{2}D)A_{2}$		2-2		927
	640	1220.879	243.3315 - 325.2229	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{2}G)4p$	$^{3}F - ^{3}G^{\circ}$	4-4		927
	810	1221.699	243.3705 - 325.2229	3d'(a'F)4s - 3d'(a'G)4p	F - 'G'	3-4		927
	320	1221.870	243.3705 - 325.2119	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ² G)4p	³ F - ³ G°	3 – 3		927
	540	1222.189	221.4290 - 303.2495	3d ⁵ (a ⁴ P)4s - 3d ⁵ (a ⁴ P)4p	³ P - ³ S°	1 - 1		927
	510	1222.788	235.7365 - 317.5175	3d ⁵ (a ² F)4s - 3d ⁵ (a ⁴ F)4p	³ F - ⁵ D°	2 - 2	1	927
	380	1223.204	234.4127 - 316.1654	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ² F)4p	${}^{5}F - {}^{3}F^{\circ}$	2 - 2		927
	520	1223.390	241.0822 - 322.8208	3d ⁵ (a ² H)4s - 3d ⁵ (a ⁴ F)4p	${}^{3}H - {}^{3}F^{\circ}$	5 – 4		927
	760	1223.444	306.9629 - 388.6989	$3d^{5}(c^{2}D)4s = 3d^{5}(c^{2}D)4n$	³ D - ³ F°	3_4		927
	60	1223.685	307 0252 - 388 7461	$3d^{5}(c^{2}D)4s = 3d^{5}(c^{2}D)4n$	³ D - ³ D°	2 1		927
	500	1223.005	216 2054 207 0020	3d(CD)4s = 3d(CD)4p $3d^{3}(c^{4}D)4c = 3d^{3}(c^{4}D)4c$	SD SD	2-1		927
	500	1224.333	210.3034 - 297.9828	$3d^{(a'D)4s} - 3d^{(a'D)4p}$	D-P	0-1		927
	680	1224.558	232.3439 - 314.2088	30°(a°D)4s - 30°(a°F)4p	D-F	3-4		927
	580	1224./58	243.3315 - 324.9802	3d'(a'F)4s - 3d'(a'G)4p	F - G	4-5		927
	510	1224.875	235.7365 - 317.3768	3d'(a'F)4s - 3d'(a'H)4p	' F − 'G'	2 - 3		927

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Multiplet Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	Reference
810	1224.948	242.2904 - 323.9263	3d5(a2G)4s - 3d5(a2H)4p	${}^{3}G - {}^{3}H^{\circ}$	3 – 4		927
530	1225.112	216.4347 - 298.0600	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ D)4p	⁵ D - ⁵ D°	1 - 0		927
380	1226.276	216.4347 - 297.9828	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ D)4p	⁵ D – ⁵ P°	1 – 1		927
240	1227.057	235.7365 - 317.2320	3d5(a2F)4s - 3d5(a4F)4p	³ F – ⁵ D°	2 - 3		927
420	1227.196	311.4703 - 392.9571	3d ⁵ (c ² D)4s - 3d ⁵ (c ² D)4p	¹ D - ¹ F°	2 - 3		927
20	1227.480	235.4206 - 316.8878	$3d^{5}(a^{2}F)4s - 3d^{5}(a^{2}H)4p$	³ F - ³ G°	4 – 4		927
190	1228.168	242.5043 - 323.9263	$3d^{5}(a^{2}G)4s - 3d^{5}(a^{2}H)4p$	³ G - ³ H°	4-4		927
700	1228 426	2425043 - 3239086	$3d^{5}(a^{2}G)4s - 3d^{5}(a^{2}G)4p$	${}^{3}G - {}^{3}H^{\circ}$	4 - 5		927
810	1229 400	251 6549 - 332 9956	$3d^{5}(h^{2}F)4s = 3d^{5}(a^{2}H)4n$	$^{1}\mathbf{F} = ^{1}\mathbf{G}^{*}$	3-4		927
810	1229 400	274 6954 - 356 0363	$3d^{5}(h^{2}G)4s = 3d^{5}(h^{2}G)4n$	G - 'G'	5-5		927
200	1229.400	235 4206 - 316 7440	$3d^{5}(a^{2}E)4s = 3d^{5}(a^{4}E)4n$	³ F - ⁵ D°	4_4		927
600	1230.062	274.7386 - 356.0363	$3d^{5}(b^{2}G)4s - 3d^{5}(b^{2}G)4p$	³ G – ³ G°	4 - 5		927
(10	1220 420	268 2720 240 5460	2d ⁵ (b ² D)4c 2d ⁵ (b ² D)4n	יתי חי	1 1 1		027
640	1230.439	208.2/39 - 349.3400	$3d^{2}(b^{2}D)4s = 3d^{2}(b^{2}D)4p$		2-2		927
320	1230.731	216.5905 - 297.8425	30'(a'D)4s = 30'(a'P)4p	D - D	2 - 2		927
580	1230.821	216.5960 - 297.8425	$3d^{\circ}(a^{\circ}D)4s = 3d^{\circ}(a^{\circ}P)4p$	D - D	3-2		927
760	1230.875	241.0822 - 322.3242	$3d^{2}(a^{2}H)4s - 3d^{2}(a^{2}H)4p$	¹ H – ¹ F	5-6		927
600	1231.030	242.2904 - 323.5232	3d'(a'G)4s - 3d'(a'F)4p	'G - 'F'	3 – 3		927
720	1231.090	216.1899 - 297.4181	3d ³ (a ⁴ D)4s - 3d ³ (a ⁴ P)4p	°D – °D°	4 - 3		927
760	1231.881	225.2007 - 306.3778	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ D)4p	${}^{3}\mathbf{D} - {}^{3}\mathbf{P}^{\circ}$	3 - 2		927
180	1232.341	208.1515 - 289.2980	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ P)4p	⁵ G – ⁵ D°	2 – 3		927
860	1232.517	208.1637 - 289.2980	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ P)4p	5G – 5D°	4 – 3		927
850	1232.801	246.2409 - 327.3566	3d ⁵ (a ² H)4s - 3d ⁵ (a ² H)4p	${}^{1}H - {}^{!}H^{\circ}$	5 – 5		927
850	1232.965	263.8058 - 344.9112	$3d^{5}(b^{2}D)4s - 3d^{5}(b^{2}D)4p$	³ D - ³ F°	3 - 4		927
710	1233.120	208.1515 - 289.2471	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	⁵ G – ⁵ F°	2 – 2		927
860	1233 268	234.0821 - 315.1682	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ⁴ F)4p	⁵ F - ⁵ F*	5 - 5		927
810	1233 324	208 1646 - 289 2471	$3d^{5}(a^{4}G)4s = 3d^{5}(a^{4}G)4n$	'G - 'F'	3-2		927
750	1233.500	274 6954 - 355 7652	$3d^{5}(h^{2}G)4s = 3d^{5}(h^{2}G)4n$	³ G - ³ G*	5_4		927
690	1233.506	274.0754 = 355.7052 236.4541 = 317.5175	$3d^{5}(a^{2}E)4s = 3d^{5}(a^{4}E)4p$	³ E - ⁵ D°	3 = 7		927
440	1233.350	230.4541 - 317.5175	$3d^{5}(a^{2}G)Ac = 3d^{5}(a^{2}G)An$	3G 3H	5 5		027
880	1233.884	242.8626 - 323.9086	$3d^{5}(a^{2}G)4s - 3d^{5}(a^{2}G)4p$	³ G – ³ H°	5-5		927
	1004.170	274 7286 265 7652	2150-2014 2150-2014				027
820	1234.163	2/4./386 - 355./652	30°(0°G)48 - 30°(0°G)4p	-G-G	4-4		927
300	1234.257	242.5043 - 323.5232	$3d^{-}(a^{-}G)4s - 3d^{-}(a^{+}F)4p$	G - F	4-3		927
810	1234.390	208.1515 - 289.1630	$3d^{3}(a^{*}G)4s - 3d^{3}(a^{*}G)4p$	G - F	2 - 1		927
770	1234.579	263.8058 - 344.8053	$3d^{\circ}(b^{2}D)4s - 3d^{\circ}(b^{2}D)4p$	°D – °D	3 – 3		927
440	1234.697	274.7735 - 355.7652	3d°(b²G)4s – 3d°(b²G)4p	°G – 'G°	3 - 4		927
270	1235.305						927
160	1235.430	311.4703 - 392.4135	$3d^{5}(c^{2}D)4s - 3d^{5}(c^{2}D)4p$	${}^{1}\mathbf{D} - {}^{3}\mathbf{P}^{\circ}$	2 ~ 2		927
680	1235.764	236.4541 - 317.3768	3d ⁵ (a ² F)4s - 3d ⁵ (a ² H)4p	³ F – ³ G°	3 - 3		927
860	1235.831	233.8392 - 314.7564	3d ⁵ (a ² I)4s - 3d ⁵ (a ⁴ F)4p	¹ I – ⁵ G°	6-6		927
810	1236.267	240.1938 - 321.0819	3d ⁵ (a ² F)4s - 3d ⁵ (a ² F)4p	${}^{1}F - {}^{1}F^{\circ}$	3 – 3		927
620	1236.664	240.1938 - 321.0564	3d ⁵ (a ² F)4s - 3d ⁵ (a ² G)4p	${}^{1}\mathbf{F} - {}^{3}\mathbf{F}^{\circ}$	3 – 4		927
690	1236.696	279.1995 - 360.0597	3d ⁵ (b ² G)4s - 3d ⁵ (b ² G)4p	¹ G - ¹ F°	4 - 3		927
270	1237.119	225.5451 - 306.3778	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ D)4p	${}^{3}\mathbf{D} - {}^{3}\mathbf{P}^{\circ}$	1 - 2		927
740	1237.197	216.5905 - 297.4179	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}D)4p$	⁵ D - ⁵ D°	2 - 1		927
560	1237.328	239.1077 - 319.9265	$3d^{5}(a^{2}D)4s - 3d^{5}(a^{2}F)4p$	$^{1}D - ^{1}D^{\circ}$	2 – 2		927
380	1237.972	232.9108 - 313.6866	$3d^{5}(a^{2}D)4s - 3d^{5}(a^{2}D)4p$	${}^{3}D - {}^{3}D^{\circ}$	1 - 2		927
640	1238.111	232.9108 - 313.6790	$3d^{5}(a^{2}D)4s - 3d^{5}(a^{2}D)4n$	${}^{3}D - {}^{3}D^{\circ}$	1-1		927
490	1238.209	225.6165 - 306.3778	$3d^{(a^{+}D)4s} - 3d^{(a^{+}D)4p}$	${}^{3}\mathbf{D} - {}^{3}\mathbf{P}^{\circ}$	2 - 2		927
280	1238 548	234 4127 - 315 1528	3d5(a4F)4e - 3d5(a4F)4n	⁵ F - ⁵ F°	2 - 1		927
200	1230.540	234.4127 - 313.1320	3u (a 1) 75 = 3u (a 1) 79p $3d^{5}(a^{2}D) Ac = 2d^{5}(a^{4}D) Am$		$\begin{vmatrix} 2 \\ 3 \\ 4 \end{vmatrix}$		027
000	1230.037	232.3437 - 313.2013	2d5(a4D)/e 2d5(a4D)/e	יתי תי			027
830	1238.098	210.1899 - 290.9193	30'(a'D)45 - 30'(a'D)4p		4-4		921
690	1238.962	208.1646 - 288.8779	3d'(a'G)4s - 3d'(a'P)4p	G - S	3-2		927
700	1239.051	216.1899 – 296.8970	3d ³ (a ⁺ D)4s - 3d ³ (a ⁺ G)4p	D - G	4-4		927
	1 1 2 2 0 5 4 0	774 0071 214 7564	742/0912340 242/0912340	1 21 2020			()'77

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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	400	1239.664	232.9108 - 313.5773	$3d^{5}(a^{2}D)4s - 3d^{5}(a^{2}D)4p$	${}^{3}D - {}^{3}P^{\circ}$	1 – 0		927
	240	1239.769	274.7386 - 355.3980	$3d^{5}(b^{2}G)4s - 3d^{5}(b^{2}G)4p$	${}^{3}G - {}^{3}G^{\circ}$	4 – 3		927
	660	1239.950	235.4206 - 316.0688	$3d^{5}(a^{2}F)4s - 3d^{5}(a^{2}F)4p$	${}^{3}F - {}^{3}G^{\circ}$	4 - 4		927
	210	1240.152	246.2409 - 326.8763	$3d^{5}(a^{2}H)4s - 3d^{5}(b^{2}F)4p$	${}^{1}H - {}^{3}F^{\circ}$	5 - 4		927
	650	1240.309	274.7735 - 355.3980	$3d^{5}(b^{2}G)4s - 3d^{5}(b^{2}G)4p$	${}^{3}G - {}^{3}G^{\circ}$	3 - 3		927
	590	1241.044	243.3315 - 323.9086	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{2}G)4p$	³ F - ³ H°	4 - 5		927
		12111011	213.3310 223.7000					, 2,
	120	1241.166	235.4206 - 315.9905	$3d^{5}(a^{2}F)4s - 3d^{5}(a^{2}H)4p$	${}^{3}F - {}^{3}H^{\circ}$	4 – 5		927
	780	1241.326	234.2752 - 314.8347	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ⁴ F)4p	⁵ F - ⁵ F°	3 - 2		927
	810	1241.422	233.8392 - 314.3920	3d ⁵ (a ² I)4s – 3d ⁵ (a ² I)4p	${}^{1}\mathbf{I} - {}^{1}\mathbf{I}^{\circ}$	6 - 6		927
	840	1241.630	229.4130 - 309.9525	3d ⁵ (a ² I)4s - 3d ⁵ (a ² I)4p	³ I – ³ H°	5 – 4		927
	810	1241.975	234.0821 - 314.5992	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ⁴ F)4p	⁵ F - ⁵ F°	5 - 4		927
	860	1242.072	229.4088 - 309.9195	$3d^{5}(a^{2}I)4s - 3d^{5}(a^{2}I)4p$	${}^{3}\mathbf{I} - {}^{3}\mathbf{H}^{\circ}$	6 – 5		927
	700	1242 124	220 4120 200 0105	2 45(-21)40 2 45(-21)40	31 3110			017
	700	1242.134	229.4130 - 309.9193	$30^{\circ}(a^{-1})4s = 30^{\circ}(a^{-1})4p$	1-H	5-5		927
	540	1242.645	234.1254 - 314.5992	3d ⁻ (a ⁺ F)4s - 3d ⁻ (a ⁺ F)4p	F - F	4 - 4		927
	800	1243.218	234.1254 - 314.5628	$3d^{3}(a^{*}F)4s - 3d^{3}(a^{*}F)4p$	$\mathbf{F} - \mathbf{F}$	4 - 3		927
	560	1243.326	235.7365 - 316.1654	3d ⁵ (a ² F)4s - 3d ⁵ (a ² F)4p	'F - 'F°	2 – 2		927
	530	1243.407	216.5905 - 297.0139	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ D)4p	$^{5}D - ^{5}D^{\circ}$	2 – 2		927
	770	1243.495	216.5960 - 297.0139	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}D)4p$	⁵ D – ⁵ D°	3 - 2		927
	230	1243 660	232 5459 - 312 9536	$3d^{5}(a^{2}D)As = 3d^{5}(a^{2}E)An$	³ D - ³ D°	3_3		977
	750	1243.000	216 1899 296 5740	$3d^{5}(a^{4}D)4a^{3}d^{5}(a^{4}D)4n$	5D 5D°	1 2		027
	000	1244.015	164 5350 244 0005	3u(aD)+s = 3u(aD)+p $2d^{5}(a^{6}S)/a = 2d^{5}(a^{6}S)/a$	D = D	4-3		927 037
	660	1244.174	104.3239 - 244.9003	30 (a 3)45 - 30 (a 3)4p	5- P	3-4		927
	520	1244.272			10.101			927
	170	1244.650	232.5459 - 312.8894	$3d^{2}(a^{2}D)4s - 3d^{2}(a^{2}F)4p$	^o D - ^o G ^o	3-3		927
	610	1244.772	229.4088 - 309.7436	$3d^{3}(a^{2}I)4s - 3d^{3}(a^{2}I)4p$	'I − 'K°	6 - 7		927
	790	1244.955	234.2752 - 314.5992	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{4}F)4p$	⁵ F - ⁵ F°	3 - 4		927
	690	1245.054	242.5043 - 322.8208	$3d^{5}(a^{2}G)4s - 3d^{5}(a^{4}F)4p$	${}^{3}G - {}^{3}F^{\circ}$	4 - 4		927
	870	1245 176	234 0821 - 314 3920	$3d^{5}(a^{4}F)4s = 3d^{5}(a^{2}I)4p$	⁵ F - 'I°	5-6		927
	530	1245 263	229 4406 - 309 7436	$3d^{5}(a^{2}I)4s = 3d^{5}(a^{2}I)4p$	31_ ¹ K°	7 _ 7		927
	600	1245.265	222.1100 - 303.1130	$3d^{5}(a^{2}D)Aa = 3d^{5}(a^{2}E)Ab$	30 30	2 2		027
	850	1245.439	225.5451 - 305.8381	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}D)4p$	$^{3}D - ^{3}P^{\circ}$	1-1		927
	650	1245.522	234.2752 - 314.5628	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ⁴ F)4p	⁵ F - ⁵ F°	3 – 3		927
	80	1245.988	243.2662 - 323.5232	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ⁴ F)4p	${}^{3}F - {}^{3}F^{\circ}$	2 – 3		927
	350	1246.115	235.1165 - 315.3661	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{2}F)4p$	⁵ F - ³ D°	1 – 2		927
	250	1246.353	232.6556 - 312.8894	$3d^{5}(a^{2}D)4s - 3d^{5}(a^{4}F)4p$	${}^{3}D - {}^{5}G^{\circ}$	2 - 3		927
	570	1246.535	225.6165 - 305.8381	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}D)4p$	$^{3}D - ^{3}P^{\circ}$	2 - 1		927
	710	1246.821	268.2739 - 348.4779	$3d^{5}(b^{2}D)4s - 3d^{5}(b^{2}D)4p$	¹ D - ¹ P°	2 – 1		927
	820	1247 269	262 7357 342 0057	$2d^{5}(h^{2}D)A_{0} = 2d^{5}(h^{2}D)A_{0}$	30 30			027
	740	1247.308	203.7337 - 343.9037	$3d^{2}(-4E)A_{0} = 2d^{2}(-4E)A_{0}$	$3E^{3E^{\circ}}$	2-2		927
	740 570	1247.000	245.5705 - 525.5252	$30^{\circ}(a + f) + 8 = 30^{\circ}(a + f) + 9$	$\Gamma - \Gamma$	3-3		927
	5/0	1247.004	234.4127 - 314.5628	$3d^{2}(a^{2}F)4s - 3d^{2}(a^{2}F)4p$	F = F	2-3		927
	650	1248.031	234.0821 - 314.2088	$3d^{2}(a^{2}F)4s - 3d^{2}(a^{2}F)4p$	$\mathbf{F} - \mathbf{F}$	5 - 4		927
	380	1248.081	232.6556 - 312.7782	3d'(a2D)4s - 3d'(a4F)4p	[°] D – [°] G°	2 – 2		927
	240	1248.217	242.5043 - 322.6176	3d3(a2G)4s - 3d3(a3F)4p	³ G – ³ D°	4 - 3		927
	550	1248.435	263.8058 - 343.9057	3d ⁵ (b ² D)4s - 3d ⁵ (b ² D)4p	$^{3}D - ^{3}D^{\circ}$	3 - 2		927
	730	1248.485	246,2409 - 326,3371	$3d^{5}(a^{2}H)4s - 3d^{5}(a^{2}G)4p$	¹ H – ¹ H°	5 - 5		927
	630	1248 814	247 2818 - 327 3566	$3d^{5}(b^{2}E)4s = 3d^{5}(a^{2}H)4p$	³ E - ¹ H°	4 - 5		927
	930	1240.014	235 1165 - 315 1528	$3d^{5}(a^{4}E)Ac = 3d^{5}(a^{4}E)An$	5E 5E°	4 -5		927
	860	1249.432	200 1310 200 1616	$3d(a^{2})+3=3d(a^{2})+p$ $3d(a^{4}C)/a=3d(a^{4}C)/m$	$\Gamma = \Gamma$	5 4	i	927
	830	1250.033	208.1637 - 288.1616	$3d^{5}(a^{4}G)4s - 3d^{5}(a^{4}G)4p$	⁵ G - ⁵ F°	3 - 4		927
	890	1250.384	208.0464 - 288.0216	$3d^{5}(a^{4}G)4s - 3d^{5}(a^{4}G)4p$	⁵ G - ⁵ H°	6 – 7		927
	740	1250.541	239.1077 - 319.0734	$3d'(a^2D)4s - 3d'(a^2D)4p$	$\mathbf{D} - \mathbf{P}^{\circ}$	2 – 1		927
	430	1250.675	242.8626 - 322.8208	$3d^{(a^{2}G)4s} - 3d^{(a^{4}F)4p}$	${}^{3}G - {}^{3}F^{\circ}$	5 - 4		927
	480	1250.772	235.4206 - 315.3701	$3d^{5}(a^{2}F)4s - 3d^{5}(a^{2}G)4p$	³ F - ³ H°	4 – 4		927
	260	1250.893	307.0252 - 386.9688	$3d^{5}(c^{2}D)4s - 3d^{5}(c^{2}D)4p$	${}^{3}D - {}^{3}F^{\circ}$	2 - 2		927
	220	1251.283	232.5459 - 312.4633	$3d^{5}(a^{2}D)4s - 3d^{5}(a^{2}F)4p$	${}^{3}D - {}^{3}G^{\circ}$	3 - 3		927
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Multiplet	el. Int.	$\lambda_{\rm v.sc}$ (in Å)	Levels (in 10^3 cm 1)	Configurations	Terms	J - J	Notes	Reference
	890	1251.821	217.0487 - 296.9329	3d5(a4G)4s - 3d5(a4G)4p	${}^{3}G - {}^{3}G^{\circ}$	5 - 5		927
	790	1252.055	232.9108 - 312.7782	3d ⁵ (a ² D)4s - 3d ⁵ (a ⁴ F)4p	³ D – ⁵ G°	1 – 2		927
	880	1252.155	307.1051 - 386.9688	$3d^{5}(c^{2}D)4s - 3d^{5}(c^{2}D)4p$	${}^{3}D - {}^{3}F^{\circ}$	1 – 2		927
	830	1252.267	229.4088 - 309.2640	3d ⁵ (a ² I)4s - 3d ⁵ (a ² I)4p	${}^{3}\mathbf{I} - {}^{3}\mathbf{H}^{\circ}$	6 - 6		927
	680	1252.336	229.4130 - 309.2640	$3d^{5}(a^{2}I)4s - 3d^{5}(a^{2}I)4p$	${}^{3}I - {}^{3}H^{\circ}$	5-6		927
	620	1252.383	217.0487 - 296.8970	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	³ G – ³ G°	5 – 4		927
	440	1252.467	225.5451 - 305.3869	3d ^s (a ⁴ D)4s - 3d ⁵ (a ⁴ D)4p	$^{3}D - ^{3}P^{\circ}$	1 – 0		927
	720	1252.707	236.4541 - 316.2803	$3d^{5}(a^{2}F)4s - 3d^{5}(a^{2}F)4p$	³ F - ³ F°	3 - 3		927
	870	1252.765	229.4406 - 309.2640	3d ⁵ (a ² I)4s - 3d ⁵ (a ² I)4p	${}^{3}\mathbf{I} - {}^{3}\mathbf{H}^{\circ}$	7 - 6		927
	680	1253.004	232.6556 - 312.4633	3d ⁵ (a ² D)4s - 3d ⁵ (a ² F)4p	${}^{3}D - {}^{3}G^{\circ}$	2 – 3		927
	580	1253.086	217.1291 - 296.9329	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	³ G – ³ G°	4 – 5		927
	850	1253.191	208.1637 - 287.9600	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	⁵ G – ⁵ F°	4 – 3		927
	810	1253.290	217.1291 - 296.9193	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ D)4p	³ G – ⁵ D°	4 - 4		927
	820	1253.486	263.7009 - 343.4782	$3d^{5}(b^{2}D)4s - 3d^{5}(b^{2}D)4p$	${}^{3}\mathbf{D} - {}^{3}\mathbf{D}^{\circ}$	1-1		927
	610	1253.588	247,1049 - 326.8763	3d ⁵ (b ² F)4s - 3d ⁵ (b ² F)4p	${}^{3}F - {}^{3}F^{\circ}$	3 - 4		927
	850	1253.654	217.1291 - 296.8970	$3d^{5}(a^{4}G)4s - 3d^{5}(a^{4}G)4p$	³ G – ³ G°	4 - 4		927
	870	1253.983	217.1010 - 296.8471	$3d^{5}(a^{4}G)4s - 3d^{5}(a^{4}G)4p$	³ G – ³ G°	3 - 3		927
	710	1254.187	240.1938 - 319.9265	$3d^{5}(a^{2}F)4s - 3d^{5}(a^{2}F)4p$	${}^{1}\mathbf{F} - {}^{1}\mathbf{D}^{\circ}$	3 - 2		927
	790	1254 412	243.2662 - 322.9845	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ⁴ F)4p	${}^{3}\mathbf{F} - {}^{3}\mathbf{D}^{\circ}$	2 - 1		927
	470	1254.530	2364541 - 3161654	$3d^{(a^{2}F)4s} - 3d^{(a^{2}F)4p}$	${}^{3}\mathbf{F} - {}^{3}\mathbf{F}^{\circ}$	3 - 2		927
	550	1254.850	247 0491 - 326 7390	$3d^{5}(a^{2}G)4s - 3d^{5}(a^{2}G)4p$	'G - 'F°	4 - 3		927
	220	1255 565	234 2752 - 313 9198	$3d^{5}(a^{4}F)4s = 3d^{5}(a^{2}D)4n$	⁵ F - ³ D °	3 - 3		927
	740	1255.505	232 6556 - 312 2910	$3d^{5}(a^{2}D)4s = 3d^{5}(a^{2}D)4p$	$^{3}D - ^{3}P^{\circ}$	2 - 1		927
	520	1255.810	235.7365 - 315.3661	$3d^{(a^{2}F)4s} - 3d^{(a^{2}F)4p}$	${}^{3}\mathbf{F} - {}^{3}\mathbf{D}^{\circ}$	2 - 2		927
	760	1256.010	208 1646 - 287 7821	$3d^{5}(a^{4}G)4s = 3d^{5}(a^{4}P)4n$	⁵ G - ⁵ D°	3-2		927
	170	1256.00	208.1040 - 287.7821	$3d^{5}(a^{4}G)As = 3d^{5}(a^{4}P)An$	⁵ G - ⁵ D°	2 - 1		927
	210	1256 292	208.1515 - 287.7555	$3d^{5}(a^{4}G)As = 3d^{5}(a^{4}G)An$	'G - 'H'	6-6		927
	500	1256 422	208.0404 = 287.0437 235.7365 = 315.3262	$3d^{5}(a^{2}E)4s = 3d^{5}(a^{2}D)4p$	³ F - ¹ F°	2-3		927
	490	1256 818	255.7505 - 515.5202	50 (a 1)+3 - 50 (a 12)+p		2.5		927
	730	1256.900	279.1995 - 358.7600	3d ^s (b ² G)4s - 3d ^s (b ² G)4p	'G - 'G°	4 – 4		927
	410	1256 080	240 9596 - 320 5138	$3d^{5}(a^{2}H)4s = 3d^{5}(a^{2}G)4n$	${}^{3}H - {}^{3}F^{\circ}$	4 - 3		927
	500	1257 120	263 7357 - 343 2810	$3d^{5}(h^{2}D)4s = 3d^{5}(h^{2}D)4p$	$^{3}D - ^{3}F^{\circ}$	2 - 3		927
	300	1257.129	203.7337 - 343.2810	$3d^{3}(a^{4}G)As = 3d^{5}(a^{4}G)Ap$	SG-SH°	5-6		927
	800	1257.020	208.1310 - 287.0439	$3d^{5}(a^{4}E)As = 3d^{5}(a^{4}E)An$	$3\mathbf{F} = 3\mathbf{F}^{\circ}$	4_4		927
	600	1258.014	243.3313 - 322.8208	3d(a T) + s = 3d(a T) + p $3d^{5}(b^{2}D) 4s = 3d^{5}(b^{2}D) 4p$	$^{3}D - {}^{3}F^{\circ}$	3_3		927
	460	1258.238	232.5459 - 312.0083	$3d^{(0)}(a^{2}D)4s - 3d^{(0)}(a^{2}F)4p$ $3d^{(a^{2}D)4s - 3d^{(a^{2}F)4p}$	³ D - ¹ G°	3 - 4		927
	620	1258.525	247.2818 - 326.7390	3d°(b°F)4s – 3d°(a°G)4p	$\mathbf{F} - \mathbf{F}$	4-3		927
	530	1259.024	240.1938 - 319.6202	3d"(a-F)4s - 3d"(a-F)4p	F - G	3-3		927
	780	1259.118	232.5459 - 311.9665	3d (a ⁻ D)4s - 3d (a ⁻ D)4p	$D - P^{*}$	3-2	1	927
	650	1259.183	235.7365 - 315.1528	$3d^{\circ}(a^{2}F)4s - 3d^{\circ}(a^{2}F)4p$	$\mathbf{F} - \mathbf{F}$	2-1		927
	800 800	1259.576	229.4130 - 308.8041 234.0821 - 313.4647	3d (a ⁻ 1)4s - 3d (a ⁻ 1)4p 3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ⁴ F)4p	⁵ F - ⁵ G [•]	5-5		927 927
					in ior			027
	820	1260.401	234.1254 - 313.4647	3d (a*F)4s - 3d (a*F)4p	F-G	4-5		927
	180	1260.748	246.2409 - 325.5586	3d'(a°H)4s - 3d'(b°F)4p	H - G	3-4		92/
	80	1260.870	232.0550 - 311.9665	3d"(a*D)4s = 3d"(a*D)4p		2-2		027
	100	1261.109	212.0958 - 291.3900	3d (a ⁻ P)4s - 3d (a ⁻ P)4p	P - P	3-2		927
	820 850	1261.222	247.0491 - 326.3371 235.4206 - 314.7022	30 (a°G)4s - 30 (a°G)4p 30 (a°F)4s - 30 (a°G)4p	³ F - ³ G°	4-5		927 927
								027
	800	1261.430	279.1995 - 358.4756	3d'(b'G)4s - 3d'(b'G)4p	'G - 'H°	4 - 5		927
	90	1261.564	234.4127 - 313.6790	3d'(a'F)4s - 3d'(a'D)4p	'F - 'D'	2 - 1		927
	850	1261.745	216.1899 - 295.4443	3d ^s (a ⁴ D)4s - 3d ^s (a ⁴ D)4p	`D - `F°	4 - 5		927
	20	1262.134			1- 1-			927
	700	1262.535	274.7386 - 353.9441	$3d^{5}(b^{2}G)4s - 3d^{5}(b^{2}G)4p$	'G - 'F°	4 - 3		927

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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm 1)	Configurations	Terms	J - J	Notes	References
	490	1262.727	263.7009 - 342.8946	3d ⁵ (b ² D)4s - 3d ⁵ (b ² D)4p	${}^{3}\mathbf{D} - {}^{3}\mathbf{F}^{\circ}$	1 – 2		927
	20	1262.974	235.4206 - 314.5992	$3d^{5}(a^{2}F)4s - 3d^{5}(a^{4}F)4p$	${}^{3}\mathbf{F} - {}^{5}\mathbf{F}^{\circ}$	4 - 4		927
	110	1263.090	274.7735 - 353.9441	3d ^s (b ² G)4s – 3d ^s (b ² G)4p	'G - 'F°	3 – 3		927
	690	1263.290	263.7357 - 342.8946	3d ⁵ (b ² D)4s – 3d ⁵ (b ² D)4p	$^{3}D - ^{3}F^{\circ}$	2 – 2		927
	770	1263.333	234.1254 - 313.2813	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ⁴ F)4p	⁵ F – ⁵ G°	4 – 4		927
	410	1263.569	235.4206 - 314.5628	$3d^{5}(a^{2}F)4s - 3d^{5}(a^{4}F)4p$	³ F – ⁵ F°	4 – 3		927
	330	1263.622	212.2534 - 291.3900	3d ⁵ (a ⁴ P)4s - 3d ⁵ (a ⁴ P)4p	⁵ P – ⁵ P°	2 - 2		927
	20	1264.002	221.0876 - 300.2010	3d ⁵ (a ⁴ P)4s - 3d ⁵ (a ⁴ D)4p	³ P – ⁵ P°	2 – 3		927
	90	1264.245	235.7365 - 314.8347	3d ⁵ (a ² F)4s - 3d ⁵ (a ⁴ F)4p	${}^{3}F - {}^{5}F^{\circ}$	2 – 2		927
	90	1264.253	235.7365 - 314.8347	3d ⁵ (a ² F)4s - 3d ⁵ (a ⁴ F)4p	³ F - ⁵ F°	2 – 2		927
	710	1264.426	212.4557 - 291.5417	3d ⁵ (a ⁴ P)4s - 3d ⁵ (a ⁴ P)4p	${}^{5}\mathbf{P} - {}^{5}\mathbf{P}^{\circ}$	1 - 1		927
	870	1264.518	164.5259 - 243.6085	3d ⁵ (a ⁶ S)4s - 3d ⁵ (a ⁶ S)4p	${}^{7}\mathbf{S} - {}^{7}\mathbf{P}^{\bullet}$	3 – 3		927
	430	1264.629	212.2534 - 291.3285	3d ⁵ (a ⁴ P)4s - 3d ⁵ (a ⁴ G)4p	⁵ P - ³ F°	2 - 3		927
	700	1264.739						927
	670	1264.920	247.2818 - 326.3371	3d ⁵ (b ² F)4s - 3d ⁵ (a ² G)4p	³ F – ¹ H°	4 – 5		927
	860	1265.655	241.7736 - 320.7831	3d ⁵ (a ² H)4s - 3d ⁵ (a ² H)4p	³ H – ³ I°	6 – 7		927
	830	1265.722	234.2752 - 313.2813	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ⁴ F)4p	⁵ F – ⁵ G°	3 - 4		927
	290	1265.874	208.1310 - 287.1280	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	⁵ G - ⁵ H°	5 - 5		927
	280	1266.124	247.0491 - 326.0299	3d ⁵ (a ² G)4s - 3d ⁵ (b ² F)4p	¹ G - ³ F°	4 - 3		927
	870	1266.395	208.1637 - 287.1280	$3d^{5}(a^{4}G)4s - 3d^{5}(a^{4}G)4p$	⁵ G – ⁵ H°	4 - 5		927
	510	1266.697	240.1938 - 319.1387	3d ⁵ (a ² F)4s - 3d ⁵ (a ² G)4p	¹ F – ¹ G°	3 – 4		927
	800	1266.859	212.4557 - 291.3900	3d5(a4P)4s - 3d5(a4P)4p	${}^{5}\mathbf{P} - {}^{5}\mathbf{P}^{\circ}$	1 - 2		927
	470	1267.027	247.1049 - 326.0299	3d ⁵ (b ² F)4s - 3d ⁵ (b ² F)4p	³ F - ³ F°	3 – 3		927
	260	1267.140						927
	860	1267.275	229.4088 - 308.3173	3d ⁵ (a ² I)4s - 3d ⁵ (a ² I)4p	³ I - ³ I°	6 - 7		927
	850	1267.803	229.4406 - 308.3173	3d ⁵ (a ² I)4s - 3d ⁵ (a ² I)4p	${}^{3}\mathbf{I} - {}^{3}\mathbf{I}^{\circ}$	7 - 7		927
	780	1267.885	236.4541 - 315.3262	3d5(a2F)4s - 3d5(a2D)4p	${}^{3}\mathbf{F} - {}^{1}\mathbf{F}^{\circ}$	3 - 3		927
	390	1267.985	247.1650 - 326.0299	3d ⁵ (b ² F)4s - 3d ⁵ (b ² F)4p	³ F - ³ F°	2 - 3		927
	640	1268.170	274.6954 - 353.5487	3d ⁵ (b ² G)4s - 3d ⁵ (b ² G)4p	³ G – ³ H°	5 – 5		927
	480	1268.746	247.1650 - 325.9822	$3d^{5}(b^{2}F)4s - 3d^{5}(b^{2}F)4p$	${}^{3}\mathbf{F} - {}^{3}\mathbf{F}^{\circ}$	2 - 2		927
	750	1268.871	274.7386 - 353.5487	3d ⁵ (b ² G)4s - 3d ⁵ (b ² G)4p	³ G - ³ H°	4 - 5		927
	710	1269.243	235.4206 - 314.2088	3d5(a2F)4s - 3d5(a2F)4p	³ F - ³ F°	4 – 4		927
	810	1269.372	241.0822 - 319.8604	3d ⁵ (a ² H)4s - 3d ⁵ (a ² H)4p	${}^{3}H - {}^{3}I^{\circ}$	5 - 6		927
	580	1269.620	234.1254 - 312.8894	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ⁴ F)4p	⁵ F – ⁵ G°	4 – 3		927
	600	1270.186	242.2904 - 321.0183	3d ⁵ (a ² G)4s - 3d ⁵ (a ² G)4p	${}^{3}G - {}^{3}F^{\circ}$	3 - 2		927
	870	1270.677	229.4406 - 308.1388	$3d^{s}(a^{2}I)4s - 3d^{s}(a^{2}I)4p$	${}^{3}\mathbf{I} - {}^{3}\mathbf{K}^{\circ}$	7 – 8		927
	640	1271.252	212.0958 - 290.7570	3d ⁵ (a ⁴ P)4s - 3d ⁵ (a ⁴ P)4p	⁵ P - ⁵ P°	3 - 3		927
	720	1271.432	274.6954 - 353.3471	3d ⁵ (b ² G)4s - 3d ⁵ (b ² G)4p	${}^{3}G - {}^{3}F^{\circ}$	5 - 4		927
	660	1272.025	234.2752 - 312.8894	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ⁴ F)4p	⁵ F - ⁵ G°	3 - 3		927
	50	1272.148	274.7386 - 353.3471	3d ⁵ (b ² G)4s - 3d ⁵ (b ² G)4p	³ G – ³ F°	4 – 4		927
	700	1272.637	208.1310 - 286.7066	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	5G − 5H°	5 – 4		927
	660	1272.710	274.7735 - 353.3471	3d ⁵ (b ² G)4s - 3d ⁵ (b ² G)4p	³ G – ³ F°	3 – 4		927
	110	1272.775						927
	30	1272.857	235.1165 - 313.6790	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{2}D)4p$	${}^{5}\mathbf{F} - {}^{3}\mathbf{D}^{\circ}$	1 – 1		927
	870	1273.198	208.1646 - 286.7066	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	⁵ G – ⁵ H°	3 - 4		927
	560	1273.728	247.0491 - 325.5586	3d ⁵ (a ² G)4s - 3d ⁵ (b ² F)4p	¹ G - ¹ G°	4 - 4		927
	830	1273.809	212.2534 - 290.7570	3d ⁵ (a ⁴ P)4s - 3d ⁵ (a ⁴ P)4p	⁵ P - ⁵ P°	2 - 3		927
	780	1274.252	234.4127 - 312.8894	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ⁴ F)4p	⁵ F – ⁵ G°	2 – 3		927
	20	1274.491						927
	720	1275.906	274.6954 - 353.0716	3d ⁵ (b ² G)4s - 3d ⁵ (b ² G)4p	³ G – ³ H°	5 - 4		927
	850	1276.415	216.5960 - 294.9396	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ D)4p	5D - 5F°	3-4		927
	160	1276.603	274.7386 - 353.0716	3d ⁵ (b ² G)4s - 3d ⁵ (b ² G)4p	³ G - ³ H°	4 - 4		927
	360	1276.882	217.1291 - 295.4443	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ D)4p	³ G - ⁵ F°	4 - 5		927
	690	1276.945	164.5259 - 242.8370	3d ⁵ (a ⁶ S)4s - 3d ⁵ (a ⁶ S)4p	⁷ S ~ ⁷ P°	3 - 2		927
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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	Referenc
	220	1277.183	274.7735 - 353.0716	3d ⁵ (b ² G)4s - 3d ⁵ (b ² G)4p	³ G - ³ H°	3 - 4		927
	290	1277 658	239 1077 - 317 3768	$3d^{5}(a^{2}D)4s - 3d^{5}(a^{2}H)4p$	${}^{1}D - {}^{3}G^{\circ}$	2-3		927
	20	1278 387	242 2904 - 320 5138	$3d^{5}(a^{2}G)4s - 3d^{5}(a^{2}G)4n$	${}^{3}G - {}^{3}F^{\circ}$	3 - 3		927
	140	1278.537	242.2204 = 320.3136	$3d^{5}(a^{2}G)4s - 3d^{5}(a^{2}G)4n$	${}^{3}G - {}^{3}F^{\circ}$	5-4		927
	140	1278.874	242.0020 - 321.0304	$3d^{5}(a^{2}E)4s = 3d^{5}(a^{2}D)4n$	³ F - ³ D°	2 - 3		927
	590	1279.030	212.0958 - 290.2620	$3d^{5}(a^{4}P)4s - 3d^{5}(a^{4}P)4p$	⁵ P - ⁵ D ^o	3 - 4		927
	570	1279.529						
	650	1279.708	208.1515 - 286.2936	$3d^{5}(a^{4}G)4s - 3d^{5}(a^{4}G)4p$	⁵ G - ⁵ H°	2 - 3		927
	120	1279.926	208.1646 - 286.2936	3d ⁻ (a ⁺ G)4s - 3d ⁻ (a ⁺ G)4p	G - H	3-3		927
	520	1280.105	247.1049 - 325.2229	3d ³ (b ² F)4s - 3d ³ (a ² G)4p	°F – `G°	3 - 4		927
	80	1280.274	247.1049 - 325.2119	3d ⁵ (b ² F)4s - 3d ⁵ (a ² G)4p	` F − ` G °	3 - 3		927
	210	1281.269	247.1650 - 325.2119	3d ⁵ (b ² F)4s - 3d ⁵ (a ² G)4p	' F - 'G°	2 - 3	}	927
	60	1281.875	242.5043 - 320.5138	$3d^{5}(a^{2}G)4s - 3d^{5}(a^{2}G)4p$	³ G - ³ F°	4 - 3		927
	600	1282.247	229.4130 - 307.3997	3d ⁵ (a ² I)4s - 3d ⁵ (a ² I)4p	${}^{3}I - {}^{3}I^{\circ}$	5-6		927
	550	1282.740	229.4406 - 307.3997	$3d^{5}(a^{2}I)4s - 3d^{5}(a^{2}I)4p$	${}^{3}I - {}^{3}I^{\circ}$	7-6	1	927
	120	1283.177	247.0491 - 324.9802	$3d^{5}(a^{2}G)4s - 3d^{5}(a^{2}G)4p$	¹ G - ³ G°	4 - 5		927
	160	1283 941	221 0876 - 298 9723	$3d^{5}(a^{4}P)4s - 3d^{5}(a^{4}D)4p$	${}^{3}\mathbf{P} - {}^{3}\mathbf{D}^{\circ}$	2 - 3		927
	560	1284 470	2165905 - 2944433	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}D)4p$	⁵ D - ⁵ F°	2 - 3		927
	470	1284.550	216.5960 - 294.4433	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}D)4p$	⁵ D - ⁵ F°	3 - 3		927
							ł	027
	300	1285.808	253.9052 - 331.6782	3d'(a-S)4s - 3d'(a-S)4p	5 - P	1-2		927
	270	1286.111	236.4541 - 314.2088	3d (a F)4s - 3d (a F)4p	$\mathbf{F} - \mathbf{F}$	3-4		927
	20	1286.465	234.2752 - 312.0083	3d'(a'F)4s - 3d'(a'F)4p	³ F - 'G°	3 - 4		927
	610	1287.576	232.5459 - 310.2126	3d ⁵ (a ² D)4s - 3d ⁵ (a ² D)4p	³ D – ³ F°	3 - 4		927
	590	1287.656	235.1165 - 312.7782	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{4}F)4p$	⁵ F - ⁵ G°	1 – 2		927
	480	1287.800	216.4347 - 294.0860	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ D)4p	⁵ D – ⁵ F°	1 - 2		927
	30	1288.519	242.2904 - 319.8991	3d ⁵ (a ² G)4s - 3d ⁵ (a ⁴ F)4p	³ G - ³ G°	3 - 4		927
	310	1289.830	216.3054 - 293.8338	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}D)4p$	⁵ D - ⁵ F°	0 - 1		927
	380	1290.393	216.5905 - 294.0860	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}D)4p$	⁵ D - ⁵ F°	2 - 2	{	927
	220	1290.479	216,5960 - 294,0860	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}D)4p$	⁵ D - ⁵ F°	3 - 2		927
	20	1290 872	236 4541 - 313 9198	$3d^{5}(a^{2}F)4s - 3d^{5}(a^{2}D)4p$	${}^{3}\mathbf{F} - {}^{3}\mathbf{D}^{\circ}$	3 - 3		927
	320	1292.013	216.4347 - 293.8338	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}D)4p$	⁵ D - ⁵ F°	1 – 1		927
	50	1202 179	242 2004 210 6202	245(a ² C)4a 245(a ⁴ E)4a	3G 3G	3_3		927
	50	1293.178	242.2904 - 319.6202	3d(a'G)4s - 3d(a'F)4p	10-0 10 10	3-3		027
	420	1295.286	212.0958 - 289.2980	30'(a'P)4s - 30'(a'P)4p	P - D	3-3		927
	490	1295.761	235.1165 - 312.2910	3d (a ⁺ F)4s - 3d (a ⁺ D)4p	$\mathbf{F} - \mathbf{P}$	1-1		927
	490	1296.198	242.5043 - 319.6527	3d ³ (a ² G)4s - 3d ³ (a ⁴ F)4p	G - G	4-5		927
	30	1297.731	239.1077 - 316.1654	$3d^{3}(a^{2}D)4s - 3d^{3}(a^{2}F)4p$	'D - 'F'	2 - 2	1	927
	70	1297.983	235.7365 - 312.7782	$3d^{(a^{2}F)4s} - 3d^{(a^{4}F)4p}$	°F - 'G°	2 - 2		927
	630	1298.733	242.8626 - 319.8604	3d ⁵ (a ² G)4s - 3d ⁵ (a ² H)4p	³ G - ³ I°	5 - 6		927
	160	1300.224	212.2534 - 289.1630	3d ⁵ (a ⁴ P)4s - 3d ⁵ (a ⁴ G)4p	⁵ P – ⁵ F°	2 - 1		927
	610	1300.981	178.0198 - 254.8850	$3d^{5}(a^{6}S)4s - 3d^{5}(a^{6}S)4p$	⁵ S – ⁵ P°	2 - 1		927
	90	1301.600	216.5905 - 293.4200	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ P)4p	${}^{5}D - {}^{3}P^{\circ}$	2 - 1		927
	490	1302,175						927
	530	1302.380	212.0958 - 288.8779	3d ⁵ (a ⁴ P)4s - 3d ⁵ (a ⁴ P)4p	⁵ P - ⁵ S°	3 - 2		927
	100	1302 833	221 0876 - 297 8425	$\frac{1}{3}d^{5}(a^{4}P)4s = 3d^{5}(a^{4}P)4n$	³ P - ³ D°	2 - 2		927
	660	1302.833	221.0370 - 277.0423	$3d^{5}(a^{2}F)4s = 3d^{5}(a^{2}F)4n$	${}^{3}F - {}^{3}G^{\circ}$	2 - 3		927
	170	1203.049	233.7303 - 312.4033	$3d^{5}(h^{2}E)As = 3d^{5}(a^{4}E)Ar$	${}^{3}F - {}^{3}F^{\circ}$	2 - 2		927
	620	1303.908	247.1030 - 323.0331	3d ⁵ (a ² I)4e 2d ⁵ (a ² I)4n	${}^{3}I = {}^{3}I^{\circ}$	5_5		927
	030	1304.800	227.4130 - 300.0490	3d (a 1) + 5 - 3d (a 1) + p $3d (a^{4}D) As = 2d (a^{4}D) A$	50 500	2 2		927
	610	1305.061	212.2534 - 288.8779 229.4088 - 305.9963	$3d^{5}(a^{2}I)4s - 3d^{5}(a^{2}I)4p$	³ I - ³ K°	6-7		927
	550	1305.933						927
	660	1306.237	229.4406 - 305.9963	3d'(a'I)4s - 3d'(a'I)4p	1 – K°	7-7		927
		1306 614	208 0464 - 284 5795	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	`G - `G°	6 - 6		927
	700	1500.014	200.0404 - 204.5775					1
	700 590	1307.595	178.0198 - 254.4956	$3d^{5}(a^{6}S)4s - 3d^{5}(a^{6}S)4p$	⁵ S - ⁵ P°	2 – 2		927
	700 590 100	1307.595	178.0198 - 254.4956 253.9052 - 330.3707	$3d^{5}(a^{6}S)4s - 3d^{5}(a^{6}S)4p$ $3d^{5}(a^{2}S)4s - 3d^{5}(a^{2}S)4p$	⁵ S - ⁵ P° ³ S - ³ P°	2 - 2		927 927

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Multiplet Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
100	1309.149				-		927
530	1309.656	208.0464 - 284.4025	$3d^{5}(a^{4}G)4s = 3d^{5}(a^{4}G)4p$	⁵ G - ⁵ G°	6-5		927
530	1310.082	221 0876 - 297 4181	$3d^{5}(a^{4}P)4s = 3d^{5}(a^{4}P)4p$	³ P - ³ D ^o	2-3		927
480	1310 249	$243 \ 3315 = 319 \ 6527$	$3d^{5}(a^{4}F)4s = 3d^{5}(a^{4}F)4p$	$^{3}F - ^{3}G^{\circ}$	4 - 5		927
250	1310.819	243.3315 - 319.6327	$3d^{5}(a^{4}F)4s = 3d^{5}(a^{4}F)4p$	$^{3}F - ^{3}G^{\circ}$	4-3		927
670	1311 106	243.3310 - 313.0202	$3d^{5}(a^{4}G)As = 3d^{5}(a^{4}G)Ap$	5G 5G	5 5		927
070	1311.100	208.1310 - 284.4023	50 (a 0)45 - 50 (a 0)4p	0-0	5-5		927
580	1311.551	241.0822 - 317.3273	$3d^{5}(a^{2}H)4s - 3d^{5}(a^{2}H)4p$	${}^{3}H - {}^{3}H^{\circ}$	5 - 6		927
610	1312.031	239.1077 - 315.3262	$3d^{3}(a^{2}D)4s - 3d^{3}(a^{2}D)4p$	'D - 'F'	2 - 3		927
650	1312.706	229.4130 - 305.5908	3d ³ (a ² I)4s - 3d ³ (a ² I)4p	°І – 'К°	5-6		927
630	1313.303	208.1637 - 284.3089	3d°(a*G)4s - 3d°(a*G)4p	°G – °G°	4 - 4		927
710	1314.330	208.1 64 6 - 284.2490	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	°G – °G°	3 - 3		927
710	1314.330	246.2409 - 322.3242	$3d^{s}(a^{2}H)4s - 3d^{s}(a^{2}H)4p$	'H – 'I°	5 - 6		927
700	1314.681	208.1515 - 284.2155	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	⁵ G – ⁵ G°	2 - 2		927
330	1314.909	208.1646 - 284.2155	$3d^{5}(a^{4}G)4s - 3d^{5}(a^{4}G)4p$	⁵ G - ⁵ G°	3 - 2	P	927
300	1314.992	232.5459 - 308.5920	$3d^{5}(a^{2}D)4s - 3d^{5}(a^{2}D)4p$	${}^{3}D - {}^{3}F^{\circ}$	3 - 3	Р	927
550	1315.269						927
450	1315.663	225.5451 - 301.5530	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}D)4p$	${}^{3}D - {}^{3}F^{\circ}$	1 - 2		927
110	1315.975	221.4290 - 297.4179	$3d^{5}(a^{4}P)4s - 3d^{5}(a^{4}D)4p$	${}^{3}P - {}^{5}D^{\circ}$	1-1		927
50	1216 207						0.27
50	1316.307	222 (55) 200 5020	215/2014 215/2014	100 1000			927
590	1316.912	232.6556 - 308.5920	$3d^{2}(a^{2}D)4s = 3d^{2}(a^{2}D)4p$	$^{\circ}D - ^{\circ}F^{\circ}$	2 - 3		927
420	1317.035	240.9596 - 316.8878	$3d^{\circ}(a^{-}H)4s - 3d^{\circ}(a^{-}H)4p$	H – 'G'	4 - 4		927
670	1317.436	233.8392 - 309.7436	$3d^{-}(a^{-}1)4s - 3d^{-}(a^{-}1)4p$	'1 – 'K'	6 - 7		927
330	1317.962	240.1938 - 316.0688	$3d^{3}(a^{2}F)4s - 3d^{3}(a^{2}F)4p$	'F - 'G°	3 – 4		927
520	1318.148	212.0958 - 287.9600	3d ⁵ (a ⁴ P)4s - 3d ⁵ (a ⁴ G)4p	⁵ P – ⁵ F°	3 - 3		927
670	1318.360						927
690	1318.513	178.0198 - 253.8627	$3d^{5}(a^{6}S)4s - 3d^{5}(a^{6}S)4p$	⁵ S – ⁵ P°	2 - 3		927
70	1318.920	247.1650 - 322.9845	$3d^{5}(b^{2}F)4s - 3d^{5}(a^{4}F)4p$	${}^{3}\mathbf{F} - {}^{3}\mathbf{D}^{\circ}$	2 - 1		927
420	1319.153	241.0822 - 316.8878	$3d^{5}(a^{2}H)4s - 3d^{5}(a^{2}H)4p$	${}^{3}H - {}^{3}G^{\circ}$	5-4		927
220	1319.745	247.0491 - 322.8208	$3d^{5}(a^{2}G)4s - 3d^{5}(a^{4}F)4p$	$^{1}G = {}^{3}F^{\circ}$	4 - 4		927
100	1320.200	243.3315 - 319.0762	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{2}H)4p$	³ F - ³ I °	4 - 5		927
560	1320 707	225 2007 300 9181	2d ⁵ /a ⁴ D)4a 2d ⁵ /a ⁴ D)4a	3D 3E°	2 4		027
340	1320.707	223.2007 - 300.9181	$3d^{2}(a^{2}D)4s = 3d^{2}(a^{2}D)4p$	D - F	3-4		927
240	1320.896	212.2534 - 287.9600	$3d^{\circ}(a^{\circ}P)4s = 3d^{\circ}(a^{\circ}G)4p$	P - F	2 - 3		927
350	1321.252	212.0958 - 287.7821	$3d^{2}(a^{4}P)4s - 3d^{2}(a^{4}P)4p$	$\mathbf{P} - \mathbf{D}^{*}$	3 - 2		927
60	1323.296	247.0491 - 322.6176	$3d^{-}(a^{-}G)4s - 3d^{-}(a^{+}F)4p$	G - D	4 - 3		927
560	1323.550	241.7736 - 317.3273	$3d^{3}(a^{2}H)4s - 3d^{3}(a^{2}H)4p$	$H - H^{\circ}$	6 - 6		927
650	1323.986	217.1010 - 292.6310	3d°(a*G)4s – 3d°(a*G)4p	³ G − ³ H ^o	3 – 4		927
440	1324.466	217.1291 - 292.6310	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	${}^{3}\mathbf{G} - {}^{3}\mathbf{H}^{\circ}$	4 - 4		927
440	1324.751	221.0876 - 296.5740	3d ⁵ (a ⁴ P)4s - 3d ⁵ (a ⁴ D)4p	$^{3}P - ^{5}D^{\circ}$	2 – 3		927
420	1325.081	251.6549 - 327.1227	3d ⁵ (b ² F)4s – 3d ⁵ (b ² F)4p	'F - 'D°	3 - 2		927
20	1325.822	233.8392 ~ 309.2640	$3d^{5}(a^{2}I)4s - 3d^{5}(a^{2}I)4p$	${}^{1}I - {}^{3}H^{\circ}$	6 - 6		927
210	1327.473	247.1049 - 322.4364	$3d^{5}(b^{2}F)4s - 3d^{5}(a^{4}F)4p$	${}^{3}\mathbf{F} - {}^{3}\mathbf{D}^{\circ}$	3 - 2		927
590	1327.640	240.9596 - 316.2803	$3d^{5}(a^{2}H)4s - 3d^{5}(a^{2}F)4p$	${}^{3}\mathbf{H} - {}^{3}\mathbf{F}^{\circ}$	4 - 3		927
610	1328.019	212.4557 - 287.7555	$3d^{5}(a^{4}P)4s = 3d^{5}(a^{4}P)4n$	⁵ P - ⁵ D°	1 - 1		927
640	1329.372	217 1291 - 292 3534	$3d^{5}(a^{4}G)4s = 3d^{5}(a^{4}G)4r$	G_H	4_5		927
150	1330.063	232 5459 - 207 7311	$3d^{5}(a^{2}D)Ae = 3d^{5}(a^{2}D)Ae$		2 2 2		027
70	1331 412	216 4347 201 5417	3d (a D)45 ~ 3d (a D)4p		3-2		927
220	1331.413	210.4547 - 291.5417	$3d^{2}(a^{2}D)4s = 3d^{2}(a^{2}P)4p$	D - P	1-1		927
610	1332.845	232.0330 - 307.7311	50"(a-D)4s - 30"(a-D)4p	D- F	2 – 2		927
470	1332.989	225.5451 - 300.5633	3d ³ (a ⁴ D)4s - 3d ⁵ (a ⁴ D)4p	'D - 'D°	1 – 1		927
500	1333.351	225.2007 - 300.2010	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ D)4p	³ D – ⁵ P°	3 – 3		927
120	1333.561	241.0822 - 316.0688	$3d^{s}(a^{2}H)4s - 3d^{s}(a^{2}F)4p$	³ H – ³ G°	5 – 4		927
540	1333.958	233.8392 - 308.8041	3d ⁵ (a ² I)4s - 3d ⁵ (a ² I)4p	'I – 'H°	6 - 5		927
510	1334.184	216.5905 - 291.5417	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ P)4p	⁵ D – ⁵ P°	2 - 1		927
560	1334.992						927
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ultiplet Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	Referen
650	1336.157	217.0487 - 291.8914	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	³ G - ³ H°	5 - 6		927
180	1336.539	232.9108 - 307.7311	$3d^{5}(a^{2}D)4s - 3d^{5}(a^{2}D)4p$	³ D - ³ F°	1 - 2		927
170	1336.636	246.2409 - 321.0564	$3d^{5}(a^{2}H)4s - 3d^{5}(a^{2}G)4p$	¹ H - ³ F°	5 - 4		927
560	1337.049	235.4206 - 310.2126	$3d^{5}(a^{2}F)4s - 3d^{5}(a^{2}D)4p$	${}^{3}F - {}^{3}F^{\circ}$	4 - 4		927
670	1330.072	235.4200 = 310.2120 225.5451 = 300.2249	$3d^{5}(a^{4}D)4s = 3d^{5}(a^{4}D)4n$	$^{3}D - ^{3}D^{\circ}$	1-2		927
370	1340 350	225.5451 = 300.2249	$3d^{5}(a^{4}D)4s = 3d^{5}(a^{4}D)4p$	${}^{3}D - {}^{3}D^{*}$	2 - 2		927
370	1340.330	225.0105 - 500.2249	5u (a D)+s - 5u (a D)+p	2-2			/21
360	1341.074	216.1899 - 290.7570	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}P)4p$	⁵ D - ⁵ P°	4 - 3		927
630	1342.177	217.0487 - 291.5546	3d ³ (a ⁴ G)4s - 3d ³ (a ⁴ G)4p	G - F	5 – 4		927
230	1342.902	242.8626 - 317.3273	3d ³ (a ² G)4s - 3d ³ (a ² H)4p	'G – 'H°	5 - 6		927
190	1343.633	217.1291 - 291.5546	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	³ G - ³ F°	4 - 4		927
380	1343.898	240.9596 - 315.3701	3d ⁵ (a ² H)4s - 3d ⁵ (a ² G)4p	³ H – ³ H°	4 – 4		927
170	1347.222	217.1010 - 291.3285	3d ⁵ (a ⁴ G)4s - 3d ⁵ (a ⁴ G)4p	³ G - ³ F°	3 - 3		927
550	1347 743	217 1291 - 291 3285	$3d^{5}(a^{4}G)4s - 3d^{5}(a^{4}G)4p$	${}^{3}G - {}^{3}F^{\circ}$	4 - 3		927
110	1348 683	243 3705 - 317 5175	$3d^{5}(a^{4}F)4s = 3d^{5}(a^{4}F)4n$	³ F - ⁵ D°	3-2		927
560	1340.065	243.3703 - 317.5175	50 (a 1)+5 - 50 (a 1)+p	1 = D	5-2		927
190	1350 868	242 8626 - 316 8878	$3d^{5}(a^{2}G)4s = 3d^{5}(a^{2}H)4n$	³ G - ³ G°	5-4		927
220	1351.070	240 1028 314 2088	$3d^{5}(a^{2}E)4s = 3d^{5}(a^{2}E)4n$	$^{1}\mathbf{F} = {}^{3}\mathbf{F}^{0}$	3-4		927
220	1351.070	240.1730 - 314.2000	$2d_{1}^{5}(a^{4}C)A_{2} = 2d_{1}^{5}(a^{4}C)A_{-}$	C F	3 1		027
640	1351.419	217.1010 - 291.0977	50°(a C)45 - 50°(a C)4p	0-r	3-2		741
180	1353.134	251.6549 - 325.5586	3d ⁵ (b ² F)4s - 3d ⁵ (b ² F)4p	'F − 'G°	3 - 4		927
260	1353.878	243.3705 - 317.2320	3d ⁵ (a ⁴ F)4s - 3d ⁵ (a ⁴ F)4p	³ F – ⁵ D°	3 - 3		927
120	1354.535	235.1165 - 308.9430	$3d^{5}(a^{4}F)4s - 3d^{5}(a^{2}D)4p$	⁵ F – [†] D°	1 - 2		927
370	1355.541	225.2007 - 298.9723	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}D)4p$	${}^{3}D - {}^{3}D^{\circ}$	3 - 3		927
350	1357 493	216 5960 - 290 2620	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}P)4p$	⁵ D - ⁵ D°	3 - 4		927
100	1358.166	217.1291 - 290.7570	$3d^{5}(a^{4}G)4s - 3d^{5}(a^{4}P)4p$	³ G – ⁵ P°	4 - 3		927
			2 150 JULY 2 150 JULY				027
150	1358.339	241.0822 - 314.7022	3d (a ⁻ H)4s - 3d (a ⁻ F)4p	H-U	5-5		927
50	1360.815	242.5043 - 315.9905	3d (a-G)4s - 3d (a-H)4p	G - H	4-5		927
20	1361.880	225.6165 - 299.0456	3d [*] (a ⁺ D)4s - 3d [*] (a ⁺ D)4p	D - P	2 - 2		927
80	1363.929	234.4127 - 307.7311	3d`(a ⁴ F)4s - 3d`(a ² D)4p	³ F - ³ F [•]	2 - 2		927
150	1366.027	242.8626 - 316.0688	3d ⁵ (a ² G)4s - 3d ⁵ (a ² F)4p	'G - 'G°	5 – 4		927
70	1366.690						927
270	1368 371	242 2904 - 315 3701	$3d^{5}(a^{2}G)4s - 3d^{5}(a^{2}G)4p$	³ G - ³ H°	3 - 4		927
130	1372 552	$216\ 3054 - 289\ 1630$	$3d^{5}(a^{4}D)4s - 3d^{5}(a^{4}G)4p$	⁵ D - ⁵ F°	0 - 1		927
200	1272 412	216.3034 - 209.1030	$3d^{5}(a^{4}D)4s = 3d^{5}(a^{4}G)4p$	'D - 'F'	1 - 2		927
290	1373.413	210.4347 - 207.2471	3d(aD)4s = 3d(aC)4p	יםי <u>סי</u>	2 3		027
200	13/5.3/6	210.5905 - 289.2980	3d(a'D)4s - 3d(a'P)4p		2-3	ļ	027
440	1376.195	242.5043 - 315.1682	3d (a G)4s - 3d (a F)4p	G - F	4-5		927
240	1376.315	216.5905 - 289.2471	3d [*] (a*D)4s - 3d [*] (a*G)4p	D - F	2 - 2		927
160	1379.217	240.9596 - 313.4647	3d5(a2H)4s - 3d5(a4F)4p	³ H – ⁵ G°	4 - 5		927
30	1379.556						927
100	1380.514	225.5451 - 297.9828	3d ⁵ (a ⁴ D)4s - 3d ⁵ (a ⁴ D)4p	³ D – ⁵ P°	1 - 1		927
170	1383.017	242.8626 - 315.1682	3d ⁵ (a ² G)4s - 3d ⁵ (a ⁴ F)4p	³ G - ⁵ F°	5 - 5		927
20	1383,489	216.5960 - 288.8779	$3d^{(a^{+}D)4s} - 3d^{(a^{+}P)4p}$	5D - 5S*	3 - 2		927
540	1384.873	233.8392 - 306.0490	$3d^{5}(a^{2}I)4s - 3d^{5}(a^{2}I)4p$	'I − ³ I°	6 - 5		927
620	1206 022	212.0050 204.2400	245(0+D)40 245(0+C)4-	SP SC	3 _ 2		927
530	1305.923	212.0730 - 204.2490	3d(a + j + s - 3d(a + G) + p) $2d^{2}(a^{2}G) A = 2d^{2}(a^{2}G) A $		4 4		927
70	1387.174	247.0491 - 319.1387	$30^{\circ}(a^{-}O)^{4}S = 30^{\circ}(a^{-}O)^{4}P$		4-4		027
20	1388.879	243.3705 - 315.3701	30 (a T)45 - 30 (a O)4p	$\mathbf{r} - \mathbf{H}$	5-4		927
240	1389.047	221.4290 - 293.4200	30 (a [*] P)4s - 30 (a [*] P)4p	P - P	1-1		927
220	1389.447	216.1899 - 288.1616	3d (a*D)4s - 3d (a*G)4p	D - F	4-4		927
490	1390.921	221.0876 - 292.9830	3d'(a*P)4s - 3d'(a*P)4p	'P – 'P °	2 - 2		927
120	1391.672	247.2818 - 319.1387	3d5(b2F)4s - 3d5(a2G)4p	³ F - ¹ G°	4 - 4		927
600	1392 484	240, 1938 - 312,0083	$3d^{5}(a^{2}F)4s - 3d^{5}(a^{2}F)4n$	¹ F - ¹ G°	3 - 4		927
560	1394 375	216 1899 - 287 9069	$3d^{(a^{+}D)4s} - 3d^{(a^{+}G)4p}$	⁵ D - ⁵ F°	4 - 5		927
440	1207 550	221 4290 202 0820	$3d^{5}(a^{4}P)Ae = 3d^{5}(a^{4}P)Ae$	3P _ 3P°	1-2		927
400	1397.330	221.4270 - 292.9030	240 240		4 2	FD	375 07
	1440.0	0.0 - 69.1561	3a° - 3a°	ga D - o P	- + - Z	F , F	575,92
			216 216		1 4 4	ED	275.00

NI V - Continued

Multiplet Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	1464.8	0.8897 - 69.1561	3d ⁶ – 3d ⁶	$ga^5D - b^3P$	3 - 2	F,P	375,927
	1471.3	0.8897 - 68.8547	3d° - 3d°	$ga^{5}D - b^{3}F$	3 - 3	F,P	375,927
	1474.3	0.8897 - 68.7187	3d ⁶ – 3d ⁶	$ga^5D - b^3F$	3 - 4	F,P	375,927
	1477.8	1.4899 - 69.1561	3d° – 3d°	$ga^5D - b^3P$	2 - 2	F,P	375,927
	1484.4	1.4899 - 68.8547	3d° - 3d°	$ga^5D - b^3F$	2 - 3	F,P	375,927
	1487.5	1.4899 - 68.7187	3d* - 3d*	$ga^{5}D - b^{3}F$	2 – 4	F,P	375,927
	1489.4	1.4899 - 68.6321	3d° – 3d°	$ga^{5}D - b^{3}F$	2 - 2	F.P	375,927
	1492.9	1.8715 - 68.8547	3d ⁶ – 3d ⁶	$ga^{5}D - b^{3}F$	1-3	F.P	375,927
	1497.9	1.8715 - 68.6321	3d ⁶ – 3d ⁶	$ga^{5}D - b^{3}F$	1 - 2	F.P	375,927
	1500.2	0.8897 - 67.5479	3d ⁶ – 3d ⁶	$ga^{5}D - b^{3}P$	3 - 1	F.P	375,927
	1502.1	2.0576 - 68.6321	3d° - 3d°	$ga^{5}D - b^{3}F$	0 - 2	F.P	375,927
	1513.8	1.4899 - 67.5479	3d° – 3d°	$ga^{5}D - b^{3}P$	2 - 1	F,P	375,927
	1522.6	1.8715 - 67.5479	3d° - 3d°	$ga^{5}D - b^{3}P$	1 - 1	F,P	375,927
	1532.6	1.4899 - 66.7378	3d ⁶ – 3d ⁶	$ga^{5}D - b^{3}P$	2-0	F.P	375,927
	1541.6	1.8715 - 66.7378	3d° – 3d°	$ga^{5}D - b^{3}P$	1-0	F.P	375,927
	1791.7	48.6070 - 104.4205	3d ⁶ – 3d ⁶	$a^{\dagger}D - b^{\dagger}D$	2 - 2	F.P	375,927
	1830.3	178.0198 - 232.6556	3d ⁵ (a ⁶ S)4s - 3d ⁵ (a ² D)4s	${}^{5}S - {}^{3}D$	2 - 2	F.P	375,927
	1834.0	178.0198 - 232.5459	3d ⁵ (a ⁶ S)4s - 3d ⁵ (a ² D)4s	${}^{5}S - {}^{3}D$	2 – 3	F,P	375,927
	1920.5	164.5259 - 216.5960	3d⁵(a°S)4s - 3d⁵(a⁴D)4s	⁷ S – ⁵ D	3 - 3	F,P	375,927
	1935.6	164.5259 - 216.1899	3d ⁵ (a ⁶ S)4s - 3d ⁵ (a ⁴ D)4s	${}^{7}S - {}^{5}D$	3 – 4	F,P	375,927

NICKEL VI (Ni ⁵⁺), Z = 28 Ground State $1s^22s^22p^63s^23p^63d^5(^6S_{5/2})$ (23 electrons) Ionization Potential [870 000] cm⁻¹; [108] eV

Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	180	224.703	67.0851 - 512.1132	3d ⁵ – 3d ⁴ (b¹D)4p	$a^2F - ^2D^\circ$	$\frac{7}{2} - \frac{5}{2}$		1093
	60	227.162	67.0851 - 507.3004	$3d^{5} - 3d^{4}(b^{1}D)4p$	$a^2F - {}^2F^\circ$	$\frac{1}{2} - \frac{1}{2}$		1093
	160	231.556	75.4417 - 507.3004	3d ⁵ – 3d ⁴ (b ¹ D)4p	$a^2G - {}^2F^\circ$	$\frac{9}{2} - \frac{7}{2}$		1093
	100	231.574	79.3914 - 511.2174	3d ⁵ - 3d ⁴ (b ¹ D)4p	$b^2 F - {}^2 D^\circ$	$\frac{5}{2} - \frac{3}{2}$		1093
	160	232.275	74.6277 - 505.1505	3d ⁵ – 3d⁴(b¹D)4p	$a^2G - {}^2F^\circ$	$\frac{7}{2} - \frac{5}{2}$		1093
	180	233.890	46.1044 - 473.6564	3d ⁵ – 3d ⁴ (b ³ F)4p	a⁴P – ⁴D°	$\frac{3}{2} - \frac{3}{2}$		1093
	220	233.969	45.8842 - 473.2924	3d⁵ – 3d⁴(b³F)4p	a⁴P – ⁴D°	$\frac{5}{2} - \frac{5}{2}$		1093
	130	234.010	46.3248 - 473.6564	3d ⁵ – 3d ⁴ (b ³ F)4p	$a^{4}P - {}^{4}D^{\circ}$	$\frac{1}{2} - \frac{3}{2}$		1093
	190	234.0/88	46.1044 - 473.2924	3d ⁵ – 3d ⁴ (b ³ F)4p	$a^4P - {}^4D^\circ$	$\frac{3}{2} - \frac{5}{2}$		1093
	300	234.403	45.8842 - 472.4973	3d ⁵ – 3d ⁴ (b ³ F)4p	a⁴P – ⁴D°	$\frac{5}{2} - \frac{7}{2}$		1093
	330	235.170	45.8842 - 471.1068	3d ⁵ - 3d ⁴ (b ³ P)4p	a ⁴ P – ⁴ S°	$\frac{5}{2} - \frac{3}{2}$		1093
	280	235.293	46.1044 - 471.1068	3d ⁵ - 3d ⁴ (b ³ P)4p	a⁴P ⁴S°	$\frac{3}{2} - \frac{3}{2}$		1093
	130	235.386	41.9209 - 466.7543	3d⁵ - 3d⁴(b³F)4p	a4G - 4G°	<u> </u>		1093
	140	235.414	46.3248 - 471.1068	3d ⁵ – 3d ⁴ (b ³ P)4p	a⁴P – ⁴S°	$\frac{1}{2} - \frac{3}{2}$		1093
	90	235.769	41.9209 - 466.0652	3d ⁵ – 3d⁴(b ³ F)4p	a⁴G - ⁴G°	<u><u><u></u></u><u><u></u><u></u><u></u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u></u>		1093
	50	235.790	42.0232 - 466.1337	3d ⁵ – 3d ⁴ (b ³ F)4p	a ⁴ G - ² F°	² / ₂ - ⁷ / ₂		1093
	70	235.825	42.0232 - 466.0652	$3d^{5} - 3d^{4}(b^{3}F)4p$	a⁴G – ⁴G°	$\frac{3}{2} - \frac{5}{2}$		1093
	40	236.399	50.6435 - 473.6564	3d ⁵ - 3d ⁴ (b ³ F)4p	a⁴D – ⁴D°	$\frac{1}{2} - \frac{3}{2}$		1093
	130	236.871	50.3310 - 472.4973	3d⁵ 3d⁴(b³F)4p	$a^4D - {}^4D^\circ$	$\frac{7}{2} - \frac{7}{2}$		1093
	150	237.124	50.7776 - 472.4973	3d ⁵ – 3d ⁴ (b ³ F)4p	$a^4D - {}^4D^\circ$	5 - 1		1093
	150	237.857	42.0232 - 462.4431	3d ⁵ – 3d ⁴ (b ³ P)4p	$a^4G - {}^4D^\circ$	3 - 7		1093
	190	237.909	50.7776 - 471.1068	3d ⁵ – 3d ⁴ (b ³ P)4p	$a^4D - {}^4S^\circ$	3-3		1093
	10	238.476	64.1524 - 483.4809	3d ⁵ – 3d ⁴ (b ³ F)4p	$a^2D - ^2D^\circ$	\$ - 3		1093
	390	238.550	41.9209 - 461.1183	3d ⁵ – 3d⁴(b³F)4p	a ⁴ G - ⁴ F°	$\frac{11}{2} - \frac{2}{2}$		1093

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tiplet Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm $^{-1}$)	Configurations	Terms	J - J Not	es Reference
260	238.890	42.0036 - 460.6036	3d ⁵ - 3d ⁴ (b ³ F)4p	a4G - 4F°	$\frac{5}{2} - \frac{3}{2}$	1093
390	238.941	42.0232 - 460.5359	3d ⁵ – 3d ⁴ (b ³ F)4p	a4G - 4F°	$\frac{9}{2} - \frac{7}{2}$	1093
210	239 029	42.0036 - 460.3646	$3d^{5} - 3d^{4}(b^{3}F)4p$	a ⁴ G - ⁴ F°	5-5	1093
310	239.046	42 0351 - 460 3646	$3d^5 - 3d^4(b^3F)4p$	$a^4G - {}^4F^\circ$	7 - 5	1093
510	239.071	61 1060 470 4818	$3d^5 - 3d^4(b^1G)4p$	$a^2I = {}^2H^\circ$	اِبْ لِبْ	1093
360	239.071	61 2795 - 479 4818	$3d^{5} - 3d^{4}(b^{1}G)4n$	$a^2I - {}^2H^\circ$	<u></u> <u></u> <u></u> <u></u> <u></u> <u></u> <u></u> <u></u> <u></u> <u></u> <u></u> <u></u> <u></u> <u></u> <u></u> <u></u> <u></u> <u></u> <u></u>	1093
300	239.110	01.2735 - 475.4018	50 - 50 (0 C)+p	a1- 11	2 2	1075
180	239.320	61.1960 - 479.0463	3d ⁵ – 3d ⁴ (b ¹ G)4p	$a^2I - {}^2G^*$	$\left \frac{11}{2} - \frac{9}{2} \right $	1093
70	239.808	45.8842 - 462.8841	3d° – 3d4(b'P)4p	a*P - *D*	2 - 2	1093
140	239.941	46.1044 - 462.8841	3d ⁵ – 3d⁴(b³P)4p	$a^4P - {}^4D^\circ$	$\frac{3}{2} - \frac{3}{2}$	1093
110	240.063	45.8842 - 462.4431	3d ⁵ - 3d ⁴ (b ³ P)4p	a⁴P – ⁴D°	$\frac{5}{2} - \frac{7}{2}$	1093
140	240.410	67.0851 - 483.0434	3d ⁵ – 3d⁴(b³F)4p	$a^2F - ^2D^\circ$	$\frac{7}{2} - \frac{5}{2}$	1093
120	240.536	45.8842 - 461.6226	$3d^{5} - 3d^{4}(b^{3}P)4p$	a⁴P - ⁴D°	$\frac{5}{2} - \frac{5}{2}$	1093
60	240 582	96 4612 - 512 1132	3d ⁵ - 3d ⁴ (b ¹ D)4n	$b^2D - ^2D^\circ$	$\frac{3}{2} - \frac{5}{2}$	1093
210	240.502	65 1735 480 7242	$3d^5 - 3d^4(b^1G)4n$	$a^2D - {}^2F^\circ$	3 5	1093
210	240.047	46 1044 461 4278	$3d^{5} - 3d^{4}(h^{3}B)/m$	aD = 1 $a^4D = 4D^9$	2^{-2} 3^{-2}	1003
130	240.771	40.1044 - 401.4378	3u - 3u (0 r) + p	a = 1	2 2 2	1093
90	240.830	50.3310 - 465.5527	30' - 30'(b'P)4p		$\frac{1}{2} - \frac{1}{2}$	1093
300	240.885	61.1960 - 476.3321	3d ² – 3d ² (b ² G)4p	a-1H	$\frac{1}{2} - \frac{1}{2}$	1093
90	240.946	68.4449 - 483.4809	3d° – 3d*(b°F)4p	$a^2F - D^2$	$\frac{2}{2} - \frac{2}{2}$	1093
180	241.104	96.4612 - 511.2174	3d ⁵ - 3d ⁴ (b ¹ D)4p	$b^2D - {}^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$	1093
100	241.167	45.8842 - 460.5359	3d ⁵ - 3d ⁴ (b ³ F)4p	a4P - 4F°	<u>\$</u> - 7	1093
160	241 268	50 3310 - 464 8078	$3d^5 - 3d^4(b^3F)4p$	a⁴D – ⁴G°	7 - 7	1093
100	241.200	50 7776 - 464 8078	$3d^{5} - 3d^{4}(b^{3}F)4n$	$a^{4}D - {}^{4}G^{\circ}$	\$ 1	1093
50	241.327	50 3710 463 3015	$3d^{5} - 3d^{4}(b^{3}P)4p$	$a^{4}D = {}^{4}P^{2}$	1 2 2	1093
100	242.140	50.7805 463.3015	$3d^{5} - 3d^{4}(b^{3}\mathbf{P})/m$	aD = 1 $a^{4}D = 4P^{2}$	2 - 2 3 5	1093
100	242.412	50.7805 - 465.5015	50 – 50 (0 F)4p	a D - 1	2 - 2	1075
180	242.576	86.5321 - 498.7730	3d ⁵ - 3d ⁴ (b ¹ D)4p	$a^2S - {}^2P^\circ$	$\frac{1}{2} - \frac{3}{2}$	1093
480	242.653	50.3310 - 462.4431	3d ⁵ − 3d ⁴ (b ³ P)4p	$a^4D - {}^4D^\circ$	$\frac{7}{2} - \frac{7}{2}$	1093
60	242.741	67.0851 - 479.0463	3d ⁵ – 3d⁴(b¹G)4p	$a^2F - C^{\circ}G^{\circ}$	$\frac{7}{2} - \frac{9}{2}$	1093
130	242.917	50.7776 - 462.4431	$3d^{5} - 3d^{4}(b^{3}P)4p$	a⁴D - ⁴D°	$\frac{5}{2} - \frac{7}{2}$	1093
60	243.084	61.1960 - 472.5795	$3d^{5} - 3d^{4}(b^{3}F)4p$	$a^2I - {}^2G^\circ$	₩ - ?	1093
270	243.403	50.7776 - 461.6226	3d ⁵ - 3d ⁴ (b ³ P)4p	a⁴D - ⁴D°	$\frac{5}{2} - \frac{5}{2}$	1093
00	242 422	50 2210 461 1192	24 ⁵ 24 ⁴ (b ³ E)4m	a ⁴ D ⁴ E°	Z 2	1093
90	243.432	50.3310 - 461.1183	3u = 3u (0 - 1)4p	aD = 1	2 2	1093
200	243.512	50.///6 - 461.43/8	3d' - 3d'(b'P)4p		2-2	1093
60	243.683	130.0259 - 540.3941	3d ³ – 3d⁺(b¹S)4p	$\mathbf{a}^{T}\mathbf{P} - \mathbf{P}^{T}$	1 1 - 1	1093
270	243.781	50.3310 - 460.5359	$3d^{5} - 3d^{4}(b^{3}F)4p$	a⁺D – ⁺F°	2 - 2	1093
110	243.927	50.6435 - 460.6036	3d⁵ – 3d⁴(b³F)4p	a ⁴ D – ⁴ F°	2-2	1093
160	244.008	50.7805 - 460.6036	$3d^{5} - 3d^{4}(b^{3}F)4p$	a ⁴ D - ⁴ F°	$\frac{3}{2} - \frac{3}{2}$	1093
150	244.051	50.7776 - 460.5359	$3d^{5} - 3d^{4}(b^{3}F)4p$	a ⁴ D - ⁴ F°	$\frac{5}{2} - \frac{7}{2}$	1093
210	244 150	50.7805 - 460.3646	$3d^5 - 3d^4(b^3F)4p$	a⁴D - ⁴F°	3-5	1093
50	244 270	64 1524 - 473 5319	$3d^5 - 3d^4(b^3F)4p$	$a^2D - C^{\circ}$	3 - 7	1093
60	244.250	67 0851 - 476 3321	$3d^{5} - 3d^{4}(h^{1}G)4n$	$a^2 \mathbf{F} = {}^2 \mathbf{H}^\circ$	2 9	1093
70	244.550	64 1524 472 8320	$3d^{5} = 3d^{4}(b^{3}P)An$	$a^2D = ^2P^\circ$	2 2	1093
20	244.088	69.4470 - 476.9356	$3d^{5} - 3d^{4}(b^{1}G)4p$	$a^{4}F - {}^{2}G^{\circ}$	$\begin{bmatrix} 2 & -2 \\ 5 \\ 2 & -\frac{7}{2} \end{bmatrix}$	1093
					7.5	
180	246.249	74.6277 - 480.7242	3d' – 3d'(b'G)4p	a G - F	$\left \frac{1}{12} - \frac{1}{2} \right $	1093
400	246.473	73.7566 - 479.4818	3d ⁵ – 3d⁴(b'G)4p	a ² H – ² H°	<u><u><u></u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>	1093
80	246.614	67.0851 - 472.5795	3d ⁵ – 3d ⁴ (b'F)4p	a²F – ⁻G°	$\frac{1}{2} - \frac{2}{2}$	1093
490	246.738	73.7566 - 479.0463	3d⁵ - 3d⁴(b¹G)4p	a ² H – ² G°	$\frac{11}{2} - \frac{9}{2}$	1093
110	246.785	68.4449 - 473.6564	3d ⁵ – 3d ⁴ (b ³ F)4p	$a^2F - {}^4D^\circ$	$\frac{5}{2} - \frac{3}{2}$	1093
60	246.861	68.4449 - 473.5319	3d ⁵ - 3d ⁴ (b ³ F)4p	$a^2F - C^\circ$	$\frac{5}{2} - \frac{7}{2}$	1093
200	247.040	75 4417 - 490 1903	3d5 - 3d4(h1G)4n	$a^2G - {}^2F^\circ$	2 1	1093
280	247.009	().1725 A72 7276	245 244/L3EVA-	a U = 1	$\begin{bmatrix} 2 & -2 \\ 3 & -1 \end{bmatrix}$	1003
140	247.180	4/3./2/0 49 2017 472 2024	345 244(L3E)/+		$2 - 2 \\ 1 - 2 \\ 5 \\ 1 - 5 \\ $	1093
180	247.225	08.8017 - 473.2924	30° - 30° (0° r')4p		$\begin{vmatrix} 2 & -\overline{2} \\ 5 & 3 \end{vmatrix}$	1093
40	247.396	69.4470 - 473.6564	3d - 3d (b F)4p	a'F - 'D'	$\left \frac{5}{5}-\frac{5}{1}\right $	1093
1 50	247.472	79.3914 - 483.4809	3d° – 3d*(b`F)4p	$\mathbf{b}^2 \mathbf{F} - \mathbf{D}^{\circ}$		1093
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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	150	247.560	68.5512 - 472.4973	3d⁵ – 3d⁴(b³F)4p	$a^{4}F - {}^{4}D^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		1093
	40	247.639	96.4612 - 500.2752	3d ⁵ – 3d⁴(b¹D)4p	$b^2D - {}^2P^\circ$	$\frac{3}{2} - \frac{1}{2}$		1093
	190	247.767	75.4417 - 479.0463	3d ⁵ – 3d ⁴ (b ¹ G)4p	$a^2G - {}^2G^\circ$	$\frac{9}{2} - \frac{9}{2}$		1093
	340	247.878	72.9088 - 476.3321	3d ⁵ – 3d⁴(b¹G)4p	$a^2H - {}^2H^\circ$	$\frac{\bar{9}}{2} - \frac{\bar{9}}{2}$		1093
	270	248.400	73.7566 - 476.3321	3d ⁵ - 3d ⁴ (b ¹ G)4p	$a^2H - {}^2H^\circ$	$\frac{11}{2} - \frac{9}{2}$		1093
	300	248.568	74.6277 – 476.9356	3d ⁵ – 3d ⁴ (b ¹ G)4p	$a^2G - {}^2G^\circ$	$\frac{7}{2} - \frac{7}{2}$		1093
	350	248 635	140 9222 - 543 1156	$3d^5 - 3d^4(b^1S)4p$	$c^2 \mathbf{D} = {}^2 \mathbf{P}^{\circ}$	5 3		1093
	40	248.689	140.9222 = 543.1150 141.0068 = 543.1156	$3d^{5} - 3d^{4}(b^{1}S)4p$	$c^2 D = r^2 P^2$	2 - 2 1 - 2		1093
	140	249.069	75 4417 - 476 9356	$3d^{5} - 3d^{4}(b^{1}G)4n$	$a^2G = {}^2G^\circ$	2 2 2 2 2 2 2		1093
	20	249 170	79 3914 - 480 7242	$3d^{5} - 3d^{4}(b^{1}G)4p$	$h^2 E - {}^2 E^\circ$	2 - 2 5 _ 5		1093
	510	249.611	72 9088 - 473 5319	$3d^{5} - 3d^{4}(b^{3}E)4n$	$a^2H = {}^2G^{\circ}$	2^{-2}_{2}		1093
	50	249.636	79.6083 - 480.1893	$3d^{5} - 3d^{4}(b^{1}G)4p$	$b^2F - {}^2F^\circ$	$\frac{2}{\frac{7}{2}} - \frac{2}{\frac{7}{2}}$		1093
	250	250 206	73 0000 473 5705	240.3014-		9 9		1002
	250	250.206	72.9088 - 472.5795	3d ² - 3d ² (b ² F)4p	$a^{2}H - G^{2}$	$\frac{1}{2} - \frac{1}{2}$		1093
	560	250.344	/9.6083 - 4/9.0463	3d ² - 3d ² (b ² G)4p	6-F	$\frac{1}{2} - \frac{1}{2}$		1093
	220	250.384	141.0068 - 540.3941	3d ² - 3d ² (b ² S)4p	$c^{2}D - P^{2}$	$\frac{5}{2} - \frac{1}{2}$		1093
	50	250.504	42.0232 - 441.2161	$3d^{2} - 3d^{2}(a^{2}D)4p$	$a^{*}G - F^{*}$	$\frac{1}{2} - \frac{1}{2}$		1093
	330	250.686	74.6277 - 473.5319	3d ² - 3d ² (b ² F)4p	a-G - 'G	$\frac{1}{2} - \frac{1}{2}$		1093
	540	250.738	/3./300 - 4/2.3/95	3 a [*] – 3 a [*] (b [*] F)4p	a-H - "G"	$\frac{1}{2} - \frac{1}{2}$		1093
	40	250.792	64.1524 - 462.8841	3d ⁵ – 3d⁴(b³P)4p	$a^2D - {}^4D^\circ$	$\frac{5}{2} - \frac{3}{2}$		1093
	470	251.128	68.5512 - 466.7543	3d ⁵ – 3d ⁴ (b ³ F)4p	$a^4F - {}^4G^\circ$	$\frac{9}{2} - \frac{11}{2}$		1093
	380	251.199	75.4417 - 473.5319	$3d^{5} - 3d^{4}(b^{3}F)4p$	$a^2G - {}^2G^\circ$	$\frac{5}{2} - \frac{7}{2}$		1093
	120	251.428	65.1735 - 462.9036	$3d^{5} - 3d^{4}(b^{3}P)4p$	$a^2D - {}^4P^\circ$	3-1		1093
	60	251.452	68.4449 - 466.1337	$3d^{5} - 3d^{4}(b^{3}F)4p$	$a^2F - {}^2F^\circ$	$\frac{1}{2} - \frac{7}{2}$		1093
	310	251.544	79.3914 - 476.9356	3d ⁵ – 3d ⁴ (b ¹ G)4p	$b^2 F - {}^2 G^\circ$	$\frac{5}{2} - \frac{7}{2}$		1093
	330	251.564	68.5512 - 466.0652	3d ⁵ - 3d⁴(b³F)4p	a⁴F - ⁴G°	2 - 2		1093
	180	251.678	79.6083 - 476.9356	$3d^{5} - 3d^{4}(b^{1}G)4p$	$b^2 F - {}^2 G^\circ$	1 1 - 1		1093
	520	251.722	107.8870 - 505.1505	$3d^{5} - 3d^{4}(b^{\dagger}D)4p$	$b^2G - {}^2F^\circ$	2 - 5		1093
	60	251.761	69.4470 - 466.6491	$3d^{5} - 3d^{4}(b^{3}F)4p$	$a^4F - {}^2F^\circ$	3-3		1093
	220	251.802	75.4417 - 472.5795	$3d^{5} - 3d^{4}(b^{3}F)4p$	$a^2G - {}^2G^\circ$	9 + 9		1093
	70	251.854	75.4417 - 472.4973	$3d^{5} - 3d^{4}(b^{3}F)4p$	$a^2G - {}^4D^\circ$	$\frac{5}{2} - \frac{7}{2}$		1093
	420	252.047	68.8017 - 465.5527	3d ⁵ – 3d ⁴ (b ³ P)4p	$a^4F - {}^2D^\circ$	7 - 5		1093
	340	252.062	79.6083 - 476.3321	$3d^{5} - 3d^{4}(b^{1}G)4p$	$b^2 F - {}^2 H^\circ$	7 - 9		1093
	130	252.088	69.4470 - 466.1337	$3d^5 - 3d^4(b^3E)4p$	$a^4 \mathbf{F} - \mathbf{F}^{\circ}$	1 1 - İ		1093
	150	252.151	69.4470 - 466.0342	$3d^{5} - 3d^{4}(b^{3}P)4p$	$a^4F - ^2D^\circ$	$\frac{2}{5} - \frac{3}{5}$		1093
	190	252.291	68.4449 - 464.8078	$3d^{5} - 3d^{4}(b^{3}F)4p$	$a^2F - {}^4G^\circ$	1 1 - Ž		1093
	250	252.362	68.5512 - 464.8078	$3d^{5} - 3d^{4}(b^{3}F)4p$	$a^4F - {}^4G^\circ$	$\frac{1}{2} - \frac{7}{2}$		1093
	140	252.386	67.0851 - 463.3015	3d ⁵ – 3d⁴(b³₽)4p	$a^2 \mathbf{F} = {}^4 \mathbf{P}^\circ$	7 5		1093
	200	252.523	68.8017 - 464.8078	$3d^5 - 3d^4(b^3F)4p$	$a^4 F - {}^4 G^\circ$	1 1 1		1093
	100	252.792	68.4449 - 464.0278	$3d^{5} - 3d^{4}(b^{3}F)4p$	$a^2 F - {}^4 G^\circ$	\$_\$		1093
	110	252.888	65.1735 - 460.6036	$3d^{5} - 3d^{4}(b^{3}F)4p$	$a^2D - {}^4F^\circ$	$\frac{1}{3} - \frac{1}{3}$		1093
	240	253.257	69.1735 - 464.0278	$3d^{5} - 3d^{4}(b^{3}F)4p$	a ⁴ F – ⁴ G°	3-5		1093
	110	253.435	69.4470 - 464.0278	$3d^{5} - 3d^{4}(b^{3}F)4p$	a⁴F – ⁴G°	$\frac{5}{2} - \frac{5}{2}$		1093
	250	253.461	67.0851 - 461.6226	3d ⁵ - 3d ⁴ (b ³ P)4n	$a^2F - {}^4D^\circ$	7 5		1093
	560	253.485	68.8017 - 463.3015	$3d^5 - 3d^4(b^3P)4p$	$a^4F - {}^4P^\circ$	1 1		1093
	510	253.524	68.4449 - 462.8841	$3d^5 - 3d^4(b^3P)4p$	$a^2 F - {}^4 D^\circ$	5 3		1093
	160	253.717	79.3914 - 473.5319	$3d^5 - 3d^4(b^3F)4p$	$b^2 F - {}^2 G^\circ$	5_1		1093
	110	253.808	50.7805 - 444.7842	$3d^5 - 3d^4(a^1D)4p$	$a^4D - {}^2D^\circ$	3 - 5		1093
	690	253.877	68.5512 - 462.4431	$3d^{5} - 3d^{4}(b^{3}P)4p$	a⁴F - ⁴D°	$\frac{2}{2} - \frac{2}{2}$		1093
	520	253.981	69,1735 - 462 9036	$3d^{5} - 3d^{4}(h^{3}P)4n$	a ⁴ F ⁴ P°	1 1		1093
	280	254.067	65 1735 - 458 7722	$3d^5 = 3d^4(a^3E)Aa$	$a^2D^2D^2$	2 2 2		1093
	540	254 105	41 9209 - 435 4594	$3d^{5} = 3d^{4}(a^{3}D)A_{2}$	aD = D	2 - 2 11 9		1093
	520	254,168	69.4470 - 462 8841	$3d^{5} - 3d^{4}(h^{3}P)Ah$	$a^4F = {}^4D^6$	2 - 2 5 - 3		1093
	60	254,273	67.0851 - 460.3646	$3d^5 = 3d^4(h^3F)4h$	$a^2 E = {}^4 E^\circ$	7 5		1093
	250	254,308	72.9088 - 466 1337	$3d^{5} - 3d^{4}(h^{3}F)4n$	$a^2H - F^{\circ}$	<u><u>2</u> <u>2</u> <u>2</u> <u>2</u> <u>2</u> <u>2</u> <u>2</u> <u>2</u> <u>2</u> <u>2</u></u>		1093
		20.000	12.7000 - 400.1357	50 - 50 (0 1)4p	an-r	2 - 2		1095

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Iultiplet Rel. Int	λ_{vac} (in Å)	Levels (in 10^3 cm^{-1})	Configurations	Terms	J - J	Notes	References
170	254.353	72.9088 - 466.0652	3d ⁵ - 3d ⁴ (b ³ F)4p	a²H – ⁴ G°	$\frac{9}{2} - \frac{9}{2}$	-	1093
470	254.393	42.0232 - 435.1162	3d ⁵ - 3d ⁴ (a ³ D)4p	a ⁴ G - ⁴ F°	$\frac{9}{2} - \frac{7}{2}$		1093
420	254.458	69.4470 - 462.4431	3d ⁵ - 3d ⁴ (b ³ P)4p	a ⁴ F – ⁴ D°	$\frac{1}{2} - \frac{1}{2}$		1093
270	254.472	79.6083 - 472.5795	3d ⁵ - 3d ⁴ (b ³ F)4p	b²F - ²G°	$\frac{1}{2} - \frac{9}{2}$		1093
660	254.570	68.8017 - 461.6226	3d ⁵ - 3d ⁴ (b ³ P)4p	a ⁴ F - ⁴ D°	$\frac{7}{2} - \frac{5}{2}$		1093
220	254.672	64.1524 - 456.8156	3d ⁵ - 3d ⁴ (a ¹ F)4p	$a^2D - ^2D^\circ$	$\frac{5}{2} - \frac{5}{2}$		1093
690	254,733	68.5512 - 461.1183	3d⁵ – 3d⁴(b³F)4p	a4F - 4F°	$\frac{9}{2} - \frac{9}{2}$		1093
80	254.810	69.1735 - 461.6226	$3d^{5} - 3d^{4}(b^{3}P)4p$	a ⁴ F - ⁴ D°	3-5		1093
470	254 897	68.8017 - 461.1183	3d ⁵ - 3d ⁴ (b ³ F)4p	a ⁴ F - ⁴ F°	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		1093
230	254 974	42 0036 - 434 2009	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^4G - {}^4F^\circ$	3-3		1093
300	255 043	68 4449 - 460 5359	$3d^{5} - 3d^{4}(h^{3}F)4p$	$a^2 F - {}^4 F^{\circ}$	3 - 1		1093
370	255.089	74.6277 - 466.6491	3d ⁵ - 3d ⁴ (b ³ F)4p	$a^2G - {}^2F^\circ$	$\frac{7}{2} - \frac{5}{2}$		1093
450	255 100	69 5512 460 5350	2d ⁵ - 3d ⁴ (h ³ F)4p	a⁴E _ 4E°	2_1		1093
430	255.109	68.3312 - 400.3333	$3d^{5} - 3d^{4}(b^{3}E)/m$	$a^2 \mathbf{F} = \mathbf{F}^{\circ}$	2 2 5 5		1093
5/0	255.155	68.9017 460.5350	$3d^{5} - 3d^{4}(b^{3}F)(h)$	a1 - 1 a4E - 4E°	2 2 2		1093
000	255.274	68.8017 - 460.3339	245 244(b3E)4=	ar - r	$\begin{vmatrix} 2 - 2 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\$		1093
80	255.385	68.8017 - 400.3040	245 2440-3E04-	$a \Gamma - \Gamma$			1093
120	255.426	/4.02// - 400.133/	$3d^{2} - 3d(0^{2}r)4p$ $3d^{5} - 3d^{4}(h^{3}r)4p$	a G - F	2^{-2}_{3}		1093
590	255.474	09.1735 - 400.0030	50 - 50 (0 P)4p		2 - 2		1075
60	255.528	42.0232 - 433.3712	3d ⁵ - 3d ⁴ (a ³ G)4p	a ⁴ G - ² G°	$\frac{9}{2} - \frac{9}{2}$		1093
330	255.630	69.1735 - 460.3646	3d ⁵ - 3d ⁴ (b ³ F)4p	a4F - 4F°	$\frac{3}{2} - \frac{5}{2}$		1093
270	255.696	69.4470 - 460.5359	3d ⁵ - 3d ⁴ (b ³ F)4p	a ⁴ F - ⁴ F°	$\frac{5}{2} - \frac{7}{2}$		1093
510	255,809	69.4470 - 460.3646	3d ⁵ - 3d ⁴ (b ³ F)4p	a ⁴ F - ⁴ F°	3 - 3		1093
110	255,907	42.0351 - 432.8001	$3d^{5} - 3d^{4}(a^{1}G)4p$	a ⁴ G - ² F°	$\frac{1}{2} - \frac{1}{2}$		1093
150	255.957	75.4417 - 466.1337	3d ⁵ – 3d ⁴ (b ³ F)4p	$a^2G - {}^2F^\circ$	$\frac{9}{2} - \frac{7}{2}$		1093
130	256.001	50 7776 - 441 4012	3d ⁵ - 3d ⁴ (a ³ D)4p	$a^4D - ^2D^\circ$	3-3		1093
150	256,196	68.4449 - 458.7722	$3d^{5} - 3d^{4}(a^{1}F)4p$	$a^2F - ^2D^\circ$	$\frac{5}{2} - \frac{3}{2}$		1093
190	256.571	0.0 - 389.7604	$3d^{5} - 3d^{4}(a^{5}D)4p$	ga ⁶ S - ⁴ P°	3 - 3		1093
250	256.587	67.0851 - 456.8156	$3d^{5} - 3d^{4}(a^{1}F)4p$	$a^2F - ^2D^\circ$	1 2 - 3		1093
320	256.675	69.1735 - 458.7722	$3d^{5} - 3d^{4}(a^{1}F)4p$	$a^4F - ^2D^\circ$	$\frac{1}{2} - \frac{1}{2}$		1093
140	256.716	50.6435 - 440.1686	3d ⁵ - 3d ⁴ (a ¹ S)4p	$a^4D - {}^2P^\circ$	$\frac{1}{2} - \frac{3}{2}$		1093
360	256 806	50.7776 - 440.1686	3d ⁵ - 3d ⁴ (a ¹ S)4p	a ⁴ D - ² P°	3-3		1093
440	256.828	75 4417 - 464 8078	$3d^{5} - 3d^{4}(b^{3}F)4p$	a ² G - ⁴ G°	<u><u>9</u> - <u>7</u></u>		1093
420	256.910	0.0 - 389.2434	$3d^{5} - 3d^{4}(a^{5}D)4p$	$ga^6S - ^6D^\circ$	3-1		1093
200	257 198	67 0851 - 455 8876	$3d^{5} - 3d^{4}(a^{1}F)4p$	$a^2 F - {}^2 G^{\circ}$	1 - 2		1093
1200	257.190	68 4449 - 456 8156	$3d^{5} - 3d^{4}(a^{1}F)4p$	$a^2 F - {}^2 D^\circ$	5 - 5		1093
150	257.593	72.9088 - 461.1183	3d ⁵ - 3d ⁴ (b ³ F)4p	a ² H – ⁴ F°	$\frac{2}{2} - \frac{2}{2}$		1093
220	257 615	46 1044 - 434 2816	3d ⁵ - 3d ⁴ (s ³ D)4n	a ⁴ P - ⁴ P°	3-1		1093
220	257.015	41,9209 - 430,0333	$3d^{5} - 3d^{4}(a^{3}G)4n$	a4G - 4G*	<u> </u>	1	1093
200	257.057	42 0232 - 430 0333	$3d^{2} - 3d^{4}(a^{3}G)4p$	a ⁴ G - ⁴ G°	1 2 11		1093
70	257.760	46 3248 - 434 2816	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^4P - {}^4P^\circ$	1 1 1		1093
590	257.831	0.0 - 387.8499	$3d^{5} - 3d^{4}(a^{5}D)4p$	$ga^6S - ^6D^6$	1 1 - 1		1093
200	258.014	41.9209 - 429.4863	$3d^{5} - 3d^{4}(a^{3}G)4p$	a ⁴ G - ⁴ G*	$\frac{11}{2} - \frac{9}{2}$		1093
210	258 002	42 0232 429 4863	3d ⁵ - 3d ⁴ (s ³ G)4n	a*G ~ *G*	2 2		1093
370	258.075	86 5321 - 473 8695	$3d^{3} - 3d^{4}(b^{3}P)4p$	$a^2S - {}^2P^\circ$	1-1		1093
250	258.170	79 3914 - 466 6491	$3d^{5} - 3d^{4}(b^{3}F)4p$	$b^2F - {}^2F^\circ$	5-5		1093
360	258 306	46 3248 - 433 4625	$3d^{5} - 3d^{4}(a^{3}D)4p$	a ⁴ P - ⁴ P°	1 - 1	1	1093
140	258.300	79 6083 - 466 6491	$3d^{5} - 3d^{4}(b^{3}E)4p$	$b^2 F - {}^2 F^\circ$	1 1 - 1		1093
130	258.397	75.4417 - 462.4431	3d ⁵ - 3d ⁴ (b ³ P)4p	a ² G - ⁴ D ⁴	$\frac{1}{2} - \frac{7}{2}$		1093
	269 474	64 1524 451 0412	3d5 2d4(a)E)4n	$a^2D = 2E^{\circ}$	5_5		1093
90	258.474	04.1324 - 431.0413	$3d^{5} - 3d(a^{2}\Gamma)^{4}P$	*G_*G*	2 2 2		1093
140	258.505	42.0232 - 428.8003	2d ⁵ 2d ⁴ (h ³ E)/h	$h^2 E = 2E^{\circ}$	2 2 2 5 7		1093
80	258.569	70 2014 466 0242	$3d^{5} = 3d(0^{2}\Gamma)^{4}P$	$b^2 E = 2D^2$	2 2 2		1093
480	258.637	/9.3914 - 400.0342	JU - JU (0 P)4p	$h^2 D^2 D^2$	2 2 2		1093
40	258.674	70.4012 - 483.0434	3d ² - 3d ² (0 ² F)4p 2d ³ 2d ⁴ (- ³ E)4-	$b^2E^2E^4$	2 2 2		1003
210	258.716	79.0083 - 466.1337	3a" - 3a"(b"F)4p	0.11.	2-2		1093
				1	1		

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Multiplet Re	el. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	210	258.755	42.0351 - 428.4965	3d⁵ - 3d⁴(a³G)4p	a ⁴ G – ⁴ G°	$\frac{7}{2} - \frac{5}{2}$		1093
	510	258.791	45.8842 - 432.2957	3d ⁵ – 3d ⁴ (a ³ D)4p	a⁴P – ⁴D°	$\frac{5}{2} - \frac{5}{2}$		1093
	130	258.867	86.5321 - 472.8330	$3d^{5} - 3d^{4}(b^{3}P)4p$	$a^2S - {}^2P^\circ$	1 - 3		1093
	440	258.941	46.1044 - 432.2957	$3d^{5} - 3d^{4}(a^{3}D)4p$	a⁴P – ⁴D°	3 - 5		1093
	610	258.962	0.0 - 386.1573	$3d^{5} - 3d^{4}(a^{5}D)4p$	ga ⁶ S – ⁴ P ^o	3-3		1093
	90	259.047	45.8842 - 431.9126	$3d^{5} - 3d^{4}(a^{3}D)4p$	a ⁴ P – ⁴ D°	$\frac{5}{2} - \frac{7}{2}$		1093
	520	259.103	79.6083 - 465.5527	3d ⁵ – 3d ⁴ (b ³ P)4p	$b^2 F - {}^2 D^\circ$	7 - 5		1093
	290	259.283	42.0232 - 427.7027	$3d^{5} - 3d^{4}(a^{3}G)4p$	$a^4G - {}^2H^\circ$	§_1		1093
	150	259.357	42.0036 - 427.5750	$3d^{5} - 3d^{4}(a^{3}F)4p$	$a^4G - {}^2G^\circ$	<u>\$</u> _ <u>7</u>		1093
	190	259.377	68.4449 - 453.9830	3d ⁵ - 3d ⁴ (a ¹ F)4p	$a^2 F - {}^2 G^\circ$	$\frac{1}{3} - \frac{1}{7}$		1093
	280	259.615	68.8017 - 453.9830	$3d^{5} - 3d^{4}(a^{1}F)4n$	$a^4F - {}^2G^\circ$	1 _ 1		1093
	620	259.650	50.3310 - 435.4594	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^4D - {}^4F^\circ$	$\frac{2}{2} - \frac{2}{2}$		1093
	210	259.682	42.0036 - 427.0960	3d⁵ - 3d⁴(a³F)4p	$a^4G - {}^2F^\circ$	<u> </u>		1093
	190	259,699	42.0351 - 427.0960	$3d^5 - 3d^4(a^3F)4p$	$a^4G - {}^2F^{\circ}$	1_5		1093
	360	259 797	461044 - 4310203	$3d^5 = 3d^4(a^3D)4p$	$a^4P - {}^4P^\circ$	3 5		1093
	230	259 830	46 1044 - 430 9719	$3d^{5} = 3d^{4}(a^{3}D)4n$	$a^4P = {}^4D^\circ$	3 3		1093
	360	259 891	67.0851 - 451.8594	$3d^{5} - 3d^{4}(a^{\dagger}E)Ap$	$a^2 \mathbf{F} = 2\mathbf{F}^{\circ}$	2 2		1093
	210	259.978	46.3248 - 430.9719	$3d^{5} - 3d^{4}(a^{3}D)4p$	a ⁴ P - ⁴ D°	$\frac{2}{1} - \frac{2}{2}$		1093
	720	260.057	41 0200 426 4510	245 244(2)(2)4-	-to -tue	шв		1002
	720	260.057	41.9209 - 426.4519	$3d^2 - 3d^2(a^3G)4p$	$a^{+}G - H^{-}$	17-7		1093
	230	260.131	/9.6083 - 464.0278	3d ² – 3d ² (b ² F)4p	b'F - 'G'	2 - 2		1093
	500	260.187	50.7776 - 435.1162	3d" - 3d"(a'D)4p	a*D - *F*	2 - 2		1093
	290	260.218	50.3310 - 434.6260	3d' - 3d'(a'D)4p	$a^{\dagger}D - {}^{\dagger}F^{\circ}$	2 - 2		1093
	340	260.238	96.4612 - 480.7242	3d ³ – 3d ⁴ (b ⁴ G)4p	$b^2D - F^{\circ}$	$\frac{2}{3} - \frac{2}{3}$		1093
	290	260.270	50.7805 - 434.9970	3d° − 3d⁴(a'G)4p	a ⁴ D - ² F°	2 - 2		1093
	790	260.351	0.0 - 384.0965	3d ⁵ - 3d ⁴ (a ⁵ D)4p	ga ⁶ S - ⁶ P°	$\frac{5}{2} - \frac{7}{2}$		1093
	230	260.446	67.0851 - 451.0413	$3d^{5} - 3d^{4}(a^{1}F)4p$	$a^2F - {}^2F^\circ$	$\frac{7}{2} - \frac{5}{2}$		1093
	530	260.522	50.7805 - 434.6260	$3d^{5} - 3d^{4}(a^{3}D)4p$	a⁴D – ⁴F°	$\frac{3}{2} - \frac{5}{2}$		1093
	790	260.592	0.0 - 383.7398	3d ⁵ - 3d ⁴ (a ⁵ D)4p	ga ⁶ S – ⁶ P°	$\frac{5}{2} - \frac{5}{2}$		1093
	630	260.661	50.6435 - 434.2816	3d ⁵ – 3d ⁴ (a ³ D)4p	a⁴D – ⁴P°	$\frac{1}{2} - \frac{1}{2}$		1093
	780	260.717	0.0 - 383.5578	3d ⁵ – 3d ⁴ (a ⁵ D)4p	ga°S – °P°	$\frac{5}{2} - \frac{3}{2}$		1093
	590	260.756	50.7805 - 434.2816	3d ⁵ - 3d ⁴ (a ³ D)4p	a⁴D - ⁴P°	$\frac{3}{2} - \frac{1}{2}$		1093
	490	260.808	50.7805 - 434.2009	$3d^{5} - 3d^{4}(a^{3}D)4p$	a⁴D - ⁴F°	$\frac{3}{2} - \frac{3}{2}$		1093
	190	260.976	68.4449 - 451.6229	$3d^{5} - 3d^{4}(a^{1}D)4p$	$a^2F - {}^2P^\circ$	$\frac{5}{2} - \frac{3}{2}$		1093
	280	261.058	68.8017 - 451.8594	3d ⁵ - 3d ⁴ (a ³ F)4p	$a^4F - {}^2F^\circ$	$\frac{7}{2} - \frac{7}{2}$		1093
	510	261.109	72.9088 - 455.8876	3d ⁵ - 3d ⁴ (a ¹ F)4p	$a^2H - {}^2G^\circ$	$\frac{9}{2} - \frac{9}{2}$		1093
	680	261.310	50.7776 - 433.4625	3d ⁵ – 3d ⁴ (a ³ D)4p	a⁴D – ⁴P°	$\frac{5}{2} - \frac{3}{2}$		1093
	660	261.436	42.0351 - 424.5370	3d ⁵ – 3d⁴(a ³ G)4p	a⁴G – ⁴H°	7 - 3		1093
	210	261.498	69.4470 - 451.8594	3d ⁵ - 3d ⁴ (a'F)4p	$a^4F - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		1093
	660	261.547	42.0232 - 424.3637	$3d^{5} - 3d^{4}(a^{3}G)4p$	a⁴G – ⁴H°	- <u><u><u></u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		1093
	440	261.622	79.3914 - 461.6226	$3d^{5} - 3d^{4}(b^{3}P)4p$	$b^2F - {}^4D^\circ$	\$ - 5		1093
	490	261.657	42.0351 - 424.2185	$3d^{5} - 3d^{4}(a^{3}G)4p$	a⁴G - ⁴F°	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		1093
	630	261.689	73.7566 - 455.8876	3d ⁵ - 3d ⁴ (a ¹ F)4p	a ² H – ² G°	$\frac{11}{2} - \frac{9}{2}$		1093
	680	261.804	50.3310 - 432.2957	3d ⁵ – 3d⁴(a³D)4n	$a^4D - {}^4D^\circ$	7 - 5		1093
	160	261.842	64.1524 - 446.0612	$3d^5 - 3d^4(a^1D)4n$	$a^2D - {}^2F^{\circ}$	2 2		1093
	340	261,888	41.9209 - 423.7633	$3d^5 - 3d^4(a^3G)4n$	$a^4G = {}^4F^{\circ}$	<u>1</u> 2		1093
	440	261.958	42.0232 - 423.7633	$3d^{5} - 3d^{4}(a^{3}G)An$	$a^{+}G = {}^{+}F^{\circ}$	2 2		1093
	160	261.982	42.0036 - 423.7105	$3d^{5} = 3d^{4}(a^{3}G)4n$	$a^{4}G = {}^{4}F^{\circ}$	\$ 3		1093
	270	262.028	42.0036 - 423.6458	3d ⁵ – 3d ⁴ (a ³ G)4p	$a^4G - {}^2F^\circ$	$\frac{2}{2} - \frac{2}{2}$		1093
	650	262.066	50 3310 - 431 9126	345 244(2)7)4-	a ⁴ D 4D°	2 7		1003
	280	262.111	50 7776 - 432 2957	$3d^{5} = 3d^{4}(a^{3}D)4p$	aD = D	2 - 2		1093
	650	262 235	42 0036 - 422 2414	ad5 ad4(aC)4p		2 - 2		1093
	460	262 255	42.0050 - 425.5414 42.0351 - 423.2414	30 - 30 (a C)4p	aG - H	$\frac{1}{2}$ $-\frac{1}{2}$		1093
	180	262 287	74 6277 - 455 2276	3d = 3d (a C) + p $2d^{5} = 2d^{4}(a C) + p$	aG - H	2 - 2		1093
	150	262 302	46 1044 - 427 3422	3d - 5d (a F)4p		3 5		1093
		202.502	-0.10++ - 427.3422	50 - 50 (a r)4p	ar-D	$\bar{2} - \bar{2}$		1093

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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	210	262.335	130.0259 - 511.2174	$3d^{5} - 3d^{4}(b^{1}D)4p$	$a^2P - ^2D^\circ$	$\frac{1}{2} - \frac{3}{2}$		1093
	230	262.372	50.7776 - 431.9126	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^4D - {}^4D^\circ$	3-3		1093
	410	262 416	72 9088 - 453 9830	$3d^{5} - 3d^{4}(a^{1}F)4n$	$a^2H - {}^2G^\circ$	9 - 7		1093
	510	262.410	42 0351 - 423 0652	$3d^{5} - 3d^{4}(a^{3}H)4p$	$a^4G - {}^2H^6$	$\frac{1}{2} - \frac{2}{3}$		1093
	180	262.447	793914 - 4603646	$3d^{5} - 3d^{4}(h^{3}F)4n$	$b^2 F - {}^4 F^\circ$	\$_\$		1093
	260	262.518	79.6083 - 460.5359	$3d^{5} - 3d^{4}(b^{3}F)4p$	$b^2F - {}^4F^\circ$	$\frac{2}{7} - \frac{2}{7}$		1093
	200	2021010						
	430	262.541	42.0036 - 422.8978	$3d^{5} - 3d^{4}(a^{3}G)4p$	$a^4G - {}^2F^\circ$	$\frac{2}{2} - \frac{2}{2}$		1093
	280	262.562	42.0351 - 422.8978	$3d^2 - 3d^3(a^3G)4p$	a'G - 'F	$\frac{5}{2} - \frac{5}{2}$		1093
	290	262.612	41.9209 - 422.7118	3d ³ – 3d [*] (a ³ H)4p	a'G - T	2 - 2		1093
	290	262.662	41.9209 - 422.6424	3d ³ – 3d ⁴ (a ³ H)4p	a'G - T	2 - 2		1093
	460	262.683	50.3310 - 431.0203	3d³ - 3d⁴(a³D)4p	a*D - *P*	2 - 2		1093
	330	262.723	42.0232 - 422.6424	3d ⁵ – 3d ⁴ (a ³ H)4p	a⁺G – ⁻I°	$\frac{3}{2} - \frac{11}{2}$		1093
	570	262.850	42.0036 - 422.4372	3d ⁵ - 3d ⁴ (a ³ F)4p	a⁴G - ⁴D°	$\frac{5}{2} - \frac{3}{2}$		1093
	390	262.931	50.6435 - 430.9719	$3d^{5} - 3d^{4}(a^{3}D)4p$	a⁴D – ⁴D°	$\frac{1}{2} - \frac{3}{2}$		1093
	490	262.963	42.0232 - 422.3066	$3d^{5} - 3d^{4}(a^{3}P)4p$	a ⁴ G - ⁴ D°	$\frac{9}{7} - \frac{7}{7}$		1093
	630	262 990	50 7776 - 431 0203	$3d^{5} - 3d^{4}(a^{3}D)4p$	a ⁴ D - ⁴ P°	5-5		1093
	560	263 026	50 7776 - 430 9719	$3d^5 - 3d^4(a^3D)4p$	$a^4D - {}^4D^\circ$	\$ _ 3		1093
	330	263.077	50.7805 - 430.8988	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^4D - {}^4D^\circ$	$\frac{1}{2} - \frac{1}{2}$		1093
				and and the s				1000
	490	263.352	61.1960 - 440.9179	3d' – 3d'(a'l)4p	$a^2I - {}^2H^3$	2 - 2		1093
	400	263.434	42.0036 - 421.6072	3d ³ – 3d ⁴ (a ³ F)4p	a*G - 2D*	2 - 2		1093
	300	263.605	74.6277 - 453.9830	$3d^{3} - 3d^{4}(a'F)4p$	a ² G – ² G°	1 - 2		1093
	500	263.653	42.0351 - 421.3243	3d ⁵ – 3d ⁴ (a ³ F)4p	$a^4G - {}^2D^\circ$	$\frac{1}{2} - \frac{2}{2}$		1093
	180	263.868	67.0851 - 446.0612	3d ⁵ – 3d ⁴ (a ¹ D)4p	$a^2 F - {}^2 F^\circ$	$\frac{7}{2} - \frac{5}{2}$		1093
	690	263.913	41.9209 - 420.8357	3d ⁵ - 3d ⁴ (a ³ F)4p	a⁴G – ⁴F°	$\frac{11}{2} - \frac{9}{2}$		1093
	190	263 984	42 0232 - 420 8357	$3d^{5} - 3d^{4}(a^{3}F)4p$	a⁴G – ⁴F°	9-9		1093
	520	264 022	61 2795 - 440 0392	$3d^{5} - 3d^{4}(a^{1})4p$	$a^{2}l - {}^{2}H^{\circ}$	मूं में		1093
[720	264.060	41 9209 - 420 6234	$3d^5 - 3d^4(a^3F)4n$	$a^4G - {}^4G^\circ$	ļų_ų		1093
	100	264.121	42.0223 420.6234	$3d^{5} - 3d^{4}(a^{3}E)4p$	$a^{4}G = {}^{4}G^{\circ}$	2 2 2 <u>1</u>		1093
	700	204.131	42.0232 - 420.0234	$3d^{5} - 3d^{4}(a^{3}E)/a$	$a^{4}C^{-4}F^{\circ}$	2 2 2		1093
	190	264.182	42.0232 - 420.3332 45.8842 - 424.3461	$3d^{5} - 3d^{4}(a^{3}G)4p$	$a^4P - {}^4F^\circ$	$\frac{2}{5} - \frac{2}{7}$		1093
						1 .		
	300	264.358	42.0351 - 420.3089	$3d^{3} - 3d^{4}(a^{3}P)4p$	a ⁴ G – ⁴ P°	2 - 2		1093
	150	264.440	41.9209 - 420.0800	3d ⁵ – 3d ⁴ (a ³ H)4p	a⁴G ~ ⁴G°	$\frac{11}{2} - \frac{9}{2}$		1093
	710	264.512	42.0232 - 420.0800	3d ⁵ – 3d ⁴ (a ³ H)4p	a⁴G – ⁴G°	$\frac{9}{2} - \frac{9}{2}$		1093
	190	264.614	46.3248 - 424.2354	3d ⁵ – 3d ⁴ (a ³ P)4p	$a^4P - {}^2P^\circ$	$\frac{1}{2} - \frac{3}{2}$		1093
	770	264.669	42.0351 - 419.8633	3d ⁵ – 3d⁴(a³H)4p	a⁴G – ⁴G°	$\frac{7}{2} - \frac{7}{2}$		1093
	350	264.718	45.8842 - 423.6458	$3d^{5} - 3d^{4}(a^{3}G)4p$	$a^4P - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		1093
	120	264 746	50 7805 - 428 4965	3d ⁵ - 3d ⁴ (a ³ G)4n	$a^{4}D = {}^{4}G^{\circ}$	3_5		1093
1	120	264.825	$46\ 1044 - 423\ 7105$	$3d^{5} - 3d^{4}(a^{3}G)4p$	$a^4P - {}^4F^\circ$	3_3		1093
	20	264.825	46.1044 423.7105	$3d^{5} - 3d^{4}(a^{3}P)4p$	$a^4P - ^2P^\circ$	1 1		1093
	20 600	204.808	40.1044 - 423.0408	$3d^{5} - 3d^{4}(a^{3}H)Ap$	$a^{4}G = {}^{4}G^{\circ}$	5 5		1093
1	540	204.979	42.0030 - 419.3903	$3d^{5} - 3d(a^{1})4p$	$a^4G^{-4}G^{\circ}$	7 5		1093
	210	265.002	42.0331 - 419.3903 64.1524 - 441.4012	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^2D - b^2$	$\frac{2}{5} - \frac{2}{5}$		1093
	250	265.103	79.6083 - 456.8156	$3d^{5} - 3d^{4}(a^{T}F)4p$	$b^2 F - D^\circ$	$\frac{1}{2} - \frac{1}{2}$		1093
	490	265.207	64.1524 - 441.2161	$3d^{2} - 3d^{2}(a^{2}D)4p$	$a^{-}D - F^{-}$	2 - 2		1093
	310	265.243	45.8842 - 422.8978	$3d^{3} - 3d^{*}(a^{*}G)4p$	$a^*P - F^*$	2 - 2		1093
1	530	265.397	46.1044 - 422.8978	$3d^{2} - 3d^{2}(a^{2}G)4p$	a'P - F	2 - 2		1093
	620	265.455	42.0036 - 418.7134	3d ³ - 3d ⁴ (a ³ P)4p	$a^{\dagger}G - {}^{\dagger}P^{\circ}$	5-5		1093
	600	265.511	41.9209 - 418.5536	30° - 30°(a°H)4p	a G - T	$\frac{1}{2} - \frac{1}{2}$		1093
	590	265.525	65.1735 - 441.7857	3d ⁵ - 3d ⁴ (a ³ D)4p	$a^2D - {}^2F^\circ$	$\frac{3}{2} - \frac{5}{2}$		1093
	420	265.565	45.8842 - 422.4372	$3d^{5} - 3d^{4}(a^{3}F)4p$	a⁴P – ⁴D°	$\frac{5}{2} - \frac{3}{2}$		1093
		265 611	42 0036 - 418 4908	$3d^{5} - 3d^{4}(a^{3}F)4p$	a⁴G – ⁴F°	2 - 3		1093
	550	1 200,011	12.0000 110.1000					
	550 680	265.658	45,8842 - 422.3066	$3d^{5} - 3d^{4}(a^{3}P)4p$	a⁴P - ⁴D°	$\frac{5}{2} - \frac{7}{2}$		1093
	550 680 730	265.658	45.8842 - 422.3066 42.0232 - 418.3688	3d ⁵ - 3d ⁴ (a ³ P)4p 3d ⁵ - 3d ⁴ (a ³ H)4p	a ⁴ P - ⁴ D° a ⁴ G - ² G°	$\frac{5}{2} - \frac{7}{2}$ $\frac{9}{2} - \frac{9}{2}$		1093 1093
	550 680 730 590	265.658 265.716 265.765	45.8842 - 422.3066 42.0232 - 418.3688 79.6083 - 455.8876	$3d^{5} - 3d^{4}(a^{3}P)4p$ $3d^{5} - 3d^{4}(a^{3}H)4p$ $3d^{5} - 3d^{4}(a^{1}F)4p$	$a^4P - {}^4D^\circ$ $a^4G - {}^2G^\circ$ $b^2F - {}^2G^\circ$	$\frac{5}{2} - \frac{7}{2}$ $\frac{9}{2} - \frac{9}{2}$ $\frac{7}{2} - \frac{9}{2}$		1093 1093 1093

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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10 ³ cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	190	265.795	65.1735 - 441.4012	3d ⁵ - 3d ⁴ (a ³ D)4p	$a^2D - {}^2D^*$	$\frac{3}{2} - \frac{5}{2}$		1093
	170	265.878	46.3248 - 422.4372	$3d^{5} - 3d^{4}(a^{3}F)4p$	a⁴P – ⁴D°	$\frac{1}{2} - \frac{3}{2}$		1093
	530	265.926	46.3248 - 422.3694	$3d^{5} - 3d^{4}(a^{3}F)4p$	$a^4P - {}^4D^\circ$	$\frac{1}{2} - \frac{1}{2}$		1093
	600	265.946	45.8842 - 421.8940	$3d^{5} - 3d^{4}(a^{3}F)4p$	$a^4P - {}^4D^\circ$	$\frac{5}{2} - \frac{5}{2}$		1093
	570	266.105	46.1044 - 421.8940	$3d^{5} - 3d^{4}(a^{3}F)4p$	a⁴P – ⁴D°	3-5		1093
	450	266.154	42.0036 - 417.7181	$3d^5 - 3d^4(a^3H)4p$	$a^4G \sim {}^2G^\circ$	5 - 7		1093
	450	200.101	1210000 1111101			2 2		1070
	280	266.180	42.0232 - 417.7181	$3d^{5} - 3d^{4}(a^{3}H)4p$	a⁴G – ² G°	$\frac{9}{2} - \frac{7}{2}$		1093
	650	266.227	41.9209 - 417.5384	3d ⁵ – 3d⁴(a³H)4p	a⁴G - ⁴G°	$\frac{11}{2} - \frac{11}{2}$		1093
	500	266.299	42.0232 - 417.5384	$3d^{5} - 3d^{4}(a^{3}H)4p$	a⁴G – ⁴G°	$\frac{9}{2} - \frac{11}{2}$		1093
	270	266.354	45.8842 - 421.3243	$3d^{5} - 3d^{4}(a^{3}F)4p$	$a^4P - ^2D^\circ$	$\frac{5}{2} - \frac{5}{2}$		1093
	670	266.473	61.2795 - 436.5503	$3d^{5} - 3d^{4}(a^{1}I)4p$	$a^{2}l - {}^{2}K^{\circ}$	$\frac{13}{2} - \frac{15}{2}$		1093
	690	266.493	41.9209 - 417.1641	$3d^{5} - 3d^{4}(a^{3}H)4p$	a⁴G – ⁴I°	$\frac{11}{2} - \frac{11}{2}$		1093
	590	266.565	42.0232 - 417.1641	3d ⁵ – 3d ⁴ (a ³ H)4p	a⁴G – ⁴I°	$\frac{9}{2} - \frac{11}{2}$		1093
	460	266.670	65.1735 - 440.1686	$3d^{5} - 3d^{4}(a^{1}S)4p$	$a^2D - {}^2P^\circ$	$\frac{3}{2} - \frac{3}{2}$		1093
	180	266.721	50.7776 - 425.7031	$3d^{5} - 3d^{4}(a^{3}P)4p$	$a^4D - {}^2D^\circ$	$\frac{5}{2} - \frac{3}{2}$		1093
	410	266.781	45.8842 - 420.7223	$3d^{5} - 3d^{4}(a^{3}P)4p$	a⁴P – ⁴S°	5-3		1093
	350	266.805	69.4470 - 444.2522	$3d^{5} - 3d^{4}(a^{1}D)4p$	a⁴F - ² D°	$\frac{5}{2} - \frac{3}{2}$		1093
	140	266.882	67.0851 - 441.7857	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^2F - {}^2F^\circ$	$\frac{7}{2} - \frac{5}{2}$		1093
	670	266.931	46.1044 - 420.7223	3d ⁵ - 3d ⁴ (a ³ P)4p	a ⁴ P - ⁴ S°	$\frac{3}{2} - \frac{3}{2}$		1093
	630	267.026	41.9209 - 416.4225	$3d^{5} - 3d^{4}(a^{3}F)4p$	a⁴G – ⁴G°	$\frac{11}{2} - \frac{9}{2}$		1093
	590	267.076	45.8842 - 420.3089	$3d^{5} - 3d^{4}(a^{3}P)4p$	$a^4P - {}^4P^\circ$	$\frac{5}{2} - \frac{5}{2}$		1093
	620	267.094	42.0232 - 416.4225	$3d^{5} - 3d^{4}(a^{3}F)4p$	a⁴G – ⁴G°	$\frac{9}{2} - \frac{9}{2}$		1093
	510	267.110	42.0351 - 416.4225	3d ⁵ - 3d ⁴ (a ³ F)4p	a⁴G – ⁴G°	$\frac{1}{2} - \frac{1}{2}$		1093
	630	267.153	67.0851 - 441.4012	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^2F - ^2D^\circ$	$\frac{7}{2} - \frac{5}{2}$		1093
	130	267.189	61.1960 - 435.4594	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^2I - {}^4F^\circ$	$\frac{11}{2} - \frac{9}{2}$		1093
	560	267.232	46.1044 - 420.3089	3d ⁵ – 3d⁴(a ³ P)4p	a⁴P – ⁴P°	$\frac{3}{2} - \frac{5}{2}$		1093
	490	267.253	68.4449 - 442.6199	3d ⁵ – 3d⁴(a³D)4p	$a^2F - ^2D^\circ$	$\frac{5}{2} - \frac{3}{2}$		1093
	90	267.285	67.0851 - 441.2161	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^2F - {}^2F^\circ$	$\frac{7}{2} - \frac{7}{2}$		1093
	630	267.367	50.3310 - 424.3461	$3d^{5} - 3d^{4}(a^{3}G)4p$	a⁴D – ⁴F°	$\frac{7}{2} - \frac{7}{2}$		1093
	560	267.408	61.1960 - 435.1654	3d⁵ – 3d⁴(a¹I)4p	$a^2I - {}^2K^\circ$	$\frac{11}{2} - \frac{13}{2}$		1093
	670	267.461	61.2795 - 435.1654	$3d^{5} - 3d^{4}(a^{1}I)4p$	$a^2I - {}^2K^\circ$	$\frac{13}{2} - \frac{13}{2}$		1093
	610	267.498	41.9209 - 415.7543	3d ⁵ – 3d⁴(a³H)4p	a⁴G – ⁴I°	$\frac{11}{2} - \frac{9}{2}$		1093
	710	267.571	61.2795 - 435.0115	$3d^{5} - 3d^{4}(a^{T}G)4p$	$a^2I - {}^2H^\circ$	14 - 11		1093
	510	267.640	42.0036 - 415.6408	$3d^{5} - 3d^{4}(a^{3}F)4p$	a'G - 'G°	$\frac{2}{2} - \frac{7}{2}$		1093
	590	267.654	42.0232 - 415.6408	$3d^{3} - 3d^{4}(a^{3}F)4p$	$a^4G - {}^4G^\circ$	2 - 2		1093
	590	267.688	50.7776 - 424.3461	$3d^{3} - 3d^{4}(a^{3}G)4p$	a ⁴ D - ⁴ F°	3-5		1093
	(72)	267 760	50 7776 101 0051			5 1		1002
	650	267.769	50.7776 - 424.2354	30" – 30"(a"P)4p	$a^{*}D - P^{*}$	2 - 2		1093
	/00	267.784	50.3310 - 423.7633	$3d^2 - 3d^2(a^2G)4p$	a D ~ 'F'	$\frac{1}{2} - \frac{1}{2}$		1093
	320	267.825	42.0036 - 415.3820	3d" – 3d"(a'F)4p	a'G - 'G'	2 - 2		1093
	390	267.848	42.0351 - 415.3820	$3d^{2} - 3d^{2}(a^{2}F)4p$	$a^{*}G - G^{*}$	2 - 2		1093
	490	267.972	69.4470 - 442.6199	$3d^{2} - 3d^{2}(a^{2}D)4p$	$a^{+}F - D^{+}$	2 - 2		1093
	240	207.993	42.0030 - 415.1445	30 - 30 (a r)4p	a0-D	2 - 2		1093
	170	268 010	42 0351 - 415 1445	$3d^5 = 2d^4(a^3\mathbf{D})da$	atG _ tD°	2 5		1093
	420	208.019	42.0331 - 413.1443	3u = 3u (a r) 4p $3d^5 = 3d^4(a^3C) 4p$		2 - 2		1093
	680	208.048	61 1060 - 424 1673	$3d^{5} = 3d^{4}(a^{2}G)/4p$		2 - 2 11 - 9		1093
	320	200.110	50 7805 - 433 7105	30 - 30 (a + 0.04p)		2 - 2		1093
	550	208.140	50.7805 423.7103	$30^{\circ} - 30^{\circ}(a^{\circ}C)4p$	aD - F	$\frac{2}{3} - \frac{2}{1}$		1093
	600	208.193	30.7803 - 423.0408 45.8842 - 418.7134	$3d^{5} = 3d^{4}(a^{3}P)4p$	aD = P $a^4D = 4D^\circ$	2 - 2		1093
	000	200.215	43.0042 - 410./134	50 - 50 (a r)4p	ar-r	$\bar{2} = \bar{2}$		1093
	190	268 262	68 4449 - 441 2161	$3d^{5} = 3d^{4}(a^{3}D)An$	$a^2 \mathbf{F} = {}^2 \mathbf{F}^{\circ}$	5 2		1093
	200	268.202	50 3310 - 422 0652	$3d^5 = 3d(a^2D)4p$	aT = F	2 2 2		1093
	570	200.200	46 1044 - 419 7124	$3d^5 = 3d^4(a^3D)4p$		2 - 2		1093
	100	208.381	50 7776 402 2414	3u = 3d(a'r)4p		2 - 2		1093
	200	200.410	70 2014 451 9504	$3d^{5} = 3d^{2}(a^{2}G)4p$	a D - 'H'	2 7		1093
	200	208.479	19.3914 ~ 431.8394 46 1044 _ 419 4000	3d = 3d(a'r)4p $2d^5 = 2d^4(a^3r)4p$	$O \Gamma - \Gamma$	2 - 2		1093
	250	208.339	40.1044 - 418.4908	50 – 50 (a r)4p	ar-r	2 - 2		1093

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Multiplet	Rel. Int.	λ_{vac} (in Å)	Levels (in 10^3 cm ⁻¹)	Configurations	Terms	J - J	Notes	References
	550	268.571	107.8483 - 480.1893	3d ⁵ - 3d ⁴ (b ¹ G)4p	b²G - ²F°	$\frac{9}{2} - \frac{7}{2}$		1093
	610	268.637	79.6083 - 451.8594	$3d^{5} - 3d^{4}(a^{1}F)4p$	$b^2 F - {}^2 F^\circ$	1 - 1		1093
	400	268.697	46.3248 - 418.4908	$3d^{5} - 3d^{4}(a^{3}F)4p$	a ⁴ P - ⁴ F°	1 - 1		1093
	530	268,732	50.7805 - 422.8978	$3d^{5} - 3d^{4}(a^{3}G)4p$	$a^4D - {}^2F^\circ$	3_3		1093
	330	268.835	50.3310 - 422.3066	$3d^{5} - 3d^{4}(a^{3}P)4p$	$a^4D - {}^4D^\circ$	1 1 1		1093
	400	268.939	45.8842 - 417.7181	3d ⁵ - 3d ⁴ (a ³ H)4p	$a^4P - {}^2G^{\circ}$	$\frac{1}{2} - \frac{7}{2}$		1093
	\$40	268 967	50 6435 - 422 4372	3d ⁵ - 3d ⁴ (a ³ F)4n	a4D - 4D*	1_3		1093
	720	269,007	61 1960 - 432 9320	$3d^{5} - 3d^{4}(a^{1})An$	$a^{2}I - 2I^{\circ}$			1093
	720	269.026	41 9209 - 413 6316	$3d^{5} - 3d^{4}(a^{3}H)4n$	a ⁴ G - ⁴ H°	1 1		1093
	670	269.020	61 2795 - 432 9320	$3d^{5} - 3d^{4}(a^{1})Ap$	a = 11 $a^{2}I = 2I^{\circ}$			1093
	430	269.114	50 7805 - 432 3694	$3d^{5} - 3d^{4}(a^{3}E)An$	$a^{4}D = {}^{4}D^{\circ}$	2 - 2 3 - 1		1093
	550	269.140	50.3310 - 421.8940	$3d^{5} - 3d^{4}(a^{3}F)4p$	$a^4D - 4D^\circ$	$\begin{array}{c} 2 - 2 \\ \frac{7}{2} - \frac{5}{2} \end{array}$		1093
	670	2(0.150	ED 777(100 20((245 244-3004-	40 400	5 7		1001
	5/0	269.159	50.7776 - 422.3066	30° - 30 (a°P)4p	$a \cdot D - D$	$\frac{1}{2} - \frac{1}{2}$		1093
	710	209.234	61.1900 - 432.0100	30° - 30 (a·1)4p	$a^{-1} - 1$	$\frac{1}{2} - \frac{1}{2}$		1093
	/00	269.298	61.2795 - 432.6166	$3d^{2} - 3d^{2}(a^{-1})^{4}p$	$a^{-1} - 1^{-1}$	$\frac{1}{2} - \frac{1}{2}$		1093
	530	269.399	107.8483 - 479.0463	3d ² - 3d ² (b ² G)4p	6'G - 'G'	$\frac{1}{2} - \frac{1}{2}$		1093
	140	269.425	107.8870 - 479.0463	3d° - 3d°(b'G)4p	0-GG	2-2		1093
	470	269.459	50.7776 - 421.8940	3d ² - 3d ² (a ² F)4p	a'D - 'D'	2-2		1093
	140	269.547	50.3310 - 421.3243	3d ⁵ - 3d ⁴ (a ³ F)4p	$a^4D - ^2D^\circ$	$\frac{7}{2} - \frac{5}{2}$	*	1093
	520	269.661	41.9209 - 412.75 11	3d ⁵ – 3d ⁴ (a ³ H)4p	a ⁴ G – ⁴ H°	$\frac{11}{2} - \frac{11}{2}$		1093
	680	269.740	42.0232 - 412.7511	3d ⁵ – 3d ⁴ (a ³ H)4p	a4G ~ 4H°	2 - 11		1093
	680	269.828	45.8842 - 416.4930	3d⁵ - 3d⁴(a³F)4p	a ⁴ P - ⁴ D*	$\frac{5}{2} - \frac{7}{2}$		1093
	350	269.874	50.7776 - 421.3243	3d ⁵ - 3d ⁴ (a ³ F)4p	$a^4D - ^2D^4$	2 - 2		1093
	90	269.903	50.3310 - 420.8357	3d ⁵ - 3d ⁴ (a ³ F)4p	a ⁴ D - ⁴ F°	$\frac{7}{2} - \frac{9}{2}$		1093
	10	269.925	64.1524 - 434.6260	3d ⁵ - 3d ⁴ (a ³ D)4p	$a^2D - {}^4F^\circ$	3-3		1093
	510	270.013	46.1044 - 416.4590	$3d^{5} - 3d^{4}(a^{3}P)4p$	a ⁴ P - ⁴ P°	3-1		1093
	50	270.035	129.9516 - 500.2752	$3d^{5} - 3d^{4}(b^{1}D)4p$	$a^2P - {}^2P^\circ$	$\frac{1}{2} - \frac{1}{2}$		1093
	220	270.090	130.0259 - 500.2752	$3d^{5} - 3d^{4}(b^{1}D)4_{D}$	$a^2P - {}^2P^\circ$	1-1		1093
	150	270.118	141.0068 - 511.2174	$3d^{5} - 3d^{4}(b^{1}D)4p$	$c^2D - ^2D^*$	1 1-1		1093
	310	270.134	96.4612 - 466.6491	$3d^{5} - 3d^{4}(b^{3}F)4p$	$b^2D - {}^2F^\circ$	$\frac{3}{2} - \frac{5}{2}$	1	1093
	480	270 156	74 6277 - 444 7842	3d ⁵ - 3d⁴(a¹D)4n	$a^2G - ^2D^2$	1_1		1093
	390	270 172	46 3248 - 416 4590	$3d^{5} - 3d^{4}(a^{3}P)4p$	a ⁴ P - ⁴ P ⁴			1093
	660	270.226	42 0351 - 412 0956	$3d^{5} - 3d^{4}(a^{3}H)An$	a4G _ 4H	1 2		1093
	600	270.287	50 3310 - 420 3089	$3d^{5} = 3d^{4}(a^{3}P)4p$	a ⁴ D - ⁴ P°	1 1		1093
	290	270 312	50 7776 - 420 7223	$3d^{5} - 3d^{4}(a^{3}P)4p$	a ⁴ D - ⁴ S ⁴	1 2 2		1093
1	260	270.401	65.1735 - 434.9970	$3d^{5} - 3d^{4}(a^{1}G)4p$	$a^2D - {}^2F^{\bullet}$	$\frac{1}{2} - \frac{1}{2}$		1093
	210	270 454	50 3310 - 420 0800	3d ⁵ - 3d ⁴ (a ³ H)4p	a4D _ 4G*	1_9		1093
	640	270.515	42.0036 - 411.6694	$3d^{5} - 3d^{4}(a^{3}H)4n$	a D = 0	2 - 2 5 _ 1		1093
	270	270 538	42.0050 411.0094	$3d^{5} - 3d^{4}(a^{3}H)An$	a4G - 4H			1093
	480	270 585	96 5665 - 466 1337	$3d^{5} - 3d^{4}(h^{3}E)4n$	$b^2D - {}^2F^{\circ}$	1 1		1093
	500	270.614	50 7776 - 420 3089	$3d^{2} - 3d(0T) + p$ $3d^{3} - 3d^{4}(a^{3}P) + p$	$a^4D - 4P^2$	2 2		1093
	360	270.635	45.8842 - 415.3820	$3d^{5} - 3d^{4}(a^{3}F)4p$	a ⁴ P - ⁴ G°	$\frac{3}{2} - \frac{3}{2}$		1093
	280	270 659	68 4449 - 437 9197	345 24461034-	2E. 2C.	5 1		1093
	200	270.030	64 1574 - 437.7177 64 1574 - 422 5172	$3u = 3u (a C)^{m}p$ $3a^{3} = 2a^{4}(a^{3}C^{2})A^{m}$	$a^{2}D - 2C^{2}$	2 2 2		1093
	250	270.730	64 1524 - 433.5175	$3d^{5} - 3d(a^{3}D)/a$	aD = O $a^2D = 4P^{\circ}$	2 - 2 5 3		1093
1	\$10	270.771	46 1044 - 415 2820	$3d^{3} - 3d(a^{2}D)mp$ $3d^{3} - 2d^{4}(a^{3}D)m$	a4P 4G*	2 2 2 3 5		1093
	\$20	270.803	40.1044 - 415.3820	$3d^{5} = 3d(a^{1})Ap$	a1 - U a4P 4D*	2 - 2		1093
	320	270.941	96.4612 - 465.5527	$3d^{5} - 3d^{4}(b^{3}P)4p$	$b^2D - ^2D^\circ$	$\frac{2}{2} - \frac{2}{2}$		1093
	~~~	270 071	46 1044 416 1446	2.45 2.44-30.4	4D 4D*	3 5		1002
	640 460	2/0.9/1	40.1044 - 413.1443	30° - 30°(a°P)4p	$a^{T} - D^{T}$	2 - 2		1093
	460	2/1.014	90.000 - 460.0027	30° - 30°(b°P)4p	$D^{-}D^{-}D^{-}D^{-}D^{-}D^{-}D^{-}D^{-}$	$\frac{1}{2}$ $\frac{-1}{2}$		1093
	340	271.135	129.9516 - 498.7730	3d" - 3d"(b'D)4p	a-P - P			1093
	450	271.179	65.1735 - 433.9369	3d ² – 3d ² (a'S)4p	a D - P	2 - 27		1093
	430	271.262	64.1524 - 432.8001	3d' - 3d'(a'G)4p	a'D - 'F"	2 - 2		1093
	460	271.383	107.8483 - 476.3321	3d° – 3d°(b'G)4p	∣ b <b>'</b> G – <b>'H</b> °	2 - 2		1093

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Multiplet	Rel. Int.	$\lambda_{\rm vac}$ (in Å)	Levels (in 10 ³ cm ³ )	Configurations	Terms	J - J N	lotes	References
	330	271.410	107.8870 - 476.3321	3d ⁵ - 3d ⁴ (b ³ G)4p	$b^2G - {}^2H^\circ$	7 - 2		1093
	90	271.463	67.0851 - 435.4594	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^2 F - {}^4 F^\circ$	Ž - 9	1	1093
	310	271 525	61 1960 - 429 4863	$3d^5 = 3d^4(a^3G)4p$	a ² I – ⁴ G°	μ_ §	1	1093
	210	271 562	96 5665 - 464 8078	$3d^{5} = 3d^{4}(h^{3}E)4p$	$h^2 D = {}^4 G^2$	2 2 2 2		1093
	140	271.502	50.5005 - 404.0078	$3d^5 = 3d^4(a^3P)4p$	$a^4D$ $4P^2$		1	1093
	610	271.089	72.0088 440.0170	$3d^{2} - 3d^{2}(a^{2}F)4p$		2 - 2		1093
	610	271.733	72.9088 - 440.9179	3d" - 3d"(a'l)4p	a ² H – ² H*	2 - 2		1093
	320	271.788	50.7776 - 418.7134	3d⁵ - 3d⁴(a³P)4p	$a^4D - {}^4P^\circ$	$\frac{5}{2} - \frac{3}{2}$		1093
	40	271.849	50.6435 - 418.4908	3d ⁵ – 3d⁴(a ³ F)4p	a⁴D – ⁴F°	$\frac{1}{2} - \frac{3}{2}$		1093
	500	271.953	50.7805 - 418.4908	$3d^{5} - 3d^{4}(a^{3}F)4p$	a⁴D – ⁴F°	$\frac{3}{2} - \frac{3}{2}$	1	1093
	680	271.990	45.8842 - 413.5531	3d ⁵ - 3d ⁴ (a ³ P)4p	$a^4P - {}^4D^\circ$	5 - 3		1093
	610	272.146	46.1044 - 413.5531	$3d^{5} - 3d^{4}(a^{3}P)4p$	a ⁴ P – ⁴ D°	3 - 3		1093
	680	272.311	46.3248 - 413.5531	$3d^{5} - 3d^{4}(a^{3}P)4p$	$a^{4}P - {}^{4}D^{\circ}$	$\frac{1}{2} - \frac{3}{2}$		1093
	280	272.361	73.7566 - 440.9179	3d ⁵ – 3d ⁴ (a'I)4p	$a^2H - {}^2H^\circ$	$\frac{11}{2} - \frac{9}{2}$	1	1093
	310	272.384	72.9088 - 440.0392	3d ⁵ – 3d⁴(a'I)4p	$a^2H - {}^2H^\circ$	$\frac{9}{2} - \frac{11}{2}$	1	1093
	550	272.548	68.5512 - 435.4594	$3d^{5} - 3d^{4}(a^{3}D)4p$	a⁴F – ⁴F°	$\frac{9}{2} - \frac{9}{2}$		1093
	580	272.587	61.1960 - 428.0515	$3d^{5} - 3d^{4}(a^{3}G)4p$	$a^2I - {}^2H^\circ$	<u><u><u></u><u></u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u></u>		1093
	280	272.629	61.1960 - 427.9956	$3d^5 - 3d^4(a^3F)4p$	$a^{2}l - {}^{2}G^{\circ}$	<u><u><u>u</u></u> - <u><u>y</u></u></u>		1093
	120	272.648	74.6277 - 441.4012	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^2G - {}^2D^\circ$	$\frac{7}{2} - \frac{5}{2}$		1093
	120	272 (70	06 5665 462 2015	215 214(130)4		5.5		1000
	120	272.678	96.5665 - 463.3015	3d ² – 3d ² (b ² P)4p	<b>b</b> ² <b>D</b> - * <b>P</b> *	5-5		1093
	200	272.726	79.3914 - 446.0612	3d' – 3d'(a'D)4p	$\mathbf{b}^2 \mathbf{F} - \mathbf{F}^*$	2 - 2		1093
	600	272.811	68.4449 - 434.9970	3d [°] – 3d⁺(a'G)4p	$\mathbf{a}^2\mathbf{F} - \mathbf{F}^*$	2 - 2		1093
	490	272.887	79.6083 - 446.0612	$3d^{5} - 3d^{4}(a^{1}D)4p$	$b^2F - {}^2F^\circ$	$\frac{7}{2} - \frac{2}{2}$		1093
	410	272.901	61.2795 - 427.7027	3d ⁵ – 3d ⁴ (a ³ G)4p	a²I – ²H°	$\frac{13}{2} - \frac{11}{2}$		1093
	190	272.942	140.9222 - 507.3004	3d ⁵ – 3d ⁴ (b ¹ D)4p	$c^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		1093
	620	272.992	68.8017 - 435.1162	3d ⁵ – 3d⁴(a³D)4p	a⁴F – ⁴F°	7 - 7		1093
	720	273.013	67.0851 - 433.3712	$3d^5 - 3d^4(a^3G)4p$	$a^2 F - {}^2 G^\circ$	1 - 2		1093
	520	273.089	68.4449 - 434.6260	$3d^5 - 3d^4(a^3D)4p$	$a^2 F - {}^4 F^\circ$	\$_\$		1093
	310	273 117	46 1044 - 412 2482	$3d^5 = 3d^4(a^3P)4p$	$a^{4}P = {}^{4}D^{\circ}$			1093
	390	273 281	46,3248 - 412,2482	$3d^5 = 3d^4(a^3P)4p$	$a^{4}P$ ${}^{4}D^{9}$			1093
	20	273 315	96 5665 - 462 4431	$3d^{5} - 3d^{4}(h^{3}P)4n$	$h^2 D = {}^4 D^2$	2 - 2 2 2		1093
	20	2.0.010	, , , , , , , , , , , , , , , , , , ,	5 <b>u</b> = 5 <b>u</b> (6 <b>r</b> )+p				1075
	460	273.358	68.8017 - 434.6260	3d⁵ – 3d⁴(a³D)4p	a⁴F – ⁴F°	$\frac{7}{2} - \frac{5}{2}$		1093
	410	273.394	75.4417 - 441.2161	$3d^{5} - 3d^{4}(a^{3}D)4p$	a ² G - ² F°	$\frac{9}{2} - \frac{7}{2}$		1093
	680	273.436	50.7776 - 416.4930	$3d^{5} - 3d^{4}(a^{3}F)4p$	a⁴D – ⁴D°	5 - 7		1093
	400	273.465	69.4470 - 435.1162	3d ⁵ - 3d ⁴ (a ³ D)4p	a⁴F – ⁴F°	3 - 7		1093
	550	273.490	107.8870 - 473.5319	$3d^{5} - 3d^{4}(b^{3}F)4p$	b ² G – ² G*	$\frac{1}{2} - \frac{1}{2}$		1093
	610	273.560	69.4470 - 434.9970	3d ⁵ - 3d ⁴ (a ¹ G)4p	$a^4F - {}^2F^\circ$	$\frac{5}{2} - \frac{5}{2}$	ĺ	1093
	540	273 616	75 4417 - 440 9179	$3d^{5} = 3d^{4}(a^{1}I)Aa$	2G 2H°	2 2		1003
	210	273 636	69 1735 - 434 6260	$3d^{5} = 3d^{4}(a^{3}T)A_{T}$	a4E_4E°	3 5		1093
	160	273.677	79.3914 - 444.7842	$3d^{5} - 3d^{4}(a^{3}D)4n$	$a \Gamma - \Gamma$	2 2 2		1093
	650	273 841	79.6083 444.7842	3d = 3d (a D) + p $3d^{5} = 3d^{4}(a   D) + p$	$b^2F = 2D^2$	$\frac{1}{2} - \frac{1}{2}$		1093
	560	273.041	75.0085 - 111.7842 86.5221 451.6420	3d - 3d (a D)4p	$D^{-}F = D^{-}$	$\frac{1}{2} - \frac{1}{2}$		1093
	580	273.904	86.5321 - 451.6229	$3d^{5} - 3d^{4}(a^{1}D)4p$	$a^2S - {}^2P^\circ$			1093
					u 0 - 1	2 - 2		1075
	630	273.965	72.9088 - 437.9197	3d ⁵ - 3d ⁴ (a ¹ G)4p	a ² H - ² G°	$\frac{9}{2} - \frac{7}{2}$		1093
	660	274.062	73.7566 - 438.6394	$3d^{5} - 3d^{4}(a^{1}G)4p$	a ² H - ² G°	<u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u>		1093
	610	274.077	79.3914 - 444.2522	$3d^{5} - 3d^{4}(a^{T}D)4p$	$b^2 F - ^2 D^\circ$	3-3		1093
	170	274.103	67.0851 - 431.9126	3d ⁵ – 3d ⁴ (a ³ D)4p	$a^2F - {}^4D^\circ$	1 - 1		1093
	520	274.156	69.4470 - 434.2009	$3d^5 - 3d^4(a^3D)4p$	$a^4 F - {}^4 F^\circ$	2 3		1093
	590	274.174	107.8483 - 472.5795	3d ⁵ – 3d ⁴ (b ³ F)4p	b²G – ²G°	$\frac{2}{2} - \frac{2}{2}$		1093
	50	274 236	107 8483 472 4972	2.45 2.44/53534	12C 4D	2 2		1002
	300	274.230	75 4417 440 0202	30° - 30°(0°1°)4p	- 'D'	$\frac{1}{2} - \frac{1}{2}$		1093
	390	274.270	/5.441/ - 440.0392	30° – 30°(a'1)4p	a'G - 'H'	$\frac{1}{2} - \frac{1}{2}$		1093
	160	274.295	68.8017 - 433.3712	3d' – 3d'(a'G)4p	a*F - 4G*	2 - 2		1093
	400	2/4.444	61.1900 - 425.5676	3d' - 3d*(a'H)4p	a ² I – ² H°	$\frac{11}{2} - \frac{11}{2}$		1093
	650	274.508	61.2795 - 425.5676	3d³ – 3d⁴(a³ <b>H</b> )4p	$a^2 I - {}^2 H^\circ$	$\frac{13}{2} - \frac{11}{2}$		1093
	120	274.618	141.0068 - 505.1505	3d ³ – 3d ⁴ (b ¹ D)4p	$c^2 D - {}^2 F^\circ$	$\frac{1}{2} - \frac{5}{2}$		1093
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Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J Notes	Reference
	260	274.676	64.1524 - 428.2214	3d ⁵ - 3d ⁴ (a ³ F)4p	$a^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{1}{2}$	1093
	150	274.726	68.8017 - 432.8001	3d ⁵ – 3d⁴(a¹G)4p	$a^4F - {}^2F^\circ$	$\frac{7}{2} - \frac{7}{2}$	1093
1	140	274.838	68.4449 - 432.2957	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^2F - {}^4D^\circ$	$\frac{5}{2} - \frac{5}{2}$	1093
	170	275 108	68 8017 - 432 2957	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^4F - {}^4D^\circ$	1 - 5	1093
ļ	100	275 163	64 1524 - 427 5750	$3d^5 = 3d^4(a^3E)4n$	$a^2D = G^{\circ}$	5_1	1093
	600	275.210	68.5512 - 431.9126	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^4F - {}^4D^\circ$	$\frac{2}{9} - \frac{2}{1}$	1093
	620	275.221	61.1960 - 424.5370	$3d^{5} - 3d^{4}(a^{3}G)4p$	$a^2I - {}^4H^\circ$	$\begin{bmatrix} 11 \\ 2 \\ 7 \end{bmatrix} = \begin{bmatrix} 9 \\ 2 \\ 7 \end{bmatrix}$	1093
	570	275.260	74.6277 - 437.9197	30° - 30°(a°C)4p		$\frac{1}{2} - \frac{1}{2}$	1093
	520	275.311	/9.3914 - 442.6199	3d ² - 3d ² (a ² D)4p	0 ⁻ F - ⁻ D	$\frac{5}{5} - \frac{7}{2}$	1093
	620	275.332	64.1524 - 427.3422	$3d^2 - 3d^2(a^2P)4p$	$a^2D - ^2D^2$	2 - 2	1093
	580	275.400	68.8017 - 431.9126	3d ⁻ – 3d ⁻ (a ⁻ D)4p	$a^{T}F - D^{T}$	$\frac{1}{2} - \frac{1}{2}$	1093
	660	275.417	61.2795 - 424.3637	3d" - 3d"(a'G)4p	a'I – 'H'	$\frac{12}{2} - \frac{11}{2}$	1093
	510	275.522	64.1524 - 427.0960	3d ⁵ – 3d⁴(a ³ F)4p	$a^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{5}{2}$	1093
	160	275.597	69.4470 - 432.2957	$3d^{5} - 3d^{4}(a^{3}D)4p$	a⁴F – ⁴D°	$\frac{5}{7} - \frac{5}{7}$	1093
	530	275.810	61,1960 - 423,7633	$3d^5 - 3d^4(a^3G)4p$	$a^{2}I - {}^{4}F^{\circ}$	<u><u><u> </u></u></u>	1093
	270	275 838	68 4449 - 430 9719	$3d^5 - 3d^4(a^3D)4n$	$a^2 \mathbf{F} - {}^4 \mathbf{D}^6$	3 - 3	1093
	340	275 879	75 4417 - 437 9197	$3d^5 - 3d^4(a^1G)4n$	$a^2G - G^{\circ}$		1093
	280	275.941	79.3914 - 441.7857	$3d^{5} - 3d^{4}(a^{3}D)4p$	$b^2 F - {}^2 F^\circ$	$\frac{2}{5} - \frac{5}{2}$	1093
	70	276.005	96.4612 - 458.7722	$3d^{2} - 3d^{4}(a^{1}F)4p$	$b^2D - {}^2D^\circ$	$\left  \frac{2}{2} - \frac{2}{2} \right $	1093
	340	276.077	68.8017 - 431.0203	$3d^{5} - 3d^{4}(a^{3}D)4p$	a⁴F – ⁴P°	$\left  \frac{1}{2} - \frac{2}{2} \right $	1093
	430	276.114	65.1735 - 427.3422	3d ⁵ – 3d ⁴ (a ³ P)4p	$a^2D - ^2D^\circ$	2-2	1093
	660	276.342	61.1960 - 423.0652	3d ⁵ – 3d ⁴ (a ³ H)4p	$a^2I - {}^2H^\circ$	$\frac{11}{2} - \frac{9}{2}$	1093
	510	276.402	79.6083 - 441.4012	3d ⁵ - 3d ⁴ (a ³ D)4p	$b^2 F - {}^2 D^\circ$	$\frac{7}{2} - \frac{5}{2}$	1093
	280	276.452	69.1735 - 430.8988	3d ⁵ - 3d ⁴ (a ³ D)4p	a⁴F – ⁴D°	$\frac{3}{2} - \frac{1}{2}$	1093
	150	276 542	70 6083 441 2161	3d ⁵ 3d ⁴ (a ³ D)/m	$b^2 E = {}^2 E^\circ$	1_1	1093
	400	270.542	64 1524 425 7021	$3d^{5} = 3d^{4}(a^{3}B)/m$	a ² D ² D ⁶	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1093
	490	270.387	64.1324 - 425.7031	3u = 3u (a + 1)4p		$\begin{bmatrix} 2 & -2 \\ 9 & 11 \end{bmatrix}$	1093
	650	276.639	68.5512 - 430.0333	$3d^2 - 3d^2(a^2G)4p$	a'F - 'G	$\frac{5}{13} - \frac{7}{2}$	1093
	/10	276.672	61.2/95 - 422./118	3d" – 3d"(a"H)4p	a-11	2-2	1093
	550 280	276.694	73.7566 - 435.1654 61.2795 - 422.6424	$3d^{5} = 3d^{4}(a^{3}H)4p$ $3d^{5} = 3d^{4}(a^{3}H)4p$	$a^2H - {}^2K^{\circ}$ $a^2I - {}^2I^{\circ}$	n _ n   n _ n	1093
	200	270.750	01.2795 - 422.0424	50 - 50 (a 11)+p	a 1 - 1	2 - 2	1075
	510	276.812	73.7566 - 435.0115	3d ⁵ - 3d ⁴ (a ¹ G)4p	$a^2H - {}^2H^\circ$	$\begin{bmatrix} \underline{\Pi} \\ \underline{2} \end{bmatrix} = \begin{bmatrix} \underline{\Pi} \\ \underline{2} \end{bmatrix}$	1093
	480	277.033	67.0851 - 428.0515	3d ^s – 3d⁴(a³G)4p	a'F – 'H°	$\frac{1}{2} - \frac{9}{2}$	1093
	330	277.058	68.5512 - 429.4863	$3d^{5} - 3d^{4}(a^{3}G)4p$	a⁺F – ⁺G°	$\frac{9}{2} - \frac{9}{2}$	1093
	240	277.074	67.0851 - 427.9956	3d ⁵ - 3d ⁴ (a ³ F)4p	a ² F – ² G°	$\frac{7}{2} - \frac{9}{2}$	1093
	600	277.250	68.8017 - 429.4863	3d ⁵ – 3d⁴(a ³ G)4p	a⁴F – ⁴G°	$\frac{7}{2} - \frac{9}{2}$	1093
	630	277.373	65.1735 - 425.7031	$3d^{5} - 3d^{4}(a^{3}P)4p$	$a^2D - ^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$	1093
	430	277 421	72 0088 422 3712	2d ⁵ 2d ⁴ (a ³ G)4a	$a^2H = 2G^{\circ}$	3 3	1093
İ	430	277.421	72.7000 - 433.3712	$3d^{5} - 3d^{4}(a^{3}G)Ap$	$a \Pi = 0$ $a^2 H - 2 H^{\circ}$		1003
	500	277.437	73.7300 - 434.1073 67.0851 - 437.3433	$3d^{2} - 3d(a^{2}G)^{4}p$	$a \Pi = \Pi$ $a^2 E^2 D^2$	2 - 2 Z 2	1093
	590	277.579	67.0831 - 427.3422	30° - 30 (a P)4p	$a^{2}\Gamma - D^{2}$	$\frac{1}{2} - \frac{1}{2}$	1093
	80	277.623	64.1524 - 424.3461	3d" – 3d"(a"G)4p	a-D - 'F'	$\frac{1}{2} - \frac{1}{2}$	1093
	410 550	277.715	64.1524 - 424.2354 68 8017 - 428 8665	$3d^{5} - 3d^{2}(a^{3}P)4p$ $3d^{5} - 3d^{4}(a^{3}G)4p$	$a^{4}D - P^{*}$	5 - 5 7 - 7	1093
	550	211.155	00.0017 - 420.0000	30 - 30 (a C)+p		2 2	1075
	630	277.765	67.0851 - 427.0960	$3d^{5} - 3d^{4}(a^{3}F)4p$	$a^2F - {}^2F^\circ$	$\left  \frac{7}{2} - \frac{5}{2} \right $	1093
	140	277.862	72.9088 - 432.8001	3d - 3d (a'G)4p	a-HF	$\frac{1}{2} - \frac{1}{2}$	1093
	210	277.958	68.4449 - 428.2214	3d ² - 3d ⁴ (a ³ F)4p	a-F F°	$\left  \frac{2}{2} - \frac{2}{2} \right $	1093
	280	278.032	68.5512 - 428.2214	$3d^{5} - 3d^{4}(a^{3}F)4p$	$a^{4}F - {}^{2}F^{\circ}$	$\frac{2}{2} - \frac{1}{2}$	1093
	410	278.075	73.7566 - 433.3712	3d ⁵ − 3d ⁴ (a ³ G)4p	a²H – ² G°	$\left  \frac{11}{2} - \frac{9}{2} \right $	1093
	540	278.118	75.4417 - 435.0115	$3d^{5} - 3d^{4}(a^{1}G)4p$	a ² G - ² H°	$\frac{9}{2} - \frac{11}{2}$	1093
	480	278 168	64 1524 - 423 6458	$3d^5 - 3d^4(a^3G)4n$	$a^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$	1093
	460	278 200	68 5512 427 0056	$3d^{5} = 3d^{4}(a^{3}E)An$	$a^4 \mathbf{F} = {}^2 \mathbf{G}^{\circ}$	2 = 2 9 = 9	1003
	400	278.209	00.3312 - 427.9930	245 - 244 3 CD4	ar - 0	$\begin{bmatrix} 2 & -2 \\ 5 & 7 \end{bmatrix}$	1093
	550	278.226	09.4470 - 428.8665	3d" – 3d"(a'G)4p	a F - G	2 - 2	1093
	600	278.301	69.1735 - 428.4965	3d³ - 3d⁴(a³G)4p	a⁺F – ⁺G°		1093
	230	278.341	141.0068 - 500.2752	$3d^{5} - 3d^{4}(b^{\dagger}D)4p$	$c^2D - {}^2P^{\circ}$	$\frac{2}{2} - \frac{1}{2}$	1093
		270 401	(0.0017 407.005/	2.15 2.146-31214	1 40 200	1 7 9 1	1003

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NI VI -- Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	640	278 435	68 5512 - 427 7027	$3d^5 - 3d^4(a^3G)4p$	9 ⁴ E - ² H°	2_Ш		1093
	590	278 448	68 4449 - 427 5750	$3d^5 = 3d^4(a^3E)Am$	$a \Gamma = \Pi$	2 - 2 5 - 1		1093
	200	278.511	60.4470 + 427.5750	3d = 3d (a T) + p	$4\Gamma - G$	2 - 2		1093
	290	278.511	<b>69.44</b> 70 - 428.4965	3d ² - 3d ³ (a ² G)4p	$a^{*}F - G^{*}$	$\frac{1}{2} - \frac{1}{2}$		1093
	320	278.526	/9.6083 - 438.6394	3d' – 3d'(a'G)4p	b ² F – ² G°	$\frac{1}{2} - \frac{1}{2}$		1093
	560	278.636	68.4449 – 427.3422	$3d^{2} - 3d^{4}(a^{3}P)4p$	$a^2 F - {}^2 D^\circ$	$\frac{2}{2} - \frac{2}{2}$		1093
	430	278.660	73.7566 - 432.6166	$3d^{5} - 3d^{4}(a^{1}I)4p$	$a^2H - {}^2I^\circ$	$\frac{11}{2} - \frac{13}{2}$		1093
	570	278.735	107.8870 - 466.6491	3d⁵ – 3d⁴(b³F)4p	$b^2G - {}^2F^\circ$	$\frac{7}{2} - \frac{5}{2}$		1093
	500	278.764	75.4417 - 434.1673	$3d^{5} - 3d^{4}(a^{1}G)4p$	$a^2G - {}^2H^\circ$	$\frac{9}{2} - \frac{9}{2}$		1093
1	180	278.829	68.4449 - 427.0960	$3d^{5} - 3d^{4}(a^{3}F)4p$	$a^2F - {}^2F^\circ$	3 - 5		1093
	420	278,915	79 3914 - 437 9197	$3d^5 - 3d^4(a^1G)4p$	$b^2 \mathbf{F} = {}^2 \mathbf{G}^2$	5 1		1093
	330	278 962	65 1735 - 423 6468	$3d^{5} - 3d^{4}(a^{3}\mathbf{P})Ap$	$a^2 D - {}^2 P^\circ$	2 - 2 3 - 1		1093
	520	279 106	107 8483 - 466 1337	$3d^{5} = 3d^{4}(h^{3}E)/(h^{3}E)$	$h^2 G^2 F^2$	2 - 2 9 2		1093
	520	279.100	107.8485 - 400.1557	50 - 50 (8 P)4p	00-r	2 - 2		1095
	470	279.201	74.6277 - 432.8001	$3d^{5} - 3d^{4}(a^{1}G)4p$	$a^2G - {}^2F^\circ$	$\frac{2}{3} - \frac{7}{3}$	1	1093
	350	279.270	75 4417 - 433 5173	$3d^5 - 3d^4(a^3G)4p$	$a^2G - {}^2G^{\circ}$	<u>9</u> <u>7</u>		1093
	450	279 385	75 4417 - 433 3712	$3d^{5} - 3d^{4}(a^{3}G)Ap$	$a^2 G^{-2} G^{\circ}$	2 - 2 9 9		1093
	310	279.410	69 4470 427 3422	$3d^{5} - 3d^{4}(a^{3}P)/a$	a = 0	2 - 2	1	1093
	310	279.410	140 0000 408 7720	30 - 30 (a r)4p	ar - D	$\frac{1}{2} - \frac{1}{2}$		1093
	320	279.445	140.9222 - 498.7730	3d ² – 3d ² (b ² D)4p	$c^{2}D - P^{2}$	$\frac{1}{2} - \frac{1}{2}$		1093
	260	279.514	141.0068 - 498.7730	3d° – 3d°(b'D)4p	$c^2D - {}^2P^*$	$\frac{2}{2} - \frac{2}{2}$		1093
	490	279.545	65.1735 - 422.8978	3d⁵ – 3d⁴(a³G)4p	$a^2D - {}^2F^\circ$	$\frac{3}{2} - \frac{5}{2}$		1093
	580	279.605	69.4470 - 427.0960	$3d^{5} - 3d^{4}(a^{3}F)4p$	$a^{4}F - {}^{2}F^{\circ}$	$\frac{5}{2} - \frac{5}{2}$		1093
	240	279.728	75.4417 - 432.9320	$3d^{5} - 3d^{4}(a^{T})4p$	$a^2G - {}^2I^\circ$	§ _ Ĥ		1093
	320	279.756	64.1524 - 421.6072	$3d^5 - 3d^4(a^3F)4n$	$a^2D - {}^2D^\circ$	\$_3		1093
	420	279 786	96 5665 - 453 9830	$3d^{5} - 3d^{4}(a^{T}F)4p$	$h^2 D = 2G^2$	$\frac{1}{5}$ $\frac{1}{2}$		1093
	310	279 830	75 4417 - 432 8001	$3d^{5} - 3d^{4}(a^{\dagger}G)Ap$	$a^2 G = C$	$\frac{2}{9}$ $\frac{2}{7}$		1093
	510	279.050	75.4417 - 452.8001	3u - 3u (a O)+p	a0- r	2 - 2		1093
	560	279.908	68.4449 - 425.7031	3d ⁵ – 3d⁴(a³P)4p	$a^2 F - {}^2 D^\circ$	$\frac{5}{2} - \frac{3}{2}$		1093
	560	279.976	64.1524 - 421.3243	3d ⁵ – 3d ⁴ (a ³ F)4p	$a^2D - {}^2D^\circ$	2 - 2		1093
	370	280.014	72.9088 - 430.0333	3d ⁵ - 3d ⁴ (a ³ G)4p	a²H - ⁴G°	3 - 4		1093
	510	280.142	107.8483 - 464.8078	$3d^{5} - 3d^{4}(b^{3}F)4p$	b²G – ⁴G°	$\frac{3}{2} - \frac{7}{2}$		1093
	490	280.330	65.1735 - 421.8940	$3d^{5} - 3d^{4}(a^{3}F)4n$	$a^2D - {}^4D^\circ$	3 _ 5		1093
	620	280.449	67.0851 - 423.6458	$3d^{5} - 3d^{4}(a^{3}G)4p$	$a^2F - {}^2F^\circ$	$\frac{1}{2} - \frac{1}{2}$		1093
	240							
	340	280.480	69.1735 - 425.7031	3d [°] – 3d [•] (a [°] P)4p	a⁴F – ² D°	2-2		1093
	210	280.556	65.1735 - 421.6072	3d ⁵ – 3d⁴(a ³ F)4p	$a^2D - {}^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$		1093
	110	280.627	61.1960 - 417.5384	3d ⁵ − 3d ⁴ (a ³ H)4p	a²I - ⁴G°	<u><u><u></u></u><u><u></u><u></u><u></u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u></u>		1093
	500	280.672	45.8842 - 402.1713	3d ⁵ – 3d ⁴ (a ⁵ D)4p	a⁴P – ⁴D°	$\frac{5}{2} - \frac{7}{2}$		1093
	390	280.696	61.2795 - 417.5384	3d ⁵ – 3d⁴(a³H)4p	a²I – ⁴G°	13 - H		1093
	410	280.786	65.1735 - 421.3243	3d ⁵ - 3d ⁴ (a ³ F)4p	$a^2D - {}^2D^\circ$	$\frac{3}{2} - \frac{5}{2}$		1093
	60	280.829	86.5321 - 442.6199	3d ⁵ − 3d ⁴ (a ³ D)4p	$a^2S - ^2D^\circ$	1-3		1093
	420	280.931	72,9088 - 428,8665	$3d^5 - 3d^4(a^3G)4n$	$a^2H - {}^4G^\circ$	$\frac{1}{9} - \frac{1}{7}$		1093
	270	280 979	68 4449 - 424 3461	$3d^5 = 3d^4(a^3G)4p$	$a^2E - {}^4E^\circ$	2 2		1093
	490	281.026	458842 - 4017209	$3d^{5} = 3d^{4}(a^{5}D)Ap$	$a^{4}P = T^{4}D^{6}$	2 2		1093
	340	281.077	68 4449 424 2185	$3d^{5} - 3d^{4}(a^{3}G)4n$	aF = D	2 2 2		1093
	490	201.077	72 7566 420 4862	30 - 30 (a O)4p		$\frac{1}{2} - \frac{1}{2}$		1093
	460	201.111	75.7500 - 429.4805	3d" - 3d"(a"G)4p	a-H - "G"	$\frac{1}{2} - \frac{1}{2}$		1093
	230	281.141	64.1524 - 419.8447	$3d^{5} - 3d^{4}(a^{3}F)4p$	$a^2D - {}^4F^\circ$	$\frac{5}{2} - \frac{5}{2}$		1093
	470	281.204	46.1044 - 401.7209	$3d^{5} - 3d^{4}(a^{5}D)4p$	$a^4P - {}^4D^\circ$	3-3		1093
	350	281.257	68.8017 - 424.3461	$3d^{5} - 3d^{4}(a^{3}G)4n$	$a^4F - {}^4F^\circ$	1 1 1		1093
	390	281.380	79.6083 - 434 9970	$3d^{5} = 3d^{4}(a^{1}G)4n$	$b^2 E = {}^2 E^\circ$	7 5		1093
	630	281 442	72 9088 - 428 2214	$3d^{5} = 3d^{4}(a^{3}E)An$	$a^2H^2E^{\circ}$	2 - 2 2 - 2 2 - 2		1093
	620	281 504	61 1960 - 416 4225	3u = 3u (a r) + p $3d^5 = 3d^4 (a^3 r) + p$		<u>2 - 2</u> Ц 9		1093
	020	201.304	01.1700 - 410.4225	30 – 30 (a r)4p	a-1 - 'G'	2 - 2		1093
	640	281.515	68.5512 - 423.7633	3d ⁵ - 3d ⁴ (a ³ G)4p	$a^{4}F - {}^{4}F^{\circ}$	$\frac{9}{2} - \frac{9}{2}$		1093
	530	281.548	46.1044 - 401.2809	3d ⁵ - 3d ⁴ (a ⁵ D)4p	a⁴P – ⁴D°	$\frac{3}{2} - \frac{3}{2}$		1093
	630	281.620	72.9088 - 427.9956	3d ⁵ – 3d ⁴ (a ³ F)4p	a ² H – ² G°	$\frac{9}{2} - \frac{9}{2}$		1093
	530	281.644	96.5665 - 451.6229	3d ⁵ – 3d ⁴ (a ¹ D)4p	$b^2D - {}^2P^\circ$	5-3		1093
	370	281.722	68.8017 - 423.7633	$3d^{5} - 3d^{4}(a^{3}G)4p$	a⁴F - ⁴F°	7 - 9		1093
	410	281.802	74.6277 - 429.4863	$3d^{5} - 3d^{4}(a^{3}G)4n$	$a^2G - {}^4G^\circ$	7 - 9		1093
						2 - 2		1095

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Aultiplet Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm 3 )	Configurations	Terms	J - J Note	es References
330	281.843	67.0851 - 421.8940	3d ⁵ - 3d ⁴ (a ³ F)4p	a²F – ⁴D°	$\frac{7}{2} - \frac{5}{2}$	1093
370	281.857	72.9088 - 427.7027	3d ⁵ – 3d⁴(a ³ G)4p	a ² H – ² H°	$\frac{9}{2} - \frac{11}{2}$	1093
610	281.955	72.9088 - 427.5750	$3d^{5} - 3d^{4}(a^{3}F)4p$	a ² H – ² G°	$\frac{9}{2} - \frac{7}{2}$	1093
480	281.975	46.3248 - 400.9621	$3d^{5} - 3d^{4}(a^{5}D)4p$	a⁴P – ⁴D°	$\frac{1}{2} - \frac{1}{2}$	1093
560	282.015	75.4417 - 430.0333	$3d^{5} - 3d^{4}(a^{3}G)4p$	a²G – ⁴G°	$\frac{9}{2} - \frac{11}{2}$	1093
320	282.038	64.1524 - 418.7134	$3d^{5} - 3d^{4}(a^{3}P)4p$	$a^2D - {}^4P^\circ$	$\frac{5}{2} - \frac{3}{2}$	1093
210	282.055	69.1735 - 423.7105	3d ⁵ – 3d⁴(a³G)4p	a⁴F – ⁴F°	$\frac{3}{5} - \frac{3}{5}$	1093
150	282.075	68.5512 - 423.0652	$3d^{5} - 3d^{4}(a^{3}H)4p$	a⁴F – ²H°	3-3	1093
120	282 118	68 4449 - 422,8978	$3d^{5} - 3d^{4}(a^{3}G)4p$	$a^2F - {}^2F^\circ$	5-5	1093
660	282 250	73.7566 - 428.0515	$3d^{5} - 3d^{4}(a^{3}G)4p$	$a^2H - {}^2H^\circ$	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>	1093
400	282 295	67.0851 - 421.3243	$3d^5 - 3d^4(a^3F)4p$	$a^2 F - {}^2 D^\circ$	2 - 5	1093
350	282.327	69.4470 - 423.6458	$3d^{5} - 3d^{4}(a^{3}G)4p$	$a^4F - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$	1093
280	202.262	86 5221 440 6802	3d ⁵ - 3d ⁴ (a ³ D)4p	$a^2S = 2P^{\circ}$	1_1	1093
280	282.302	80.3321 - 440.0893	$3d^{5} - 3d^{4}(a^{3}G)Ap$	$a^2 - r$ $b^2 F - c^2 C^2$	2 - 2 2 - 2	1093
530	282.385	/9.3914 - 433.31/3	$3d^{5} - 3d(a^{2}G)4p$	$a^4E^{-2}E^{\circ}$	2 2 2	1093
330	282.410	08.8017 - 422.8978	3d = 3d (a C)/4p	a F - F	2 2	1093
100	282.451	/5.4417 - 429.4863	3d - 3d (a G)4p		2 - 2	1093
570	282.492	68.4449 - 422.4372 73.7566 - 427.7027	$3d^{2} - 3d(a^{2}F)^{4}P$ $3d^{5} - 3d^{4}(a^{3}G)^{4}P$	$a^2H - ^2H^\circ$	ή _ ή 2 - 2	1093
5/0	202.525	15.1500 - 421.1021				
370	282.594	68.4449 - 422.3066	3d ⁵ – 3d⁴(a³P)4p	a²F – ⁴D°	$\frac{2}{2} - \frac{7}{2}$	1093
640	282.676	68.5512 - 422.3066	3d ⁵ – 3d ⁴ (a ³ P)4p	a⁴F – ⁴D°	$\frac{2}{2} - \frac{7}{2}$	1093
540	282.833	64.1524 - 417.7181	3d ⁵ – 3d⁴(a³H)4p	$a^2D - C^{\circ}G^{\circ}$	$\frac{2}{2} - \frac{7}{2}$	1093
490	282.853	65.1735 - 418.7134	3d ⁵ – 3d⁴(a³P)4p	a ² D – ⁴P°	$\frac{3}{2} - \frac{3}{2}$	1093
420	282.924	69.4470 - 422.8978	3d ⁵ – 3d⁴(a ³ G)4p	a ⁴ F - ² F°	5-5	1093
390	282.946	74.6277 - 428.0515	3d ⁵ - 3d⁴(a ³ G)4p	a ² G - ² H°	$\frac{7}{2} - \frac{9}{2}$	1093
350	282,990	74.6277 - 427.9956	3d ⁵ – 3d⁴(a ³ F)4p	a ² G - ² G°	$\frac{7}{2} - \frac{9}{2}$	1093
250	283.032	65.1735 - 418.4908	$3d^{5} - 3d^{4}(a^{3}F)4p$	$a^2D - {}^4F^\circ$	3-3	1093
160	283.071	69.1735 - 422.4372	3d ⁵ – 3d ⁴ (a ³ F)4p	a⁴F – ⁴D°	$\frac{3}{3} - \frac{3}{3}$	1093
160	283,107	67.0851 - 420.3089	$3d^{5} - 3d^{4}(a^{3}P)4p$	$a^2F - {}^4P^\circ$	$\frac{7}{3} - \frac{5}{3}$	1093
400	283.131	79.6083 - 432.8001	$3d^{5} - 3d^{4}(a^{1}G)4p$	$b^2F - F^\circ$	$\frac{7}{3} - \frac{7}{3}$	1093
390	283.213	68.8017 - 421.8940	3d ⁵ – 3d ⁴ (a ⁵ F)4p	a⁴F – ⁴D°	$\frac{7}{2} - \frac{5}{2}$	1093
520	283 327	74 6277 - 427 5750	3d ⁵ – 3d⁴(a ³ F)4n	$a^2G - C^{\circ}$	1-1	1093
190	283.327	$68\ 4449\ -\ 421\ 3743$	$3d^{4} = 3d^{4}(a^{3}F)4p$	$a^{2}F - D^{2}$	\$_\$	1093
570	203.371	754417 - 4282214	$3d^{5} - 3d^{4}(a^{3}F)4p$	$a^2G = {}^2F^{\circ}$	2 1	1093
540	283.403	74 6277 - 427 3422	$3d^{5} - 3d^{4}(a^{3}P)4p$	$a^2G = ^2D^2$	1	1093
520	283.515	75 4417 428 0515	$3d^{5} - 3d^{4}(a^{3}G)4n$	$a^2G = {}^2H^\circ$	2 2	1093
70	283.645	75.4417 - 427.9956	$3d^{5} - 3d^{4}(a^{3}F)4p$	a ² G - ² G°	$\frac{2}{2} - \frac{2}{2}$	1093
			215 2146-3534-		7 5	1002
120	283.670	68.8017 - 421.3243	30° - 30°(a°F)4p			1093
510	283.713	/4.62// - 42/.0960	3d - 3d(ar)4p		2 2 2	1093
390	283.732	69.4470 - 421.8940	3d ² - 3d ² (a ² F)4p		$\frac{2}{5} - \frac{2}{2}$	1093
260	283.816	64.1524 - 416.4930	3d - 3d (a r) 4p		2 2	1093
580	283.862	68.5512 - 420.8357 75.4417 - 427.7027	$3d^{5} - 3d(aF)4p$ $3d^{5} - 3d^{4}(a^{3}G)4p$	$a^2G - H^\circ$	$\frac{2}{2} - \frac{2}{11}$	1093
730	283.977	41.9209 - 394.0610	3d` - 3d⁴(a`D)4p	a⁺G - ⁺F°	$\frac{11}{2} - \frac{2}{2}$	1093
410	284.033	68.5512 - 420.6234	3d ⁵ – 3d ⁴ (a ⁵ F)4p	a⁴F – ⁴G°	$\frac{2}{2} - \frac{11}{2}$	1093
460	284.059	42.0232 - 394.0610	3d ³ - 3d ⁴ (a ³ D)4p	a'G - 'F'	2-2	1093
130	284.192	69.4470 - 421.3243	3d³ – 3d⁴(a°F)4p	a'F - D'		1093
680	284.219	50.3310 - 402.1713 73.7566 425.5676	3d ³ - 3d ⁴ (a ³ D)4p 3d ⁵ - 3d ⁴ (a ³ H)4p	$a^{2}H = {}^{2}H^{\circ}$	<u>й – й</u>	1093
020	204.243	15.1500 - 425.5010	50 - 50 (a 11)+p			
480	284.292	68.8017 - 420.5532	3d ⁵ – 3d⁴(a ³ F)4p	a ⁴ F - ⁴ F°	$\frac{1}{2} - \frac{7}{2}$	1093
450	284.392	72.9088 - 424.5370	3d' - 3d'(a'G)4p	a-H - 'H'	2 - 2	1093
220	284.458	61.1960 - 412.7511	3d ³ – 3d ⁴ (a'H)4p	a-I - "H"	2 - 2	1093
460	284.507	64.1524 - 415.6408	3d' – 3d'(a'F)4p	a-D - "G"	2 - 2	1093
730	284.539	42.0232 - 393.4682	3d' - 3d'(a'D)4p	a'G - 'F'	2-2	1093
650	284.580	50.7776 - 402.1713	3d' - 3d*(a'D)4p	a'D - 'D'	2 - 2	1093
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NI VI -- Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J No	es References
	630	284 671	68 8017 - 420 0800	$3d^{5} - 3d^{4}(a^{3}H)4n$	$a^4F - {}^4G^\circ$	7 - 9	1093
	560	284 845	42 0036 - 393 0720	$3d^{5} - 3d^{4}(a^{5}D)4n$	$a^{\dagger}G = {}^{\dagger}F^{\circ}$	<u>\$</u> _ <u>\$</u>	1093
	710	284 868	42.0351 - 393.0720	$3d^{5} - 3d^{4}(a^{5}D)4n$	$a^4G - {}^4F^\circ$	2 5	1093
	660	284.000	50 7776 - 401 7209	$3d^{5} - 3d^{4}(a^{5}D)4n$	$a^{+}D = {}^{+}D^{\circ}$	5 5	1093
	710	284.940	50.7776 - 401.7209	3d = 3d (a D)4p	a D - D	2 2 2	1093
	/10	285.057	42.0036 - 392.8081	$3d^2 - 3d^2(a^2D)4p$		2 - 2	1093
	230	285.112	72.9088 - 423.6458	3d° – 3d°(a°G)4p	a-H - F	2 - 2	1093
	510	285.195	50.6435 - 401.2809	3d ⁵ - 3d ⁴ (a ⁵ D)4p	a ⁴ D - ⁴ D°	$\frac{1}{2} - \frac{3}{2}$	1093
	490	285.220	73.7566 - 424.3637	3d ⁵ – 3d⁴(a³G)4p	a ² H – ⁴ H°	$\left \frac{11}{2} - \frac{11}{2}\right $	1093
	540	285.304	50.7776 - 401.2809	3d ⁵ – 3d ⁴ (a ⁵ D)4p	a⁴D - ⁴D°	$\frac{5}{2} - \frac{3}{2}$	1093
	290	285.375	69.4470 - 419.8633	$3d^{5} - 3d^{4}(a^{3}H)4p$	a⁴F - ⁴G°	5 - 7	1093
	430	285.456	50.6435 - 400.9621	$3d^{5} - 3d^{4}(a^{5}D)4p$	$a^4D - {}^4D^\circ$	<u>i</u> - i	1093
	440	285.471	96.5665 - 446.8638	$3d^{5} - 3d^{4}(a^{\dagger}D)4p$	$b^2D - {}^2F^{\circ}$	$\frac{5}{2} - \frac{7}{2}$	1093
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	280	285.537	69.1735 - 419.3905	$3d^{3} - 3d^{4}(a^{3}H)4p$	a'F – 'G°	$\frac{1}{2} - \frac{2}{2}$	1093
	430	285.566	50.7805 - 400.9621	3d ⁵ - 3d ⁴ (a ⁵ D)4p	a⁴D – ⁴D°	$\frac{3}{2} - \frac{1}{2}$	1093
	370	285.587	72.9088 - 423.0652	3d⁵ – 3d⁴(a³H)4p	a ² H - ² H°	$\frac{9}{2} - \frac{9}{2}$	1093
	170	285.611	75.4417 - 425.5676	$3d^{5} - 3d^{4}(a^{3}H)4p$	a ² G - ² H°	$\frac{2}{2} - \frac{11}{2}$	1093
	550	285.710	73.7566 - 423.7633	$3d^{5} - 3d^{4}(a^{3}G)4p$	$a^2H - {}^4F^\circ$	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>	1093
	280	285.789	74.6277 - 424.5370	3d ⁵ - 3d ⁴ (a ³ G)4p	a ² G - ⁴ H°	$\frac{7}{2} - \frac{9}{2}$	1093
	(10	285.022	72.0088 422.6424	245 244-311.4-	-211 219	9 11	1002
	010	285.932	72.9088 - 422.0424	$3d^2 = 3d^2(a^2H)4p$		$\frac{1}{2} - \frac{1}{2}{5}$	1093
	170	286.040	96.4612 - 446.0612	3d" – 3d"(a'D)4p	$\mathbf{b}^{2}\mathbf{D} - \mathbf{F}^{2}$	1 2 - 2	1093
	360	286.127	96.5665 - 446.0612	3d` – 3d*(a'D)4p	b ⁻ D - ⁻ F°	2-2	1093
	210	286.200	67.0851 - 416.4930	$3d^{3} - 3d^{4}(a^{3}F)4p$	$a^2F - D^\circ$	$\frac{1}{2} - \frac{1}{2}$	1093
	150	286.257	67.0851 - 416.4225	3d ⁵ - 3d ⁴ (a ³ F)4p	a ² F – ⁴ G°	$\frac{7}{2} - \frac{9}{2}$	1093
	370	286.310	68.4449 - 417.7181	$3d^{5} - 3d^{4}(a^{3}H)4p$	$a^2F - C^\circ$	$\frac{5}{2} - \frac{7}{2}$	1093
	310	286.421	74.6277 - 423.7633	3d ⁵ - 3d⁴(a³G)4p	$a^2G - {}^4F^{\circ}$	7 - 2	1093
	380	286 448	75 4417 - 424 5370	$3d^5 = 3d^4(a^3G)4n$	$a^2G = {}^4H^\circ$	2 2	1093
	420	286 547	68 5512 - 417 5384	$3d^{5} - 3d^{4}(a^{3}H)4n$	$a^{4}F = {}^{4}G^{\circ}$	а́_ц	1093
	420	286.540	72 7566 422 7119	$3d^{5} - 3d^{4}(a^{3}H)An$			1093
	460	286.509	75.7500 - 422.7118	3d - 3d (a H)+p	a = 1	$\frac{2}{9} = \frac{2}{11}$	1093
	400	280.397	73.4417 - 424.3037	3d - 3d (a G)4p		$\frac{1}{11} - \frac{1}{11}$	1093
	160	280.024	13.1300 - 422.0424	3d' - 3d'(a'H)4p	a-H1	$\frac{1}{2} - \frac{1}{2}$	1093
	150	286.670	79.3914 - 428.2214	3d ⁵ - 3d⁴(a ³ F)4p	$b^2F - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$	1093
	180	286.768	74.6277 - 423.3414	$3d^{5} - 3d^{4}(a^{3}G)4p$	a²G – ⁴H°	$\frac{7}{2} - \frac{7}{2}$	1093
	360	286.806	67.0851 - 415.7543	$3d^{5} - 3d^{4}(a^{3}H)4p$	$a^2F - {}^4I^\circ$	$\frac{7}{2} - \frac{9}{2}$	1093
	610	286.851	79.6083 - 428.2214	$3d^{5} - 3d^{4}(a^{3}F)4p$	$b^2F - {}^2F^\circ$	$\frac{7}{2} - \frac{7}{2}$	1093
	610	286.977	86.5321 - 434.9958	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^2S - {}^2P^\circ$	$\frac{1}{2} - \frac{3}{2}$	1093
	610	286.991	74.6277 - 423.0652	3d ⁵ – 3d ⁴ (a ³ H)4p	a²G - ²H°	$\frac{7}{2} - \frac{9}{2}$	1093
	90	287 035	79 6083 - 427 9956	$3d^{5} - 3d^{4}(a^{3}F)4n$	$h^2 E = {}^2 G^2$	Z_2	1093
	260	287.089	96 4612 - 444 7842	$3d^{5} - 3d^{4}(a^{1}D)4n$	$h^2D = 2D^2$	3 5	1093
	430	287 134	74 6277 - 422 8978	$3d^{5} - 2d^{4}(a^{3}C)An$	$^{2}G$ $^{2}F^{\circ}$	Ž Š	1093
	520	287.134	06 5665 444 7842	3d = 3d (a G) + p		2 2	1093
	240	287.170	70.3003 - 444.7842	$3d^{2} - 3d(aD)4p$		$\frac{2}{5} - \frac{2}{7}$	1093
	340	287.203	19.3914 - 427.3730	3d' - 3d'(a'F)4p	$\mathbf{b}^{\mathbf{F}} - \mathbf{G}^{\mathbf{F}}$	$\frac{5}{2} - \frac{5}{2}$	1093
	230	287.320	107.8483 - 455.8876	3d ² - 3d ² (a ² F)4p	0-GG	2 - 2	1093
	640	287.387	79.6083 - 427.5750	3d ⁵ - 3d ⁴ (a ³ F)4p	b²F - ²G°	$\frac{1}{2} - \frac{1}{2}$	1093
	220	287.470	68.5512 - 416.4225	$3d^{5} - 3d^{4}(a^{3}F)4p$	a⁴F – ⁴G°	3-3	1093
	490	287.530	96.4612 - 444.2522	$3d^{5} - 3d^{4}(a^{1}D)4p$	$b^2D - {}^2D^\circ$	3-3	1093
	520	287.577	79.6083 - 427.3422	$3d^{5} - 3d^{4}(a^{3}P)4p$	$b^2F - {}^2D^\circ$	7 - 5	1093
	480	287.599	79.3914 - 427.0960	3d ⁵ - 3d ⁴ (a ³ F)4p	$b^2 F - {}^2 F^\circ$	5_5	1093
	480	287.668	68.8017 - 416.4225	$3d^{5} - 3d^{4}(a^{3}F)4p$	a⁴F – ⁴G°	$\frac{1}{2} - \frac{1}{2}$	1093
					47. 1-1		
	280	287.701	45.8842 - 393.4682	3d [°] – 3d ⁴ (a [°] D)4p	$a^{*}P - {}^{*}F^{\circ}$	2 - 2	1093
	460	287.778	79.6083 - 427.0960	3d' - 3d'(a'F)4p	b ² F – ² F°	$\frac{1}{2} - \frac{2}{2}$	1093
	370	287.848	86.5321 - 433.9369	3d ⁵ – 3d ⁴ (a ¹ S)4p	$a^2S - {}^2P^\circ$	$\frac{1}{2} - \frac{1}{2}$	1093
	150	287.965	74.6277 - 421.8940	3d ⁵ – 3d ⁴ (a ³ F)4p	a ² G - ⁴ D [•]	$\frac{7}{2} - \frac{5}{2}$	1093
	570	287.999	129.9516 - 477.1771	$3d^{5} - 3d^{4}(a^{3}P)4p$	$a^2P - {}^2S^\circ$	$\frac{3}{2} - \frac{1}{2}$	1093
	240	288.028	45.8842 - 393.0720	3d ⁵ - 3d ⁴ (a ⁵ D)4p	a ⁴ P - ⁴ F°	5-5	1093

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Iultiplet Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm $^{-1}$ )	Configurations	Terms	J - J N	lotes	Referen
240	288.059	130.0259 - 477.1771	$3d^{5} - 3d^{4}(a^{3}P)4p$	$a^2P - {}^2S^\circ$	$\frac{1}{2} - \frac{1}{2}$		1093
500	288.222	72.9088 - 419.8633	$3d^{5} - 3d^{4}(a^{3}H)4p$	a²H – ⁴G°	$\frac{9}{2} - \frac{7}{2}$		1093
90	288.296	73.7566 - 420.6234	$3d^{5} - 3d^{4}(a^{3}F)4n$	a ² H – ⁴ G°	<u>1</u> – <u>1</u>		1093
150	288 437	46 1044 - 392 8081	$3d^{5} - 3d^{4}(a^{5}D)4n$	$a^{4}P - {}^{4}F^{\circ}$	3 3		1093
110	288 613	46 3248 302 8081	$3d^{5} - 3d^{4}(a^{5}D)/a^{5}$	$a^4 P 4 F^\circ$			1003
400	288.013	40.3248 - 332.8081	$3d^5 - 3d^4(a^3\mathbf{P})Ap$	$h^2 E = {}^2 D^2$	2 2 2 2 2 3		1093
400	200.737	79.3914 - 423.7031	50 - 50 (a r)4p	0r-D	2 - 2		1095
400	288.854	69.4470 - 415.6408	$3d^{5} - 3d^{4}(a^{3}F)4p$	$a^4F - {}^4G^\circ$	$\frac{5}{2} - \frac{7}{2}$		1093
240	288.885	96.4612 - 442.6199	3d ³ – 3d ⁴ (a ³ D)4p	$b^2D - {}^2D^\circ$	$\frac{2}{2} - \frac{2}{2}$		1093
180	288.937	107.8870 - 453.9830	3d ⁵ – 3d⁴(a¹F)4p	b ² G – ² G°	$\frac{1}{2} - \frac{1}{2}$		1093
300	288.971	96.5665 - 442.6199	$3d^{5} - 3d^{4}(a^{3}D)4p$	$b^2D - {}^2D^\circ$	$\frac{5}{2} - \frac{3}{2}$	ĺ	1093
40	289.038	69.1735 - 415.1445	$3d^{5} - 3d^{4}(a^{3}P)4p$	a ⁴ F – ⁴ D°	$\frac{3}{2} - \frac{5}{2}$		1093
70	289.077	69.4470 - 415.3820	$3d^{5} - 3d^{4}(a^{3}F)4p$	a⁴F – ⁴G°	\$ - \$		1093
260	289.467	72 9088 - 418 3688	$3d^5 - 3d^4(a^3H)4n$	$a^2H = {}^2G^2$	2 2		1093
430	200.593	96 4612 441 7857	$3d^{5} - 3d^{4}(a^{3}D)/a$	h ² D ² E ⁹	2 2		1003
430	209.303	90.4012 - 441.7837	3u = 3u (a D) + p		2 - 2		1093
300	289.995	90.3003 - 441.4012	$3d^2 = 3d^2(a^2D)4p$		$\frac{1}{2} - \frac{1}{2}$ 9 7	Í	1093
240	290.014	72.9088 - 417.7181	$3d^2 = 3d^2(a^2H)4p$	a-HG	$\frac{1}{2} - \frac{1}{2}$		1093
350	290.149	96.5665 - 441.2161	3d ² – 3d ² (a ² D)4p	b"D - "F"	$\frac{1}{2} - \frac{1}{2}$		1093
160	290.181	73.7566 - 418.3688	3d° – 3d*(a'H)4p	a²H – ²G°	$\frac{11}{2} - \frac{2}{2}$		1093
80	290.326	86.5321 - 430.9719	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^2S - {}^4D^\circ$	$\frac{1}{2} - \frac{3}{2}$		1093
150	290.388	86.5321 - 430.8988	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^2S - {}^4D^\circ$	$\frac{1}{3} - \frac{1}{3}$		1093
100	290.429	79.3914 - 423.7105	$3d^5 - 3d^4(a^3G)4p$	b ² F – ⁴ F°	$\frac{5}{2} - \frac{3}{2}$		1093
310	290 504	96 4612 - 440 6893	$3d^5 - 3d^4(a^3D)4n$	$h^2D - P^{\circ}$	3_1		1093
340	290.666	79 6083 - 423 6458	$3d^{5} - 3d^{4}(a^{3}G)4n$	$b^2 \mathbf{F} = {}^2 \mathbf{F}^2$			1093
270	200.687	107 8483 451 8504	$3d^{5} = 3d^{4}(a^{\dagger}E)/a$	$h^2 G^{-2} F^{\circ}$	$\frac{2}{9}$ $\frac{2}{7}$	ĺ	1003
220	290.087	107.6463 - 451.6594	50 – 50 (a 1 ⁻ )4p	00-1	2 - 2		1095
90	290.739	79.3914 - 423.3414	3d ⁵ - 3d ⁴ (a ³ G)4p	$b^2 F - {}^4 H^\circ$	$\frac{5}{2} - \frac{7}{2}$		1093
590	290.802	45.8842 - 389.7604	3d³ – 3d⁴(a³D)4p	a ⁴ P – ⁴ P°	$\frac{2}{2} - \frac{2}{2}$	Ì	1093
170	290.830	130.0259 - 473.8695	3d ⁵ – 3d ⁴ (b ³ P)4p	$a^2P - {}^2P^\circ$	$\frac{1}{2} - \frac{1}{2}$		1093
520	290.925	50.3310 - 394.0610	3d⁵ – 3d⁴(a⁵D)4p	a⁴D - ⁴F°	$\frac{7}{2} - \frac{9}{2}$		1093
480	290.988	46.1044 - 389.7604	3d ⁵ – 3d ⁴ (a ⁵ D)4p	$a^{4}P - {}^{4}P^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		1093
270	291.035	96.5665 - 440.1686	$3d^{5} - 3d^{4}(a^{1}S)4p$	$b^2D - {}^2P^\circ$	$\frac{5}{2} - \frac{3}{2}$		1093
220	291 115	79 3914 - 422 8978	3d ⁵ - 3d ⁴ (a ³ G)4n	$b^2 F - {}^2 F^\circ$	5-5	ĺ	1093
170	291 201	73 7566 - 417 1641	$3d^5 = 3d^4(a^3H)4n$	2 ² H - 41°	<u> </u>		1093
560	201.264	45 8842 389 2140	$3d^{5} = 3d^{4}(a^{5}D)/a$		$\begin{bmatrix} 2 & - & 2 \\ 5 & 3 \end{bmatrix}$		1003
500	291.204	45.8842 - 585.2140	$3d^{2} = 3d(a^{2}D)^{4}p$	$a \mathbf{r} = \mathbf{D}$ $\mathbf{h}^2 \mathbf{E} = 2 \mathbf{E}^\circ$	$\frac{2}{7}$ $\frac{2}{5}$		1093
200	291.297	79.0083 - 422.8978	3d = 3d (a G) + p		$\frac{2}{7}$ $\frac{2}{7}$		1095
370	291.427	50.3310 - 393.4682 74.6277 - 417.7181	$3d^{5} = 3d^{4}(a^{3}H)4p$ $3d^{5} = 3d^{4}(a^{3}H)4p$	$a^2D = F^2$	$\frac{5}{7} - \frac{5}{7}$		1093
220	271.400	,4.02,7, 417.7101	5 <b>u</b> 5 <b>u</b> ( <b>u</b> 11) (p				10/5
150	291.609	75.4417 - 418.3688	$3d^{5} - 3d^{4}(a^{3}H)4p$	$a^2G - {}^2G^{\circ}$	$\frac{9}{2} - \frac{9}{2}$		1093
480	291.641	46.3248 - 389.2140	3d ³ – 3d ⁴ (a ³ D)4p	a⁺P – °D°	2 - 2		1093
460	291.703	46.1044 - 388.9186	3d⁵ 3d⁴(a⁵D)4p	a⁺P – °D°	$\frac{2}{2} - \frac{1}{2}$		1093
420	291.806	50.7776 - 393.4682	3d ⁵ – 3d ⁴ (a ⁵ D)4p	a*D – *F°	$\frac{2}{2} - \frac{7}{2}$		1093
250	291.891	46.3248 - 388.9186	3d ⁵ – 3d ⁴ (a ⁵ D)4p	$a^4P - b^\circ$	$\frac{1}{2} - \frac{1}{2}$		1093
220	291.918	140.9222 - 483.4809	3d ⁵ – 3d ⁴ (b ³ F)4p	$c^2D - C^2D^\circ$	$\frac{5}{2} - \frac{3}{2}$		1093
440	291,990	141.0068 - 483.4809	$3d^{5} - 3d^{4}(h^{3}F)4n$	$c^2D - ^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$		1093
450	292.146	50.7805 - 393.0720	$3d^{5} - 3d^{4}(a^{5}D)4n$	a ⁴ D - ⁴ F°	$\frac{1}{3} = \frac{1}{5}$		1093
30	292.208	79.3914 - 421.6072	$3d^{5} - 3d^{4}(a^{3}F)4n$	$b^2 F - {}^2 D^\circ$	3 3		1093
240	292.256	50 6435 - 392 8081	$3d^5 = 3d^4(a^5\Pi)4n$	$a^{4}D - F^{6}$	$\left  \frac{2}{1} - \frac{2}{3} \right $		1093
540	202 204	140 0222 - 483 0424	3d ⁵ - 2d ⁴ (h ³ E)/h	$\begin{bmatrix} a^2 D & -1 \\ a^2 D & -2 D^2 \end{bmatrix}$	2 5		1002
440	292.367	141.0068 - 483.0434	$3d^{5} - 3d^{4}(b^{3}F)4p$	$c^2D - D^2$	2 - 2 3 - 2		1093
280	292.402	73.7566 - 415.7543	$3d^{-} - 3d^{+}(a^{-}H)4p$	a'H - 'I'	$\left \frac{11}{2} - \frac{9}{2}\right $		1093
510	292.427	45.8842 - 387.8499	3d° – 3d4(a°D)4p	a*P - *D*	$\frac{2}{2} - \frac{2}{2}$		1093
140	292.456	79.3914 - 421.3243	$3d^{5} - 3d^{4}(a^{3}F)4p$	$b^2 F - D^\circ$	$\frac{5}{2} - \frac{5}{2}$		1093
360	292.616	46.1044 - 387.8499	3d ⁵ - 3d ⁴ (a ⁵ D)4p	a ⁴ P – ⁶ D°	$\frac{3}{2} - \frac{5}{2}$		1093
80	292.784	42.0036 - 383.5578	$3d^{5} - 3d^{4}(a^{5}D)4p$	a4G - 6P°	$\frac{5}{2} - \frac{3}{2}$		1093
40	293.059	79.6083 - 420.8357	$3d^{5} - 3d^{4}(a^{3}F)4p$	b ² F - ⁴ F°	7 - 9		1093
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NI VI - Continued

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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	1 - 1	Notes	References
	70	293.248	74.6277 - 415.6408	3d ⁵ – 3d ⁴ (a ³ F)4p	$a^2G - {}^4G^\circ$	$\frac{7}{2} - \frac{7}{2}$		1093
	140	293.467	42.0036 - 382.7589	$3d^{5} - 3d^{4}(a^{5}D)4p$	a⁴G - ⁶ F°	5 - I		1093
	190	293.482	42.0232 - 382.7589	$3d^{5} - 3d^{4}(a^{5}D)4p$	a ⁴ G - ⁶ F°	2 - 2		1093
	110	293.517	79.6083 - 420.3089	$3d^{5} - 3d^{4}(a^{3}P)4p$	$b^2 F - {}^4 P^\circ$	1 - 5		1093
	200	293,849	75 4417 - 415 7543	$3d^5 - 3d^4(a^3H)4n$	$a^2G = {}^4I^\circ$	2 2		1093
	570	293 883	45 8842 - 386 1573	$3d^{5} - 3d^{4}(a^{5}D)4n$	$a^4P = {}^4P^\circ$	5 3		1093
	570	275.005	45.0042 - 500.1575	50 - 50 (a D)+p	a1~1	2 - 2		1075
	60	293.944	75.4417 - 415. <b>64</b> 08	3d ⁵ - 3d ⁴ (a ³ F)4p	a²G − ⁴ G°	$\frac{9}{2} - \frac{7}{2}$		1093
	140	294.074	46.1044 - 386.1573	3d ⁵ − 3d ⁴ (a ⁵ D)4p	$a^{4}P - {}^{4}P^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		1093
	290	294.121	79.3914 - 419.3905	3d⁵ – 3d⁴(a³H)4p	b²F – ⁴G°	$\frac{5}{2} - \frac{5}{2}$		1093
	110	294.224	73.7566 - 413.6316	$3d^{5} - 3d^{4}(a^{3}H)4p$	$a^2H - {}^4H^\circ$	12 - 13		1093
	480	294.264	42.0036 - 381.8328	$3d^{5} - 3d^{4}(a^{5}D)4p$	a⁴G - ⁶ F°	3 - 5		1093
	330	294.290	42.0351 - 381.8328	$3d^{5} - 3d^{4}(a^{5}D)4p$	a ⁴ G - ⁶ F°	Ž - ž		1093
	350	294.362	141.0068 - 480.7242	3d' – 3d'(b'G)4p	$c^2D - F^{\circ}$	$\frac{2}{2} - \frac{3}{2}$		1093
	190	294.507	50.3310 - 389.8832	$3d^{5} - 3d^{4}(a^{5}D)4p$	a⁴D – °D°	$\frac{1}{2} - \frac{9}{2}$		1093
	640	294.613	50.3310 - 389.7604	3d ⁵ − 3d ⁴ (a ⁵ D)4p	$a^4D - {}^4P^\circ$	$\frac{7}{2} - \frac{5}{2}$		1093
	490	294.754	140.9222 - 480.1893	3d ⁵ – 3d⁴(b¹G)4p	$c^2D - F^\circ$	$\frac{5}{2} - \frac{7}{2}$		1093
	130	294.819	72.9088 - 412.0956	$3d^{5} - 3d^{4}(a^{3}H)4p$	$a^2H - {}^4H^\circ$	$\frac{9}{2} - \frac{9}{2}$		1093
	180	294.850	42.0036 - 381.1638	3d ⁵ - 3d ⁴ (a ⁵ D)4p	a⁴G – ⁰F°	$\frac{5}{2} - \frac{3}{2}$		1093
	600	295 001	50 7776 - 389 7604	3d ⁵ – 3d⁴(a ⁵ D)4p	a ⁴ D . ⁴ P°	5 5		1093
	570	295.001	79 6083 418 3688	$3d^5 - 3d^4(a^3H)/4p$	aD = r $b^2E^{-2}C^{\circ}$	$\frac{2}{7}$ $\frac{2}{9}$		1093
	590	295.194	75.0085 - 418.3088 46.1044 - 384.7474	$3d^{2} - 3d(a H) + p$	$D^{+}F = {}^{+}G$	$\frac{1}{3} - \frac{1}{1}$	1	1093
	380	293.298	40.1044 - 384.7474	3d ² - 3d (a ² D)4p	aP-P	$\frac{5}{2} - \frac{5}{2}$		1093
	270	295.362	50.6435 - 389.2140	3d" – 3d"(a D)4p	$a^{*}D - {}^{\circ}D^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		1093
	150	295.389	96.4612 - 434.9970	3d ³ – 3d ⁴ (a'G)4p	$b^2D - F^3$	2 - 2		1093
	590	295.480	50.7805 - 389.2140	3d ⁵ – 3d ⁴ (a ⁵ D)4p	$a^{4}D - b^{\circ}D^{\circ}$	$\frac{2}{2} - \frac{2}{2}$		1093
	520	295.573	79.3914 - 417.7181	$3d^{5} - 3d^{4}(a^{3}H)4p$	$b^2 F - {}^2 G^{\circ}$	5 - 7		1093
	590	295.622	50.6435 - 388.9186	$3d^{5} - 3d^{4}(a^{5}D)4p$	a⁴D – ⁵D°	1 <u>1</u> - <u>1</u>		1093
	530	296.009	96.4612 - 434.2816	$3d^{5} - 3d^{4}(a^{3}D)4p$	$b^2D - {}^4P^\circ$	3-1		1093
	210	296.145	45.8842 - 383.5578	$3d^{5} - 3d^{4}(a^{5}D)4n$	$a^{4}P - {}^{6}P^{6}$	2 3		1093
	100	296.238	64.1524 - 401.7209	$3d^5 = 3d^4(a^5D)4p$	$a^2D = D^{\circ}$	5_5		1093
	570	296.279	50.3310 - 387.8499	$3d^{5} - 3d^{4}(a^{5}D)4p$	$a^{4}D - b^{\circ}D^{\circ}$	2 2 2		1093
						2 2		
	110	296.310	96.4612 - 433.9369	$3d^{5} - 3d^{4}(a^{1}S)4p$	$b^2 D - {}^2 P^\circ$	$\frac{3}{2} - \frac{1}{2}$	1	1093
	70	296.531	46.3248 - 383.5578	3d ⁵ – 3d ⁴ (a ⁵ D)4p	a ⁴ P – ⁶ P°	$\frac{1}{2} - \frac{3}{2}$		1093
	270	296.630	86.5321 - 423.6468	$3d^{5} - 3d^{4}(a^{3}P)4p$	$a^2S - {}^2P^\circ$	$\frac{1}{2} - \frac{1}{2}$		1093
	460	296.672	50.7776 - 387.8499	$3d^{5} - 3d^{4}(a^{5}D)4p$	a⁴D – °D°	$\frac{5}{2} - \frac{5}{2}$		1093
	60	296.831	79.6083 - 416.4930	$3d^{5} - 3d^{4}(a^{3}F)4p$	b²F - ⁴D°	$\frac{7}{2} - \frac{7}{2}$		1093
	50	296.846	45.8842 - 382.7589	3d ⁵ - 3d ⁴ (a ⁵ D)4p	a ⁴ P – ⁶ F [°]	$\frac{5}{2} - \frac{7}{2}$		1093
	70	296,901	79.6083 - 416.4225	$3d^{5} - 3d^{4}(a^{3}E)4p$	$h^2 F - {}^4 G^{\circ}$	7 9		1093
	150	297.001	129.9516 - 466 6491	$3d^5 - 3d^4(h^3F)4p$	$a^2 P = {}^2 F^{\circ}$	1 2 2		1093
	250	297.400	79.3914 - 415.6408	$3d^{5} - 3d^{4}(a^{3}E)4n$	$h^2 E = {}^4 G^{\circ}$	2 Z		1093
	360	297 490	79 6083 - 415 7543	$3d^{5} - 3d^{4}(a^{3}H)An$	5 ² E 47°	2 - 2 2 - 2		1093
	170	297.526	65 1735 - 401 2809	$3d^{5} - 3d^{4}(a^{5}D)/a$		2 - 2		1093
	180	297.520	129 9516 466 0342	3d - 3d (a D) + p		3 3		1093
	100	277.544	129.9310 - 400.0342	5 <b>u</b> - 5 <b>u</b> (0 F)4p	ar - D	2 - 2		1093
	420	297.612	130.0259 - 466.0342	3d ^s - 3d⁴(b³P)4p	$a^2P - {}^2D^\circ$	1 - 3		1093
	120	297.659	45.8842 - 381.8328	$3d^{5} - 3d^{4}(a^{5}D)4p$	$a^4P - {}^6F^\circ$	š _ š		1093
	220	297.806	65,1735 - 400,9621	$3d^5 - 3d^4(a^5D)4n$	$a^2D - {}^4D^\circ$	3_1		1093
	370	297.973	129.9516 - 465 5527	$3d^{5} = 3d^{4}(h^{3}P)4h$	$a^2 P = 2 D^{\circ}$	3 5		1093
	170	298 049	50 6435 - 386 1573	3d ⁵ - 3d ⁴ (a ⁵ D)/a	at - D	2 - 2 1 3		1093
	520	298.170	50.7776 - 386.1573	$3d^{5} - 3d^{4}(a^{5}D)4n$	$a^{4}D - P^{\circ}$	4 4		1093
						2 - 2		
	210	298.832	67.0851 - 401.7209	3d ⁵ - 3d ⁴ (a ⁵ D)4p	$a^{2}F - {}^{4}D^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		1093
	410	299.305	50.6435 - 384.7474	3d° - 3d⁺(a'D)4p	a*D – *P°	2-2		1093
	350	299.341	129.9516 - 464.0278	3d³ – 3d⁴(b³F)4p	a²P – ⁴G°	2 - 2		1093
	350	299.417						1093
	580	299.495	107.8870 - 441.7857	3d ⁵ - 3d ⁴ (a ³ D)4p	$b^2G - {}^2F^\circ$	$\frac{7}{2} - \frac{5}{2}$		1093
	700	299.742	68.5512 - 402.1713	3d ⁵ – 3d ⁴ (a ⁵ D)4p	a⁴F – ⁴D°	$\frac{9}{2} - \frac{7}{2}$		1093

NI VI - Continued

Multiplet Rel.	Int. $\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	Reference
63	30 299.967	107.8483 - 441.2161	3d ⁵ - 3d ⁴ (a ³ D)4p	$b^2G - {}^2F^\circ$	$\frac{9}{2} - \frac{7}{2}$		1093
30	299.996	107.8870 - 441.2161	3d ⁵ – 3d⁴(a³D)4p	b ² G – ² F°	$\frac{1}{2} - \frac{1}{2}$	i	1093
52	20 300.053	68.4449 - 401.7209	3d⁵ – 3d⁴(a⁵D)4p	$a^2F - {}^4D^\circ$	$\frac{5}{2} - \frac{5}{2}$		1093
49	300.272	107.8870 - 440.9179	$3d^{5} - 3d^{4}(a^{1}I)4p$	b ² G - ² H°	$\frac{7}{2} - \frac{9}{2}$		1093
27	70 300.334	50.7776 - 383.7398	$3d^{5} - 3d^{4}(a^{5}D)4p$	a⁴D – °P°	5-5		1093
67	70 300.372	68.8017 - 401.7209	$3d^{5} - 3d^{4}(a^{5}D)4p$	a⁴F - ⁴D°	$\frac{1}{2} - \frac{5}{2}$		1093
44	40 300.426	141.0068 - 473.8695	3d ⁵ - 3d ⁴ (b ³ P)4p	$c^2 D - {}^2 P^\circ$	$\frac{3}{2} - \frac{1}{2}$		1093
58	300.447	68.4449 - 401.2809	3d" - 3d"(a"D)4p	$a^{2}F - D$	2 - 2		1093
20	300.499	50.7776 - 383.5578	3d' – 3d'(a'D)4p	$a^{*}D - {}^{*}P^{*}$	2 - 2		1093
25	50 300.545	69.4470 - 402.1713	3d ³ – 3d ⁴ (a ³ D)4p	a*F - *D*	2 - 2		1093
12	20 300.707	69.1735 - 401.7209	3d° - 3d4(a°D)4p	a⁴F - ⁴D°	$\frac{2}{2} - \frac{2}{2}$		1093
	300.89	0.0 - 332.3448	3d ³ – 3d ⁴ (a ³ P)4s	ga°S – ⁴ P	$\frac{2}{2} - \frac{2}{2}$	F,P	375,109
36	60 300.955	69.4470 - 401.7209	3d ⁵ – 3d⁴(a ⁵ D)4p	a⁴F – ⁴D°	\$ - \$		1093
47	70 301 031	107 8483 - 440 0392	$3d^{5} - 3d^{4}(a^{T})4p$	$b^2G - {}^2H^\circ$	3 - 4		1093
4	50 301 107	69.1735 - 401.2809	$3d^5 - 3d^4(a^5D)4n$	$a^4F - {}^4D^\circ$	3 - 3		1093
	201.174	06 4612 428 4065	$3d^{5} - 3d^{4}(a^{3}G)An$	$h^2 D = {}^4 G^2$	3_5		1093
3	301.174	140 0222 472 8220	$3d^{5} - 3d^{4}(h^{3}B)/m$	$a^2 D = C$	$\frac{2}{5}$		1003
40	301.286	140.9222 - 472.8330	30° - 30°(0° F)4p	$c^{4}E^{-4}D^{\circ}$	2 - 2		1093
52	301.355	69.4470 - 401.2809	3d" - 3d"(a"D)4p	ar - D	2-2		1093
58	80 301.396	69.1735 - 400.9621	3d⁵ - 3d⁴(a⁵D)4p	a⁴F - ⁴D°	$\frac{3}{2} - \frac{1}{2}$		1093
54	40 301.518	96.5665 - 428.2214	3d ⁵ – 3d⁴(a³F)4p	$b^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		1093
2	20 301.739	130.0259 - 461.4378	3d ⁵ – 3d⁴(b³P)4p	$a^2P - {}^4P^\circ$	$\frac{1}{2} - \frac{3}{2}$		1093
ç	302.065	50.7805 - 381.8328	$3d^{5} - 3d^{4}(a^{5}D)4p$	a⁴D - °F°	3-5		1093
14	40 302 108	96 5665 - 427 5750	$3d^{5} - 3d^{4}(a^{3}F)4p$	$b^2D - G^\circ$	\$ - 7		1093
37	70 302.224	96.4612 - 427.3422	3d ⁵ - 3d ⁴ (a ³ P)4p	$b^2D - {}^2D^\circ$	3 - 2		1093
		107 0402 420 (204	245 246-004-		9 9		1002
3/	70 302.306	107.8483 - 438.0394	30 - 30 (a O)4p		3 5		1093
23	30 302.448	96.4612 - 427.0960	3d" – 3d"(a"F)4p	$\mathbf{D}^{*}\mathbf{D} - \mathbf{F}^{*}$	5-3		1093
18	80 302.536	96.5665 - 427.0960	3d ⁻ – 3d ⁻ (a ⁻ F)4p	b ² D - ² F ²	1 1 - 1		1093
18	80 303.001	107.8870 - 437.9197	3d` - 3d*(a'G)4p	b-GG*	2 - 2		1093
	303.03	0.0 - 330.0016	$3d^{5} - 3d^{4}(a^{3}P)4s$	ga ^a S – ⁴ P	$\frac{2}{2} - \frac{2}{2}$	F,P	375,10
	304.47	0.0 - 328.4372	3d ⁵ - 3d ⁴ (a ³ P)4s	ga ⁶ S – ⁴ P	2-2	F,P	375,109
1	70 305.220	65.1735 - 392.8081	3d ⁵ - 3d⁴(a ⁵ D)4p	a²D – ⁴F°	3-3		1093
74	50 305 658	107 8483 - 435 0115	$3d^{5} - 3d^{4}(a^{T}G)4n$	$b^2G - {}^2H^\circ$	1 3 _ H	1	1093
24	306.056	75 4417 - 402 1713	$3d^{5} - 3d^{4}(a^{5}D)4p$	$a^2 G = {}^4 D^2$	<u>9</u> _1		1093
2	10 306.399	67.0951 202.4692	$3d^5 - 3d^4(a^5D)Ap$	$a^2 \mathbf{E} = {}^4 \mathbf{E}^{\circ}$	i_i		1093
11	10 300.388	07.0631 - 373.4082	3d = 3d (a D) + p		$\frac{2}{1}$ $\frac{2}{2}$		1003
29	90 306.489	107.8870 - 434.1673	3d - 3d (a C)4p		$\frac{1}{7}$ $\frac{1}{7}$		1093
57	70 307.097	107.8870 - 433.5173	3d" - 3d"(a'G)4p	0°G ~ °G	2 - 2		1093
71	10 307.207	68.5512 - 394.0610	3d ⁵ - 3d ⁴ (a ⁵ D)4p	a⁴F – ⁴F°	$\frac{9}{2} - \frac{9}{2}$		1093
9	90 307.383	96.5665 - 421.8940	3d ⁵ – 3d ⁴ (a ³ F)4p	b ² D – ⁴ D°	2 - 2		1093
20	60 307.449	68.8017 - 394.0610	3d ⁵ - 3d⁴(a ⁵ D)4p	a ⁴ F – ⁴ F°	$\frac{1}{2} - \frac{9}{2}$		1093
47	20 307.492	140.9222 - 466.1337	3d ⁵ - 3d ⁴ (b ³ F)4p	$c^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{1}{2}$		1093
6	90 307.592	140.9222 - 466.0342	$3d^{5} - 3d^{4}(b^{3}P)4p$	$c^2D - {}^2D^\circ$	$\frac{5}{7} - \frac{3}{7}$		1093
10	60 307.613	107.8483 - 432.9320	3d ⁵ - 3d ⁴ (a'I)4p	b ² G - ² I°	$\frac{1}{2} - \frac{11}{2}$		1093
	10 207 (70	69 4440 202 4692	245 244(-50)4-	a ² E ⁴ E ^o	<u>5</u> 2		1003
2	50 507.670	08.4449 - 393.4082	30 - 30 (a D)4p		2 2		1093
37	70 307.773	08.0012 - 393.4082	50° - 30°(a°D)4p		2-2		1093
17	70 307.819	96.4612 - 421.3243	30" - 30"(a"F)4p	0'D - 'D'	2-3		1093
58	80 308.009	68.8017 - 393.4682	3d' - 3d'(a'D)4p	a'F - 'F'	2-2		1093
44	40 308.046	140.9222 - 465.5527	3d [°] - 3d⁴(b [°] P)4p	c ⁻ D - ⁻ D°	1 2 - 2		1093
30	00 308.299	68.4449 - 392.8081	3d' - 3d*(a'D)4p	a'F - *F*	2 - 2		1093
	80 308.385	68.8017 - 393.0720	3d ⁵ - 3d⁴(a ⁵ D)4p	a⁴F - ⁴F°	2 - 5		1093
25		(0.4470, 000,4400	$3d^5 - 3d^4(a^5D)4p$	$a^{4}F - {}^{4}F^{\circ}$	3-2		1093
2	80 308 623	694470 - 3934687					
22	80 308.623	69.4470 - 393.4682	$3d^{5} = 3d(a^{2}b)^{4}p^{2}$	$c^2 D = {}^4 G^2$	ž_1		1093
2	80 308.623   70 308.755   20 208.002	69.4470 - 393.4682 140.9222 - 464.8078	$3d^5 - 3d^4(b^3F)4p$ $3d^5 - 3d^4(b^3F)4p$	$c^2 D - {}^4 G^\circ$	\$ - ⁷ / ₂		1093
2: 1: 3: 5:	80 308.623   70 308.755   20 308.993	69.4470 - 393.4682 140.9222 - 464.8078 69.4470 - 393.0720	3d ⁵ - 3d ⁴ (b ³ F)4p 3d ⁵ - 3d ⁴ (a ⁵ D)4p 3d ⁵ - 3d ⁴ (a ⁵ D)4p	$c^2D - {}^4G^\circ$ $a^4F - {}^4F^\circ$	5-72 5-72 5-72 5-72 5-72 5-72 5-72 5-72		1093 1093
2: 11 3: 5: 1	80 308.623   70 308.755   20 308.993   10 309.252	69.4470 - 393.4682 140.9222 - 464.8078 69.4470 - 393.0720 69.4470 - 392.8081	$3d^{5} - 3d^{4}(a^{5}D)4p$ $3d^{5} - 3d^{4}(a^{5}D)4p$ $3d^{5} - 3d^{4}(a^{5}D)4p$ $3d^{5} - 3d^{4}(a^{5}D)4p$	$c^{2}D - {}^{4}G^{\circ}$ $a^{4}F - {}^{4}F^{\circ}$ $a^{4}F - {}^{4}F^{\circ}$			1093 1093 1093

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**NI VI** — Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	220	309.581	141.0068 - 464.0278	3d ⁵ – 3d ⁴ (b ³ F)4p	$c^2D - {}^4G^\circ$	$\frac{3}{2} - \frac{5}{2}$		1093
	110	310.316	96.4612 - 418.7134	$3d^{5} - 3d^{4}(a^{3}P)4p$	$b^2D - {}^4P^\circ$	$\frac{3}{2} - \frac{3}{2}$		1093
	120	310.383	107.8483 - 430.0333	$3d^{5} - 3d^{4}(a^{3}G)4p$	$b^2G - {}^4G^\circ$	<u><u><u></u><u></u><u><u></u><u></u><u><u></u><u></u><u></u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u></u></u></u>		1093
	120	310.441	79.6083 - 401.7209	$3d^{5} - 3d^{4}(a^{5}D)4p$	$b^2 F - {}^4 D^\circ$	1 - 5		1093
	50	310.948	107 8870 - 429 4863	$3d^{5} - 3d^{4}(a^{3}G)4p$	$h^2G - {}^4G^\circ$	7 - 9		1093
	170	311 023	140.9222 - 462.4431	3d ⁵ - 3d ⁴ (h ³ P)4n	$c^2 D = {}^4 D^2$	<u><u><u></u></u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u>		1093
	170	511.025	140.7222 - 402.4451	3u - 3u (0 r)+p	CD-D	2 - 2		1075
	580	311.202	68.5512 - 389.8832	3d ⁵ − 3d ⁴ (a ⁵ D)4p	a⁴F – °D°	$\frac{9}{2} - \frac{9}{2}$		1093
	300	311.542	65.1735 - 386.1573	3d ⁵ − 3d ⁴ (a ⁵ D)4p	$a^2D - {}^4P^\circ$	$\frac{3}{2} - \frac{3}{2}$		1093
	100	312.173	107.8870 - 428.2214	3d⁵ – 3d⁴(a³F)4p	$b^2G - {}^2F^\circ$	$\frac{7}{2} - \frac{7}{2}$		1093
	170	312.302	107.8483 - 428.0515	3d ⁵ – 3d⁴(a ³ G)4p	b²G – ²H°	$\frac{9}{2} - \frac{9}{2}$		1093
	120	312.335	107.8870 - 428.0515	$3d^{5} - 3d^{4}(a^{3}G)4p$	$b^2G - {}^2H^\circ$	$\frac{7}{2} - \frac{9}{2}$		1093
	510	312.390	107.8870 - 427.9956	3d ⁵ – 3d ⁴ (a ³ F)4p	$b^2G - {}^2G^\circ$	$\frac{7}{2} - \frac{9}{2}$		1093
			107.0402 427.7027			9 11		1002
	2/0	312.645	107.8483 - 427.7027	3d" – 3d"(a"G)4p	<b>b</b> - <b>GH</b>	2 - 2		1093
	170	313.858	75.4417 - 394.0610	3d ³ – 3d ⁴ (a ³ D)4p	$a^2G - F^*$	$\frac{1}{2} - \frac{1}{2}$		1093
	310	314.743	107.8483 - 425.5676	3d [°] – 3d [•] (a [°] H)4p	b ² G – ² H°	$\frac{1}{2} - \frac{11}{2}$		1093
	350	315.944	107.8483 - 424.3637	3d° - 3d*(a°G)4p	b ² G - ⁴ H°	$\frac{3}{2} - \frac{11}{2}$		1093
	130	316.916	68.5512 - 384.0965	3d ⁵ – 3d ⁴ (a ⁵ D)4p	a⁴F – °P°	$\frac{9}{2} - \frac{7}{2}$		1093
	660	317.291	68.8017 - 383.9602	$3d^{5} - 3d^{4}(a^{5}D)4p$	a⁴F - [°] F°	$\frac{7}{2} - \frac{9}{2}$		1093
	150	317 631	129 9516 - 444 7842	3d ^s – 3d⁴(a¹D)4p	$a^2P - ^2D^\circ$	3_3		1093
	420	318 260	68 5512 - 382 7589	$3d^{5} - 3d^{4}(a^{5}D)4p$	$a^4F - {}^6F^{\circ}$	<u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u>		1093
	100	310.200	1299516 - 4426199	$3d^{5} - 3d^{4}(a^{3}D)4p$	$a^2 P - {}^2 D^\circ$	$\frac{2}{3}$ $\frac{2}{3}$		1093
	210	319.828	129.9510 - 442.0199	$3d^{5} - 3d^{4}(a^{3}D)4n$	$a^2 P + D^2$		1	1093
	210	319.899	130.0259 - 442.0199	$3d^2 - 3d(a^2D)4p$	$a^{-}P - D$	$\frac{1}{2} - \frac{1}{2}$		1093
	190	321.897	130.0259 - 440.6893	$3d^{2} - 3d^{2}(a^{2}D)4p$	$\mathbf{a}^{T}\mathbf{P} - \mathbf{P}^{T}$	2 - 2		1093
	180	322.356	129.9516 - 440.1686	3d ³ - 3d ² (a'S)4p	a P – P	2 - 2		1093
	160	322.434	130.0259 - 440.1686	3d ⁵ – 3d⁴(a¹S)4p	$a^2P - {}^2P^\circ$	$\frac{1}{2} - \frac{3}{2}$		1093
		322.60	0.0 - 309.9771	3d ⁵ – 3d⁴(a ⁵ D)4s	ga°S - ⁴ D	$\frac{5}{2} - \frac{7}{2}$	F,P	375,1093
	170	322.753	107.8870 - 417.7181	3d ⁵ – 3d⁴(a³H)4p	b ² G – ² G°	$\frac{1}{2} - \frac{7}{2}$		1093
	180	323.298	107.8483 - 417.1641	$3d^{5} - 3d^{4}(a^{3}H)4p$	b ² G – ⁴ I°	3 - 4		1093
		323.57	0.0 - 309.0549	$3d^{5} - 3d^{4}(a^{5}D)4s$	$ga^{b}S - {}^{4}D$	3-5	E.P	375,1093
		324.33	0.0 - 308.3238	3d ^s – 3d ⁴ (a ^s D)4s	ga°S – ⁴D	$\frac{5}{2} - \frac{3}{2}$	F,P	375,1093
	450	221 670						1003
	450	331.570						1093
	590	332.787						1093
		335.42	0.0 - 298.1305	3d [°] – 3d ⁺ (a [°] D)4s	ga°S – °D	2-2	F,P	375,1093
		336.30	0.0 - 297.3505	3d³ – 3d⁴(a³D)4s	ga°S – °D	2-1	F,P	375,1093
		337.04	0.0 – 296.6967	3d° – 3d⁴(a°D)4s	ga°S - °D	$\frac{2}{2} - \frac{2}{2}$	F,P	375,1093
		337.61	0.0 - 296.1981	$3d^{5} - 3d^{4}(a^{5}D)4s$	ga°S – °D	$\frac{2}{2} - \frac{1}{2}$	F,P	375,1093
	170	896.886	309.0549 - 420.5532	3d⁴(a⁵D)4s – 3d⁴(a³F)4p	4D - 4F°	5 - 7		1093
	370	902.047	309.9771 - 420.8357	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{3}F)4p$	⁴ D - ⁴ F°			1093
	130	905.889	308.3238 - 418.7134	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{3}P)4p$	${}^{4}D - {}^{4}P^{\circ}$	$\frac{3}{3} - \frac{3}{3}$		1093
	50	906.380	309.9771 - 420.3089	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{3}P)4p$	${}^{4}D - {}^{4}P^{\circ}$	1 - š		1093
	40	948.324	339 3358 - 444 7842	$3d^{4}(a^{3}F)4s = 3d^{4}(a^{1}D)4p$	$^{2}F - ^{2}D^{\circ}$	Ž_Š		1093
	20	965.287	347.4452 - 451.0413	$3d^{4}(a^{1}G)4s - 3d^{4}(a^{1}F)4p$	${}^{2}G - {}^{2}F^{\circ}$	1 - 5	ĺ	1093
					10.10			
	20	970.672	343.8420 - 446.8638	3d*(a'G)4s - 3d*(a'D)4p	-GF°	2 - 2		1093
	50	979.761	339.3358 - 441.4012	3d*(a'F)4s - 3d*(a'D)4p	${}^{2}\mathbf{F} - {}^{2}\mathbf{D}^{\circ}$	$\frac{1}{2} - \frac{2}{2}$		1093
	20	981.539	339.3358 - 441.2161	3d ⁺ (a'F)4s - 3d ⁺ (a'D)4p	${}^{2}F - {}^{2}F^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		1093
	390	994.120	382.8891 - 483.4809	3d ⁴ (b ³ F)4s - 3d ⁴ (b ³ F)4p	${}^{2}F - {}^{2}D^{\circ}$	2 - 2		1093
	360	996.349	382.6771 - 483.0434	$3d^{4}(b^{3}F)4s - 3d^{4}(b^{3}F)4p$	${}^{2}F - {}^{2}D^{\circ}$	$\frac{1}{2} - \frac{5}{2}$		1093
	280	1002.559	366.2898 - 466.0342	$3d^{4}(a^{1}F)4s - 3d^{4}(b^{3}P)4p$	${}^{2}\mathbf{F} - {}^{2}\mathbf{D}^{\circ}$	$\frac{5}{2} - \frac{3}{2}$		1093
	430	1004,309	332.3436 - 431.9126	$3d^{4}(a^{3}F)4s = 3d^{4}(a^{3}D)4n$	⁴ F - ⁴ D°	2 _ 2		1093
	580	1005.497	330.5805 - 430.0333	$3d^{4}(a^{3}H)4s = 3d^{4}(a^{3}G)4r$	4H - 4G*	13 _ 11		1093
	420	1006 593	330 1410 - 420 4863	$3d^{4}(a^{3}H)Ae^{-2d^{4}(a^{3}G)Am}$	44 +0*	1 2 2		1093
	320	1007 512	266 2000 466 5627	3d(a H) + 8 - 3d(a U) + p		$\frac{2}{7} - \frac{2}{5}$		1093
	320	1007.515	300.2776 - 403.3327	3u (a r)4s - 30 (0 r)4p		1		1093
	700	1008.005	333.9700 - 433.1102	30 (a C)4s - 30 (a D)4p	G-F	2-2		1093
	/80	1008.944	329.7542 - 428.8005	30'(a'H)4s - 30'(a'G)4p	"H - "G"	2 - 2		1093

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Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	560	1009.797	336.4304 - 435.4594	3d ⁴ (a ³ G)4s - 3d ⁴ (a ³ D)4p	⁴G - ⁴F°	$\frac{11}{2} - \frac{9}{2}$		1093
	560	1009.992	329.4862 - 428.4965	3d4(a3H)4s - 3d4(a3G)4p	⁴H – ⁴G°	$\frac{1}{2} - \frac{5}{2}$		1093
	20	1011.667	332.1754 - 431.0203	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}D)4p$	⁴ F – ⁴ P°	$\frac{7}{2} - \frac{5}{2}$		1093
	240	1011.978	335,3845 - 434,2009	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}D)4p$	⁴ G – ⁴ F°	5-3		1093
	410	1012 437	336.3449 - 435.1162	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}D)4p$	⁴G - ⁴F°	$\frac{2}{7} - \frac{7}{7}$		1093
	260	1013.680	335.9760 - 434.6260	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}D)4p$	⁴ G – ⁴ F°	$\frac{1}{2} - \frac{5}{2}$		1093
		1016 35/	274 8420 472 2024	244(530)40 244(535)40	4D 4D°	5 5		1003
	60	1015.756	3/4.8439 - 4/3.2924	3d (b [*] P)4s - 3d (b [*] P)4p	P - D	$\frac{1}{2} - \frac{1}{2}$		1093
	20	1015.877	339.4824 - 437.9197	$3d^{2}(a^{2}F)4s = 3d^{2}(a^{2}G)4p$	F - G	$\frac{2}{7}$ $\frac{-2}{9}$		1093
	170	1021.804	343.0520 - 440.9179	$3d^{*}(a^{*}G)4s - 3d^{*}(a^{*}I)4p$	$G - H^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		1093
	600	1021.923	330.1410 - 427.9956	$3d^{2}(a^{2}H)4s - 3d^{2}(a^{2}F)4p$	H - G	2 - 2		1093
	140	1022.270	329.7542 - 427.5750	3d'(a'H)4s - 3d'(a'F)4p	H - G	3 - 2		1093
	200	1023.645	332.3436 - 430.0333	3d*(a°F)4s - 3d*(a°G)4p	"F - "G"	2 - 2		1093
	630	1024.030	374.8439 - 472.4973	3d ⁴ (b ³ P)4s - 3d ⁴ (b ³ F)4p	$^{4}P - ^{4}D^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		1093
	130	1026.968	343.8426 - 441.2161	3d⁴(a³G)4s - 3d⁴(a³D)4p	$^{2}G - ^{2}F^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		1093
	560	1029.628	330.5805 - 427.7027	3d ⁴ (a ³ H)4s - 3d ⁴ (a ³ G)4p	⁴ H – ² H°	$\frac{13}{2} - \frac{11}{2}$		1093
	200	1030.722	337.9939 - 435.0115	3d4(a3H)4s - 3d4(a1G)4p	² H – ² H°	<u><u><u></u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		1093
	500	1031.470	376.3437 - 473.2924	3d ⁴ (b ³ P)4s - 3d ⁴ (b ³ F)4p	${}^{4}\mathbf{P} - {}^{4}\mathbf{D}^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		1093
	770	1032.799	375.6730 - 472.4973	3d ⁴ (b ³ F)4s - 3d ⁴ (b ³ F)4p	⁴F – ⁴D°	$\frac{9}{2} - \frac{7}{2}$		1093
	320	1032 908	332 0516 - 428 8665	3d⁴(a³F)4s - 3d⁴(a³G)4n	4F - 4G°	\$_2		1093
	360	1036 166	337.0077 - 433.5173	$3d^{4}(a^{3}H)4s = 3d^{4}(a^{3}G)4n$	² H - ² G ^o	<u><u><u></u></u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u>		1093
	500	1036 656	332.0318 - 428.4965	$3d^{4}(a^{3}F)4s = 3d^{4}(a^{3}G)4p$	⁴ F - ⁴ G°	3_5		1093
	120	1038 830	374 8439 471 1068	$3d^4(h^3P)4s = 3d^4(h^3P)4p$	${}^{4}P - {}^{4}S^{\circ}$	1 1		1093
	120	1030.630	3/4.0437 - 4/1.1000	$3d^{4}(a^{3}G)4c = 3d^{4}(a^{1}I)4p$	${}^{2}G - {}^{2}H^{\circ}$	2 <u>1</u>		1093
	260	1039.337	297.3505 - 393.4682	$3d^4(a^5D)4s - 3d^4(a^5D)4p$	⁶ D – ⁴ F [°]	$\frac{1}{2} - \frac{1}{2}$		1093
					4D 4D1	99		1001
	650	1042.418	298.1305 - 394.0610	$3d^{-}(a^{-}D)4s - 3d^{-}(a^{-}D)4p$	D - F	$\frac{1}{2} - \frac{1}{2}$		1093
	280	1042.493	337.0077 - 432.9320	$3d^{2}(a^{2}H)4s - 3d^{2}(a^{2}I)4p$		$\frac{1}{2} - \frac{1}{2}$		1093
	680	1043.057	330.5805 - 426.4519	3d*(a*H)4s - 3d*(a*G)4p	H - H	$\frac{1}{2} - \frac{1}{2}$		1093
	20	1043.596	332.1754 - 427.9956	$3d^{-}(a^{-}F)4s - 3d^{-}(a^{-}F)4p$	F - G	$\frac{5}{1}$		1093
	220	1047.928	330.1410 - 425.5676	$3d^{-}(a^{-}H)4s - 3d^{-}(a^{-}H)4p$	H - H	$\frac{1}{2} - \frac{1}{2}$		1093
	590	1048.468	337.9939 - 433.3712	3d*(a*H)4s - 3d*(a*G)4p	-HG*	2 - 2		1093
	170	1048.664	332.3436 - 427.7027	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}G)4p$	${}^{4}\mathbf{F} - {}^{2}\mathbf{H}^{\circ}$	⁹ / ₂ − ¹¹ / ₂		1093
		1052.2	45.8842 - 140.9222	3d ⁵ - 3d ⁵	$a^4P - c^2D$	3-3	F,P	375,1093
		1053.7	46.1044 - 141.0068	3d ⁵ - 3d ⁵	$a^4P - c^2D$	2 - 2	F,P	375,1093
	290	1054.105	343.0520 - 437.9197	3d ⁴ (a ³ G)4s - 3d ⁴ (a ¹ G)4p	$^{2}G - ^{2}G^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		1093
		1054.7	46.1044 - 140.9222	3d ^s – 3d ^s	$a^4P - c^2D$	3-2	F,P	375,1093
	270	1054.879	343.8426 - 438.6394	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{1}G)4p$	² G – ² G°	$\frac{9}{2} - \frac{9}{2}$		1093
	510	1055.037	329.7542 - 424.5370	$3d^{4}(a^{3}H)4s - 3d^{4}(a^{3}G)4p$	⁴ H – ⁴ H°	$\frac{9}{2} - \frac{9}{2}$		1093
	250	1055.260	376.3437 - 471.1068	$3d^{4}(b^{3}P)4s - 3d^{4}(b^{3}P)4p$	$^{4}P - ^{4}S^{\circ}$	$\frac{3}{5} - \frac{1}{5}$		1093
		1056.2	46.3248 - 141.0068	$3d^{5} - 3d^{5}$	$a^4P - c^2D$	$\frac{1}{2} - \frac{3}{2}$	F,P	375,1093
	20	1056.820	337.9939 - 432.6166	$3d^{4}(a^{3}H)4s - 3d^{4}(a^{1}I)4p$	${}^{2}H - {}^{2}I^{\circ}$	<u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u></u>		1093
		1057.1	46.3248 - 140.9222	$3d^{5} - 3d^{5}$	$a^4P - c^2D$	1 - 5	F,P	375,1093
	660	1061.319	330.1410 - 424.3637	3d ⁴ (a ³ H)4s - 3d ⁴ (a ³ G)4p	⁴ H − ⁴ H°	$\frac{11}{2} - \frac{11}{2}$		1093
	310	1063 435	330 3358 433 3712	$3d^{4}(a^{3}F)4s = 3d^{4}(a^{3}G)4n$	$^{2}\mathbf{F} = ^{2}\mathbf{G}^{\circ}$	1 2		1093
	810	1063 811	378 4377 - 477 4377	$3d^{4}(a^{3}P)4s = 3d^{4}(a^{3}F)4n$	⁴ P - ⁴ D°	1_3		1093
	20	1064 505	328,4372 - 422,4572	$3d^{4}(a^{3}P)As = 3d^{4}(a^{3}F)An$	⁴ P - ⁴ D°			1093
	720	1065 479	320.4572 - 422.3094	$3d^4(a^3H)4s = 3d^4(a^3G)4r$	⁴ H – ⁴ H°	1 1 1	1	1093
	20	1067.460	329.4002 - 423.3414	$3d^{4}(h^{1}G)4e = 3d^{4}(h^{3}F)4n$	$^{2}G - ^{2}D^{\circ}$	1 2 5		1093
	180	1068.132	330.1410 - 423.7633	3d ⁴ (a ³ H)4s - 3d ⁴ (a ³ G)4p	'H - ⁺F°	$\frac{11}{2} - \frac{9}{2}$		1093
						р п		1003
	760	1068.350	336.4304 - 430.0333	3d"(a"G)4s - 3d"(a"G)4p	G-G	2 - 2		1093
	410	1068.606	329.4862 - 423.0652	3d'(a'H)4s - 3d'(a'H)4p	H - H	$\frac{1}{2} - \frac{1}{2}$		1093
	730	1068.796	296.1981 - 389.7604	3d*(a*D)4s - 3d*(a*D)4p	"D - "P"	2-2		1093
	20	1069.927	339.3358 - 432.8001	3d'(a'F)4s – 3d'(a'G)4p	F - F	2 - 2		1093
	280	1070.238	307.8439 - 401.2809	3d*(a'D)4s - 3d*(a'D)4p	"D - "D"	2 - 2		1093
	350	1070.695	308.3238 - 401.7209	3d*(a°D)4s – 3d*(a°D)4p	י <b>ט</b> י - טי	2 - 2		1093
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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	670	1071.450	295.8827 - 389.2140	3d⁴(a ⁵ D)4s - 3d⁴(a ⁵ D)4p	⁶ D – ⁶ D°	$\frac{1}{2} - \frac{3}{2}$		1093
	310	1071.676	329.7542 - 423.0652	$3d^{4}(a^{3}H)4s - 3d^{4}(a^{3}H)4p$	${}^{4}H - {}^{2}H^{\circ}$	2-2		1093
	780	1073.638	336,3449 - 429,4863	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}G)4p$	⁴ G – ⁴ G°	$\frac{5}{2} - \frac{5}{2}$		1093
	670	1073.924	309.0549 - 402.1713	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	⁴ D – ⁴ D°	$\frac{5}{2} - \frac{7}{2}$		1093
	700	1073.975	335,3845 - 428,4965	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}G)4p$	⁴ G - ⁴ G°	5-5		1093
	720	1074.535	296 6967 - 389 7604	$3d^4(a^5D)4s - 3d^4(a^5D)4p$	°D – ⁴P°	\$ - 5		1093
	,20	10/11050	270.0701 307.17004					10/0
	350	1074.856	295.8827 - 388.9186	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	⁶ D - ⁶ D ⁶	$\frac{1}{2} - \frac{1}{2}$		1093
	790	1075.781	308.3238 - 401.2809	$3d^{2}(a^{2}D)4s - 3d^{2}(a^{2}D)4p$	·D - ·D·	$\frac{5}{2} - \frac{5}{2}$		1093
	370	1076.344	358.7166 - 451.6229	$3d^{-}(a'D)4s - 3d^{-}(a'D)4p$	$^{2}D - ^{2}P^{2}$	2 - 2		1093
	780	1076.542	335.9760 - 428.8665	3d*(a*G)4s - 3d*(a*G)4p	*G - *G*	$\frac{1}{2} - \frac{1}{2}$		1093
	120	1077.412	358.8279 - 451.6420	3d*(a'D)4s – 3d*(a'D)4p	$^{2}D - ^{2}P^{\circ}$	2 - 2		1093
	70	1077.635	358.8279 - 451.6229	3d ⁴ (a'D)4s - 3d ⁴ (a'D)4p	$^{2}D - ^{2}P^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		1093
	620	1078.035	347.2785 - 440.0392	3d⁴(a'G)4s - 3d⁴(a'I)4p	² G – ² H°	$\frac{9}{2} - \frac{11}{2}$		1093
	680	1078.509	296.1981 - 388.9186	3d4(a5D)4s - 3d4(a5D)4p	⁶ D ~ ⁶ D°	$\frac{3}{2} - \frac{1}{2}$		1093
	800	1079.144	309.0549 - 401.7209	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	${}^{4}D - {}^{4}D^{\circ}$	3 - 3		1093
	690	1079.472	308.3238 - 400.9621	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	⁴ D - ⁴ D°	3 - 1		1093
	180	1080.255	330 1410 - 422 7118	$3d^{4}(a^{3}H)4s = 3d^{4}(a^{3}H)4p$	⁴ H - ² I°	μ_μ		1093
	820	1080.537	296.6967 - 389.2434	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	°D - °D°	$\frac{5}{2} - \frac{7}{2}$		1093
					65 650	7 9		1000
	810	1080.694	297.3505 - 389.8832	$3d^{*}(a^{*}D)4s - 3d^{*}(a^{*}D)4p$	°D – °D	2 - 2		1093
	750	1080.875	296.6967 – 389.2140	3d*(a*D)4s – 3d*(a*D)4p	°D – °D°	2 - 2		1093
	650	1081.320	366.2898 - 458.7722	3d*(a'F)4s – 3d*(a'F)4p	$^{2}\mathbf{F} - ^{2}\mathbf{D}^{\circ}$	$\frac{2}{2} - \frac{2}{2}$		1093
	680	1082.141	297.3505 - 389.7604	3d ⁴ (a ⁵ D)4s - 3d ⁴ (a ⁵ D)4p	°D – ⁴P°	$\frac{1}{2} - \frac{2}{2}$		1093
	430	1083.487	332.0516 - 424.3461	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}G)4p$	<b>'F</b> − <b>'F</b> °	$\frac{2}{2} - \frac{7}{2}$		1093
	570	1084.296	309.0549 - 401.2809	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	⁴ D – ⁴ D°	$\frac{2}{2} - \frac{3}{2}$		1093
	820	1084.672	309.9771 - 402.1713	3d ⁴ (a ⁵ D)4s - 3d ⁴ (a ⁵ D)4p	⁴ D - ⁴ D°	$\frac{7}{2} - \frac{7}{2}$		1093
	590	1084.946	332.1754 - 424.3461	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}G)4p$	⁴ F – ⁴ F°	$\frac{7}{2} - \frac{7}{2}$		1093
	790	1085.226	347.8924 - 440.0392	$3d^{4}(a^{1}I)4s - 3d^{4}(a^{1}I)4p$	$^{2}I - ^{2}H^{\circ}$	मिं – में		1093
	130	1086.069	347.9639 - 440.0392	$3d^{4}(a^{1}I)4s - 3d^{4}(a^{1}I)4p$	${}^{2}I - {}^{2}H^{\circ}$	ļ ų́ _ ų́		1093
	540	1086.489	337,9939 - 430,0333	3d ⁴ (a ³ H)4s - 3d ⁴ (a ³ G)4p	² H – ⁴G°	<u> </u>		1093
	40	1086.727	335.9760 - 427.9956	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}F)4p$	⁴ G – ² G°	$\frac{7}{2} - \frac{9}{2}$		1093
	410	1096 021	222 2426 424 2461	244(-35)4-244(-30)4-	4E 4E°	9 7		1002
	100	1080.931	332.3430 - 424.3401	3d(a r) + s = 3d(a G) + p	F - F	2 - 2		1093
	190	1087.457	335.3845 - 427.3422	$3d^{2}(a^{2}G)4s - 3d^{2}(a^{2}P)4p$	G - D	$\frac{1}{2} - \frac{1}{2}$		1093
	810	1088.223	297.3505 - 389.2434	$3d^{-}(a^{-}D)4s - 3d^{-}(a^{-}D)4p$	$^{\circ}D - ^{\circ}D^{\circ}$	2 - 2		1093
	830	1089.885	298.1305 ~ 389.8832	$3d^{-}(a^{-}D)4s - 3d^{-}(a^{-}D)4p$	$^{\circ}D - ^{\circ}D^{\circ}$	2 - 2		1093
	550	1089.992	309.9771 - 401.7209	$3d^{(a'D)4s} - 3d^{(a'D)4p}$	$D - D^{2}$	$\hat{2} - \hat{2}$		1093
	20	1090.445	336.3449 - 428.0515	$3d^{-}(a^{-}G)4s - 3d^{-}(a^{-}G)4p$	'G - 'H'	$\frac{1}{2} - \frac{1}{2}$		1093
	810	1091.097	296.1981 - 387.8499	3d ⁴ (a ⁵ D)4s - 3d ⁴ (a ⁵ D)4p	°D – °D°	$\frac{3}{2} - \frac{5}{2}$		1093
	200	1091.509	332.0318 - 423.6468	3d ⁴ (a ³ F)4s - 3d ⁴ (a ³ P)4p	${}^{4}\mathbf{F} - {}^{2}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{1}{2}$		1093
	20	1091.651	330.0016 - 421.6072	$3d^{4}(a^{3}P)4s - 3d^{4}(a^{3}F)4p$	$^{4}P - ^{2}D^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		1093
	70	1091.745	335.9760 - 427.5750	3d ⁴ (a ³ G)4s - 3d ⁴ (a ³ F)4p	⁴ G – ² G°	$\frac{7}{2} - \frac{7}{2}$		1093
	350	1091.851	332.1754 - 423.7633	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}G)4p$	${}^{4}\mathbf{F} - {}^{4}\mathbf{F}^{\circ}$	$\frac{7}{2} - \frac{9}{2}$		1093
	810	1093.380	343.9996 - 435.4594	$3d^{4}(a^{3}D)4s - 3d^{4}(a^{3}D)4p$	⁴ D − ⁴ F°	$\frac{7}{2} - \frac{9}{2}$		1093
	190	1093.853	332.3436 - 423.7633	3d ⁴ (a ³ F)4s - 3d ⁴ (a ³ G)4p	⁴ F – ⁴ F°	$\frac{9}{1} - \frac{9}{1}$		1093
	780	1094,560	347.2785 - 438.6394	$3d^{4}(a^{1}G)4s - 3d^{4}(a^{1}G)4n$	$^{2}G - ^{2}G^{\circ}$	9 9		1093
	380	1095 092	351 3040 - 442 6199	$3d^{4}(a^{3}D)4s = 3d^{4}(a^{3}D)4n$	² ² – ²	3 3		1093
	510	1095 271	332 3436 - 423 6458	$3d^{4}(a^{3}F)A_{5} = 3d^{4}(a^{3}G)A_{5}$	4F - 2F°	2 2		1093
	700	1095.631	336 4304 - 427 7027	$3d^{4}(a^{3}G)Aa = 3d^{4}(a^{3}G)Aa$	4G 240			1093
	600	1096.875	343.8426 - 435.0115	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{1}G)4p$	$^{2}G - ^{2}H^{\circ}$	$\frac{2}{9} - \frac{1}{1}$		1093
		1005 55			(D) (D)			
	630	1097.055	296.6967 - 387.8499	3d [*] (a [*] D)4s - 3d [*] (a [*] D)4p	"D - "D"	$\frac{5}{2} - \frac{2}{2}$		1093
	660	1097.539	298.1305 - 389.2434	3d*(a'D)4s - 3d*(a'D)4p	°D ~ °D°	$\frac{2}{2} - \frac{1}{2}$		1093
	780	1097.931	375.6730 - 466.7543	3d*(b'F)4s - 3d*(b'F)4p	*F - *G*	$\frac{2}{2} - \frac{11}{2}$		1093
	790	1099.960	344.2035 - 435.1162	3d ⁺ (a ³ D)4s - 3d ⁴ (a ³ D)4p	⁴ D - ⁴ F°	$\frac{2}{2} - \frac{7}{2}$		1093
	300	1100.235	389.2996 - 480.1893	3d ⁴ (b ¹ G)4s - 3d ⁴ (b ¹ G)4p	$^{2}G - ^{2}F^{\circ}$	$\frac{2}{2} - \frac{2}{2}$		1093
	230	1100.991	389.3625 - 480.1893	$3d^4(b^1G)4s - 3d^4(b^1G)4p$	$^{2}G - ^{2}F^{\circ}$	$\frac{1}{2} - \frac{7}{2}$		1093
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Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	80	1101.585	375.8708 - 466.6491	3d ⁴ (b ³ F)4s - 3d ⁴ (b ³ F)4p	${}^{4}\mathbf{F} - {}^{2}\mathbf{F}^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		1093
	470	1102.262	375.9271 - 466.6491	3d ⁴ (b ³ F)4s – 3d ⁴ (b ³ F)4p	${}^{4}\mathbf{F} - {}^{2}\mathbf{F}^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		1093
		1102.8	50.3310 - 141.0068	3d ⁵ – 3d ⁵	$a^4D - c^2D$	$\frac{7}{2} - \frac{3}{2}$	F,P	375,1093
	650	1103.249	347.2785 - 437.9197	3d ⁴ (a ¹ G)4s - 3d ⁴ (a ¹ G)4p	${}^{2}G - {}^{2}G^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		1093
		1103.8	50.3310 - 140.9222	3d ⁵ – 3d ⁵	$a^4D - c^2D$	$\frac{7}{2} - \frac{5}{2}$	F,P	375,1093
		1103.9	50.3310 - 140.9222	3d ⁵ - 3d ⁵	$a^4D - c^2D$	$\frac{7}{2} - \frac{5}{2}$	F,P	375,1093
-	140	1104.150	337.0077 - 427.5750	3d ⁴ (a ³ H)4s - 3d ⁴ (a ³ F)4p	${}^{2}H - {}^{2}G^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		1093
	430	1104.773	366.2998 - 456.8156	3d4(a1F)4s - 3d4(a1F)4p	$^{2}\mathbf{F} - ^{2}\mathbf{D}^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		1093
	170	1104.977	297.3505 - 387.8499	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	° <b>D</b> – ° <b>D</b> °	$\frac{7}{2} - \frac{5}{2}$		1093
	460	1105.193	351.3040 - 441.7857	3d ⁴ (a ³ D)4s - 3d ⁴ (a ³ D)4p	${}^{2}D - {}^{2}F^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		1093
	490	1105.284	347.4452 - 437.9197	3d ⁴ (a'G)4s – 3d ⁴ (a'G)4p	${}^{2}G - {}^{2}G^{\circ}$	$\frac{7}{2} - \frac{7}{2}$		1093
	770	1105.393	343.0520 - 433.5173	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}G)4p$	² G – ² G°	$\frac{7}{2} - \frac{7}{2}$		1093
	440	1106.366	332.0516 - 422.4372	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}F)4p$	⁴ F – ⁴ D°	$\frac{5}{2} - \frac{3}{2}$		1093
	230	1106.479	329.4862 - 419.8633	3d ⁴ (a ³ H)4s - 3d ⁴ (a ³ H)4p	⁴ H – ⁴ G°	$\frac{7}{2} - \frac{7}{2}$		1093
	540	1106.948	332.0318 - 422.3694	3d⁴(a³F)4s - 3d⁴(a³F)4p	⁴ F - ⁴ D°	$\frac{1}{2} - \frac{1}{2}$		1093
1	330	1107.102	329.7542 - 420.0800	3d ⁴ (a ³ H)4s - 3d ⁴ (a ³ H)4p	⁺H – ⁺G°	$\frac{9}{2} - \frac{9}{2}$		1093
	200	1107.319	330.0016 - 420.3089	$3d^{4}(a^{3}P)4s - 3d^{4}(a^{3}P)4p$	⁴ P – ⁴ P°	$\frac{3}{2} - \frac{5}{2}$		1093
		1108.3	50.7805 - 141.0068	$3d^{5} - 3d^{5}$	$a^4D - c^2D$	$\frac{3}{2} - \frac{3}{2}$	F,P	375,1093
		1108.3	50.7776 - 141.0068	3d ⁵ – 3d ⁵	$a^4D - c^2D$	$\frac{5}{2} - \frac{3}{2}$	F,P	375,1093
	710	1108.863	351.0330 - 441.2161	$3d^{4}(a^{3}D)4s - 3d^{4}(a^{3}D)4p$	${}^{2}D - {}^{2}F^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		1093
	730	1108.909	344.4474 - 434.6260	$3d^{4}(a^{3}D)4s - 3d^{4}(a^{3}D)4p$	⁴ D – ⁴ F°	$\frac{3}{2} - \frac{5}{2}$		1093
		1109.3	50.7776 - 140.9222	$3d^{5} - 3d^{5}$	$a^4D - c^2D$	5 - 5	F,P	375,1093
	880	1109.410	375.9271 - 466.0652	3d ⁴ (b ³ F)4s - 3d ⁴ (b ³ F)4p	⁴ F – ⁴ G°	$\frac{7}{2} - \frac{9}{2}$		1093
	820	1109.760	329.7542 - 419.8633	$3d^{4}(a^{3}H)4s - 3d^{4}(a^{3}H)4p$	⁴H - ⁴G°	$\frac{9}{2} - \frac{7}{2}$		1093
	900	1110.503						1093
	870	1110.842	336.4304 - 426.4519	3d ⁴ (a ³ G)4s - 3d ⁴ (a ³ G)4p	⁴ G – ⁴ H°	11 - 13		1093
	810	1111.557	332.3448 - 422.3066	$3d^{4}(a^{3}P)4s - 3d^{4}(a^{3}P)4p$	⁴ P – ⁴ D°	$\frac{5}{2} - \frac{7}{2}$		1093
	790	1111.854	330.1410 - 420.0800	$3d^{4}(a^{3}H)4s - 3d^{4}(a^{3}H)4p$	⁴H – ⁴G°	μ <u>-</u> 2		1093
	780	1112.305	329.4862 - 419.3905	$3d^{4}(a^{1}H)4s - 3d^{4}(a^{1}H)4p$	⁴H - ⁴G°	$\frac{7}{2} - \frac{5}{2}$		1093
	540	1114.236	389.2996 - 479.0463	3d ⁴ (b ¹ G)4s – 3d ⁴ (b ¹ G)4p	² G – ² G°	$\frac{9}{2} - \frac{9}{2}$		1093
	580	1114.590	332.1754 - 421.8940	3d ⁴ (a ³ F)4s - 3d ⁴ (a ³ F)4p	⁴ F – ⁴ D°	$\frac{7}{2} - \frac{5}{2}$		1093
	580	1115.017	389.3625 - 479.0463	3d ⁺ (b ¹ G)4s - 3d ⁺ (b ¹ G)4p	² G – ² G°	$\frac{7}{2} - \frac{9}{2}$		1093
	840	1116.192	344.6100 - 434.2009	3d ⁴ (a ³ D)4s - 3d ⁴ (a ³ D)4p	⁴ D - ⁴ F°	$\frac{1}{2} - \frac{3}{2}$		1093
	790	1116.235	366.2998 - 455.8876	$3d^{4}(a^{1}F)4s - 3d^{4}(a^{1}F)4p$	${}^{2}F - {}^{2}G^{\circ}$	$\frac{7}{2} - \frac{9}{2}$		1093
	510	1116.368	332.0318 - 421.6072	3d4(a3F)4s - 3d4(a3F)4p	${}^{4}F - {}^{2}D^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		1093
	810	1116.962	343.8426 - 433.3712	3d4(a3G)4s - 3d4(a3G)4p	$^{2}G - ^{2}G^{\circ}$	$\frac{9}{2} - \frac{9}{2}$		1093
	20	1117.445	344.4474 - 433.9369	3d⁴(a³D)4s – 3d⁴(a'S)4p	⁴ D - ² P°	$\frac{3}{2} - \frac{1}{2}$		1093
	170	1117.812	296.6967 - 386.1573	3d⁴(a⁵D)4s – 3d⁴(a⁵D)4p	° <b>D</b> − ⁴ <b>P</b> °	$\frac{5}{2} - \frac{3}{2}$		1093
	330	1118.783	339.4824 - 428.8665	3d⁴(a³F)4s – 3d⁴(a³G)4p	² F – ⁴ G°	$\frac{5}{2} - \frac{7}{2}$		1093
	700	1119.867	336.4048 - 425.7031	3d ⁴ (a ³ P)4s - 3d ⁴ (a ³ P)4p	${}^{2}P - {}^{2}D^{\circ}$	$\frac{1}{2} - \frac{3}{2}$		1093
ĺ	250	1120.165	332.0516 - 421.3243	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}F)4p$	⁴ F − ² D°	2 - 2		1093
	210	1120.334	344.2035 - 433.4625	$3d^{4}(a^{3}D)4s - 3d^{4}(a^{3}D)4p$	⁴ D – ⁴ P°	$\frac{5}{2} - \frac{3}{2}$		1093
1	780	1120.801	336.3449 - 425.5676	3d⁴(a³G)4s - 3d⁴(a³H)4p	⁴ G - ² H°	⁹ / ₂ − ¹¹ / ₂		1093
	620	1121.881	351.0330 - 440.1686	$3d^{4}(a^{3}D)4s - 3d^{4}(a^{3}S)4p$	${}^{2}D - {}^{2}P^{\circ}$	$\frac{5}{2} - \frac{3}{2}$		1093
	340	1122.689	351.0962 - 440.1686	3d ⁴ (a'S)4s - 3d ⁴ (a'S)4p	${}^{2}S - {}^{2}P^{\circ}$	$\frac{1}{2} - \frac{3}{2}$		1093
	660	1123.412	344.4474 - 433.4625	$3d^{4}(a^{3}D)4s - 3d^{4}(a^{3}D)4p$	${}^{4}D - {}^{4}P^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		1093
	890	1124.195	330.5805 - 419.5335	$3d^{4}(a^{3}H)4s - 3d^{4}(a^{3}H)4p$	⁴ H − ⁴ l°	$\frac{13}{2} - \frac{15}{2}$		1093
	660	1125.050	339.3358 - 428.2214	3d ⁴ (a ³ F)4s - 3d ⁴ (a ³ F)4p	${}^{2}\mathbf{F} - {}^{2}\mathbf{F}^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		1093
	370	1125.305	295.8827 - 384.7474	3d ⁴ (a ⁵ D)4s - 3d ⁴ (a ⁵ D)4p	°D - ⁴P°	$\frac{1}{2} - \frac{1}{2}$		1093
	520	1125.395	375.9498 - 464.8078	3d ⁴ (b ³ F)4s - 3d ⁴ (b ³ F)4p	⁴ F − ⁴ G°	$\frac{5}{2} - \frac{7}{2}$		1093
	220	1125.481	335.3845 - 424.2354	3d ⁴ (a ³ G)4s - 3d ⁴ (a ³ P)4p	${}^{4}G - {}^{2}P^{\circ}$	5-3		1093
	230	1126.917	339.4824 - 428.2214	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}F)4p$	${}^{2}F - {}^{2}F^{\circ}$	5-7		1093
	750	1127.206	339.3358 - 428.0515	3d ⁴ (a ³ F)4s - 3d ⁴ (a ³ G)4p	${}^{2}F - {}^{2}H^{\circ}$	$\frac{1}{2} - \frac{2}{3}$		1093
	80	1127.766	332.0516 - 420.7223	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}P)4p$	4F - 4S°	$\frac{5}{2} - \frac{3}{2}$		1093

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NI VI -- Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J Notes	References
	880	1127.935	347.8924 - 436.5503	$3d^{4}(a^{1}I)4s - 3d^{4}(a^{1}I)4p$	${}^{2}I - {}^{2}K^{\circ}$	13 _ 15	1093
	840	1120 173	235.9760 424.5370	$3d^{4}(a^{3}G)As = 3d^{4}(a^{3}G)An$	⁴ G - ⁴ H°	Z 9	1093
	040	1129.175	335.9700 - 424.5370	3 (a C)+s = 3 (a C)+p	11 - U	$\begin{bmatrix} 2 \\ 3 \\ 3 \end{bmatrix}$	1003
	310	1129.325	296.1981 - 384.7474	3d (a ⁻ D)4s - 3d (a ⁻ D)4p	D - P	$\frac{1}{2} - \frac{1}{2}$	1093
	310	1129.917	332.0516 - 420.5532	3d ⁴ (a ³ F)4s - 3d ⁴ (a ³ F)4p	'F – ⁺F°	5 - 5	1093
	820	1130.049	332.3436 - 420.8357	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}F)4p$	⁺F – ⁺F°	2 - 2	1093
	840	1130.477	337.9939 - 426.4519	3d ⁴ (a ³ H)4s - 3d ⁴ (a ³ G)4p	² H – ⁴ H°	$\frac{11}{2} - \frac{13}{2}$	1093
	000	1121.064	330 1410 418 5536	$3d^{4}(a^{3}H)Ac = 3d^{4}(a^{3}H)Ac$	4H 410	ц_ц	1093
	000	1131.004	530.1410 - 418.5550	3u(a 11)4s = 3u(a 11)4p	1 - 1	2 - 2 5 3	1003
	730	1131.508	332.3448 - 420.7223	3d(a'P)4s - 3d(a'P)4p	P-5	$\frac{1}{2} - \frac{1}{2}$	1093
	730	1131.508	332.1754 - 420.5532	3d ⁻ (a'F)4s - 3d ⁻ (a'F)4p	*F - *F*	$\frac{1}{2} - \frac{1}{2}$	1093
	160	1132.190	335.3845 - 423.7105	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}G)4p$	⁴G - ⁴F°	$\frac{2}{2} - \frac{2}{2}$	1093
	150	1132.550	343.9996 - 432.2957	$3d^{4}(a^{3}D)4s - 3d^{4}(a^{3}D)4p$	⁴ D – ⁴ D°	$\frac{7}{2} - \frac{5}{2}$	1093
	850	1132.759	332.3436 - 420.6234	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}F)4p$	⁴F – ⁴G°	$\frac{9}{2} - \frac{11}{2}$	1093
	660	1122 226	225.0760 424.2185	24*(03)(2)40 24*(03)(2)40	AC AF	7 5	1092
	000	1133.230	335.9760 - 424.2185	30 (a'G)4s - 30 (a'G)4p	G-F	$\frac{1}{2} - \frac{1}{2}$	1093
	280	1133.295	339.3358 - 427.5750	3d*(a'F)4s - 3d*(a'F)4p	F – G*	$\frac{1}{2} - \frac{1}{2}$	1093
	270	1133.442	330.1410 - 418.3688	3d ⁴ (a ³ H)4s - 3d ⁴ (a ³ H)4p	⁴ H – ¹ G°	$\left \frac{11}{2} - \frac{5}{2}\right $	1093
	460	1133.935					1093
	580	1134,470	358 7166 - 446 8638	$3d^{4}(a^{\dagger}D)4s - 3d^{4}(a^{\dagger}D)4p$	${}^{2}D - {}^{2}F^{\circ}$	5 - 7	1093
	360	1134.989	336.4304 - 424.5370	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}G)4p$	⁴G – ⁴H°	$\frac{11}{2} - \frac{9}{2}$	1093
						5 5	1002
	820	1135.179	344.2035 - 432.2957	$3d^{*}(a^{*}D)4s - 3d^{*}(a^{*}D)4p$	$^{1}D - ^{1}D^{2}$	2 - 2	1093
	400	1135.299	339.2601 - 427.3422	3d ⁴ (a ³ P)4s - 3d ⁴ (a ³ P)4p	-P - D°	$\frac{2}{2} - \frac{2}{2}$	1093
	800	1136.127	336.3449 - 424.3637	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}G)4p$	⁺G ⁺H°	$\frac{9}{2} - \frac{11}{2}$	1093
	270	1136.298	339.3358 - 427.3422	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}P)4p$	${}^{2}F - {}^{2}D^{\circ}$	$\frac{7}{2} - \frac{5}{2}$	1093
	660	1136 352	336 3449 - 424 3461	$3d^{4}(a^{3}G)4s = 3d^{4}(a^{3}G)4n$	$^{4}G - ^{4}F^{\circ}$	<u>9</u> 7	1093
	680	1136 820	332 3448 - 420 3089	$3d^{4}(a^{3}P)4s = 3d^{4}(a^{3}P)4n$	4D 4D°	5 5	1093
	080	1150.820	332.3448 - 420.3089	5u (a 1)+5 - 5u (a 1)+p	1 - 1	2 - 2	1075
	820	1136.922	335.3845 - 423.3414	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}G)4p$	⁴G - ⁴H°	2 - 2	1093
	840	1137.491	343.9996 - 431.9126	$3d^{4}(a^{3}D)4s - 3d^{4}(a^{3}D)4p$	$  ^{4}D - ^{4}D^{\circ}$	$\frac{1}{2} - \frac{1}{2}$	1093
	720	1137.598	332.1754 - 420.0800	3d ⁴ (a ³ F)4s - 3d ⁴ (a ³ H)4p	⁴ F – ⁴ G°	$\frac{7}{2} - \frac{9}{2}$	1093
	360	1138.186	339.4824 - 427.3422	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}P)4p$	$^{2}\mathbf{F} - ^{2}\mathbf{D}^{\circ}$	5-5	1093
	620	1138 484	339 2601 - 427 0960	$3d^{4}(a^{3}P)4s = 3d^{4}(a^{3}F)4p$	${}^{2}P - {}^{2}F^{\circ}$	3 5	1093
	520	1138.799	332.0318 - 419.8447	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}F)4p$	⁴ F – ⁴ F°	$\frac{2}{3} - \frac{2}{5}$	1093
	-00					5 5	1000
	500	1139.040	332.0516 - 419.8447	3d*(a*F)4s - 3d*(a*F)4p	$\mathbf{F} = \mathbf{F}^{*}$	2 - 2	1093
	860	1139.168	329.7542 - 417.5384	3d ⁴ (a ³ H)4s - 3d ⁴ (a ³ H)4p	⁴ H - ⁴ G°	2 - 1	1093
	800	1139.825	347.2785 - 435.0115	$3d^{4}(a^{1}G)4s - 3d^{4}(a^{1}G)4p$	² G - ² H°	$\frac{9}{2} - \frac{11}{2}$	1093
	780	1140.347	366.2898 - 453.9830	$3d^{4}(a^{1}F)4s - 3d^{4}(a^{1}F)4p$	${}^{2}F - {}^{2}G^{\circ}$	$\frac{5}{3} - \frac{7}{3}$	1093
	320	1140.571	295.8827 - 383.5578	$3d^{4}(a^{5}D)4s = 3d^{4}(a^{5}D)4n$	°D – °P°	1_1	1093
	70	1141.084	389.2996 - 476.9356	$3d^{4}(b^{1}G)4s - 3d^{4}(b^{1}G)4p$	² G - ² G°	$\frac{9}{2} - \frac{7}{2}$	1093
					100 1000		
	280	1141.386	339.4824 - 427.0960	30 (a F)4s - 30 (a F)4p	$\mathbf{F} = \mathbf{F}$	2 - 2	1093
	550	1141.563	374.8439 - 462.4431	3d*(b'P)4s – 3d*(b'P)4p	*P – *D*	5 - 5	1093
	810	1141.889	337.9939 - 425.5676	$3d^{4}(a^{3}H)4s - 3d^{4}(a^{3}H)4p$	$^{2}H - ^{2}H^{\circ}$	1	1093
	670	1142.171	347.4452 - 434.9970	3d ⁴ (a ¹ G)4s - 3d ⁴ (a ¹ G)4p	${}^{2}G - {}^{2}F^{\circ}$	$\frac{7}{2} - \frac{5}{2}$	1093
	140	1142.313	296.1981 - 383.7398	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	⁶ D – ⁶ P ^e	3 - 5	1093
	290	1142.478	337.0077 - 424.5370	$3d^{4}(a^{3}H)4s - 3d^{4}(a^{3}G)4p$	² H – ⁴ H°	2 - 2	1093
	-		200 7540		1	9 11	1000
	/40	1144.047	329./542 - 417.1641	3d (a H)4s - 3d (a H)4p	"H – "l"	$\frac{1}{2} - \frac{1}{2}$	1093
	890	1144.290	298.1305 - 385.5209	3d ⁴ (a ⁵ D)4s - 3d ⁴ (a ⁵ D)4p	°D - °F°	2 - 2	1093
	770	1144.686	332.0318 - 419.3905	3d4(a3F)4s - 3d4(a3H)4p	4F - 4G°	3-3	1093
	60	1144,790	375.9498 - 463.3015	$3d^{4}(b^{3}F)4s - 3d^{4}(b^{3}P)4p$	⁴ F - ⁴ P°	5 - 5	1093
	130	1144.973	332 0516 - 419 3905	$3d^{4}(a^{3}F)4s = 3d^{4}(a^{3}H)4r$	F-fO	2 2	1093
	750	1145.048	336.4304 - 423.7633	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}G)4p$	⁴G - ⁴F°	$\frac{11}{2} - \frac{9}{2}$	1093
	150	1145.398	336.4048 - 423.7105	3d*(a`P)4s - 3d*(a`G)4p	² P - ⁴ F°	$\frac{1}{2} - \frac{2}{2}$	1093
	160	1145.453	336.3449 - 423.6458	3d ⁴ (a ³ G)4s - 3d ⁴ (a ³ G)4p	⁴ G − ² F°	$\frac{9}{2} - \frac{7}{2}$	1093
	620	1145.835	347.8924 - 435.1654	$3d^{4}(a^{1}I)4s - 3d^{4}(a^{1}I)4p$	${}^{2}I - {}^{2}K^{\circ}$	13 - 13	1093
	440	1146.342	358.8279 - 446.0612	$3d^{4}(a^{1}D)4s - 3d^{4}(a^{1}D)4p$	${}^{2}D - {}^{2}F^{\circ}$	3_5	1093
	840	1146 776	347 9639 - 435 1654	3d4(a)1)4e 2d4(a)1)4n	21 21 0	<u>п</u> 13	1003
	040	1147.029	247 4462 424 4240	2 14 (a 1)45 - 30 (a 1)4p		$\frac{2}{7}$ $\frac{2}{5}$	1093
	00	1147.038	347.4432 - 434.0200	50 (a·C)45 - 30 (a·D)4p	-0- F	2 - 2	1093
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#### NI VI - Continued

lultiplet Rel. 1	nt. $\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	Reference
100	1147.855	347.8924 - 435.0115	$3d^{4}(a^{1}I)4s - 3d^{4}(a^{1}G)4p$	${}^{2}\mathbf{I} - {}^{2}\mathbf{H}^{\circ}$	<u>13 – 11</u>		1093
330	1148.257	335.9760 - 423.0652	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}H)4p$	${}^{4}G - {}^{2}H^{\circ}$	1 - 2		1093
670	1148 861	296 6967 - 383 7398	$3d^4(a^5D)4s = 3d^4(a^5D)4p$	"D - "P"	5 5		1093
570	1140.000	380 2006 476 3321	$3d^{4}(h^{1}G)/4s = 3d^{4}(h^{1}G)/4p$	² G ² H ^o	2 2 2 9		1093
740	1149.000	342 0006 431 0303	3d(00)4s = 3d(00)4p $3d^4(a^3D)4a = 3d^4(a^3D)4p$	4D 4P	2 - 2 2 1		1093
/40	1149.155	343.9990 - 431.0203	3d(a'D)4s - 3d(a'D)4p	D - P	2 2 2		1093
450	1149.828	389.3625 - 476.3321	3d"(b'G)4s - 3d"(b'G)4p	G-'H'	$\frac{1}{2} - \frac{1}{2}$		1093
720	1149.979	330.5805 - 417.5384	3d4(a3H)4s - 3d4(a3H)4p	⁴H – ⁴G°	$\frac{13}{2} - \frac{11}{2}$		1093
850	1150.267	329.4862 - 416.4225	3d ⁴ (a ³ H)4s - 3d ⁴ (a ³ F)4p	⁴H - ⁴G°	$\frac{7}{2} - \frac{9}{2}$		1093
640	1151.253	296.6967 - 383.5578	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	°D - °P°	$\frac{5}{2} - \frac{3}{2}$		1093
130	1151.857	344.2035 - 431.0203	$3d^{4}(a^{3}D)4s - 3d^{4}(a^{3}D)4p$	${}^{4}D - {}^{4}P^{\circ}$	3-5		1093
570	1152.355	374.8439 - 461.6226	$3d^{4}(b^{3}P)4s - 3d^{4}(b^{3}P)4p$	⁴ <b>P</b> – ⁴ <b>D</b> °	$\frac{5}{2} - \frac{5}{2}$		1093
64(	1152.492	375.6730 - 462.4431	$3d^{4}(b^{3}F)4s - 3d^{4}(b^{3}P)4p$	⁴ F − ⁴ D°	$\frac{\tilde{9}}{2} - \frac{\tilde{7}}{2}$		1093
710	1152 789	207 3505 384 0965	$3d^{4}(a^{5}D)Ac = 3d^{4}(a^{5}D)Ac$	<b>6D – 6</b> B	1_1		1003
710	1152.700	297.3505 - 384.0905	3d(aD)+s = 3d(aD)+p	$2C$ $2U^{\circ}$	$2^{-2}$		1093
//(	1153.121	347.4432 - 434.1073	30 (a C)4s - 30 (a C)4p	45 4D	$\frac{1}{2} - \frac{1}{2}$		1093
240	1153.654	332.0318 - 418./134	3d ⁻ (a ⁻ F)4s - 3d ⁻ (a ⁻ F)4p	$\mathbf{F} - \mathbf{P}$	2 - 2		1093
880	1154.605	297.3505 - 383.9602	3d*(a°D)4s - 3d*(a°D)4p	°D – °F°	$\frac{1}{2} - \frac{2}{2}$		1093
220	1154.804	374.8439 - 461.4378	$3d^{4}(b^{3}P)4s - 3d^{4}(b^{3}P)4p$	⁴ P − ⁴ P°	$\frac{2}{2} - \frac{2}{2}$		1093
810	1154.960	330.5805 - 417.1641	$3d^{4}(a^{3}H)4s - 3d^{4}(a^{3}H)4p$	⁴ H – ⁴ I°	$\frac{13}{2} - \frac{11}{2}$		1093
180	1155.735	344.4474 - 430.9719	$3d^{4}(a^{3}D)4s - 3d^{4}(a^{3}D)4p$	⁴ D - ⁴ D°	$\frac{3}{2} - \frac{3}{2}$		1093
210	1155 857	375 9271 - 462 4431	$3d^4(h^3F)4s = 3d^4(h^3P)4p$	${}^{4}\mathbf{F} - {}^{4}\mathbf{D}^{\circ}$	1 1		1093
400	1156.632	330.0016 416.4590	$3d^{4}(a^{3}P)As = 3d^{4}(a^{3}P)Ap$	4 <b>D</b> _4 <b>D</b> °	3_1		1003
400	1156.032	244 4474 420 2022	3d(ar)+s = 3d(ar)+p $2d^{4}(a^{3}D)/a = 2d^{4}(a^{3}D)/a =$		2 - 2 3 1		1093
180	1156.730	344.4474 - 430.8988	$3d^{2}(a^{2}D)4s = 3d^{2}(a^{2}D)4p$		$\frac{1}{2} - \frac{1}{2}$		1093
190	1156.844	339.2601 - 425.7031	3d ⁻ (a ² P)4s - 3d ⁻ (a ² P)4p	P - D	$\frac{1}{2} - \frac{1}{2}$		1093
360	1156.955	343.0520 - 429.4863	3d*(a'G)4s - 3d*(a'G)4p	² G – *G*	$\frac{1}{2} - \frac{2}{2}$		1093
830	1157.552	297.3505 - 383.7398	3d4(a5D)4s - 3d4(a5D)4p	⁶ D – ⁶ P°	$\frac{7}{2} - \frac{5}{2}$		1093
760	1157.805	332.3448 - 418.7134	$3d^{4}(a^{3}P)4s - 3d^{4}(a^{3}P)4p$	⁴ P - ⁴ P°	$\frac{5}{2} - \frac{3}{2}$		1093
590	1158,792	336.3449 - 422.6424	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}H)4p$	⁴ G − ² I°	<u><u>8</u>_<u><u><u></u></u></u></u>		1093
860	1158,996	3301410 - 4164225	$3d^{4}(a^{3}H)4s - 3d^{4}(a^{3}F)4n$	⁴ H - ⁴ G°	<u> </u>		1093
780	1159 178	329 4862 - 415 7543	$3d^4(a^3H)4s = 3d^4(a^3H)4p$	⁴ H – ⁴ I°	<u>1</u> <u>9</u>		1093
80	1159.574	347.2785 - 433.5173	$3d^{4}(a^{1}G)4s - 3d^{4}(a^{3}G)4p$	${}^{2}G - {}^{2}G^{\circ}$	$\frac{2}{9} - \frac{7}{2}$		1093
				20 404	9 11		1003
680	1160.221	343.8426 - 430.0333	$3d^{-}(a^{-}G)4s - 3d^{-}(a^{-}G)4p$	-G - G	$\frac{1}{2} - \frac{1}{2}$		1093
400	1160.823	332.3448 - 418.4908	3d*(a`P)4s - 3d*(a`F)4p	*P - *F*	$\frac{2}{2} - \frac{2}{2}$		1093
440	1161.533	347.2785 - 433.3712	3d ⁴ (a ¹ G)4s - 3d ⁴ (a ³ G)4p	${}^{2}G - {}^{2}G^{\circ}$	$\frac{9}{2} - \frac{9}{2}$		1093
500	1161.825	347.4452 - 433.5173	$3d^{4}(a^{1}G)4s - 3d^{4}(a^{3}G)4p$	$^{2}G - ^{2}G^{\circ}$	$\frac{7}{2} - \frac{7}{2}$		1093
250	1161.872	358.7166 - 444.7842	$3d^{4}(a^{1}D)4s - 3d^{4}(a^{1}D)4p$	$^{2}D - ^{2}D^{\circ}$	2 - 2 2 - 2		1093
880	1161.952	296.6967 - 382.7589	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	°D - °F°	$\frac{5}{2} - \frac{7}{2}$		1093
840	1162.007	337 0077 - 423 0652	$3d^{4}(a^{3}H)As = 3d^{4}(a^{3}H)As$	2 <b>11</b> _211°	2 2		1093
860	1163 252	208 1305 384 0965	$3d^{4}(a^{5}D)As = 3d^{4}(a^{5}D)An$	•D - •P	$\frac{2}{9}$ $\frac{2}{7}$		1093
140	1164.200	298.1303 - 384.0905	3d(aD)4s = 3d(aD)4p $3d^{4}(a^{3}H)4a = 3d^{4}(a^{3}E)4p$	4U 4C°	2 2		1093
140	1164.200	329.4862 - 415.3820	3d(a'H)4s - 3d(a'F)4p		2 - 2		1093
430	1164.329	329.7542 - 415.6408	$3d^{2}(a^{2}H)4s - 3d^{2}(a^{2}F)4p$	"H - "G"	$\frac{2}{9} - \frac{1}{9}$		1093
850	1165.098	298.1305 - 383.9602	$3d^{*}(a^{*}D)4s - 3d^{*}(a^{*}D)4p$	⁶ D - ⁶ F ⁶	$\frac{1}{2} - \frac{1}{2}$		1093
120	1165.907	337.9939 - 423.7633	3d'(a'H)4s - 3d'(a'G)4p	² H - *F*	$\frac{11}{2} - \frac{3}{2}$		1093
90	1167.219	375.9498 - 461.6226	$3d^{4}(b^{3}F)4s - 3d^{4}(b^{3}P)4p$	⁴ F – ⁴ D°	\$ - 5		1093
30	1167.319	332.0516 - 417.7181	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}H)4p$	${}^{4}\mathbf{F} - {}^{2}\mathbf{G}^{\circ}$	5 - 7		1093
870	1167.748	296.1981 - 381.8328	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	⁶ D - ⁶ F [•]	3-5		1093
550	1168.061	330,1410 - 415,7543	$3d^{4}(a^{3}H)4s - 3d^{4}(a^{3}H)4n$	${}^{4}H - {}^{4}I^{\circ}$	Ц _ 2		1093
510	1168 788	366 2998 - 451 8594	$3d^{4}(a^{1}F)4s = 3d^{4}(a^{1}F)4r$	${}^{2}\mathbf{F} - {}^{2}\mathbf{F}^{0}$	1_1		1093
200	1168.981	332.1754 - 417.7181	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}H)4p$	${}^{4}\mathbf{F} - {}^{2}\mathbf{G}^{\circ}$	$\frac{2}{7} - \frac{7}{2}$		1093
710	1169.297	347.2785 - 432.8001	$3d^{4}(a^{1}G)4s - 3d^{4}(a^{1}G)4p$ $3d^{4}(b^{3}E)4c - 3d^{4}(b^{3}E)4c$	${}^{2}\mathbf{G} - {}^{2}\mathbf{F}^{\circ}$ ${}^{4}\mathbf{E} - {}^{4}\mathbf{E}^{\circ}$	$\frac{2}{2} - \frac{1}{2}$ $\frac{2}{2} - \frac{1}{2}$		1093
/40	1170.327	3/3.0/30 - 401.1183	30 (0°F)48 - 30 (0°F)4p	r - r	$\frac{2}{3} - \frac{2}{3}$		1093
100	1170.631	358.8279 - 444.2522	3d"(a'D)4s - 3d"(a'D)4p	D - D	2 - 2		1093
	11170 846	297.3505 - 382.7589	3d [*] (a ³ D)4s - 3d [*] (a ³ D)4p	"D - "F"	$\frac{1}{2} - \frac{1}{2}$		1093
850	11/0.040			1	0 1	1	
850	1171.324	332.3436 - 417.7181	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}H)4p$	${}^{4}\mathbf{F} - {}^{2}\mathbf{G}^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		1093

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NI VI - Continued

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Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	550	1173.786	332.3436 - 417.5384	3d ⁴ (a ³ F)4s - 3d ⁴ (a ³ H)4p	⁴ F − ⁴ G°	<u> 2</u> _ <del>1</del>		1093
	720	1174 495	330 0016 - 415 1445	$3d^{4}(a^{3}P)4s = 3d^{4}(a^{3}P)4n$	⁴ P – ⁴ D°	3_5		1093
	940	1174 500	206 6067 391 9329	$\frac{3}{2}d^{4}(a^{5}D)(a) = \frac{3}{2}d^{4}(a^{5}D)(a)$	6D 6E	5 5		1002
	700	1174.390	270.0707 - 381.8528	3u(aD)4s = 3u(aD)4p	40 40	2 - 2 1 3		1093
	/80	1174.885	328.4372 - 413.5531	30 (a°P)4s - 30 (a°P)4p	P - D	$\begin{bmatrix} \bar{2} - \bar{2} \\ 13 \end{bmatrix}$		1093
	440	1175.926	347.8924 - 432.9320	3d⁴(a'I)4s – 3d⁴(a'I)4p	$\mathbf{I} - \mathbf{I}^{\circ}$	$\frac{13}{2} - \frac{11}{2}$		1093
	220	1176.461	343.0520 - 428.0515	3d⁴(a³G)4s - 3d⁴(a³G)4p	² G – ² H°	$\frac{7}{2} - \frac{9}{2}$		1093
	170	1176.803	339,2601 - 424,2354	3d ⁴ (a ³ P)4s - 3d ⁴ (a ³ P)4p	${}^{2}P - {}^{2}P^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		1093
	870	1176 937	296 1981 - 381 1638	$3d^4(a^5D)4s = 3d^4(a^5D)4p$	6D - 6E	1 1 1		1093
	740	1177 356	342.0520 427.0056	$\frac{3}{4} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}$	20 200	2 2 2 2 2		1002
	740	1177.250	343.0320 - 427.9930	50 (a C)48 - 50 (a F)4p	0-0	2 - 2		1093
	820	1178.217	295.8827 - 380.7567	$3d^{-}(a^{-}D)4s - 3d^{-}(a^{-}D)4p$	°D - °F	$\frac{1}{2} - \frac{1}{2}$		1093
	300	1178.364	375.6730 - 460.5359	3d⁴(b'F)4s – 3d⁴(b'F)4p	*F – *F*	$\frac{1}{2} - \frac{1}{2}$		1093
	310	1178.959	332.3436 - 417.1641	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}H)4p$	⁴F ⁴I°	$\frac{9}{2} - \frac{11}{2}$		1093
	840	1179.960	308.3238 - 393.0720	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	⁴ D – ⁴ F°	3-5		1093
	850	1180 295	347 8924 - 432 6166	$3d^4(a^1I)4s = 3d^4(a^1I)4n$	² I - ² I ⁹	یئ یُب ا		1093
	840	1100.255	227 0020 422 7110	$244(a^{3}II)Aa - 244(a^{3}II)Aa$	211 210			1003
	840	1180.363	557.9939 - 422.7118	30 (a H)48 - 30 (a H)4p	-n1	$\frac{1}{2} - \frac{1}{2}$		1093
	590	1181.293	375.9498 - 460.6036	3d*(b'F)4s - 3d*(b'F)4p	*F - *F*	2 - 2		1093
	150	1181.641	298.1305 - 382.7589	3d*(a'D)4s - 3d*(a'D)4p	°D − °F°	$\frac{9}{2} - \frac{1}{2}$		1093
	370	1181.899	375.9271 - 460.5359	3d4(b3F)4s - 3d4(b3F)4p	⁴ F – ⁴ F°	$\frac{7}{2} - \frac{7}{2}$		1093
	690	1182.605	296.1981 - 380.7567	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	°D - °F°	3_1		1093
	700	1183 671	297 3505 - 381 8328	$3d^4(a^5D)4a = 3d^4(a^5D)4a$	0 - F	ž ž		1093
	710	1183.071	297.5565 - 581.6528	3d(aD)As = 3d(aD)Ap		2 - 2 5 3		1093
	/10	1183.897	296.6967 - 381.1638	3d (a ⁻ D)4s - 3d (a ⁻ D)4p	$^{\circ}D - ^{\circ}F^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		1093
	20	1183.991	335.3845 - 419.8447	3d*(a'G)4s – 3d*(a'F)4p	⁴G - ⁴F°	$\frac{2}{2} - \frac{2}{2}$		1093
	100	1184.311	375.9271 - 460.3646	3d ⁴ (b ³ F)4s – 3d ⁴ (b ³ F)4p	⁴F - ⁴F°	$\frac{1}{2} - \frac{5}{2}$	1	1093
	20	1184.445	339.3358 - 423.7633	3d ⁴ (a ³ F)4s - 3d ⁴ (a ³ G)4p	² F – ⁴ F°	$\frac{7}{2} - \frac{9}{2}$		1093
	860	1184.659	309.0549 - 393.4682	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	⁴ D – ⁴ F°	5 - 2		1093
	170	1184 753	336 4304 - 420 8357	$3d^4(a^3G)4s = 3d^4(a^3F)4n$	${}^{4}G - {}^{4}F'$	<u> </u>		1093
	210	1195 024	230 2601 422 6469	$2d^{4}(a^{3}D)Aa = 2d^{4}(a^{3}D)Aa$	$2\mathbf{D}$ $2\mathbf{D}^{0}$	$2^{-2}$		1003
	210	1185.024	559.2001 - 425.0408	30 (a P)4s - 30 (a P)4p	P - P	$\frac{1}{2} - \frac{1}{2}$		1093
	430	1185.140	343.8426 - 428.2214	3d*(a'G)4s – 3d*(a'F)4p	$^{2}G - {}^{2}F^{*}$	$\frac{1}{2} - \frac{1}{2}$		1093
	440	1186.984	332.1754 - 416.4225	3d⁴(a³F)4s – 3d⁴(a³F)4p	⁴F – ⁴G°	$\frac{1}{2} - \frac{9}{2}$		1093
	570	1187.529	336.3449 - 420.5532	3d⁴(a³G)4s - 3d⁴(a³F)4p	⁴G - ⁴F°	$\frac{9}{2} - \frac{7}{2}$		1093
	840	1188.364	332,3436 - 416,4930	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}F)4p$	4F - 4D°	$\frac{2}{3} - \frac{7}{3}$		1093
		1188 5	45 8842 - 130 0259	$3d^5 - 3d^5$	$a^4 \mathbf{P} = a^2 \mathbf{P}$	1 1	FP	375 1093
	070	1100.0	200 0771 204 0(10			$2^{-2}_{7}$	г,г	1002
	8/0	1189.300	309.9771 - 394.0610	3d (a D)4s - 3d (a D)4p	D - F	$\frac{5}{2} - \frac{7}{2}$		1093
		1189.5	45.8842 - 129.9516	$3d^{3} - 3d^{3}$	$a^{*}P - a^{*}P$	2 - 2	F,P	375,1093
	20	1189.859	343.0520 - 427.0960	3d*(a'G)4s - 3d*(a'F)4p	$G - F^{\circ}$	$\frac{1}{2} - \frac{2}{2}$		1093
	390	1190.237	309.0549 - 393.0720	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	⁴D - ⁴F°	$\frac{5}{2} - \frac{5}{2}$		1093
	310	1190.326						1093
	300	1191.015	351.0330 - 434.9958	$3d^{4}(a^{3}D)4s - 3d^{4}(a^{3}D)4n$	${}^{2}\mathbf{D} - {}^{2}\mathbf{P}^{\circ}$	5 - 3		1093
		1191.6	46 1044 - 130 0259	3d ⁵ - 3d ⁵	$a^4 P = a^2 D$	1 1	FD	375 1093
	100	1101 000	251.00(2 424.0059	244-1914-244-3014		2 - 2 1 3	1',1	1002
	190	1191.090	331.0962 - 434.9938	30 (a ⁻ 5)4s - 30 (a ⁻ D)4p	-3-P	$\frac{1}{2} - \frac{1}{2}$		1093
	560	1192.110	335.9760 - 419.8633	3d ⁻ (a ³ G)4s - 3d ⁻ (a ³ H)4p	*G - *G*	$\frac{1}{2} - \frac{1}{2}$		1093
	50	1192.346	335.9760 - 419.8447	3d*(a'G)4s - 3d*(a'F)4p	"G - "F"	$\frac{1}{2} - \frac{3}{2}$		1093
	790	1192.469	343.8426 - 427.7027	3d⁴(a³G)4s - 3d⁴(a³G)4p	${}^{2}G - {}^{2}H^{\circ}$	2 - 11		1093
		1192.6	46.1044 - 129.9516	$3d^{5} - 3d^{5}$	$a^4P - a^2P$	3-3	F.P	375,1093
	480	1193,159	328 4372 - 412 2482	$3d^{4}(a^{3}P)4s = 3d^{4}(a^{3}P)4n$	4P - 4D*	i_i	- ,-	1093
	70	1102 459	358 8270 442 6100	2d4(alD)4a 2d4(-3D)4=	20 20	3 3		1003
	10	1193,438	330.0277 - 442.0199		<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>	2 - 2		1093
	400	1193.883	382.8891 - 466.6491	3d"(b"F)4s - 3d"(b"F)4p	'F - 'F"	2 - 2		1093
	440	1194.274	336.3449 - 420.0800	3d*(a'G)4s – 3d*(a'H)4p	*G – ⁴G°	$\frac{1}{2} - \frac{1}{2}$		1093
		1194.7	46.3248 - 130.0259	3d ⁵ – 3d ⁵	a⁴P – a²P	$\frac{1}{2} - \frac{1}{2}$	F,P	375,1093
	20	1195.948	337.0077 - 420.6234	$3d^{4}(a^{3}H)4s - 3d^{4}(a^{3}F)4n$	$^{2}H - {}^{4}G^{\circ}$	§ 1		1093
	590	1196 328	332 0516 - 415 6409	$3d^4(a^3FMa = 3d^4(a^3FMa)$	${}^{4}E = {}^{4}C^{4}$	2 2		1003
	20	1106 477	220 1754 415 7540	34(-3E)/(-34(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E)/(-3E	40 41	2 2		1075
	20	1170.4//	332.1/34 - 413./343	50 (a r)45 - 50 (a'H)4p	T - T	2 - 2		1093
	310	1196.788	336.4048 ~ 419.9615	3d*(a'P)4s - 3d*(b'P)4p	² P - ² S°	$\frac{1}{2} - \frac{1}{2}$		1093
	540	1196.867	330.0016 - 413.5531	$3d^{4}(a^{3}P)4s - 3d^{4}(a^{3}P)4p$	⁴P – ⁴D°	$\frac{3}{2} - \frac{3}{2}$		1093
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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	40	1196.967	337.0077 - 420.5532	3d ⁴ (a ³ H)4s - 3d ⁴ (a ³ F)4p	² <b>H</b> - ⁴ <b>F</b> °	$\frac{9}{2} - \frac{7}{2}$		1093
	470	1197.754	330.1410 - 413.6316	3d ⁴ (a ³ H)4s - 3d ⁴ (a ³ H)4p	⁴ H – ⁴ H°	$\frac{11}{2} - \frac{13}{2}$		1093
	590	1198.111	332.1754 - 415.6408	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}F)4p$	⁴ F - ⁴ G°	$\frac{7}{2} - \frac{7}{2}$		1093
	330	1198.239	382.6771 - 466.1337	$3d^{4}(b^{3}F)4s - 3d^{4}(b^{3}F)4p$	${}^{2}F - {}^{2}F^{\circ}$	7 - 7		1093
	420	1198,893	332,3436 - 415,7543	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}H)4p$	4F - 4I°	1		1093
	620	1199.764	332.0318 - 415.3820	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}F)4p$	⁺F - ⁴G°	3-5		1093
	020	1177.704	552.0510 - 415.5020			2 2		10/5
	560	1200.041	332.0516 - 415.3820	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}F)4p$	⁴ F - ⁴ G ^e	$\frac{5}{2} - \frac{5}{2}$		1093
	30	1202.128	351.0962 - 434.2816	3d (a S)4s - 3d (a D)4p	-S - P	$\frac{2}{13} - \frac{2}{13}$		1093
	850	1204.085	330.5805 - 413.6316	3d*(a ⁻ H)4s - 3d*(a ⁻ H)4p	H - H	$\frac{1}{2} - \frac{1}{2}$		1093
	700	1205.264	332.1754 - 415.1445	$3d^{*}(a^{*}F)4s - 3d^{*}(a^{*}P)4p$	$^{4}F - ^{4}D^{4}$	$\frac{1}{2} - \frac{1}{2}$		1093
	330	1207.107	351.0962 - 433.9369	3d*(a'S)4s – 3d*(a'S)4p	$^{2}S - ^{2}P^{*}$	2-2		1093
	130	1207.735	332.3448 - 415.1445	3d⁴(a [.] P)4s – 3d⁴(a [.] P)4p	*P - *D*	$\frac{2}{2} - \frac{2}{2}$		1093
	90	1209.427	358.7166 - 441.4012	3d ⁴ (a ¹ D)4s - 3d ⁴ (a ³ D)4p	${}^{2}D - {}^{2}D^{\circ}$	$\frac{5}{2} - \frac{5}{2}$		1093
	860	1210.512	330,1410 - 412,7511	$3d^{4}(a^{3}H)4s - 3d^{4}(a^{3}H)4p$	4H - 4H°	<u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u></u>		1093
	30	1211 271	339 3358 - 421 8940	$3d^{4}(a^{3}F)4s = 3d^{4}(a^{3}F)4n$	${}^{2}F - {}^{4}D^{9}$	1 - 5		1093
	120	1213 704	335 9760 - 418 3688	$3d^{4}(a^{3}G)4s = 3d^{4}(a^{3}H)4p$	${}^{4}G - {}^{2}G^{*}$	1 - 2		1093
	820	1214 453	329 7542 - 412 0956	$3d^{4}(a^{3}H)4s = 3d^{4}(a^{3}H)4n$	4H - 4H	2 2		1093
	520	1214.581	335.3845 - 417.7181	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}H)4p$	⁴ G - ² G°	$\frac{2}{5} - \frac{1}{2}$		1093
	870	1216.798	329.4862 - 411.6694	3d*(a`H)4s – 3d*(a`H)4p	⁴ H – ⁴ H°	$\frac{1}{2} - \frac{1}{2}$		1093
	10	1216.977	330.5805 - 412.7511	3d ⁺ (a'H)4s – 3d ⁺ (a'H)4p	*H – *H*	$\frac{12}{2} - \frac{11}{2}$		1093
	20	1217.419	347.8924 - 430.0333	3d⁴(a¹I)4s – 3d⁴(a³G)4p	² I – ⁴ G°	<u><u>1</u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>		1093
	720	1217.572	382.6771 - 464.8078	3d ⁴ (b ³ F)4s – 3d ⁴ (b ³ F)4p	² F - ⁴ G°	$\frac{7}{2} - \frac{7}{2}$		1093
	510	1217.672	339.4824 - 421.6072	3d ⁴ (a ³ F)4s - 3d ⁴ (a ³ F)4p	${}^{2}F - {}^{2}D^{\circ}$	$\frac{5}{2} - \frac{3}{2}$		1093
	20	1219.164	336.3449 - 418.3688	3d⁴(a³G)4s - 3d⁴(a³H)4p	⁴ G – ² G°	$\frac{9}{2} - \frac{9}{2}$		1093
	910	1219 662	339 3358 - 421 3243	$3d^{4}(a^{3}F)4s = 3d^{4}(a^{3}F)4n$	² F - ² D°	1_1		1093
	380	1220 191	330 1410 - 412 0956	$3d^{4}(a^{3}H)4s = 3d^{4}(a^{3}H)4p$	⁴ H - ⁴ H ^o	[ μ_ 2		1093
	470	1220.171	336 4304 - 418 3688	$3d^{4}(a^{3}G)4s = 3d^{4}(a^{3}H)4n$	'G_'G'	<u>1</u> 2		1093
	150	1220.420	382 8801 464 8078	$3d^{4}(h^{3}E)4e = 3d^{4}(h^{3}E)4e$	- F - + G*	2 2 2 2		1093
	110	1220.709	220 7542 411 6604	$3d^{4}(a^{3}\mathbf{H})Ac = 3d^{4}(a^{3}\mathbf{H})Ac$	U • U + U •	$\frac{2}{2}$ $\frac{2}{2}$		1093
	110	1226.961	332.0516 - 413.5531	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}P)4p$	⁴ F - ⁴ D°	$\frac{2}{2} - \frac{2}{2}$		1093
	20	1227.556	339.2601 - 420.7223	3d ⁴ (a ⁴ P)4s - 3d ⁴ (a ⁴ P)4p	-P - ⁺S°	2-2		1093
	20	1227.957	308.3238 - 389.7604	3d ⁴ (a ⁵ D)4s - 3d ⁴ (a ⁵ D)4p	*D – *P*	1 1 - 1		1093
	300	1228.903	336.3449 - 417.7181	3d ⁴ (a ³ G)4s - 3d ⁴ (a ³ H)4p	⁴ G - ² G°	$\frac{9}{2} - \frac{7}{2}$		1093
	20	1229.084	337.0077 - 418.3688	3d4(a3H)4s - 3d4(a3H)4p	² H - ² G°	$\frac{9}{2} - \frac{9}{2}$		1093
	800	1232.957	336.4304 - 417.5384	3d ⁴ (a ³ G)4s - 3d ⁴ (a ³ H)4p	⁴ G - ⁴ G°	<u><u><u></u></u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u>		1093
	160	1233.436	307.8439 - 388.9186	3d4(a5D)4s - 3d4(a5D)4p	⁴ D - ⁶ D°	$\frac{1}{2} - \frac{1}{2}$		1093
	320	1237.325	336,3449 - 417,1641	3d ⁴ (a ³ G)4s - 3d ⁴ (a ³ H)4p	⁺G - ⁺I°	<u> </u>		1093
	600	1238.637	336.4304 - 417.1641	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}H)4p$	⁺G - ⁺I°	<u><u></u><u><u></u><u><u></u><u></u><u></u><u><u></u><u></u><u></u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u></u></u></u>		1093
	680	1238.970	337.0077 - 417.7181	$3d^{4}(a^{3}H)4s - 3d^{4}(a^{3}H)4p$	² H – ² G°	2 - 7		1093
	680	1239.041	309.0549 - 389.7604	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	⁴ D - ⁴ P°	3 - 3		1093
	240	1240.767	308 3238 - 388 9186	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	⁴ D - ⁶ D ⁶	3_1		1093
	230	1241.254	366.2998 - 446.8638	3d ⁴ (a ¹ F)4s - 3d ⁴ (a ¹ D)4p	² <b>F</b> - ² <b>F</b> °	$\frac{1}{2} - \frac{1}{2}$		1093
	250	1241 007	242 9426 424 2627	241636340 24163634-		2 11		1002
	250	1241.907	343.8420 - 424.303/	3d(a O)45 - 3d(a O)4p		1 2 - 2 11 2		1093
	850	1244.177	337.3737 - 418.3088	30 (a 1)45 - 30 (a 1)4p	-n - 0	2 - 2		1093
	20	1247.062	309.0349 - 389.2434	30 (a D)45 - 30 (a D)4p		2 - 2		1093
	460	1247.513	309.0349 - 389.2140	30 (a D)45 - 30 (a D)4p		$\frac{1}{2} - \frac{5}{2}$		1093
	420	1248.807	330.3449 - 416.4225 295.8827 - 375.9498	3d'(a'C)4s - 3d'(a'F)4p 3d ⁴ (a'D)4s - 3d ⁴ (b'F)4s	"D - 'F	1 - 5	F.P	375.1093
			27010021 97017470				- ,-	,
	310	1249.792	343.0520 - 423.0652	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}H)4p$	$^{2}G - ^{2}H^{\circ}$	1 - 2 5 - 5		1093
	780	1250.031	335.3845 - 415.3820	3d*(a`G)4s - 3d*(a`F)4p	"G - "G"	2 - 2		1093
		1250.2	295.8827 - 375.8708	3d*(a'D)4s - 3d*(b'F)4s	°D - 'F	2-2	F,P	375,1093
	110	1251.240	343.8426 - 423.7633	3d ⁴ (a ³ G)4s - 3d ⁴ (a ³ G)4p	² G - ⁴ F°	$\frac{9}{2} - \frac{9}{2}$		1093
	700	1251.467	309.9771 - 389.8832	3d⁴(a⁵D)4s - 3d⁴(a⁵D)4p	⁴ D – ⁶ D°	$\frac{1}{2} - \frac{2}{2}$		1093
	310	1252.411	343.0520 - 422.8978	3d⁴(a³G)4s - 3d⁴(a³G)4p	${}^{2}G - {}^{2}F^{\circ}$	$\frac{7}{2} - \frac{5}{2}$		1093

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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	400	1253 079	343 8426 - 423 6458	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}G)4p$	${}^{2}G - {}^{2}F^{\circ}$	$\frac{9}{2} - \frac{7}{2}$		1093
	790	1253 398	309 9771 - 389 7604	$3d^{4}(a^{5}D)4s = 3d^{4}(a^{5}D)4n$	${}^{4}D = {}^{4}P^{\circ}$	Ž_Ž		1093
	260	1253 581	344 4474 - 424 2185	$3d^{4}(a^{3}D)4s = 3d^{4}(a^{3}G)4p$	${}^{4}D - {}^{4}F^{\circ}$	3_5		1093
	200	1253.561	206 1091 275 0409	$3d^{4}(a^{5}D)Aa = 3d^{4}(b^{3}E)Aa$	°D ⁴ E	3 5	ED	375 1093
		1253.9	290.1981 - 375.9498	3d(aD)4s - 3d(bF)4s		$\frac{2}{3}$ $\frac{2}{7}$	F,F	375,1093
		1254.2	296.1981 - 375.9271	$3d^{(a)}D 4s - 3d^{(b)}F 4s$	^o D - 'F	$\frac{1}{2} - \frac{1}{2}$	F,P	375,1093
		1255.1	296.1981 - 375.8708	3d ⁴ (a ³ D)4s - 3d ⁴ (b ³ F)4s	°D – ⁺F	2-2	F,P	375,1093
	160	1255.260	335.9760 - 415.6408	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}F)4p$	⁴ G − ⁴ G°	$\frac{7}{2} - \frac{7}{2}$		1093
		1255.5	296.6967 - 376.3437	3d ⁴ (a ⁵ D)4s - 3d ⁴ (b ⁴ P)4s	°D – 'P	2-2	F,P	375,1093
	110	1255.881	344.6100 - 424.2354	$3d^{4}(a^{3}D)4s - 3d^{4}(a^{3}P)4p$	${}^{4}\mathbf{D} - {}^{2}\mathbf{P}^{\circ}$	$\frac{1}{2} - \frac{3}{2}$		1093
		1256.0	50.3310 - 129.9516	3d ⁵ – 3d ⁵	a ⁴ D – a ² P	$\frac{7}{2} - \frac{3}{2}$	F,P	375,1093
		1259.7	50.6435 - 130.0259	3d ⁵ - 3d ⁵	$a^4D - a^2P$	1 - 1	F,P	375,1093
		1261.8	296.6967 - 375.9498	3d4(a5D)4s - 3d4(b3F)4s	°D – ⁴F	$\frac{5}{2} - \frac{5}{2}$	F,P	375,1093
		1261.9	50.7805 - 130.0259	3d ^s - 3d ^s	$a^4D - a^2P$	$\frac{3}{7} - \frac{1}{7}$	F,P	375,1093
		1262.1	296 6967 - 375 9271	$3d^{4}(a^{5}D)4s - 3d^{4}(b^{3}F)4s$	°D - ⁴F	$\frac{5}{3} - \frac{7}{3}$	F.P	375,1093
	30	1262 120	339 4824 - 418 7134	$3d^{4}(a^{3}F)4s = 3d^{4}(a^{3}P)4n$	${}^{2}\mathbf{F} - {}^{4}\mathbf{P}^{\circ}$	\$ _ 3		1093
		1263.0	50 7776 - 129 9516	$3d^5 - 3d^5$	$a^4D = a^2P$	1 2 1	FP	375 1093
		1263.0	50.7805 - 129.9516	3d ⁵ - 3d ⁵	$a^4 D = a^2 P$	1 1	FP	375 1093
	400	1205.1	30.7603 - 127.7510	3d = 3d		2 2 2	1,1	1003
	400	1205.280	339.3338 - 418.3088	50 (a r)48 - 50 (a r)4p	T-0	2-2		1093
		1265.9	297.3505 - 376.3437	3d ⁴ (a ⁵ D)4s - 3d ⁴ (b ³ P)4s	°D - ⁴P	$\frac{7}{2} - \frac{3}{2}$	F,P	375,1093
		1266.2	296.6967 - 375.6730	$3d^{4}(a^{5}D)4s - 3d^{4}(b^{3}F)4s$	°D - 'F	5-3	F.P	375,1093
	60	1268.350	343.0520 - 421.8940	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}F)4p$	${}^{2}G - {}^{4}D^{\circ}$	$\frac{7}{2} - \frac{5}{2}$	, ·	1093
	220	1269 113	309 0549 - 387 8499	$3d^{4}(a^{5}D)4s = 3d^{4}(a^{5}D)4n$	⁴ D - "D"	\$_\$		1093
	100	1269.870	337 0077 - 415 7543	$3d^{4}(a^{3}H)4s = 3d^{4}(a^{3}H)4n$	² H - ⁴ I°	2 2		1093
	120	1271.718	337.0077 - 415.6408	$3d^4(a^3H)4s - 3d^4(a^3F)4p$	² H – ⁴ G°	$\frac{1}{2} - \frac{7}{2}$		1093
		1272 6	207 2505 275 0271	2d4/05D140 2d4/b3E140	¢D ∔E	1 1 1	ED	275 1002
	20	1272.0	297.3303 - 373.9271	3d(aD)4s - 3d(0T)4s		$\frac{2}{11}$ $\frac{2}{9}$	F,F	373,1093
	20	1275.029	337.9939 - 410.4225	30(a H)4s - 30(a F)4p	H-G	$\frac{1}{2}$ $-\frac{1}{2}$		1093
	90	1278.173	339.4824 - 417.7181	$3d^{*}(a^{*}F)4s - 3d^{*}(a^{*}H)4p$	F - G*	$\frac{2}{2} - \frac{1}{2}$		1093
		1279.6	296.6967 - 374.8439	3d ⁴ (a ⁵ D)4s - 3d ⁴ (b ⁵ P)4s	${}^{\circ}\mathbf{D} - {}^{\circ}\mathbf{P}$	2 - 2	F,P	375,1093
	560	1284.137	309.9771 - 387.8499	$3d^{4}(a^{D})4s - 3d^{4}(a^{D})4p$	$^{\circ} \mathbf{C}^{*} - \mathbf{C}^{*}$	$\frac{1}{2} - \frac{2}{2}$		1093
	180	1284.782	308.3238 - 386.1573	3d ⁴ (a ⁵ D)4s - 3d ⁴ (a ⁵ D)4p	⁴ D – ⁴ P°	2 - 2		1093
	90	1285.975	337.9939 - 415.7543	3d ⁴ (a ³ H)4s - 3d ⁴ (a ³ H)4p	² H - ⁴ I°	$\frac{11}{2} - \frac{9}{2}$		1093
		1289.6	298.1305 - 375.6730	3d4(a5D)4s - 3d4(b3F)4s	°D – ⁴F	$\frac{9}{2} - \frac{9}{2}$	F,P	375,1093
		1290.4	297.3505 - 374.8439	$3d^{4}(a^{5}D)4s - 3d^{4}(b^{3}P)4s$	°D – 4P	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>	F.P	375,1093
	210	1295.315	336.4304 - 413.6316	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}H)4p$	⁺G - ⁺H°	ų_ų		1093
	320	1296.970	309.0549 - 386.1573	$3d^{4}(a^{5}D)4s - 3d^{4}(a^{5}D)4p$	⁴ D – ⁴ P°	5-3		1093
	20	1297.239	339.3358 - 416.4225	$3d^{4}(a^{3}F)4s - 3d^{4}(a^{3}F)4p$	² F - ⁴G°	1 - 2		1093
	110	1300.331	307.8439 - 384.7474	3d⁴(a ⁵ D)4s - 3d⁴(a ⁵ D)4p	⁴ D - ⁴ P°	4-4		1093
		1301.2	64.1524 - 141.0068	$3d^{5} - 3d^{5}$	$a^2D - c^2D$	3 - 3	F.P	375,1093
		1302.6	64.1524 - 140.9222	$3d^{5} - 3d^{5}$	$a^2 D - c^2 D$	5 5	FP	375,1093
		1303.5	298 1305 - 374 8439	$3d^{4}(a^{5}D)4s = 3d^{4}(b^{3}P)4s$	°D - 'P	2 5	FP	375 1093
	250	1308.496	308 3238 - 384 7474	$3d^4(a^5D)4s = 3d^4(a^5D)4n$	⁴ D - ⁴ P°	1 1	1,1	1093
	90	1308.781	336.3449 - 412.7511	$3d^{4}(a^{3}G)4s - 3d^{4}(a^{3}H)4p$	⁴ G – ⁴ H°	$\begin{vmatrix} 2 & -2 \\ \frac{9}{2} - \frac{11}{2} \end{vmatrix}$		1093
	120	1310 963	335 3845 - 411 6604	3d4(03G)/10 2d4(03L1)/1-	40.411	2 1		1092
	130	1212 040	220 4924 415 6400	2d4(a)E)4a 2d4(a)E)4a	20-11	2 - 1		1075
	20	1313.049	337.4824 - 413.0408	30 (a F)45 - 30 (a F)4p	-F - G	2 - 2		1093
	210	1313.720	335.9700 - 412.0956	30 (a G)4s - 30 (a H)4p	-'H' - Đ'	1 1 - 1		1093
		1318.7	65.1735 - 141.0068	3d' - 3d'	$a^2D - c^2D$	2 - 2	F,P	375,1093
		1320.2	65.1735 - 140.9222	3d ⁵ - 3d ⁵	$a^2D - c^2D$	$\frac{2}{2} - \frac{2}{2}$	F,P	375,1093
	20	1322.078	337.9939 - 413.6316	3d4(a'H)4s – 3d4(a'H)4p	² H – ⁴ H°	$\frac{11}{2} - \frac{13}{2}$		1093
		1352.8	67.0851 - 141.0068	3d ⁵ – 3d ⁵	$a^2F - c^2D$	$\frac{7}{2} - \frac{3}{2}$	F,P	375,1093
		1354.3	67.0851 - 140.9222	3d ⁵ – 3d ⁵	$a^2F - c^2D$	$\frac{1}{2} - \frac{5}{2}$	F,P	375,1093
		1354.4	309.0549 - 382.8891	3d ⁴ (a ⁵ D)4s - 3d ⁴ (b ³ F)4s	⁴ D - ² F	3-3	F.P	375,1093
		1358.3	309.0549 - 382.6771	$3d^{4}(a^{5}D)4s - 3d^{4}(b^{3}F)4s$	${}^{4}D - {}^{2}F$	1 1 I	EP	375,1093
	Ì	1375.5	309.9771 - 382.6771	$3d^4(a^5D)4s = 3d^4(b^3F)4s$	4D - 2F	i_i	EP	375 1093
		1378.1	68 4449 - 141 0068	$3d^{5} = 3d^{5}$	$a^2 \mathbf{F} = c^2 \mathbf{D}$	5 3	FP	375 1002
			00.1112 01110000	Ju - Ju	areco	2 - 2	1,1	575,1095

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Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
		1379.7	68.4449 - 140.9222	3d ⁵ - 3d ⁵	$a^2F - c^2D$	$\frac{5}{2} - \frac{5}{2}$	F,P	375,1093
		1381.8	68.5512 - 140.9222	3d ⁵ - 3d ⁵	$a^4F - c^2D$	$\frac{9}{2} - \frac{5}{2}$	F,P	375,1093
		1384.9	68.8017 - 141.0068	3d ⁵ – 3d ⁵	$a^4F - c^2D$	$\frac{1}{2} - \frac{3}{2}$	F,P	375,1093
		1386.6	68.8017 - 140.9222	3d ⁵ - 3d ⁵	$a^4F - c^2D$	$\frac{1}{2} - \frac{5}{2}$	F,P	375,1093
		1397.4	69.4470 - 141.0068	3d ⁵ - 3d ⁵	$a^4F - c^2D$	$\frac{5}{2} - \frac{3}{2}$	F,P	375,1093
		1468.3	307.8439 - 375.9498	3d4(a5D)4s - 3d4(b3F)4s	4 <b>D</b> - 4F	$\frac{1}{2} - \frac{5}{2}$	F,P	375,1093
		1470.0	307.8439 - 375.8708	3d⁴(a ⁵ D)4s - 3d⁴(b³F)4s	4D - 4F	$\frac{1}{2} - \frac{3}{2}$	F,P	375,1093
		1470.2	308.3238 - 376.3437	3d4(a5D)4s - 3d4(b3P)4s	4D - 4P	$\frac{3}{2} - \frac{3}{2}$	F,P	375,1093
		1478.7	308.3238 - 375.9498	3d4(a5D)4s - 3d4(b3F)4s	4D - 4F	$\frac{3}{2} - \frac{5}{2}$	F,P	375,1093
1		1479.2	308.3238 - 375.9271	3d4(a5D)4s - 3d4(b3F)4s	⁴ D – ⁴ F	$\frac{3}{2} - \frac{7}{2}$	F,P	375,1093
		1480.4	308.3238 - 375.8708	3d4(a5D)4s - 3d4(b3F)4s	⁴ D - ⁴ F	$\frac{3}{2} - \frac{3}{2}$	F,P	375,1093
		1486.1	309.0549 - 376.3437	3d4(a5D)4s - 3d4(b3P)4s	⁴D - ⁴P	$\frac{5}{2} - \frac{3}{2}$	F,P	375,1093
		1494.9	309.0549 - 375.9498	3d⁴(a ⁵ D)4s - 3d⁴(b ³ F)4s	⁴D - ⁴F	$\frac{5}{2} - \frac{5}{2}$	F,P	375,1093
		1495.4	309.0549 - 375.9271	3d⁴(a⁵D)4s - 3d⁴(b³F)4s	4 <b>D</b> - 4 <b>F</b>	$\frac{5}{2} - \frac{7}{2}$	F,P	375,1093
		1501.1	309.0549 - 375.6730	3d4(a5D)4s - 3d4(b3F)4s	⁴ D – ⁴ F	$\frac{5}{2} - \frac{9}{2}$	F,P	375,1093
		1506.8	309.9771 - 376.3437	3d⁴(a ^s D)4s - 3d⁴(b³P)4s	4D – 4P	$\frac{7}{2} - \frac{3}{2}$	F,P	375,1093
		1515.9	41.9209 - 107.8870	3d ⁵ – 3d ⁵	a ⁴ G - b ² G	$\frac{11}{2} - \frac{7}{2}$	F,P	375,1093
		1516.3	309.9771 - 375.9271	3d4(a5D)4s - 3d4(b3F)4s	⁴ D – ⁴ F	$\frac{7}{2} - \frac{7}{2}$	F,P	375,1093
		1516.8	41.9209 - 107.8483	3d ⁵ – 3d ⁵	a ⁴ G - b ² G	$\frac{11}{2} - \frac{9}{2}$	F,P	375,1093
		1518.1	64.1524 - 130.0259	3d ⁵ - 3d ⁵	$a^2D - a^2P$	$\frac{5}{2} - \frac{1}{2}$	F,P	375,1093
		1518.3	42.0232 - 107.8870	3d ⁵ – 3d ⁵	$a^4G - b^2G$	$\frac{9}{2} - \frac{7}{2}$	F,P	375,1093
		1518.6	42.0351 - 107.8870	3d ⁵ – 3d ⁵	$a^4G - b^2G$	$\frac{7}{2} - \frac{7}{2}$	F,P	375,1093
		1519.2	42.0232 - 107.8483	3d ⁵ – 3d ⁵	$a^4G - b^2G$	$\frac{9}{2} - \frac{9}{2}$	F,P	375,1093
		1519.8	64.1524 - 129.9516	3d ⁵ - 3d ⁵	$a^2D - a^2P$	$\frac{5}{2} - \frac{3}{2}$	F,P	375,1093
		1520.0	309.0549 - 374.8439	3d4(a5D)4s - 3d4(b3P)4s	4D - 4P	\$ - 5	F,P	375,1093
		1522.2	309.9771 - 375.6730	3d4(a5D)4s - 3d4(b3F)4s	⁴ D – ⁴ F	$\frac{7}{2} - \frac{9}{2}$	F,P	375,1093
		1541.6	309.9771 - 374.8439	3d4(a5D)4s - 3d4(b3P)4s	⁴ D – ⁴ P	7 - 5	F,P	375,1093
		1542.0	65.1735 - 130.0259	$3d^{5} - 3d^{5}$	$a^2D - a^2P$	$\frac{3}{2} - \frac{1}{2}$	F,P	375,1093
		1543.7	65.1735 - 129.9516	3d ⁵ – 3d ⁵	$a^2D - a^2P$	$\frac{3}{2} - \frac{3}{2}$	F,P	375,1093
		1623.0	79.3914 - 141.0068	$3d^{5} - 3d^{5}$	$b^2 F - c^2 D$	$\frac{5}{2} - \frac{3}{2}$	F,P	375,1093
		1625.2	79.3914 - 140.9222	3d ⁵ – 3d ⁵	$b^2 F - c^2 D$	$\frac{5}{2} - \frac{5}{2}$	F,P	375,1093
		1628.7	79.6083 - 141.0068	3d ⁵ – 3d ⁵	$b^2 F - c^2 D$	$\frac{1}{2} - \frac{1}{2}$	F,P	375,1093
		1631.0	79.6083 - 140.9222	3d ⁵ – 3d ⁵	$b^2 F - c^2 D$	1 - 5	F,P	375,1093
		1711.0	307.8439 - 366.2898	3d4(a5D)4s - 3d4(aF)4s	${}^{4}D - {}^{2}F$	1 - 5	F,P	375,1093
		1724.8	308.3238 - 366.2998	3d4(a5D)4s - 3d4(a1F)4s	${}^{4}D - {}^{2}F$	$\frac{1}{2} - \frac{7}{2}$	F,P	375,1093
		1725.1	308.3238 - 366.2898	3d4(a5D)4s - 3d4(a1F)4s	4 <b>D</b> − ² F	$\frac{3}{2} - \frac{5}{2}$	F,P	375,1093
		1746.9	309.0549 - 366.2998	3d4(a5D)4s - 3d4(a1F)4s	4 <b>D</b> – ² <b>F</b>	5-7	F,P	375,1093
		1747.2	309.0549 - 366.2898	3d4(a5D)4s - 3d4(aF)4s	${}^{4}D - {}^{2}F$	$\frac{5}{2} - \frac{5}{2}$	F,P	375,1093
		1775.5	309.9771 - 366.2998	3d ⁴ (a ⁵ D)4s - 3d ⁴ (a ¹ F)4s	${}^{4}D - {}^{2}F$	$\frac{1}{2} - \frac{1}{2}$	F,P	375,1093
		1969.3	0.0 - 50.7805	3d ⁵ – 3d ⁵	ga ⁶ S – a ⁴ D	$\frac{5}{2} - \frac{3}{2}$	F,P	375,1093
		1969.4	0.0 - 50.7776	3d ⁵ – 3d ⁵	ga ⁶ S − a ⁴ D	$\frac{5}{2} - \frac{5}{2}$	F,P	375,1093
		1980.0	308.3238 - 358.8279	3d4(a5D)4s - 3d4(a1D)4s	${}^{4}\mathbf{D} - {}^{2}\mathbf{D}$	$\frac{3}{2} - \frac{3}{2}$	F,P	375,1093
		1981.7	46.1044 - 96.5665	3d ⁵ - 3d ⁵	a ⁴ P - b ² D	$\frac{3}{2} - \frac{5}{2}$	F,P	375,1093
		1985.8	46.1044 - 96.4612	3d ⁵ - 3d ⁵	$a^4P - b^2D$	$\frac{3}{2} - \frac{3}{2}$	F,P	375,1093
		1986.8	0.0 - 50.3310	3d ⁵ - 3d ⁵	ga ⁶ S – a ⁴ D	$\frac{5}{2} - \frac{1}{2}$	F,P	375,1093
		1990.4	46.3248 - 96.5665	3d ⁵ - 3d ⁵	$a^4P - b^2D$	$\frac{1}{2} - \frac{5}{2}$	F,P	375,1093
		1994.6	46.3248 - 96.4612	3d ⁵ - 3d ⁵	$a^4P - b^2D$	$\frac{1}{2} - \frac{3}{2}$	F,P	375,1093
		1994.6	46.3248 - 96.4612	$3d^{5} - 3d^{5}$	a⁴P – b²D	$\frac{1}{2} - \frac{3}{2}$	F,P	

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	28	204.979	0.804 - 488.665	3d ⁴ - 3d ³ (a ⁴ P)4p	ga ⁵ D - ⁵ P°	2 - 3		622
	78	205.278	1.520 - 488.665	$3d^4 - 3d^3(a^4P)4p$	ga ⁵ D - ⁵ P°	3 - 3		622
	32	205.369	0.279 - 487.207	$3d^4 - 3d^3(a^4P)4p$	ga ⁵ D – ⁵ P°	1-2		622
	88	205.591	0.804 - 487.207	$3d^4 - 3d^3(a^4P)4p$	$ga^{5}D - {}^{5}P^{\circ}$	2 - 2		622
	140	205.645	2.392 - 488.665	$3d^4 - 3d^3(a^4P)4p$	ga ⁵ D - ⁵ P°	4 – 3		622
	28	205.697	0.0 - 486.151	$3d^4 - 3d^3(a^4P)4p$	$ga^{5}D - {}^{5}P^{\circ}$	0-1		622
					<b>0</b>			
	72	205.816	0.279 - 486.151	3d ⁴ – 3d ³ (a ⁴ P)4p	ga ⁵ D - ⁵ P°	1-1		622
	108	205.896	1.520 - 487.207	$3d^4 - 3d^3(a^4P)4p$	$ga^{5}D - {}^{5}P^{\circ}$	3 - 2		622
	62	206.038	0.804 - 486.151	$3d^4 - 3d^3(a^4P)4p$	$ga^{5}D - {}^{5}P^{\circ}$	2 - 1		622
	104	208.195	31.672 - 511.991	$3d^4 - 3d^3(a^2H)4p$	$a^{3}H - {}^{3}G^{\circ}$	4 – 3		622
	104	208.589	32.286 - 511.698	$3d^4 - 3d^3(a^2H)4p$	a ³ H – ³ G°	5 - 4		622
	94	208.691	32.286 - 511.464	$3d^4 - 3d^3(a^2H)4p$	$a^{3}H - {}^{3}G^{\circ}$	5 - 5		622
	[							
	104	208.948	32.877 - 511.464	3d ⁴ – 3d ³ (a ² H)4p	a ³ H - ³ G°	6 - 5		622
	98	210.020	2.392 - 478.534	$3d^4 - 3d^3(a^4F)4p$	ga ⁵ D – ³ G°	4 - 5		622
	98	211.046	38.160 - 511.991	$3d^4 - 3d^3(a^2H)4p$	a ³ G - ³ G°	3 - 3		622
	62	211.307	38.746 - 511.991	$3d^4 - 3d^3(a^2H)4p$	a ³ G - ³ G°	4 – 3		622
	104	211.438	38.746 - 511.698	$3d^4 - 3d^3(a^2H)4p$	a ³ G - ³ G°	4 - 4		622
	24	211.541	38.746 - 511.464	$3d^4 - 3d^3(a^2H)4p$	a ³ G - ³ G°	4 - 5		622
	114	211.615	0.804 - 473.360	3d⁴ – 3d³(a⁴F)4p	$ga^{5}D - {}^{3}D^{\circ}$	2 - 3		622
	126	211.660	39.247 - 511.698	3d⁴ – 3d³(a²H)4p	$a^{3}G - {}^{3}G^{\circ}$	5 - 4		622
	118	211.767	39.247 - 511.464	$3d^4 - 3d^3(a^2H)4p$	a'G - 'G°	5 - 5		622
	100	212.001	0.279 - 471.976	3d ⁴ – 3d ³ (a ⁴ F)4p	$ga^{5}D - {}^{3}D^{\circ}$	1 - 2		622
	70	212.202	0.0 - 471.250	3d⁴ – 3d³(a⁴F)4p	$ga^{5}D - {}^{5}F^{\circ}$	0 - 1		622
	70	212.328	2.392 - 473.360	3d ⁴ – 3d ³ (a ⁴ F)4p	$ga^{5}D - {}^{3}D^{\circ}$	4 – 3		622
	160	212.521	1.520 - 472.067	3d⁴ - 3d³(a⁴F)4p	ga ⁵ D - ⁵ F°	3 – 4		622
	166	212.533	2.392 - 472.907	3d⁴ – 3d³(a⁴F)4p	ga ⁵ D - ⁵ F°	4 - 5		622
	20	212.56	1.520 - 471.976	3d⁴ – 3d³(a⁴F)4p	$ga^{5}D - {}^{3}D^{\circ}$	3 - 2		548
	28	212.635	0.804 - 471.096	3d⁴ – 3d³(a⁴F)4p	ga ⁵ D – ⁵ F°	2 – 3		622
	20	212.86	0.279 – 470.056	3d⁴ – 3d³(a⁴F)4p	ga ^s D – ^s F°	1 - 2		548
	174	212.913	2.392 - 472.067	3d⁴ – 3d³(a⁴F)4p	ga ⁵ D – ⁵ F°	4 – 4		622
	156	212.958	1.520 - 471.096	3d ⁴ – 3d ³ (a ⁴ F)4p	ga ⁵ D - ⁵ F°	3 – 3		622
	126	213.104	0.804 - 470.056	$3d^{4} - 3d^{3}(a^{4}F)4p$	$ga^{D} - F^{o}$	2 – 2		622
	80	213.13	0.0 - 469.175	3d ² - 3d ² (a ² F)4p	ga D – D	0-1		548
	110	213.151	0.0 - 469.175	$3d^{2} - 3d^{3}(a^{4}F)4p$	$ga^{3}D - {}^{3}D^{\circ}$	0-1		622
	40	213.207	0.279 - 469.175	$3d^{2} - 3d^{2}(a^{2}F)4p$	$ga^{T}D - D^{*}$	1 - 1		622
	/0	213.340	2.392 - 471.096	3d* - 3d*(a*F)4p	ga D - F	4 - 3		622
	106	213 431	1 520 - 470 056	2d4 2d3(a4E)4m	and D SE?			622
	142	213.506	0.804 - 469.175	$3d^{4} - 3d^{3}(a^{4}E)Ap$	$ga^{*}D = F$	3-2		622
	154	213.500	1 520 - 469 844	$3d^4 - 3d^3(a^4E)4p$	ga D = D	2 - 1		622
	138	213.527	0.804 - 468.690	$3d^4 - 3d^3(a^4E)4p$	ga D - D	3-4		622
	180	213.926	2392 - 469844	$3d^{4} - 3d^{3}(a^{4}F)4p$	$ga^{5}D = D^{2}$		-	622
	152	213.938	0.279 - 467.705	$3d^4 - 3d^3(a^4F)4p$	gaD = D	1_2		622
				50 - 50 (a i )4p	ga D = D	1-2		022
	144	214.053	1.520 - 468.690	$3d^4 - 3d^3(a^4F)4n$	oa ⁵ D - ⁵ D°	3_3		622
	128	214.126	0.0 - 467.015	$3d^4 - 3d^3(a^4F)4p$	$ga^{5}D = ^{3}D^{\circ}$	0 - 1		622
	98	214.180	0.804 - 467.705	$3d^4 - 3d^3(a^4F)4p$	$ga^{5}D = ^{5}D^{6}$	2_2		622
	52	214.252	0.279 - 467.015	$3d^4 - 3d^3(a^4F)4p$	$a^{5}D = ^{3}D^{6}$	1 - 1		622
	72	214.456	2.392 - 468.690	$3d^4 - 3d^3(a^4F)4n$	$a^{5}D = {}^{5}D^{2}$	4 - 3		622
	68	214.507	1.520 - 467.705	$3d^4 - 3d^3(a^4F)4n$	$ga^{5}D - {}^{5}D^{6}$	3_2		622
				50 - 50 (a 1 )+p	54 D - D	5-2		022
	148	215.767	32.877 - 496.340	$3d^4 - 3d^3(a^2G)4n$	$a^{3}H - {}^{3}G^{\circ}$	6-5		622
	146	216.074	32.286 - 495.087	$3d^4 - 3d^3(a^2G)4n$	$a^{3}H - {}^{3}G^{\circ}$	5 - 4		622
	120	216.417	31.672 - 493.743	$3d^4 - 3d^3(a^2G)4n$	$a^{3}H - {}^{3}G^{\circ}$	4 - 3		622
	86	216.562	34.576 - 496.340	$3d^4 - 3d^3(a^2G)4n$	$a^{3}F - {}^{3}G^{\circ}$	4 - 5		622
	96	217.029	34.317 - 495.087	$3d^4 - 3d^3(a^2G)4n$	$a^{3}F - {}^{3}G^{\circ}$	3-4		622
	110	217.151	34.576 - 495.087	$3d^4 - 3d^3(a^2G)4p$	$a^{3}F - {}^{3}G^{\circ}$	4-4		622
						1.4		

# NICKEL VII (Ni ⁶⁺), Z = 28 Ground State 1s²2s²2p⁶3s²3p⁶3d⁴(⁶D₀) (22 electrons) Ionization Potential [1 070 000] cm⁻¹; [133] eV

**ANIE**S Notes

NI VII - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm 1 )	Configurations	Terms	J - J	Notes	References
	72	217.630	34.247 - 493.743	3d ⁴ - 3d ³ (a ² G)4p	a ³ F - ³ G°	2 - 3		622
	92	217.663	34.317 - 493.743	3d ⁴ - 3d ³ (a ² G)4p	a ³ F – ³ G°	3 – 3	1 1	622
	10	217.78	34.576 - 493.743	3d⁴ – 3d³(a²G)4p	a ³ F - ³ G°	4 - 3		548
	100	218.53	38.746 - 496.340	3d ⁴ – 3d ³ (a ² G)4p	a ³ G – ³ G°	4 - 5		548
	98	218.774	39.247 - 496.340	3d ⁴ - 3d ³ (a ² G)4p	a ³ G – ³ G°	5 - 5		622
	20	218.85	38.160 - 495.087	3d ⁴ - 3d ³ (a ² G)4p	a ³ G - ³ G°	3 – 4		548
	50	219.137	38.746 - 495.087	3d ⁴ – 3d ³ (a ² G)4p	a ³ G - ³ G°	4 – 4		622
	116	219.499	38.160 - 493.743	$3d^4 - 3d^3(a^2G)4p$	a ³ G – ³ G°	3 – 3		622
	20	219.78	38.746 - 493.743	$3d^4 - 3d^3(a^2G)4p$	a ³ G – ³ G°	4 – 3		548
	20	223.25	34.317 - 482.229	$3d^4 - 3d^3(a^4F)4p$	$a^{3}F - {}^{3}F^{\circ}$	3 - 4		548
	98	223.387	34.576 - 482.229	$3d^4 - 3d^3(a^4F)4p$	a ³ F - ³ F°	4 - 4		622
	60	223.76	31.672 - 478.534	3d ⁴ – 3d ³ (a ⁴ F)4p	a ³ H - ³ G°	4 - 5		548
	26	223,791	34.247 - 481.091	3d⁴ – 3d³(a⁴F)4p	$a^{3}F - {}^{3}F^{\circ}$	2 - 3		622
	52	223.826	34.317 - 481.091	$3d^4 - 3d^3(a^4F)4p$	$a^{3}F - {}^{3}F^{\circ}$	3-3		622
	26	223.954	34.576 - 481.091	$3d^4 - 3d^3(a^4F)4n$	$a^{3}F - {}^{3}F^{\circ}$	4 - 3		622
	82	224 363	34 247 - 479 950	$3d^4 - 3d^3(a^4F)4p$	$a^{3}F - {}^{3}F^{\circ}$	2 - 2		622
	152	224 388	32 877 - 478 534	$3d^4 - 3d^3(a^4F)4p$	$a^{3}H - {}^{3}G^{\circ}$	6-5		622
	146	224.733	32.286 - 477.261	$3d^4 - 3d^3(a^4F)4p$	a'H - 'G°	5 - 4		622
	126	224 028	21 672 476 258	2d ⁴ 2d ³ (a ⁴ E)4p	a'H_'C°	4 3		622
	130	224.920	31.072 - 470.238	3d = 3d (aT) + p $3d^4 = 3d^3(a^4E)Ap$	aH = O	3_4		622
	10	225.191	36.100 - 462.229	3d - 3d(a F) + p		3-4		622
	30	223.240	34.370 - 478.334	3d - 3d (a F) + p	ar = 0	4-5		622
	40	225.487	38.740 - 482.229	30 - 30 (a r )4p		4-4		622
	134	225.742	39.247 - 482.229	3d = 3d (a + p) + p	a'G - F	3-4		622
	/0	223.707	34.317 - 477.201	30° - 30°(a F)4p	ar-G	3-4		622
	38	225.894	34.576 - 477.261	$3d^{4} - 3d^{3}(a^{4}F)4p$	$a^{3}F - {}^{3}G^{\circ}$	4 - 4		622
	110	226.069	38.746 - 481.091	3d* – 3d*(a*F)4p	a'G - 'F'	4-3		622
	48	226.238	34.247 - 476.258	3d* – 3d*(a*F)4p	a F - G	2 - 3		622
	46	226.273	34.317 - 476.258	3d* - 3d*(a*F)4p	a'F - 'G'	3 - 3		622
	102	226.352	38.160 - 479.950	3d ⁴ - 3d ³ (a ⁴ F)4p	a G - 'F°	3 – 2		622
	20	226.40	34.576 - 476.258	3d ⁴ – 3d ³ (a ⁴ F)4p	a'F - 'G°	4 - 3		548
	44	226.668	30.077 - 471.250	3d⁴ – 3d³(a⁴F)4p	<b>a</b> ³ <b>P</b> - ⁵ <b>F</b> °	0 – 1		622
	102	227.200	31.836 - 471.976	3d ⁴ – 3d ³ (a ⁴ F)4p	a ³ P – ³ D°	1 – 2		622
	46	227.256	32.877 - 472.907	3d ⁴ – 3d ³ (a ⁴ F)4p	a'H – ^s F°	6-5		622
	80	227.377	38.746 - 478.534	3d ⁴ - 3d ³ (a ⁴ F)4p	a'G - 'G°	4 - 5		622
	90	227.581	31.836 - 471.250	3d ⁴ - 3d ³ (a ⁴ F)4p	a ³ P ~ ⁵ F°	1 – 1		622
	126	227.642	39.247 - 478.534	3d ⁴ – 3d ³ (a ⁴ F)4p	a ³ G - ³ G°	5 – 5		622
	50	227.738	38.160 - 477.261	3d⁴ – 3d³(a⁴F)4p	a ³ G - ³ G°	3 - 4		622
	130	227.893	34.555 - 473.360	3d ⁴ – 3d ³ (a ⁴ F)4p	a'P - 'D°	2 - 3		622
	116	227.907	34.576 - 473.360	3d ⁴ - 3d ³ (a ⁴ F)4p	a ³ F - ³ D°	4 – 3		622
	102	228.043	38.746 - 477.261	3d ⁴ - 3d ³ (a ⁴ F)4p	a'G - 'G°	4 – 4		622
	68	228.262	38.160 - 476.258	3d ⁴ – 3d ³ (a ⁴ F)4p	a'G - 'G°	3 – 3		622
	10	228.30	39.247 - 477.261	3d ⁴ – 3d ³ (a ⁴ F)4p	a'G - 'G°	5 – 4		548
	72	228.489	34.317 - 471.976	3d ⁴ – 3d ³ (a⁴F)4p	$a^{3}F - {}^{3}D^{\circ}$	3 - 2		622
	100	228.54	38.746 - 476.258	3d ⁴ - 3d ³ (a ⁴ F)4p	a'G - 'G°	4 - 3		548
	34	228.613	34.555 - 471.976	3d ⁴ - 3d ³ (a ⁴ F)4p	$a^{3}P - {}^{3}D^{\circ}$	2 – 2		622
	34	228.831	34.247 - 471.250	$3d^{4} - 3d^{3}(a^{4}F)4p$	a'F - 'F°	2 - 1		622
	26	228,865	30.077 - 467.015	$3d^4 - 3d^3(a^4F)4p$	$a^{3}P - {}^{3}D^{\circ}$	0 - 1		622
	20	228.93	34.247 - 471.096	3d⁴ - 3d³(a⁴F)4p	a'F - 'F°	2 – 3		548
	30	229 427	31 836 - 467 705	3d ⁴ - 3d ³ (a ⁴ F)4n	a ³ P - ³ D°	1-2		622
	24	229.705	31 836 - 467 015	$3d^4 = 3d^3(a^4F)4n$	$a^{3}P - {}^{3}D^{2}$	1-1		622
	24	229.795	34 555 - 468 600	$3d^4 - 3d^3(a^4E)An$	a'P_'D'	2_1		622
	28	230.342	30 347 473 007	3u - 3u (a r) + p $2d^4 - 2d^3(a^4 r) + a$	ar-D	5 4		622
	18	230.398	37.247 - 472.907	3u = 3u (a r) + p $3d^4 = 3d^3 (a^4 r) + p$	au-r	3-3		622
	20	230.739	34.517 - 407.705	3u - 3u (a r)4p		3-2		622
	10	230.800	34.333 - 407.703	3u – 3u (a r)4p	ar-D	2-2		022

NI VII - Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	168	231.071	34.247 - 467.015	3d ⁴ - 3d ³ (a ⁴ F)4p	a ³ F - ³ D°	2 – 1		622

# NICKEL VIII (Ni ⁷⁺), Z = 28 Ground State $1s^22s^22p^63s^23p^63d^3({}^4F_{3/2})$ (21 electrons) Ionization Potential [1 310 000] cm⁻¹; [162] eV

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	80	167.07	0.0 - 598.570	3d ³ – 3d ² ( ³ P)4p	ga ⁴ F – ⁴ P°	$\frac{3}{2} - \frac{5}{2}$		003
	20	167.35	1.012 - 598.638	$3d^{3} - 3d^{2}(^{1}G)4p$	$ga^4F - {}^2G^\circ$	5-7		003
	10	167.66	2.184 - 598.638	$3d^{3} - 3d^{2}(^{1}G)4p$	$ga^4F - G^\circ$	$\frac{1}{3} - \frac{1}{3}$		003
	40	167.97	3.721 - 599.079	$3d^3 - 3d^2({}^1G)4p$	$ga^4F - G^\circ$	$\frac{1}{2} - \frac{1}{2}$		003
	20	168.08	3.721 - 598.638	$3d^3 - 3d^2(^1G)4p$	$ga^4F - {}^2G^\circ$			003
	10	168.33	0.0 - 594.068	$3d^3 - 3d^2(^3P)4p$	$ga^{4}F - {}^{4}D^{6}$	3 - 5		003
					8	1 2 2		000
	150	168.58	3.721 - 596.908	3d ³ – 3d ² ( ³ P)4p	ga⁴F - ⁴D°	$\frac{9}{2} - \frac{7}{2}$		003
	10	168.62	1.012 - 594.068	3d ³ – 3d ² ( ³ P)4p	ga⁴F – ⁴D°	$\frac{5}{2} - \frac{5}{2}$		003
	40	168.87	0.0 - 592.175	$3d^{3} - 3d^{2}(^{3}P)4p$	ga⁴F - ⁴D°	$\frac{3}{2} - \frac{3}{2}$		003
	20	168.95	2.184 - 594.068	$3d^{3} - 3d^{2}(^{3}P)4p$	ga ⁴ F - ⁴ D°	$\frac{1}{2} - \frac{5}{2}$		003
	400	169.16	1.012 - 592.175	$3d^3 - 3d^2(^3P)4p$	ga⁴F - ⁴D°	$\frac{5}{2} - \frac{3}{2}$		003
	40	169.27	0.0 - 590.764	$3d^{3} - 3d^{2}(^{3}P)4p$	ga⁴F – ⁴D°	$\frac{3}{2} - \frac{1}{2}$		003
	80	170.17	28.068 - 615.725	3d ³ – 3d ² ( ¹ G)4p	a ² G - ² H°	$\frac{9}{2} - \frac{11}{2}$		003
	20	170.27	0.0 - 587.305	$3d^{3} - 3d^{2}(^{3}P)4p$	ga⁴F – ⁴S°	$\frac{3}{2} - \frac{3}{2}$		003
	250	170.52	26.977 - 613.417	$3d^{3} - 3d^{2}(^{1}G)4p$	$a^2G - {}^2H^\circ$	$\frac{7}{2} - \frac{9}{2}$		003
	10	170.84	28.068 - 613.417	3d ³ – 3d ² ( ¹ G)4p	a ² G - ² H°	$\frac{9}{2} - \frac{9}{2}$		003
	40	172.10	2.184 - 583.241	3d ³ – 3d ² ( ³ F)4p	ga⁴F - ⁻ G°	$\frac{7}{2} - \frac{9}{2}$		003
	20	172.32	1.012 - 581.337	$3d^{3} - 3d^{2}(^{3}F)4p$	$ga^4F - {}^2G^\circ$	$\frac{5}{2} - \frac{7}{2}$		003
	40	172.67	2.184 - 581.337	$3d^3 - 3d^2(^3F)4p$	$ga^4 F - {}^2G^6$	2 - 2		003
	20	172.93	37.475 - 615.725	$3d^3 - 3d^2({}^1G)4p$	$a^2H - {}^2H^\circ$	ļ ų́ _ ų́		003
	750	173.41	36.754 - 613.417	$3d^3 - 3d^2('G)4p$	$a^{2}H - {}^{2}H^{\circ}$	3 - 2		003
	40	173.95	23.710 - 598.570	$3d^{3} - 3d^{2}(^{3}P)4n$	$a^{4}P - {}^{4}P^{\circ}$	1 1 2		003
	10	174.22	24.669 - 598.638	$3d^3 - 3d^2(^1G)4p$	$a^4P - {}^2G^9$	<u>5</u> _1		003
	750	174.24	24.669 - 598.570	$3d^{3} - 3d^{2}({}^{3}P)4p$	$a^4P - {}^4P^\circ$	3-3		003
	400	174.36	23.261 - 596.770	3d ³ – 3d ² ( ³ P)4p	a⁴P – ⁴P°	1 2 - 1		003
	250	174.46	23.710 - 596.905	$3d^{3} - 3d^{2}(^{3}P)4p$	a⁴P – ⁴P°	$\frac{3}{2} - \frac{3}{2}$		003
	10	174.50	23.710 - 596.770	$3d^{3} - 3d^{2}(^{3}P)4p$	a ⁴ P - ⁴ P°	$\frac{3}{2} - \frac{1}{2}$		003
	40	174.75	24.669 - 596.908	3d ³ – 3d ² ( ³ P)4p	a ⁴ P – ⁴ D°	$\frac{5}{2} - \frac{7}{2}$		003
	150	174.79	26.977 - 599.079	3d ³ – 3d ² ( ¹ G)4p	$a^2G - {}^2G^\circ$	$\frac{1}{2} - \frac{9}{2}$		003
	80	174.88	0.0 - 571.845	$3d^{3} - 3d^{2}(^{3}F)4p$	$ga^4F - {}^2D^\circ$	$\frac{3}{2} - \frac{5}{2}$		003
	750	174.92	26.977 - 598.638	3d ³ - 3d ² ( ¹ G)4n	$a^2G - {}^2G^2$	1_1		003
	40	174.95	0.0 - 571.517	$3d^3 - 3d^2(^3F)4n$	$\sigma a^4 F = {}^4 D^4$	3 5		003
	400	175.13	28.068 - 599.079	$3d^3 - 3d^2(^1G)4p$	$a^2G - C^2$	2 2		003
	40	175.26	28 068 - 598 638	$3d^{3} - 3d^{2}(^{1}G)4p$	$a^{2}G = {}^{2}G^{2}$	$2^{-2}_{2}$		003
	40	175.28	1.012 - 571.517	$3d^3 - 3d^2(^3E)4n$	$a^{4}F = {}^{4}D^{6}$	2 2 2		003
	400	175.32	0.0 - 570.353	$3d^{3} - 3d^{2}({}^{3}F)4n$	$ga^4F = 4D^6$	$\frac{2}{3}$ $\frac{2}{1}$		003
					5	2 - 2		005
	20	175.49	0.0 - 569.839	3d ³ – 3d ² ( ³ F)4p	ga⁴F - ⁴D°	$\frac{3}{2} - \frac{3}{2}$		003
	40	175.54	2.184 - 571.845	3d ³ – 3d ² ( ³ F)4p	ga⁴F – ²D°	$\frac{7}{2} - \frac{5}{2}$		003
	750	175.56	3.721 - 573.327	$3d^{3} - 3d^{2}(^{3}F)4p$	ga⁴F – ⁴D°	$\frac{9}{2} - \frac{7}{2}$		003
	20	175.62	24.669 - 594.068	$3d^{3} - 3d^{2}(^{3}P)4p$	a ⁴ P - ⁴ D°	\$ - 3		003
	400	175.64	2.184 - 571.517	$3d^3 - 3d^2(^3F)4p$	ga⁴F - ⁴D°	$\frac{1}{2} - \frac{5}{2}$		003
	400	175.67	3.721 - 572.969	$3d^{3} - 3d^{2}(^{3}F)4p$	ga⁴F - ⁴G°	$\frac{9}{2} - \frac{11}{2}$		003
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NI VIII - Continued

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Multiplet Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
1000	175.80	1.012 - 569.839	3d ³ - 3d ² ( ³ F)4p	ga⁴F - ⁴D°	$\frac{5}{2} - \frac{3}{2}$		003
1000	175.82	2.184 - 570.960	3d ³ – 3d ² ( ³ F)4p	ga ⁴ F – ⁴ F°	$\frac{7}{2} - \frac{9}{2}$	1	003
40	175.91	23.710 - 592.175	3d ³ – 3d ² ( ³ P)4p	a ⁴ P - ⁴ D°	$\frac{3}{2} - \frac{3}{2}$		003
750	175.94	2.184 - 570.546	3d ³ – 3d ² ( ³ F)4p	$ga^4F - {}^2F^\circ$	$\frac{7}{2} - \frac{5}{2}$		003
400	176.03	3.721 - 571.804	$3d^3 - 3d^2(^3F)4p$	$ga^4F - {}^2F^\circ$	$\frac{9}{2} - \frac{7}{2}$		003
250	176.13	1.012 - 568.746	$3d^3 - 3d^2(^3F)4p$	ga⁴F - ⁴F°	$\frac{5}{2} - \frac{7}{2}$		003
10	176.21	23.261 - 590.764	$3d^3 - 3d^2(^3P)4p$	a⁴P – ⁴D°	1-1	.	003
80	176.25	2 184 - 569 564	$3d^3 - 3d^2({}^3F)4n$	$ga^4F - {}^4G^\circ$	1 1 - 9		003
250	176.29	3 721 - 570 960	$3d^3 - 3d^2({}^3F)4p$	$ga^4F - {}^4F^\circ$	<u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u>		003
200	176.35	23 710 - 590 764	$3d^3 = 3d^2(^3P)4p$	²⁴ P - ⁴ D ⁶	1 <u>1</u>		003
40	176.33	00 - 566 831	$3d^{3} - 3d^{2}(^{3}E)Ap$	a T = D	2 2 2		003
150	176.50	2.184 - 568.746	$3d^{3} - 3d^{2}(^{3}F)4p$	$ga^4F - 4F^\circ$	$\frac{2}{7} - \frac{2}{7}$		003
80	176.69	1.012 - 566.964	3d' – 3d²('F)4p	ga ⁴ F – ⁴ G°	$\frac{2}{2} - \frac{1}{2}$		003
250	176.74	1.012 - 566.831	3d ³ – 3d ² ( ³ F)4p	ga4F - 4F°	$\frac{2}{2} - \frac{2}{2}$		003
750	176.87	0.0 - 565.388	3d ³ – 3d ² ( ³ F)4p	ga ⁴ F – ⁴ F°	$\frac{3}{2} - \frac{3}{2}$		003
250	176.95	0.0 - 565.124	3d ³ – 3d ² ( ³ F)4p	ga⁴F - ⁴G°	$\frac{3}{2} - \frac{5}{2}$		003
40	176.98	3.721 - 568.746	3d ³ – 3d ² ( ³ F)4p	ga ⁴ F – ⁴ F°	$\frac{9}{2} - \frac{7}{2}$		003
10	177.10	2.184 - 566.831	3d ³ – 3d ² ( ³ F)4p	$ga^4F - {}^4F^\circ$	$\frac{7}{2} - \frac{5}{2}$		003
400	177 19	1 012 - 565 388	$3d^3 - 3d^2(^3E)4n$	$ga^4F - {}^4F^\circ$	5_3		003
80	177.29	23 261 - 587 305	$3d^{3} - 3d^{2}({}^{3}P)4p$	a4P - 4S°	1 1		003
40	177.32	34 680 - 508 638	$3d^{3} - 3d^{2}(^{1}G)An$	$a^2 D = {}^2 G^2$	2 2 2		003
+0	177.32	23 710 597 305	$3d^{3} - 3d^{2}(^{3}\mathbf{P})An$	aD = C $a^4D = 4S^\circ$	3 3		003
80	177.43	23.710 - 387.303	3d = 3d (F)4p $3d^3 = 3d^2(^3E)4p$	a = 3			003
10	177.03	2.184 - 303.124	$3d^{3} - 3d(r)^{4}p$	$ga \Gamma = O$	2 - 2 5 - 3		003
40	1//./5	24.009 - 587.305	3u - 3u ( r)4p	ar-s	$\frac{1}{2} - \frac{1}{2}$		003
10	177.83	36.754 - 599.079	3d ³ - 3d ² ( ¹ G)4p	$a^{2}H - {}^{2}G^{\circ}$	$\frac{9}{2} - \frac{9}{2}$		003
10	177.87	34.689 - 596.905	3d' – 3d ² ('P)4p	$a^2D - P^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		003
20	177.97	36.754 - 598.638	3d ³ – 3d ² ( ¹ G)4p	$a^2H - {}^2G^\circ$	$\frac{1}{2} - \frac{1}{2}$		003
20	178.06	37.475 - 599.079	3d ³ – 3d ² ( ¹ G)4p	$a^2H - {}^2G^\circ$	$\frac{11}{2} - \frac{9}{2}$		003
80	178.52	36.754 - 596.908	$3d^3 - 3d^2(^3P)4p$	$a^2H - {}^4D^\circ$	$\frac{9}{2} - \frac{7}{2}$		003
400	178.77	34.689 - 594.068	3d ³ – 3d ² ( ³ P)4p	$a^2D - {}^4D^\circ$	$\frac{2}{2} - \frac{2}{2}$		003
250	178.91	35,120 - 594.068	3d ³ – 3d ² ( ³ P)4p	$a^2D - {}^4D^\circ$	$\frac{3}{2} - \frac{5}{2}$		003
40	179.77	26.977 - 583.241	$3d^3 - 3d^2(^3F)4p$	$a^2G - {}^2G^\circ$	$\frac{7}{2} - \frac{9}{2}$		003
550	179.97	35.120 - 590.764	$3d^3 - 3d^2(^3P)4p$	$a^2D - {}^4D^\circ$	$\frac{1}{3} - \frac{1}{2}$		003
250	180.12	28.068 - 583.241	$3d^{3} - 3d^{2}({}^{3}F)4p$	$a^2G - {}^2G^\circ$	$\frac{1}{2} - \frac{1}{2}$		003
250	180.39	26.977 - 581.337	$3d^3 - 3d^2(^3F)4p$	$a^2G - {}^2G^\circ$	$\frac{1}{2} - \frac{1}{2}$		003
40	180.74	28.068 - 581.337	3d ³ – 3d ² ( ³ F)4p	$a^2G - {}^2G^\circ$	$\frac{\tilde{9}}{2} - \frac{\tilde{7}}{2}$		003
40	181.10	35 120 - 587 305	$3d^3 = 3d^2(^3\mathbf{P})4n$	a ² D - ⁴ S°	3_3		003
20	182.27	24 669 - 573 327	$3d^{3} - 3d^{2}({}^{3}E)Ap$	$a^4P - {}^4D^\circ$	2 - 2		003
400	182.27	23,710 - 571,845	$3d^{3} - 3d^{2}({}^{3}F)4p$	$a^{4}P = {}^{2}D^{\circ}$	3 5		003
40	182.44	23.710 - 571.845	$3d^{3} - 3d^{2}(^{3}E)/ap$	$a^{4}P = {}^{4}D^{\circ}$	2 2 2		003
40	182.55	23.710 - 371.317	3d - 3d (F) + p	a F = D	2 - 2 5 5		003
20	182.70	23.261 - 570.353	$3d^{2} - 3d(T)4p$ $3d^{3} - 3d^{2}(^{3}F)4p$	$a^{4}P - b^{6}$	$\begin{array}{c} 2 - 2 \\ 1 \\ - 1 \\ 2 - 2 \end{array}$		003
80	182.87	24.669 - 571.517	$3d^{3} - 3d^{2}({}^{3}F)4p$	a⁴P - ⁴D°	$\frac{2}{2} - \frac{2}{2}$		003
40	182.94	23.710 - 570.353	3d ³ – 3d ² ( ³ F)4p	$a^4P - {}^4D^\circ$	$\frac{3}{2} - \frac{1}{2}$		003
80	182.96	23.261 - 569.839	3d ³ – 3d ² ( ³ F)4p	$a^4P - {}^4D^\circ$	$\frac{1}{2} - \frac{3}{2}$		003
40	182.99	36.754 - 583.241	3d ³ – 3d ² ( ³ F)4p	$a^2H - {}^2G^\circ$	$\frac{9}{2} - \frac{9}{2}$		003
40	183.02	23.261 - 569.667	3d ³ - 3d ² ( ³ F)4p	$a^4P - {}^2D^\circ$	$\frac{1}{2} - \frac{3}{2}$		003
10	183.16	23.710 - 569.667	3d ³ – 3d ² ( ³ F)4p	$a^4P - {}^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$		003
10	183.23	37.475 - 583.241	3d ³ – 3d ² ( ³ F)4p	$a^2H - {}^2G^\circ$	<u><u> </u></u>		003
20	183.39	28.068 - 573.327	$3d^3 - 3d^2({}^3F)4n$	$a^2G - {}^4D^\circ$	<u>9</u> - 7		003
40	183.44	24 669 - 569 839	$3d^3 = 3d^2(3F)4n$	$a^4P - {}^4D^9$	5_1		003
150	183.51	28.068 - 572.060	$3d^{3} = 3d^{2}(^{3}F)^{4}F$	$a^2G - {}^4G^{\circ}$	5 <u>1</u>		003
150	182.62	36 754 591 227	3d = 3d (17) + p $2d^3 = 2d^2/3E M_{ex}$	a ² H - ² C ^o	2 2 2		003
10	183.05	30.754 - 301.337 24.660 - 540 744	3d - 3d ( F)4p 3d ³ 2d ² / ³ EMa	a ⁴ D 4E°	2 2 2		003
40	103.00	24.007 - 308.740	за – за (г <i>)</i> 4р	ar - r	2 - 2		005

NI VIII -- Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	900	183.83	26.977 - 570.960	3d ³ - 3d ² ( ³ F)4p	$a^2G - {}^4F^\circ$	$\frac{7}{2} - \frac{9}{2}$		003
	80	183.91	28.068 - 571.804	$3d^3 - 3d^2(^3F)4p$	$a^2G - {}^2F^\circ$	$\frac{9}{2} - \frac{7}{2}$		003
	20	183.97	26.977 - 570.546	$3d^3 - 3d^2(^3F)4p$	$a^2G - {}^2F^\circ$	$\frac{7}{2} - \frac{5}{2}$		003
	900	184.12	23.710 - 566.831	$3d^3 - 3d^2(^3F)4p$	<b>a</b> ⁴P – ⁴ F°	$\frac{3}{2} - \frac{5}{2}$		003
	10	184.20	28.068 - 570.960	$3d^{3} - 3d^{2}(^{3}F)4p$	$a^2G - {}^4F^\circ$	$\frac{9}{2} - \frac{9}{2}$		003
	10	184.40	24.669 - 566.964	$3d^3 - 3d^2(^3F)4p$	a⁴P – ⁴G°	$\frac{5}{2} - \frac{7}{2}$		003
	550	184.44	24.669 - 566.831	3d ³ – 3d ² ( ³ F)4p	a ⁴ P - ⁴ F°	$\frac{5}{2} - \frac{5}{2}$		003
	10	184.58	26.977 - 568.746	$3d^{3} - 3d^{2}(^{3}F)4p$	$a^2G - {}^4F^\circ$	$\frac{1}{2} - \frac{1}{2}$		003
	10	184.62	23.710 - 565.388	$3d^3 - 3d^2(^3F)4p$	$a^4P - {}^4F^\circ$	$\frac{3}{2} - \frac{3}{2}$		003
	40	184.68	28.068 - 569.564	$3d^{3} - 3d^{2}({}^{3}F)4p$	$a^2G - {}^4G^\circ$	$\frac{9}{2} - \frac{9}{2}$		003
	40	184.95	28.068 - 568.746	$3d^{3} - 3d^{2}(^{3}F)4p$	a ² G – ⁴ F°	$\frac{9}{2} - \frac{7}{2}$		003
	20	185.18	26.977 - 566.964	$3d^{3} - 3d^{2}(^{3}F)4p$	$a^2G - {}^4G^\circ$	$\frac{7}{2} - \frac{7}{2}$		003
	10	185.23	26.977 - 566.831	3d ³ - 3d ² ( ³ F)4p	a ² G – ⁴ F°	$\frac{7}{2} - \frac{5}{2}$		003
	80	185.65	34.689 - 573.327	$3d^{3} - 3d^{2}(^{3}F)4p$	a²D - ⁴D°	$\frac{5}{2} - \frac{7}{2}$		003
	10	185.82	26.977 - 565.124	$3d^3 - 3d^2(^3F)4p$	a²G - ⁴G°	$\frac{1}{2} - \frac{5}{2}$		003
	10	186.16	34.689 - 571.845	3d ³ - 3d ² ( ³ F)4p	$a^2D - {}^2D^\circ$	$\frac{5}{2} - \frac{5}{2}$		003
	80	186.18	34.689 - 571.804	3d ³ - 3d ² ( ³ F)4p	$a^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		003
	10	186.31	35.120 - 571.845	$3d^3 - 3d^2(^3F)4p$	$a^2D - {}^2D^\circ$	$\frac{3}{2} - \frac{5}{2}$		003
	250	186.49	36.754 - 572.969	3d ³ – 3d ² ( ³ F)4p	a²H – ⁴G°	$\frac{9}{7} - \frac{11}{7}$		003
	10	186.76	35.120 - 570.546	$3d^{3} - 3d^{2}(^{3}F)4p$	$a^2D - {}^2F^\circ$	$\frac{3}{2} - \frac{5}{2}$		003
	10	186.86	34.689 - 569.839	$3d^3 - 3d^2(^3F)4p$	$a^2D - {}^4D^\circ$	$\frac{5}{2} - \frac{3}{2}$		003
	40	186.93	34.689 - 569.667	$3d^3 - 3d^2(^3F)4p$	$a^2D - {}^2D^\circ$	$\frac{5}{2} - \frac{3}{2}$		003
	10	187.08	35.120 - 569.667	$3d^{3} - 3d^{2}(^{3}F)4p$	$a^2D - {}^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$		003
	20	187.20	36.754 - 570.960	3d ³ - 3d ² ( ³ F)4p	$a^{2}H - {}^{4}F^{\circ}$	$\frac{9}{2} - \frac{9}{2}$		003
	10	187.23	34.689 568.746	3d ³ - 3d ² ( ³ F)4p	$a^2D - {}^4F^\circ$	5 - 7		003
	10	187.87	34.689 - 566.964	$3d^3 - 3d^2(^3F)4p$	$a^2D - {}^4G^\circ$	\$ - 7		003
	20	188.06	35.120 - 566.831	$3d^3 - 3d^2(^3F)4p$	$a^2D - {}^4F^\circ$	$\frac{3}{2} - \frac{5}{2}$		003
	150	188.58	35.120 - 565.388	$3d^3 - 3d^2(^3F)4p$	$a^2D - {}^4F^\circ$	$\frac{3}{2} - \frac{3}{2}$		003

# NICKEL IX (Ni ⁸⁺), Z = 28 Ground State $1s^22s^22p^63s^23p^63d^2({}^3F_2)$ (20 electrons) Ionization Potential [1 560 000] cm⁻¹; [193] eV

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	80	101.657	0.0 - 983.704	3p ⁶ ( ¹ S)3d ² - 3p ⁶ ( ¹ S)3d4f	$g^{3}F - {}^{3}G^{\circ}$	2 - 3		207
	80	101.701	1.880 - 985.144	3p6(1S)3d2 - 3p6(1S)3d4f	g ³ F - ³ G°	3 - 4		207
	100	101.846	4.070 - 985.944	3p6(1S)3d2 - 3p6(1S)3d4f	$g^{3}F - {}^{3}G^{\circ}$	4 - 5		207
	20	101.932	4.070 - 985.144	3p ⁶ ( ¹ S)3d ² - 3p ⁶ ( ¹ S)3d4f	$g^{3}F - {}^{3}G^{\circ}$	4 - 4		207
	10	102.283	0.0 - 977.68	3p ⁶ ( ¹ S)3d ² - 3p ⁶ ( ¹ S)3d4f	$g^{3}F - {}^{3}F^{\circ}$	2 - 3		207
	60	102.340	0.0 - 977.13	$3p^{6}(^{1}S)3d^{2} - 3p^{6}(^{1}S)3d4f$	$g^{3}F - {}^{3}F^{\circ}$	2 – 2		207
	1	102.364	1.880 - 978.74	$3p^{6}(^{1}S)3d^{2} - 3p^{6}(^{1}S)3d4f$	$g^{3}F - {}^{3}F^{\circ}$	3 - 4		207
	60	102.480	1.880 - 977.68	$3p^{6}(^{1}S)3d^{2} - 3p^{6}(^{1}S)3d4f$	$g^{3}F - {}^{3}F^{\circ}$	3 - 3		207
	1	102.539	1.880 - 977.13	$3p^{6}(^{1}S)3d^{2} - 3p^{6}(^{1}S)3d4f$	$g^{3}F - {}^{3}F^{\circ}$	3 - 2		207
	100	102.602	4.070 - 978.74	$3p^{6}(^{1}S)3d^{2} - 3p^{6}(^{1}S)3d4f$	$g^{3}F - {}^{3}F^{\circ}$	4-4		207
	1	102.710	4.070 - 977.68	$3p^{6}(^{1}S)3d^{2} - 3p^{6}(^{1}S)3d4f$	$g^{3}F - {}^{3}F^{\circ}$	4 - 3		207
	40	103.428	21.900+X - 988.76+X	3p ⁶ ( ¹ S)3d ² - 3p ⁶ ( ¹ S)3d4f	${}^{1}D - {}^{3}D^{\circ}$	2 - 3		207
	80	103.620	21.900 + X - 986.96 + X	$3p^{6}(^{1}S)3d^{2} - 3p^{6}(^{1}S)3d4f$	'D - 'F°	2 - 3		207
	60	103.871	21.900 + X - 984.63 + X	$3p^{6}(^{1}S)3d^{2} - 3p^{6}(^{1}S)3d4f$	$^{1}\mathbf{D} - ^{1}\mathbf{D}^{\circ}$	2 - 2		207
	1	103.926	17.80 + R - 980.02 + R	$3p^{6}(^{1}S)3d^{2} - 3p^{6}(^{1}S)3d4f$	${}^{3}P - {}^{3}D^{\circ}$	0-1		207
	100	103.981	22.00 + K - 983.71 + K	$3p^{6}(^{1}S)3d^{2} - 3p^{6}(^{1}S)3d4f$	${}^{3}\mathbf{P} - {}^{3}\mathbf{D}^{\circ}$	1-2		207
	100	103.993	27.160 + X - 988.76 + X	$3p^{6}(^{1}S)3d^{2} - 3p^{6}(^{1}S)3d4f$	$^{3}P - ^{3}D^{\circ}$	2-3		207
	10	140.542	0.0 - 711.52	$3p^{6}({}^{1}S)3d^{2} - 3p^{5}({}^{2}P^{\circ})3d^{3}({}^{4}F)$	$g^{3}F - {}^{3}D^{\circ}$	2 - 2		1056

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Multiplet Rel. I	nt. $\lambda_{vac}$ (in Å)	Levels (in 10 ³ cm ¹ )	Configurations	Terms	J - J	Notes	References
85	140.917	1.880 - 711.52	3p ⁶ ( ¹ S)3d ² - 3p ⁵ ( ² P ^o )3d ³ ( ⁴ F)	$g^{3}F - {}^{3}D^{\circ}$	3 - 2		1056
50	141.002	0.0 - 709.21	$3p^{6}(^{1}S)3d^{2} - 3p^{5}(^{2}P^{\circ})3d^{3}(^{4}F)$	$g^{3}F - {}^{3}D^{\circ}$	2 - 1		1056
120	141.356	4.070 - 711.51	$3p^{(1)}S^{(2)}S^{(2)} - 3p^{(2)}S^{(2)}S^{(4)}F^{(4)}$	$g^{3}F - {}^{3}D^{\circ}$	4 - 3		1056
85	147.013	35.898 + C - 716.11 + C	$3p^{6}(^{1}S)3d^{2} - 3p^{5}(^{2}P^{\circ})3d^{3}(^{2}H)$	⁻¹ G - ¹ G°	4 – 4		1056
10	150.32	1.880 - 667.08	$3p^{6}({}^{1}S)3d^{2} - 3p^{5}({}^{2}P^{\circ})3d^{3}({}^{4}F)$	$g^{3}F - {}^{3}F^{\circ}$	3 - 4		1056
10	150.574	0.0 - 664.08	$3p^{6}(^{1}S)3d^{2} - 3p^{5}(^{2}P^{\circ})3d^{3}(^{4}F)$	g ³ F - ³ F°	2 - 3		1056
85	150.836	4.070 - 667.08	3p ⁶ ( ¹ S)3d ² - 3p ⁵ ( ² P ^o )3d ³ ( ⁴ F)	$g^{3}F - {}^{3}F^{\circ}$	4 - 4		1056
85	151.022	1.880 - 664.08	$3p^{6}(^{1}S)3d^{2} - 3p^{5}(^{2}P^{\circ})3d^{3}(^{4}F)$	$g^{3}F - {}^{3}F^{\circ}$	3 - 3		1056
50	151.281	0.0 - 661.05	$3p^{6}(^{1}S)3d^{2} - 3p^{5}(^{2}P^{\circ})3d^{3}(^{4}F)$	$g^{3}F - {}^{3}F^{\circ}$	2 - 2		1056
10	151.700	1.880 - 661.05	$3p^{(1)}S^{(2)}S^{(2)} - 3p^{(2)}S^{(3)}S^{(4)}F^{(4)}$	$g^{3}F - {}^{3}F^{\circ}$	3 - 2		1056
150	165.436	4.070 - 608.53	$3p^{6}(^{1}S)3d^{2} - 3p^{5}(^{2}P^{\circ})3d^{3}(^{2}H)$	$g^{3}F - {}^{3}G^{\circ}$	4 - 5		1056
85	166.079	1.880 - 604.00	3p ⁶ ( ¹ S)3d ² - 3p ⁵ ( ² P ^o )3d ³ ( ² H)	$g^{3}F - {}^{3}G^{\circ}$	3 - 4		1056
85	166.306	0.0 - 601.30	3p ⁶ ( ¹ S)3d ² - 3p ⁵ ( ² P°)3d ³ ( ² H)	$g^{3}F - {}^{3}G^{\circ}$	2 - 3		1056
	1769.	21.900 + X - 78.43 + W	$3p^{6}(^{1}S)3d^{2} - 3p^{6}(^{1}S)3d^{2}$	['] D - 'S	2 - 0	F.P	375,1051
	1772.	22.00 + K - 78.43 + W	$3p^{6}(^{1}S)3d^{2} - 3p^{6}(^{1}S)3d^{2}$	³ P - ³ S	1-0	F,P	375,1051
	1950.	27.160 + X - 78.43 + W	$3p^{(1)}S)3d^{2} - 3p^{(1)}S)3d^{2}$	${}^{3}P - {}^{1}S$	2 - 0	F.P	375,1051

NI IX - Continued

NICKEL X (Ni  $^{9+}$ ), Z = 28 Ground State 1s²2s²2p⁶3s²3p⁶3d(²D_{3/2}) (19 electrons) Ionization Potential [1 812 000] cm⁻¹; [224.6] eV

Muniplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	1	61.809	0.0 - 1617.89	3p^('S)3d - 3p^('S)7f	$g^2D - {}^2F^\circ$	$\frac{3}{2} - \frac{5}{2}$		207
	1	61.915	3.178 - 1618.31	3p*('S)3d – 3p*('S)7f	$g^2D - {}^2F^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		207
	10	66.542	0.0 - 1502.81	3p ⁶ ( ¹ S)3d - 3p ⁶ ( ¹ S)6f	$g^2D - {}^2F^\circ$	$\frac{3}{2} - \frac{5}{2}$		207
	10	66.687	3.178 - 1502.72	3p ⁶ ( ¹ S)3d - 3p ⁶ ( ¹ S)6f	$g^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		207
	20	74.097	0.0 - 1349.58	3p ⁶ ( ¹ S)3d - 3p ⁶ ( ¹ S)5f	$g^2D - {}^2F^\circ$	$\frac{3}{2} - \frac{5}{2}$		207
	30	74.266	3.178 - 1349.69	3p*('S)3d - 3p*('S)5f	$g^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		207
	2	82.892	0.0 - 1206.41	3p^('S)3d – 3p ⁵ 3d('3D°)4s	$g^2D - {}^2D^\circ$	$\frac{3}{2} - \frac{5}{2}$		315
	25	83.108	3.178 - 1206.41	3p ⁶ ( ¹ S)3d - 3p ⁵ 3d( ³ D°)4s	$g^2D - {}^2D^\circ$	$\frac{5}{2} - \frac{5}{2}$		315
	2	83.326	3.178 - 1203.27	3p ⁶ ( ¹ S)3d – 3p ⁵ 3d( ³ D°)4s	$g^2D - {}^2D^\circ$	$\frac{5}{2} - \frac{3}{2}$		315
	10	83.676	3.178 - 1198.26	3p ⁶ ( ¹ S)3d - 3p ⁵ 3d( ¹ F [°] )4s	$g^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		315
	2	84.194	0.0 - 1187.75	3p ⁶ ( ¹ S)3d - 3p ⁵ 3d( ³ D°)4s	$g^2D - {}^4D^\circ$	$\frac{3}{2} - \frac{5}{2}$		315
	5	84.418	3.178 - 1187.75	3p ⁶ ( ¹ S)3d - 3p ⁵ 3d( ³ D [•] )4s	$g^2D - {}^4D^\circ$	$\frac{5}{2} - \frac{5}{2}$		315
	5	84.659	3.178 - 1184.39	3p ⁶ ( ¹ S)3d - 3p ⁵ 3d( ³ D°)4s	g ² D - ⁴ D°	$\frac{5}{2} - \frac{7}{2}$		315
	25	85.523	0.0 - 1169.30	3p ⁶ ( ¹ S)3d - 3p ⁵ 3d( ³ F ^e )4s	$g^2D - {}^2F^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		315
	5	85.753	3.178 - 1169.30	3p ⁶ ( ¹ S)3d - 3p ⁵ 3d( ³ F ^o )4s	$g^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{5}{2}$		315
	60	86.300	3.178 - 1161.93	3p ⁶ ( ³ S)3d – 3p ⁵ 3d( ³ F°)4s	$g^{2}D - {}^{2}F^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		315
	5	86.464	0.0 - 1156.55	3p ⁶ ( ¹ S)3d – 3p ⁵ 3d( ³ F°)4s	g ² D – ⁴ F°	$\frac{3}{2} - \frac{5}{2}$		315
	2	86.865	3.178 - 1154.39	3p ⁶ ( ¹ S)3d - 3p ⁵ 3d( ³ F [*] )4s	g ² D - ⁴ F°	$\frac{5}{2} - \frac{7}{2}$		315
	1	87.077	0.0 - 1148.42	3p ⁶ ( ¹ S)3d - 3p ⁵ 3d( ³ P°)4s	$g^2D - {}^2P^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		315
	25	87.317	3.178 - 1148.42	3p ⁶ ( ¹ S)3d – 3p ⁵ 3d( ³ P°)4s	$g^2D - {}^2P^\circ$	$\frac{5}{2} - \frac{3}{2}$		315
	15	87.680	0.0 - 1140.51	3p*('S)3d – 3p ⁵ 3d('P°)4s	$g^2D - {}^2P^\circ$	$\frac{3}{2} - \frac{1}{2}$		315
	40	91.527	0.0 - 1092.57	3p ⁶ ( ¹ S)3d – 3p ⁶ ( ¹ S)4f	$g^2D - {}^2F^\circ$	$\frac{3}{2} - \frac{5}{2}$		207
	60	91.790	3.178 - 1092.62	3p ⁶ ( ¹ S)3d - 3p ⁶ ( ¹ S)4f	g ² D - ² F°	$\frac{5}{2} - \frac{7}{2}$		207
	10	128.273	0.0 - 779.600	3p ⁶ ( ¹ S)3d - 3p ⁶ ( ¹ S)4p	$g^2D - {}^2P^\circ$	$\frac{3}{2} - \frac{3}{2}$		1085
	120	128.796	3.178 - 779.600	3p*('S)3d – 3p*('S)4p	$g^2D - {}^2P^\circ$	$\frac{5}{2} - \frac{3}{2}$		1085
	70	129.258	0.0 - 773.647	3p ⁶ ('S)3d - 3p ⁶ ('S)4p	$g^2D - {}^2P^\circ$	$\frac{3}{2} - \frac{1}{2}$		1085
	400	144.216	0.0 - 693.404	$3p^{6}(^{1}S)3d - 3p^{5}(^{2}P^{\circ})3d^{2}(^{3}F)$	$g^2D - {}^2D^\circ$	$\frac{3}{2} - \frac{3}{2}$		1085
	100	144.323	0.0 - 692.890	3p ⁶ ( ¹ S)3d - 3p ⁵ ( ² P ⁶ )3d ² ( ³ F)	$g^2D - ^2D^\circ$	$\frac{3}{2} - \frac{5}{2}$		1085
	80	144.880	3.178 - 693.404	3p ⁶ ( ¹ S)3d - 3p ⁵ ( ² P [•] )3d ² ( ³ F)	$g^2D - ^2D^\circ$	$\frac{5}{2} - \frac{3}{2}$		1085
	500	144.988	3.178 - 692.890	$3p^{6}(^{1}S)3d - 3p^{5}(^{2}P^{*})3d^{2}(^{3}F)$	$g^2D - ^2D^\circ$	$\frac{5}{2} - \frac{5}{2}$		1085

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NI X — Continued

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Multiplet Rel. Int.	λ _{vac} (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
100	145.061	0.0 - 689.365	$3p^{6}(^{1}S)3d - 3p^{5}(^{2}P^{\circ})3d^{2}(^{3}P)$	$g^2D - {}^2P^\circ$	$\frac{3}{2} - \frac{3}{2}$		1085
400	145.733	3.178 - 689.365	$3p^{6}(^{1}S)3d - 3p^{5}(^{2}P^{\circ})3d^{2}(^{3}P)$	$g^2D - P^\circ$	$\frac{5}{2} - \frac{3}{2}$		1085
250	146.081	0.0 - 684.552	$3p^{6}(^{1}S)3d - 3p^{5}(^{2}P^{\circ})3d^{2}(^{3}P)$	$g^2D - {}^2P^\circ$	$\frac{3}{2} - \frac{1}{2}$		1085
600	158.377	3.178 - 634.583	$3p^{6}(^{1}S)3d - 3p^{5}(^{2}P^{\circ})3d^{2}(^{3}F)$	$g^2D - {}^2F^\circ$	$\frac{5}{2} - \frac{7}{2}$		1085
600	159.977	0.0 - 625.091	$3p^{6}(^{1}S)3d - 3p^{5}(^{2}P^{\circ})3d^{2}(^{3}F)$	$g^2D - {}^2F^\circ$	$\frac{3}{2} - \frac{5}{2}$		1085
40	160.794	3.178 - 625.091	$3p^{6}(^{1}S)3d - 3p^{5}(^{2}P^{\circ})3d^{2}(^{3}F)$	$g^2D - {}^2F^{\circ}$	$\frac{5}{2} - \frac{5}{2}$		1085
150	184.937	0.0 - 540.725	$3p^{6}(^{1}S)3d - 3p^{5}(^{2}P^{\circ})3d^{2}(^{1}D)$	$g^2D - {}^2F^\circ$	$\frac{3}{2} - \frac{5}{2}$		1085
250	192.599	3.178 - 522.391	$3p^{6}({}^{1}S)3d - 3p^{5}({}^{2}P^{\circ})3d^{2}({}^{1}D)$	$g^2D - F^\circ$	5-7		1085
170	197.405	3.178 - 509.751	$3p^{6}({}^{1}S)3d - 3p^{5}({}^{2}P^{\circ})3d^{2}({}^{1}G)$	$g^2D - F^\circ$	$\frac{5}{2} - \frac{7}{2}$		1085
150	197.909	0.0 - 505.283	$3p^{6}(^{1}S)3d - 3p^{5}(^{2}P^{\circ})3d^{2}(^{1}G)$	$g^2D - {}^2F^\circ$	$\frac{3}{2} - \frac{5}{2}$		1085

# NICKEL XI (Ni¹⁰⁺), Z = 28 Ground State $1s^22s^22p^63s^23p^6(^1S_0)$ (18 electrons) Ionization Potential [2 589 000] cm⁻¹; [321.0] eV

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	20	62.730	0.0 - 1594.13	$3s^23p^6 - 3s^23p^54d$	$g^{1}S - (\frac{1}{2}, \frac{3}{2})^{\circ}$	0 - 1		207
	40	63.641	0.0 - 1571.31	$3s^23p^6 - 3s^23p^54d$	$g^{1}S - (\frac{3}{2}, \frac{5}{2})^{\circ}$	0 - 1		207
	80	77.393	0.0 - 1292.11	$3s^{2}3p^{6} - 3s^{2}3p^{5}(^{2}P_{1/2}^{\circ})4s$	g'S - 111°	0 - 1		207
	60	78.744	0.0 - 1269.94	$3s^23p^6 - 3s^23p^5(^2P_{3/2}^{\circ})4s$	g'S - रेडिंग	0 - 1		207
	30	81.138	469.31 - 1701.8	$3s^{2}3p^{5}3d - 3s^{2}3p^{5}(^{2}P_{3/2}^{\circ})4f$	${}^{3}\mathbf{P}^{\circ} - \frac{1}{2}\left[\frac{3}{2}\right]$	0 - 1		729
	50	81.213	472.95 - 1704.3	$3s^{2}3p^{5}3d - 3s^{2}3p^{5}(^{2}P^{o}_{3/2})4f$	${}^{3}P^{\circ} - \frac{3}{2}\left[\frac{3}{2}\right]$	1 – 2		729
	40	81.378	472.95 - 1701.8	3s ² 3p ⁵ 3d - 3s ² 3p ⁵ ( ² P _{3/2} )4f	${}^{3}\mathbf{P}^{\circ} - \frac{3}{2}\left[\frac{3}{2}\right]$	1 – 1		729
	70	81.468	480.77 - 1708.3	$3s^{2}3p^{5}3d - 3s^{2}3p^{5}(^{2}P_{3/2}^{o})4f$	${}^{3}P^{\circ} - \frac{3}{2} \begin{bmatrix} 5\\2 \end{bmatrix}$	2 - 3		729
	50	81.732	480.77 - 1704.3	$3s^{2}3p^{5}3d - 3s^{2}3p^{5}(^{2}P_{3/2}^{\circ})4f$	${}^{3}\mathbf{P}^{\circ} - \frac{3}{2}\left[\frac{3}{2}\right]$	2 - 2		729
	100	82.417	493.06 - 1706.4	$3s^{2}3p^{5}3d - 3s^{2}3p^{5}(^{2}P_{3/2}^{\circ})4f$	${}^{3}\mathbf{F}^{\circ} - \frac{3}{3}\left[\frac{9}{7}\right]$	4 - 5		729
	70	82.530	496.95 - 1708.6	$3s^{2}3p^{5}3d - 3s^{2}3p^{5}(^{2}P_{3/2}^{\circ})4f$	${}^{3}\mathbf{F}^{\circ} - {}^{3}_{2}[{}^{9}_{2}]$	3 – 4		729
	60	82.625	500.0+S - 1710.3+S	$3s^23p^53d - 3s^23p^5(^2P_{3/2}^{\circ})4f$	${}^{3}\mathbf{F}^{\circ} - {}^{3}_{2}[{}^{7}_{2}]$	2 - 3		729
	10	83.02	534.81 - 1739.4	$3s^{2}3p^{5}3d - 3s^{2}3p^{5}(^{2}P_{1/2}^{\circ})4f$	${}^{3}D^{\circ} - \frac{1}{2} [\frac{5}{2}]$	1 - 2		729
	60	83.139	530.05 - 1732.9	$3s^{2}3p^{5}3d - 3s^{2}3p^{5}(^{2}P_{1/2}^{o})4f$	'D° - 1[5]	2 - 3		729
	40	83.546	539.07 - 1736.0	$3s^{2}3p^{5}3d - 3s^{2}3p^{5}(^{2}P_{1/2}^{\circ})4f$	${}^{3}D^{\circ} - \frac{1}{2}\left[\frac{7}{2}\right]$	2 – 3	í	729
	60	83.798	543.04 - 1736.4	$3s^{2}3p^{5}3d - 3s^{2}3p^{5}(^{2}P_{1/2}^{\circ})4f$	${}^{1}\mathbf{F}^{\circ} - \frac{1}{2} \begin{bmatrix} 2 \\ 2 \end{bmatrix}$	3 - 4		729
	70	84.092	527.22 - 1716.4	$3s^23p^53d - 3s^23p^5(^2P_{3/2}^{\circ})4f$	${}^{3}D^{\circ} - \frac{3}{2} \begin{bmatrix} 7\\2 \end{bmatrix}$	3 – 4		729
	10	85.226	543.04 - 1716.4	$3s^23p^53d - 3s^23p^5(^2P^{o}_{3/2})4f$	${}^{1}\mathbf{F}^{\circ} - \frac{3}{2} \begin{bmatrix} 7\\ 2 \end{bmatrix}$	3 - 4		729
	20	85.798	543.04 - 1708.6	3s ² 3p ⁵ 3d - 3s ² 3p ⁵ ( ² P _{3/2} )4f	${}^{1}\mathbf{F}^{\circ} - \frac{3}{2}\left[\frac{9}{2}\right]$	3 – 4	Q	729
	10	93.85	673.85 - 1739.4	$3s^{2}3p^{5}3d - 3s^{2}3p^{5}(^{2}P_{1/2}^{\circ})4f$	${}^{1}P^{\circ} - \frac{1}{2}[\frac{5}{2}]$	1 – 2		729
	100	148.402	0.0 - 673.85	3s ² 3p ⁶ - 3s ² 3p ⁵ 3d	$g^{1}S - {}^{1}P^{\circ}$	0 – 1		207
		497.8	472.95 - 673.85	3s ² 3p ⁵ 3d - 3s ² 3p ⁵ 3d	${}^{3}\mathbf{P}^{\circ} - {}^{1}\mathbf{P}^{\circ}$	1 – 1	F,P	375,1108
		517.9	480.77 - 673.85	3s ² 3p ⁵ 3d - 3s ² 3p ⁵ 3d	³ P° – ¹ P°	2 – 1	F,P	375,1108
		1427.	472.95 - 543.04	3s²3p⁵3d – 3s²3p⁵3d	${}^{3}\mathbf{P}^{\circ} - {}^{1}\mathbf{F}^{\circ}$	1 – 3	F,P	375,1108
		1433.	469.31 - 539.07	3s ² 3p ⁵ 3d - 3s ² 3p ⁵ 3d	³ P° - ³ D°	0 – 2	F,P	375,1108
		1512.	472.95 - 539.07	3s ² 3p ⁵ 3d - 3s ² 3p ⁵ 3d	³ P° – ³ D°	1 – 2	F,P	375,1108
		1527.	469.31 - 534.81	3s ² 3p ⁵ 3d - 3s ² 3p ⁵ 3d	${}^{3}P^{\circ} - {}^{3}D^{\circ}$	0 – 1	F,P	375,1108
		1606.	480.77 - 543.04	3s ² 3p ⁵ 3d - 3s ² 3p ⁵ 3d	${}^{3}P^{\circ} - {}^{1}F^{\circ}$	2 - 3	F.P	375,1108
		1617.	472.95 - 534.81	$3s^23p^53d - 3s^23p^53d$	${}^{3}P^{\circ} - {}^{3}D^{\circ}$	1 – 1	F.P	375,1108
		1646.	469.31 - 530.05	3s ² 3p ⁵ 3d - 3s ² 3p ⁵ 3d	${}^{3}\mathbf{P}^{\circ} - {}^{1}\mathbf{D}^{\circ}$	0 – 2	F,P	375,1108
		1715.	480.77 - 539.07	3s²3p⁵3d - 3s²3p⁵3d	³ P° – ³ D°	2 – 2	F,P	375,1108
		1751.	472.95 - 530.05	3s ² 3p ⁵ 3d - 3s ² 3p ⁵ 3d	${}^{3}P^{\circ} - {}^{1}D^{\circ}$	1 – 2	F,P	375,1108
		1843.	472.95 - 527.22	3s ² 3p ⁵ 3d - 3s ² 3p ⁵ 3d	${}^{3}P^{\circ} - {}^{3}D^{\circ}$	1 - 3	F,P	375,1108

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References	
		60.02	0.0 - 1666.1	3s ² 3p ⁵ - 3s ² 3p ⁴ ( ³ P)4d	$g^2 P^\circ - {}^2 D$	$\frac{3}{2} - \frac{5}{2}$		854	
		71.4	0.0 - 1401.0	$3s^23p^5 - 3s^23p^4(^1D)4s$	$g^2 P^\circ - {}^2 D$	$\frac{1}{2} - \frac{5}{2}$	1	854	
		72.17	0.0 - 1385.6	$3s^23p^5 - 3s^23p^4(^3P)4s$	$g^2 P^\circ - {}^2 P$	$\frac{3}{2} - \frac{1}{2}$		854	
		72.57	23.52 - 1401.6	$3s^23p^5 - 3s^23p^4(^1D)4s$	$\mathbf{g}^2 \mathbf{P}^\circ - {}^2 \mathbf{D}$	$\frac{1}{2} - \frac{3}{2}$		854	
		72.77	0.0 - 1374.2	$3s^{2}3p^{5} - 3s^{2}3p^{4}(^{3}P)4s$	$\mathbf{g}^2 \mathbf{P}^\circ - \mathbf{P}$	$\frac{3}{2} - \frac{3}{2}$		854	
		74.44	454.00 + X - 1797.4 + X	3s ² 3p ⁴ ( ³ P)3d - 3s ² 3p ⁴ ( ³ P)4f	⁴ D - ⁴ F°	$\frac{1}{2} - \frac{9}{2}$		854	
		75.62	485.57 + X - 1808.0 + X	3s ² 3p ⁴ ( ³ P)3d - 3s ² 3p ⁴ ( ³ P)4f	4F - 4G°	$\frac{9}{2} - \frac{11}{2}$		854	
		75.69	527.23 + X - 1848.4 + X	3s ² 3p ⁴ ( ¹ D)3d - 3s ² 3p ⁴ ( ¹ D)4f	² G – ² H°	$\frac{9}{2} - \frac{11}{2}$		854	
		75.83	492.75 + X - 1811.4 + X	$3s^{2}3p^{4}(^{3}P)3d - 3s^{2}3p^{4}(^{3}P)4f$	⁴ F - ⁴ G°	$\frac{1}{2} - \frac{9}{2}$		854	
	1	147.847	0.0 - 676.37	$3s^23p^5 - 3s^23p^4(^3P)3d$	$g^2 P^\circ - {}^2 D$	$\frac{3}{2} - \frac{3}{2}$		302	
	1	152.152	0.0 - 657.24	$3s^23p^5 - 3s^23p^4(^3P)3d$	$\mathbf{g}^2 \mathbf{P}^\circ - \mathbf{P}$	$\frac{1}{2} - \frac{1}{2}$		302	
	15	152.153	0.0 - 657.23	$3s^23p^5 - 3s^23p^4(^3P)3d$	$\mathbf{g}^{2}\mathbf{P}^{\circ}-^{2}\mathbf{D}$	$\frac{3}{2} - \frac{5}{2}$		302	
	5	153.174	23.52 - 676.37	3s ² 3p ⁵ - 3s ² 3p ⁴ ( ³ P)3d	$g^2 P^\circ - {}^2 D$	$\frac{1}{2} - \frac{3}{2}$		302	
	15	154.175	0.0 - 648.62	3s ² 3p ⁵ - 3s ² 3p ⁴ ( ³ P)3d	$g^2 P^\circ - {}^2 P$	$\frac{1}{2} - \frac{3}{2}$		302	
	2	157.798	23.52 - 657.24	$3s^23p^5 - 3s^23p^4(^{3}P)3d$	$g^2 P^\circ - {}^2 P$	$\frac{1}{2} - \frac{1}{2}$		302	
	1	159.975	23.52 - 648.62	$3s^23p^5 - 3s^23p^4(^3P)3d$	$g^2 P^\circ - {}^2 P$	$\frac{1}{2} - \frac{3}{2}$		302	
	2	160.554	0.0 - 622.84	$3s^23p^5 - 3s^23p^4(^1D)3d$	$g^2 P^\circ - {}^2 S$	$\frac{3}{2} - \frac{1}{2}$		302	
		166.856	23.52 - 622.84	$3s^23p^5 - 3s^23p^4(^1D)3d$	$g^2 P^\circ - {}^2 S$	$\frac{1}{2} - \frac{1}{2}$	Р	375	
		883.4	454.00 + X - 567.20 + X	3s ² 3p ⁴ ( ³ P)3d - 3s ² 3p ⁴ ( ¹ D)3d	${}^{4}D - {}^{2}F$	$\frac{7}{2} - \frac{7}{2}$	F,P	375,1108	
		1225.	485.57 + X - 567.20 + X	$3s^{2}3p^{4}(^{3}P)3d - 3s^{2}3p^{4}(^{1}D)3d$	⁴ <b>F</b> − ² <b>F</b>	$\frac{9}{2} - \frac{7}{2}$	F,P	375,1108	
	ļ	1343.	492.75 + X - 567.20 + X	$3s^{2}3p^{4}(^{3}P)3d - 3s^{2}3p^{4}(^{1}D)3d$	${}^{4}\mathbf{F} - {}^{2}\mathbf{F}$	$\frac{1}{2} - \frac{1}{2}$	F,P	375,1108	
	1	1366.	454.00 + X - 527.23 + X	$3s^{2}3p^{4}(^{3}P)3d - 3s^{2}3p^{4}(^{1}D)3d$	${}^{4}D - {}^{2}G$	$\frac{1}{2} - \frac{9}{2}$	F,P	375,1108	
		1371.	454.00 + X - 526.96 + X	$3s^{2}3p^{4}(^{3}P)3d - 3s^{2}3p^{4}(^{1}D)3d$	${}^{4}D - {}^{2}G$	$\frac{1}{2} - \frac{1}{2}$	F,P	375,1108	
		1687.	454.00 + X - 513.29 + X	$3s^{2}3p^{4}(^{3}P)3d - 3s^{2}3p^{4}(^{3}P)3d$	${}^{4}D - {}^{2}F$	$\frac{1}{2} - \frac{7}{2}$	F,P	375,1108	
		1855.	513.29+X - 567.20+X	3s ² 3p ⁴ ( ³ P)3d - 3s ² 3p ⁴ ( ¹ D)3d	${}^{2}F - {}^{2}F$	$\frac{7}{2} - \frac{7}{2}$	F,P	375,1108	

## NICKEL XII (Ni¹¹⁺), Z = 28 Ground State 1s²2s²2p⁶3s²3p⁵(²P³_{3/2}) (17 electrons) Ionization Potential [2 840 000] cm⁻¹; [352] eV

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# NICKEL XIII (Ni¹²⁺), Z = 28 Ground State $1s^22s^22p^63s^23p^4(^3P_2)$ (16 electrons) Ionization Potential [3 097 000] cm⁻¹; [384] eV

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	1 - 1	Notes	Reference
		56.18	47.0329 - 1827.01	$3s^23p^4 - 3s^23p^3(^2D^\circ)4d$	¹ <b>D</b> - ¹ <b>F</b> °	2 - 3		854
		56.39	47.0329 - 1820.38	$3s^{2}3p^{4} - 3s^{2}3p^{3}(^{2}D^{\circ})4d$	$^{1}D - ^{1}D^{\circ}$	2 - 2		854
		56.57	0 1767.72	$3s^{2}3p^{4} - 3s^{2}3p^{3}(^{4}S^{\circ})4d$	g ³ P - ³ D°	2 - 3		854
		69.25	597.5+D-2041.55+D	3s ² 3p ³ ( ⁴ S°)3d - 3s ² 3p ³ ( ⁴ S°)4f	5D° - 5F	3 - 4		854
		69.37	600.00+D-2041.55+D	3s ² 3p ³ ( ⁴ S°)3d - 3s ² 3p ³ ( ⁴ S°)4f	⁵ D° – ⁵ F	4 - 5		854
		70.07	950.00 + L - 2377.15 + L	$3s^{2}3p^{3}(^{2}D^{\circ})3d - 3s^{2}3p^{3}(^{2}D^{\circ})4f$	³ G° – ³ H	5 - 6		854
		155.12	0 644.66	$3s^23p^4 - 3s^23p^3(^4S^\circ)3d$	$g^{3}P - {}^{3}D^{\circ}$	2 - 2		240
	50	157.55	47.0329 - 681.70	$3s^{2}3p^{4} - 3s^{2}3p^{3}(^{2}D^{\circ})3d$	¹ D - ¹ F°	2-3		240,295
	35	157.730	0 634.00	$3s^23p^4 - 3s^23p^3(^4S^\circ)3d$	$g^{3}P - {}^{3}D^{\circ}$	2-3		856
1	50	158.77	20.0469 - 649.84	$3s^{2}3p^{4} - 3s^{2}3p^{3}({}^{4}S^{\circ})3d$	$g^{3}P - {}^{3}D^{\circ}$	0 - 1		240,256
		159.97	19.5418 - 644.66	$3s^23p^4 - 3s^23p^3(^4S^\circ)3d$	$g^{3}P - {}^{3}D^{\circ}$	1 – 2		240
	50	161.56	47.0329 - 665.95	$3s^23p^4 - 3s^23p^3(^2D^\circ)3d$	$^{1}D - ^{1}D^{\circ}$	2 - 2		240,256
		161.78	97.8362 - 715.95	$3s^23p^4 - 3s^23p^3(^2D^\circ)3d$	¹ S - ¹ P°	0 - 1		240
	35	164.146	0 609.20	$3s^23p^4 - 3s^23p^3(^2D^\circ)3d$	$g^{3}P - {}^{3}P^{\circ}$	2 - 2		856
		303.31	0 329.70	$3s^23p^4 - 3s3p^5$	$g^{3}P - {}^{3}P^{\circ}$	2 - 2		240
		1022.1	0. – 97.8362	$3s^23p^4 - 3s^23p^4$	$g^{3}P - {}^{1}S$	2 - 0	F,P	375,1108
	0	1277.23	19.5418 - 97.8362	$3s^23p^4 - 3s^23p^4$	g ³ P - ¹ S	1-0	F	940
		1968.4	47.0329 - 97.8362	$3s^23p^4 - 3s^23p^4$	ⁱ D - 'S	2-0	F,P	375,1108
		1908.4	47.0329 - 97.8362	- 38°3p - 3	s-эр	s sp D - S	s sp D - 3 2-0	s sp D - S 2 - 0 F,r

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
		62.52	53.5690 - 1653.07	$3s^23p^3 - 3s^23p^24d$	$^{2}D^{\circ} - ^{2}D$	$\frac{5}{2} - \frac{5}{2}$		851
		63.50	53.5690 - 1628.37	$3s^23p^3 - 3s^23p^24d$	$^{2}D^{\circ} - ^{2}P$	$\frac{5}{2} - \frac{3}{2}$		851
		64.79	560. + D - 2103.45 + D	$3s^{2}3p^{2}(^{3}P)3d - 3s^{2}3p^{2}(^{3}P)4f$	⁴ F – ⁴ G°	2 - 11		854
		65.01	580. + R - 2118.2 + R	$3s^{2}3p^{2}(^{3}P)3d - 3s^{2}3p^{2}(^{3}P)4f$	${}^{4}D - {}^{4}F^{\circ}$	$\frac{7}{2} - \frac{9}{2}$		854
		65.40	600. + S - 2129.05 + S	3s ² 3p ² ( ¹ D)3d - 3s ² 3p ² ( ¹ D)4f	$^{2}G - ^{2}H^{\circ}$	2-11		854
		164.146	53.5690 - 662.77	$3s^23p^3 - 3s^23p^2(^1D)3d$	$^{2}D^{\circ} - ^{2}F$	$\frac{5}{2} - \frac{7}{2}$		240
		164.80	85.1267 - 691.88	$3s^{2}3p^{3} - 3s^{2}3p^{2}(^{3}P)3d$	${}^{2}P^{\circ} - {}^{2}D$	$\frac{1}{2} - \frac{3}{2}$		240
		168.12	0. – 594.81	$3s^23p^3 - 3s^23p^2(^3P)3d$	g⁴S° - ⁴P	3-1		240
		168.37	96.6738+X-690.56+X	$3s^23p^3 - 3s^23p^2(^3P)3d$	$^{2}P^{\circ} - ^{2}D$	$\frac{1}{2} - \frac{5}{2}$		240
	30	169.69	0 589.31	$3s^{2}3p^{3} - 3s^{2}3p^{2}(^{3}P)3d$	g⁴S° – ⁴P	$\frac{1}{2} - \frac{3}{2}$	-	240,856
		170.50	45.7678 - 632.29	$3s^{2}3p^{3} - 3s^{2}3p^{2}(^{1}D)3d$	$^{2}\mathbf{D}^{\circ} - ^{2}\mathbf{D}$	$\frac{3}{2} - \frac{3}{2}$		240
	40	171.37	0 583.53	$3s^23p^3 - 3s^23p^2(^3P)3d$	$g^4S^\circ - {}^4P$	$\frac{3}{2} - \frac{5}{2}$		240,856
		172.16	53.5690 - 634.41	3s ² 3p ³ - 3s ² 3p ² ( ¹ D)3d	${}^{2}\mathbf{D}^{\circ} - {}^{2}\mathbf{D}$	$\frac{5}{2} - \frac{5}{2}$		240
		177.28	96.6738 + X - 660.71 + X	$3s^23p^3 - 3s^23p^2(^1D)3d$	$^{2}\mathbf{P}^{\circ} - ^{2}\mathbf{P}$	$\frac{3}{2} - \frac{3}{2}$		240
		177.56	85.1267 - 648.27	$3s^{2}3p^{3} - 3s^{2}3p^{2}(^{1}D)3d$	$^{2}\mathbf{P}^{\circ} - ^{2}\mathbf{P}$	$\frac{1}{2} - \frac{1}{2}$		240
		253.69	53.5690 - 447.74	$3s^{2}3p^{3} - 3s3p^{4}$	${}^{2}D^{\circ} - {}^{2}P$	$\frac{5}{2} - \frac{3}{2}$		240
		292.03	53.5690 - 395.99	$3s^23p^3 - 3s3p^4$	${}^{2}D^{\circ} - {}^{2}D$	5-5		240
		302.27	0 330.83	$3s^23p^3 - 3s3p^4$	$g^4S^\circ - {}^4P$	$\frac{3}{2} - \frac{3}{2}$		240
		316.53	0. – 315.926	$3s^23p^3 - 3s3p^4$	g ⁴ S° – ⁴ P	3-5		240
		1034.41	0. – 96.6738 + X	$3s^{2}3p^{3} - 3s^{2}3p^{3}$	$g^4S^\circ - {}^2P^\circ$	3-3	F,P	726
	0	1174.72	0 85.1267	$3s^{2}3p^{3} - 3s^{2}3p^{3}$	$g^4S^\circ - {}^2P^\circ$	$\frac{1}{2} - \frac{1}{2}$	F	442
	1	1866.75	0 53.5690	$3s^{2}3p^{3} - 3s^{2}3p^{3}$	$g^4S^\circ - {}^2D^\circ$	3-5	F	442
		1964.	45.7678 - 96.6738 + X	$3s^23p^3 - 3s^23p^3$	$^{2}D^{\circ} - ^{2}P^{\circ}$	$\frac{3}{2} - \frac{3}{2}$	F,P	375,726

## NICKEL XIV (Ni¹³⁺), Z = 28 Ground State $1s^22s^22p^63s^23p^3({}^4S_{3/2}^\circ)$ (15 electrons) Ionization Potential [3 470 000] cm⁻¹; [430] eV

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## NICKEL XV (Ni¹⁴⁺), Z = 28 Ground State $1s^22s^22p^63s^23p^2({}^{3}P_0)$ (14 electrons) Ionization Potential [3 740 000] cm⁻¹; [464] eV

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
		49.39	14.9175 - 2039.6	$3s^23p^2 - 3s^23p4d$	$g^{3}P - {}^{3}P^{\circ}$	1-0		970
		49.58	0. – 2016.9	$3s^23p^2 - 3s^23p4d$	$g^{3}P - {}^{3}D^{\circ}$	0 - 1		970
		49.626	27.3765 - 2042.4	$3s^{2}3p^{2} - 3s^{2}3p4d$	$g^{3}P - {}^{3}F^{\circ}$	2 – 3		970
		49.914	14.9175 - 2018.4	$3s^23p^2 - 3s^23p4d$	$g^{3}P - {}^{3}D^{\circ}$	1-2		970
		50.172	27.3765 - 2020.5	$3s^23p^2 - 3s^23p4d$	$g^{3}P - {}^{3}D^{\circ}$	2 - 3		970
		50.249	62.8521 - 2052.9	$3s^23p^2 - 3s^23p4d$	ⁱ D – ⁱ F°	2 - 3		970
		50.947	111.7029+S-2074.5+S	$3s^23p^2 - 3s^23p4d$	'S - 'P°	0-1		970
		58.330	574.33 - 2288.7	$3s^23p3d - 3s^23p4f$	' <b>D</b> ° – 'F	2 – 3		970
		58.715	27.3765 - 1730.52	$3s^23p^2 - 3s^23p4s$	$g^{3}P - {}^{3}P^{\circ}$	2 - 2		970
		59.58	62.8521 - 1741.29	$3s^{2}3p^{2} - 3s^{2}3p4s$	$\mathbf{D} - \mathbf{P}^{\circ}$	2 - 1		854
		60.890	563.82 + D - 2206.1 + D	$3s^23p3d - 3s^23p4f$	${}^{3}F^{\circ} - {}^{3}G$	4 - 5		970
		61.152	570.00 + D - 2205.3 + D	3s ² 3p3d - 3s ² 3p4f	${}^{3}F^{\circ} - {}^{3}G$	3 - 4		970
		62.369	570.00 + R - 2173.4 + R	3s ² 3p3d – 3s ² 3p4f	${}^{3}P^{\circ} - {}^{3}D$	0 - 1		970
		63.069	585.16 - 2170.7	$3s^{2}3p3d - 3s^{2}3p4f$	${}^{3}D^{\circ} - {}^{3}F$	3-4		970
		64.635	638.46 - 2185.7	$3s^23n3d - 3s^23n4f$	¹ F [°] - ¹ G	3-4		970
		65.415	590.0 + K - 2118.7 + K	$3s^23p3d - 3s^23p4f$	$^{1}P^{\circ} - ^{1}D$	1-2		970
		173.73	62.8521 - 638.46	$3s^23p^2 - 3s^23p3d$	'D - 'F°	2 - 3		240
		174.99	14.9175 - 586.41	$3s^23p^2 - 3s^23p3d$	$g^{3}P - {}^{3}D^{\circ}$	1 - 2		240

Multiplet F	Rel. Int.	$\lambda_{\rm vac}$ (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	1 - 1	Notes	References
		176.10	14.9175 - 582.76	$3s^23p^2 - 3s^23p3d$	$g^{3}P - {}^{3}D^{\circ}$	1 - 1		240
		176.70	0 565.93	$3s^23p^2 - 3s^23p3d$	$g^{3}P - {}^{3}P^{\circ}$	0 - 1		240
		178.75	14.9175 - 574.33	$3s^23p^2 - 3s^23p3d$	$g^{3}P - D^{\circ}$	1 - 2		240
		178.87	27.3765 - 586.41	$3s^{2}3p^{2} - 3s^{2}3p3d$	$\mathbf{g}^{3}\mathbf{P} - {}^{3}\mathbf{D}^{\circ}$	2 - 2		240
	20	179.28	27.3765 - 585.16	$3s^23p^2 - 3s^23p3d$	$g^{3}P - {}^{3}D^{\circ}$	2-3	1 1	240,856
		180.06	27.3765 - 582.76	$3s^23p^2 - 3s^23p3d$	$g^{3}P - {}^{3}D^{\circ}$	2 – 1		240
		184.89	14.9175 - 555.84	$3s^23p^2 - 3s^23p3d$	g ³ P - ³ P°	1 - 2		240
		189.21	27.3765 - 555.84	$3s^23p^2 - 3s^23p3d$	$g^{3}P - {}^{3}P^{\circ}$	2 - 2		240
		195.52	62.8521 - 574.33	$3s^23p^2 - 3s^23p3d$	$\mathbf{\tilde{D}} - \mathbf{D}^{*}$	2 - 2		240
		209.18	0 478.01	$3s^23p^2 - 3s3p^3$	$g^{3}P - {}^{3}S^{\circ}$	0 - 1		240
		215.94	14.9175 - 478.01	$3s^23p^2 - 3s3p^3$	$g^{3}P - {}^{3}S^{\circ}$	1 - 1		240
		221.93	27.3765 - 478.01	$3s^23p^2 - 3s3p^3$	$g^{3}P - {}^{3}S^{\circ}$	2 - 1		240
		224.04	62.8521 - 509.22	$3s^23p^2 - 3s3p^3$	'D - 'P°	2 - 1		240
		281.4	62.8521 - 418.24 + M	$3s^23p^2 - 3s3p^3$	'D - 'D°	2 - 2	P	375
		284.2	27.3765 - 379.24 + L	$3s^23p^2 - 3s3p^3$	$g^{3}P - {}^{3}P^{\circ}$	2 - 2	P	375
		311.73	14.9175 - 335.70	$3s^23p^2 - 3s3p^3$	$\mathbf{g}^{3}\mathbf{P} - {}^{3}\mathbf{D}^{\circ}$	1 – 2		240
	200	319.03	27.3765 - 340.84	$3s^23p^2 - 3s3p^3$	$g^{3}P - {}^{3}D^{\circ}$	2-3		437
		1033.	14.9175 – 111.7029 + S	$3s^23p^2 - 3s^23p^2$	g ³ P – 'S	1 – 0	F,P	375,1108
		1186.	27.3765 - 111.7029 + S	$3s^23p^2 - 3s^23p^2$	$g^{3}P - {}^{1}S$	2 - 0	F,P	375,1108

NI XV -- Continued

NICKEL XVI (Ni¹⁵⁺), Z = 28 Ground State  $1s^22s^22p^63s^23p(^2P_{1/2}^{\circ})$  (13 electrons) Ionization Potential [4 020 000] cm⁻¹; [499] eV

Multiplet Rel	. Int. λ	vac (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
		47.184	0.0 - 2119.36	3s ² 3p - 3s ² 4d	$g^2P^\circ - {}^2D$	$\frac{1}{2} - \frac{3}{2}$		854
i i		47.772	27.7614 - 2121.04	$3s^{2}3p - 3s^{2}4d$	$g^2 P^\circ - {}^2 D$	$\frac{3}{2} - \frac{5}{2}$		854
		57.137	1749.82 + S - 3500.00 + S	3s3p3d - 3s3p4f	⁴ F° – ⁴ G	$\frac{9}{2} - \frac{11}{2}$		854
1		57.257	1753.49 + S - 3500.00 + S	3s3p3d - 3s3p4f	⁺F° – ⁴G	$\frac{5}{2} - \frac{7}{2}$		854
		57.349	1756.29 + S - 3500.00 + S	3s3p3d - 3s3p4f	⁺F° – ⁺G	$\frac{1}{2} - \frac{9}{2}$		854
		59.217	539.87 - 2228.57	$3s^23d - 3s^24f$	${}^{2}D - {}^{2}F^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		854
		59.336	543.12 - 2228.49	$3s^23d - 3s^24f$	${}^{2}\mathbf{D} - {}^{2}\mathbf{F}^{\bullet}$	<u>5</u> - 7		854
	1	85.23	0.0 - 539.87	$3s^23p - 3s^23d$	$g^2 P^\circ - {}^2 D$	1 - 3		240
	1	94.04	27.7614 - 543.12	$3s^23p - 3s^23d$	$g^{2}P^{\circ} - {}^{2}D$	3-5		240
	2	18.39	0.0 - 457.90	$3s^23p - 3s3p^2$	$g^2 P^\circ - {}^2 P$	$\frac{1}{2} - \frac{3}{2}$		240
	2	23.09	0.0 - 448.23	$3s^{2}3p - 3s^{2}3p^{2}$	$\mathbf{g}^{2}\mathbf{P}^{\circ} - \mathbf{P}^{2}\mathbf{P}$	$\frac{1}{2} - \frac{1}{2}$		240
	30 2	32.48	27.7614 - 457.90	$3s^23p - 3s3p^2$	$g^2P^\circ - {}^2P$	$\frac{3}{2} - \frac{3}{2}$		437
	50 2	37.84	27.7614 - 448.23	$3s^23p - 3s3p^2$	$g^2 P^\circ - {}^2 P$	$\frac{3}{5} - \frac{1}{5}$		437
	2	39.53	0.0 - 417.48	$3s^23p - 3s3p^2$	$g^2P^\circ - {}^2S$	<u>1</u> - 1		240
	3	09.40	27.7614 - 350.97	$3s^2 3p - 3s 3p^2$	$g^2 P^\circ - {}^2 D$	3-5		240

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# NICKEL XVII (Ni¹⁶⁺), Z = 28 Ground State $1s^22s^22p^63s^2(^1S_0)$ (12 electrons) Ionization Potential 4 607 800 cm⁻¹; 571.30 eV

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	30	12.830	0.0 - 7794.2	$3s^2 - 2p^5 3s^2 3d$	$g^1S - {}^1P^o$	0 - 1		716
		30.91	0.0 - 3235.2	$3s^2 - 3s5n$	$g^{1}S - P^{0}$	0-1		266
	6	33 249	264 62 - 3272 23	$3s_{3n} - 3s_{5d}$	³ P° - ³ D	0-1		237
	2	33 340	27270 - 327210	$3s_{3}p = 3s_{5}d$	$^{3}P^{\circ} - ^{3}D$	1 - 2		237
	3	33 567	293 77 - 3272 89	3s3p = 3s5d	$^{3}P^{\circ} - ^{3}D$	2_3		237
	5	33.507	775 70 2720 4	3.3d 3.6f	3D 3E	2-5		257
		33.90	775.70 - 3720.4	3550 - 3501	D- F	3-4		200
		35.698	293.77 - 3095.05	3s3p - 3s5s	${}^{3}P^{\circ} - {}^{3}S$	2 – 1		851
		38.96	864.52 - 3431.2	3s3d – 3s5f	'D – 'F°	2 - 3		266
	3	39.346	771.23 - 3312.78	3s3d - 3s5f	${}^{3}\mathbf{D} - {}^{3}\mathbf{F}^{\circ}$	1 - 2		237
	6	39.373	773.02 - 3312.81	3s3d - 3s5f	${}^{3}D - {}^{3}F^{\circ}$	2 - 3		237
	10	39.415	775.70 - 3312.83	3s3d – 3s5f	³ D – ³ F°	3 - 4		237
		42.0	293.77 – 2674.8	3s3p - 3p4p	³ P° – ³ D	2 – 3		851
	20	42.855	0.0 - 2333.45	3s ² - 3s4p	g'S – 'P°	0 – 1		237
	6	44.850	264.62 - 2494.25	3s3p - 3s4d	${}^{3}P^{\circ} - {}^{3}D$	0 - 1		237
	10	44,995	272.70 - 2495.34	3s3p - 3s4d	${}^{3}\mathbf{P}^{\circ} - {}^{3}\mathbf{D}$	1 - 2		237
	1	45.018	272.70 - 2494.25	3s3p - 3s4d	${}^{3}\mathbf{P}^{\circ} - {}^{3}\mathbf{D}$	1-1		237
	20	45.382	293.77 - 2497.35	$3s_{3}n - 3s_{4}d$	${}^{3}\mathbf{P}^{\circ} - {}^{3}\mathbf{D}$	2 - 3		237
	6	45 424	293 77 - 2495 34	$3s_{3n} - 3s_{4d}$	$^{3}P^{\circ} = ^{3}D$	2-2		237
	Ŭ	15.121	275.77 2175.51			22		201
		47.663	401.316 - 2499.38	3s3p - 3s4d	$^{1}P^{\circ} - ^{1}D$	1 - 2		854
		50.958	638.87 - 2601.27	3p ² – 3s4f	¹ <b>D</b> - ¹ <b>F</b> °	2 - 3		854
	6	52.000	264.62 - 2187.70	3s3p – 3s4s	³ P° – ³ S	0 - 1		237
	10	52.224	272.70 - 2187.70	3s3p – 3s4s	${}^{3}P^{\circ} - {}^{3}S$	1 - 1		237
	6	52.802	293.77 - 2187.70	3s3p - 3s4s	${}^{3}P^{\circ} - {}^{3}S$	2 - 1		237
		54.384	1059.55 + N - 2898.32 + N	3p3d - 3p4f	${}^{3}F^{\circ} - {}^{3}F$	3 - 4		970
		54.451	1062.60 + D - 2899.11 + D	3n3d - 3n4f	³ F° – ³ G	4 - 5		970
		54.628	$1059.55 \pm N = 2890.11 \pm N$	3n3d - 3n4f	${}^{3}F^{*} - {}^{3}G$	3-4		970
		55.007	1111.00 + L - 2928.95 + L	3p3d - 3p4f	¹ D° – ¹ F	2 - 3		970
	6	55.136	771.23 - 2584.93	3s3d - 3s4f	'D - 'F'	1-2		970.237
	10	55,186	773.02 - 2585.07	3s3d - 3s4f	$^{3}D - ^{3}F^{\circ}$	2-3		970.237
	20	55.258	775.70 - 2585.39	3s3d - 3s4f	³ D - ³ F°	3 - 4		970,237
		55 261	1080 00 1 0 2886 22 1 0	2-2-1 2-46	300 300	0.1		070
		55.501	1080.00 + P - 2880.33 + P	3p3d - 3p4i	P-D	0-1		970
		55.511	1100.00 + P = 2901.44 + P	3p3d - 3p4i	$\mathbf{P} - \mathbf{D}$	1-2		970
		55.000	1103.00 + N = 2903.37 + N	3p3d - 3p4i		2-3		970
		55 022	109.00 + N = 2896.52 + N	3p3d - 3p4i		3-4		970
		56.09	11099.00 + N = 2880.83 + N	3p3d - 3p4i	D - F	1-2		970
		50.08	1105.00+14 - 2888.10+14	5p5d - 5p4i	D-0	2-3		970
		57.348	1200.00+S-2943.74+S	3p3d - 3p4f	¹ <b>F</b> ° – ¹ <b>G</b>	3 - 4		970
		57.573	864.52 - 2601.27	3s3d - 3s4f	'D - 'F°	2 - 3		970
		197.39	264.62 - 771.23	3s3p - 3s3d	'P° – 'D	0 - 1		854
		199.87	272.70 - 773.02	3s3p - 3s3d	' <b>P°</b> – ' <b>D</b>	1 – 2		854
		200.59	272.70 - 771.23	3s3p - 3s3d	'P° – 'D	1 - 1	Р	854
		207.50	293.77 – 775.70	3s3p – 3s3d	'P° – 'D	2 - 3		854
		208.66	293.77 - 773.02	3s3p - 3s3d	³ P° - ³ D	2 – 2		854
		215.89	401.316 - 864.52	3s3p - 3s3d	'P° – 'D	1 – 2		854
		249.180	0.0 - 401.316	$3s^2 - 3s3p$	$g^{1}S - {}^{1}P^{\circ}$	0 - 1		240
		251.97	272.70 - 669.52	$3s3p - 3p^2$	${}^{3}P^{\circ} - {}^{3}P$	1 - 2		854
		263.7	264.62 - 643.84	$3s3p - 3p^2$	³ P° - ³ P	0-1	Р	854
		266.15	293.77 - 669.52	$3s3p - 3p^2$	${}^{3}P^{\circ} - {}^{3}P$	2 - 2		854
		269 44	272 70 - 643 84	$3e^{3}n - 2m^{2}$	3D° 3D	<b>,</b> ,		954
		273.10	272.70 - 043.04	$3c^{2}p - 3p^{-1}$		1-1	P	375 954
		281 50	272.70 - 630.07	$353p - 3p^{-1}$		1-2	r	3/3,834
		201.50	401 214 754 7	$3s_{2}p - 3p^{-1}$	P - P	1-0		854
		205.	401.310 - /34./	$3s3p - 3p^{-}$	P - 'S	1-0	r	3/3,988
		205.00	273.77 - 043.04	$3s3p - 3p^2$	P - P	2-1		834
		207.11	273.77 - 038.87	ssop – sp-	'P' - 'D	2-2	P	3/3,834

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NI XVII - Continued

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	12	366.7 420.96	0.0 - 272.70 401.316 - 638.87	3s² - 3s3p 3s3p - 3p²	g'S - ³ P° ¹ P° - ¹ D	0 - 1 1 - 2	Р	1131 854

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# NICKEL XVIII (Ni¹⁷⁺), Z = 28 Ground State $1s^22s^22p^63s(^2S_{1/2})$ (11 electrons) Ionization Potential 4 896 200 cm⁻¹; 607.06 eV

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
		14.10	0.0 - 7092.	$2p^{6}3s - 2p^{5}3s^{2}$	$g^2S - {}^2P^\circ$	<u><u>+</u>_<u>+</u></u>		265
		14.37	0.0 - 6959.	$2p^63s - 2p^53s^2$	$g^2S - {}^2P^\circ$	$\frac{1}{2} - \frac{3}{2}$		265
	1	24.881	311.976 - 4330.99	$2p^{\circ}3p - 2p^{\circ}8d$	$^{2}P^{\circ} - ^{2}D$	1 - 3		237
	3	25.070	342.501 - 4331.29	$2p^{6}3p - 2p^{6}8d$	$^{2}P^{\circ} - ^{2}D$	3-5		237
	6	26.020	0.0 - 3843.2	$2p^63s - 2p^66p$	$g^2S - {}^2P^\circ$	1-1		237
	3	26.046	0.0 - 3839.36	2p°3s – 2p°6p	$g^2S - {}^2P^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		237
	10	26.218	342.501 - 4156.63	2p ⁶ 3p - 2p ⁶ 7d	$^{2}P^{\circ} - ^{2}D$	$\frac{3}{2} - \frac{5}{2}$		237
		27.98	765.64 - 4339.53	$2p^{6}3d - 2p^{6}8f$	${}^{2}D - {}^{2}F^{\circ}$	3-5		237
	20	27.982	311.976 - 3885.59	$2p^{\circ}3p - 2p^{\circ}6d$	${}^{2}P^{\circ} - {}^{2}D$	$\frac{1}{2} - \frac{1}{2}$		237
	3	28.018	770.30 - 4339.33	$2p^{6}3d - 2p^{6}8f$	${}^{2}D - {}^{2}F^{\circ}$	5 - 7		237
	35	28.220	342.501 - 3886.05	$2p^{\circ}3p - 2p^{\circ}6d$	${}^{2}P^{\circ} - {}^{2}D$	3-5		237
	3	29.383	765.64 - 4168.88	$2p^{b}3d - 2p^{b}7f$	${}^{2}D - {}^{2}F^{*}$	$\frac{3}{2} - \frac{5}{2}$		237
	3	29.422	770.30 - 4169.02	2p°3d - 2p°7f	${}^{2}D - {}^{2}F^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		237
	35	29.779	0.0 - 3358.07	$2p^{\circ}3s - 2p^{\circ}5p$	$g^2S - {}^2P^{\circ}$	$\frac{1}{2} - \frac{3}{2}$		237
	20	29.829	0.0 - 3352.44	$2p^{\circ}3s - 2p^{\circ}5p$	$g^2S - {}^2P^\circ$	$\frac{1}{2} - \frac{1}{2}$		237
	20	31.845	765.64 - 3905.76	2p°3d – 2p°6f	${}^{2}D - {}^{2}F^{\circ}$	3-5		237
	20	31.890	770.30 - 3905.98	$2p^{6}3d - 2p^{6}6f$	${}^{2}D - {}^{2}F^{\circ}$	5 - 7		237
	60	32.034	311.976 - 3433.54	$2p^{\circ}3p - 2p^{\circ}5d$	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{D}$	$\frac{1}{2} - \frac{3}{2}$		237
	90	32.340	342.501 - 3434.60	2p°3p – 2p°5d	$^{2}P^{\circ} - ^{2}D$	$\frac{3}{2} - \frac{5}{2}$		237
	60	36.990	765.64 - 3468.25	2p°3d - 2p°5f	${}^{2}D - {}^{2}F^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		237
	60	37.049	770.30 - 3468.29	2p°3d - 2p°5f	$^{2}D - ^{2}F^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		237
	125	41.015	0.0 - 2438.13	2p'3s - 2p'4p	$g^2S - {}^2P^\circ$	$\frac{1}{2} - \frac{3}{2}$		237
	90	41.218	0.0 - 2426.12	$2p^{6}3s - 2p^{6}4p$	$g^2S - {}^2P^\circ$	$\frac{1}{2} - \frac{1}{2}$		237
	200	43.814	311.976 - 2594.35	2p°3p – 2p°4d	$^{2}\mathbf{P}^{\circ} - ^{2}\mathbf{D}$	$\frac{1}{2} - \frac{3}{2}$		237
	250	44.365	342.501 - 2596.53	2p°3p – 2p°4d	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{D}$	$\frac{3}{2} - \frac{5}{2}$		237
	35	44.405	342.501 - 2594.35	2p ⁶ 3p - 2p ⁶ 4d	${}^{2}P^{\circ} - {}^{2}D$	$\frac{3}{2} - \frac{3}{2}$		237
	20	50.253	311.976 - 2301.63	2p ⁶ 3p - 2p ⁶ 4s	² <b>P</b> ° – ² <b>S</b>	$\frac{1}{2} - \frac{1}{2}$		237
	35	51.042	342.501 - 2301.63	2p°3p – 2p°4s	${}^{2}P^{\circ} - {}^{2}S$	$\frac{3}{2} - \frac{1}{2}$		237
	200	52.615	765.64 - 2666.24	2p*3d - 2p*4f	${}^{2}D - {}^{2}F^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		237
	250	52.720	770.30 - 2667.11	$2p^{6}3d - 2p^{6}4f$	$^{2}\mathbf{D} - ^{2}\mathbf{F}^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		237
		59.950	770.30 - 2438.13	2p°3d – 2p°4p	${}^{2}\mathbf{D} - {}^{2}\mathbf{P}^{\circ}$	$\frac{5}{2} - \frac{1}{2}$		854
		60.212	765.64 - 2426.12	2p°3d – 2p°4p	${}^{2}\mathbf{D} - {}^{2}\mathbf{P}^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		854
	110	114.46	2594.35 - 3468.25	2p°4d – 2p°5f	${}^{2}D - {}^{2}F^{\circ}$	$\frac{3}{2} - \frac{5}{2}$		1091
	110	114.74	2596.53 - 3468.29	2p°4d – 2p°5f	${}^{2}D - {}^{2}F^{\circ}$	$\frac{5}{2} - \frac{7}{2}$		1091
	200	123.965	2666.24 - 3472.92	2p ⁶ 4f - 2p ⁶ 5g	${}^{2}F^{\circ} - {}^{2}G$	$\frac{5}{2} - \frac{7}{2}$	P	753,1091
	200	124.050	2667.11 - 3473.24	2p°4f – 2p°5g	2 <b>F°</b> – 2 <b>G</b>	$\frac{7}{2} - \frac{9}{2}$	Р	753,1091
	85	220.428	311.976 - 765.64	2p°3p – 2p°3d	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{D}$	$\frac{1}{2} - \frac{3}{2}$		753,730
	150	233.756	342.501 - 770.30	2p ⁶ 3p - 2p ⁶ 3d	$^{2}\mathbf{P}^{\circ}-^{2}\mathbf{D}$	$\frac{3}{2} - \frac{5}{2}$		753,730
	3	236.36	342.501 - 765.64	2p°3p – 2p°3d	$^{2}\mathbf{P}^{\circ} - ^{2}\mathbf{D}$	$\frac{3}{2} - \frac{3}{2}$		237
	350	291.970	0.0 - 342.501	2p°3s – 2p°3p	$g^2S - {}^2P^\circ$	$\frac{1}{2} - \frac{3}{2}$		753,730
	300	320.537	0.0 - 311.976	2p ⁶ 3s – 2p ⁶ 3p	$g^2S - {}^2P^\circ$	$\frac{1}{2} - \frac{1}{2}$		753,437

## NICKEL XIX (Ni¹⁸⁺), Z = 28 Ground State $1s^22s^22p^6(^1S_0)$ (10 electrons) Ionization Potential 12 430 000 cm⁻¹; 1541 eV

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
		8.487	0.0 - 11783.	$2s^{2}2p^{6} - 2s^{2}2p^{5}(^{2}P^{o}_{3/2})8d$	$g^{1}S - (\frac{3}{2}, \frac{5}{2})^{\circ}$	0 - 1	Р	643
		8.512	0.0 - 11748.	$2s^22p^6 - 2s^22p^5(^2P_{1/2}^{\circ})7d$	$g^{1}S - (\frac{1}{2}, \frac{3}{2})^{\circ}$	0 - 1	Р	643
		8.614	0.0 - 11609.	$2s^22p^6 - 2s^22p^5(^2P_{3/2}^{\circ})7d$	$g^{1}S - (\frac{3}{2}, \frac{5}{2})^{\circ}$	0 – 1	P	643
	10	8.725	0.0 - 11461.	$2s^{2}2p^{6} - 2s^{2}2p^{5}(^{2}P_{1/2}^{\circ})6d$	$g^{\dagger}S - (\frac{1}{2}, \frac{3}{2})^{\circ}$	0 – 1	]	716
	20	8.838	0.0 - 11315.	$2s^22p^6 - 2s^22p^5(^2P_{3/2}^{\circ})6d$	$g^{1}S - (\frac{3}{2}, \frac{5}{2})^{\circ}$	0 – 1		716
	30	9.130	0.0 - 10953.	$2s^22p^6 - 2s^22p^5(^2P_{1/2}^{\circ})5d$	$g^{1}S - (\frac{1}{2}, \frac{1}{2})^{\circ}$	0 – 1		716
		9.140	0.0 - 10941.	2s ² 2p ⁶ - 2s2p ⁶ 4p	g'S – 'P°	0 – 1		1094
		9.153	0.0 - 10925.	$2s^2 2p^6 - 2s 2p^6 4p$	$g^{t}S - {}^{3}P^{\circ}$	0 - 1		1094
	30	9.236	0.0 - 10827.	$2s^22p^6 - 2s^22p^5(^2P_{3/2}^{\circ})5d$	$g^{1}S - (\frac{3}{2}, \frac{5}{2})^{\circ}$	0-1		716
		9.262	0.0 - 10797.	$2s^2 2p^6 - 2s^2 2p^5 ({}^2P_{3/2}^{\circ})5d$	$g^{1}S - (\frac{3}{2}, \frac{3}{2})^{\circ}$	0-1		1094
	8	9.441			0 0.0			1089
	15	9.545						1089
	30	9.967	0.0 - 10033.	$2s^22p^6 - 2s^22p^5(^2P_{1/2}^{\circ})4d$	$g^{1}S - (\frac{1}{2}, \frac{1}{2})^{\circ}$	0 – 1	Р	643.716
	30	10.102	0.0 - 9899.0	$2s^22p^6 - 2s^22p^5(^2P_{1/2}^a)4d$	$g^{1}S - (\frac{1}{2}, \frac{5}{2})^{\circ}$	0 - 1	-	716
		10,157	0.0 - 9845.4	$2s^22p^6 - 2s^22p^5(^2P_{1/2}^{\circ})4d$	$g^{1}S - (\frac{3}{2}, \frac{3}{2})^{\circ}$	0 - 1		1094
	20	10.306	0.0 - 9703.1	$2s^22p^6 - 2s^22p^5(^2P_{1/2}^{\circ})4s$	$g^{1}S = (\frac{1}{2}, \frac{1}{2})^{\circ}$	0 - 1		716
	20	10.417	0.0 - 9599.7	$2s^22p^6 - 2s^22p^5(^2P_{1/2}^2)4s$	$g^{1}S - (\frac{3}{2}, \frac{1}{2})^{\circ}$	0 - 1		716
	90	11.529	0.0 - 8673.8	2s ² 2p ⁶ – 2s2p ⁶ 3p	$g^{1}S - P^{\circ}$	0 - 1		643
	70	11.587	0.0 - 8630.4	$2s^22p^6 - 2s2p^63p$	g ⁱ S – ³ P°	0 – 1		643
	150	12.430	0.0 - 8045.0	$2s^22p^6 - 2s^22p^5(^2P_{1/2}^{\circ})3p$	$g^{1}S - (\frac{1}{2}, \frac{3}{2})^{\circ}$	0 - 1		643
	120	12.654	0.0 - 7902.6	$2s^22p^6 - 2s^22p^5(^2P_{1/2}^2)$ 3d	$g^{1}S - (\frac{3}{2}, \frac{5}{2})^{\circ}$	0 - 1		643
	50	12.809	0.0 - 7807.0	$2s^{2}2p^{6} - 2s^{2}2p^{5}(^{2}P_{3/2}^{*})3d$	$g^{1}S - (\frac{3}{2}, \frac{3}{2})^{\circ}$	0 – 1		643
	80	13.777	0.0 - 7258.5	$2s^{2}2p^{6} - 2s^{2}2p^{5}(^{2}P_{1/2}^{\circ})3s$	$g^{1}S - (\frac{1}{2},\frac{1}{2})^{\circ}$	0 - 1		643
	100	14.040	0.0 - 7122.5	$2s^{2}2p^{6} - 2s^{2}2p^{5}(^{2}P^{o}_{3/2})3s$	$g^{1}S - (\frac{3}{2}, \frac{1}{2})^{\circ}$	0 – 1		643
	36	14.081	0.0 - 7101.8	$2s^22p^6 - 2s^22p^5(^2P_{3/2}^6)3s$	$g^{1}S - (\frac{3}{2}, \frac{1}{2})^{\circ}$	0-2	F	464
		33.25	7925.9+C - 10933.+C	$2s^22p^53d - 2s^22p^5(^2P_{3/2}^{\circ})5f$	${}^{3}\mathbf{F}^{\circ} - \frac{3}{2}$	4 - 5	Р	1055
		40.650	7436.2+C-9896.2+C	$2s^22p^53p - 2s^22p^54d$	$^{1}\mathbf{P} - ^{1}\mathbf{D}^{\circ}$	1 - 2		395
		40.731	7404.2+C-9859.3+C	$2s^22p^33p - 2s^22p^54d$	${}^{3}D - {}^{3}D^{\circ}$	2 - 3		395
		41.132	7428.1 + C - 9859.3 + C	$2s^22p^53p - 2s^22p^54d$	${}^{3}D - {}^{3}F^{\circ}$	3 – 4		395
		41.385	7453.9+C-9870.2+C	2s ² 2p ⁵ 3p - 2s ² 2p ⁵ 4d	${}^{3}P - {}^{3}F^{\circ}$	2 - 3		395

# NICKEL XX (Ni¹⁹⁺), Z = 28 Ground State $1s^22s^22p^5({}^2P_{3/2}^{\circ})$ ( 9 electrons) Ionization Potential [13 290 000] cm⁻¹; [1648] eV

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	10	9.338	143.980 - 10853.	$2s^22p^5 - 2s^22p^4(^1S)4d$	$g^2 P^\circ - {}^2 D$	$\frac{1}{2} - \frac{3}{2}$		1094,716
	30	9.366	0.0 - 10677.	$2s^22p^5 - 2s^22p^4(^1D)4d$	$g^2 P^\circ - {}^2 F$	3-5		1094,716
		9.385	0.0 - 10655.	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{1}D)4d$	$g^2 P^\circ - {}^2S$	$\frac{3}{2} - \frac{1}{2}$		1094
		9.385	0.0 - 10655.	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{1}D)4d$	$\mathbf{g}^{2}\mathbf{P}^{\circ} - \mathbf{D}$	3-5		1094
	10	9.446	0.0 - 10581.	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{3}P)4d$	$g^2 P^\circ - {}^2 P$	3-3	0	716
		9.455	0.0 - 10576.	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{3}P)4d$	$g^2 P^\circ - {}^4 P$	$\frac{3}{2} - \frac{5}{2}$	ì	1094
	20	9.497	143.980 - 10674.	$2s^22p^5 - 2s^22p^4(^1D)4d$	$g^2 \mathbf{P}^\circ - {}^2 \mathbf{D}$	$\frac{1}{2} - \frac{3}{2}$		1094,716
	30	9.558	0.0 - 10462.	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{3}P)4d$	$g^2P^\circ - {}^2D$	3-3		1094.716
		9.581	143.980 - 10581.	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{3}P)4d$	$g^2 P^\circ - {}^2 P$	1-3		1094
	10	9.630	143.980 - 10530.	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{3}P)4d$	$g^2 P^\circ - {}^4 F$	1 1	o	716
	10	9.693	0.0 - 10317.	$2s^22p^5 - 2s^22p^4(^3P)4s$	$g^2 P^\circ - {}^4 P$	3 - 3	×	1094.716
		9.821	0.0 - 10182.	$2s^22p^5 - 2s^22p^4(^3P)4s$	$\mathbf{g}^2 \mathbf{P}^\circ - \mathbf{P}$	$\frac{3}{2} - \frac{3}{2}$		1094

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NI XX - Continued

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Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm 1 )	Configurations	Terms	J - J	Notes	References
		10.772	0.0 - 9283.3	2s ² 2p ⁵ – 2s2p ⁵ ( ¹ P°)3p	$g^2 P^\circ - {}^2 D$	$\frac{3}{2} - \frac{5}{2}$		1094
		10.918	143.980 - 9303.2	$2s^{2}2p^{5} - 2s^{2}p^{5}(^{1}P^{\circ})3p$	$g^2 P^\circ - {}^2 P$	$\frac{1}{2} - \frac{3}{2}$		1094
		10.936	143.980 - 9288.1	$2s^{2}2p^{5} - 2s^{2}p^{5}(^{1}P^{\circ})3p$	$g^2 P^\circ - {}^2 P$	$\frac{1}{2} - \frac{1}{2}$		1094
		10.982	143.980 - 9249.8	$2s^{2}2p^{5} - 2s^{2}p^{5}(P^{\circ})^{3}p$	$g^2 P^\circ - {}^2 D$	$\frac{1}{2} - \frac{3}{2}$		1094
		11.158	0.0 - 8962.2	$2s^{2}2p^{5} - 2s^{2}p^{5}(^{3}P^{\circ})^{3}p$	$g^2 P^\circ - {}^2 P$	$\frac{3}{2} - \frac{3}{2}$		1094
		11.176	143.980 - 9091.7	2s ² 2p ⁵ - 2s2p ⁵ ( ³ P [•] )3p	$g^2 P^\circ - {}^2 S$	$\frac{1}{2} - \frac{1}{2}$		1094
		11.226	143.980 - 9051.9	2s ² 2p ⁵ – 2s2p ⁵ ( ³ P°)3p	$g^2 P^\circ - {}^2 D$	$\frac{1}{2} - \frac{3}{2}$		1094
		11.282	143.980 - 9007.7	$2s^{2}2p^{5} - 2s^{2}p^{5}(^{3}P^{\circ})3p$	$g^2 P^\circ - {}^4 P$	$\frac{1}{2} - \frac{3}{2}$		1094
	6	11.733	143.980 - 8667.0	$2s^22p^5 - 2s^22p^4(^1S)3d$	$g^2 P^\circ - {}^2 D$	$\frac{1}{2} - \frac{3}{2}$		964
	21	11.779	0.0 - 8495.4	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{1}D)3d$	$g^2 P^\circ - {}^2 P$	$\frac{3}{2} - \frac{1}{2}$		1094,964
		11.787	0.0 - 8483.7	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{1}D)3d$	$\mathbf{g}^{2}\mathbf{P}^{\circ}-^{2}\mathbf{D}$	$\frac{1}{2} - \frac{3}{2}$		1094
	32	11.832	0.0 - 8451.7	$2s^22p^5 - 2s^22p^4(^1D)3d$	$\mathbf{g}^2 \mathbf{P}^\circ - {}^2 \mathbf{D}$	$\frac{3}{2} - \frac{5}{2}$		1094,964
		11.846	0.0 - 8441.7	$2s^22p^5 - 2s^22p^4(^1D)3d$	$g^2 P^\circ - {}^2 P$	$\frac{3}{2} - \frac{3}{2}$		1094
	18	11.874	0.0 - 8422.1	$2s^22p^5 - 2s^22p^4(^{1}D)3d$	$g^2 P^\circ - {}^2 S$	$\frac{3}{2} - \frac{1}{2}$		1094,964
	21	11.961	0.0 - 8360.5	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{3}P)3d$	$g^2 P^\circ - {}^2 D$	3-5		1094,964
	22	11.974	0.0 - 8353.5	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{3}P)3d$	$g^2 P^\circ - {}^2 P$	3-3		1094,964
		11.991	143.980 - 8483.7	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{1}D)3d$	$g^2 P^\circ - {}^2 D$	1		1094
	8	12.006	0.0 - 8329.2	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{3}P)3d$	$g^2 P^\circ - {}^4 D$	$\frac{3}{2} - \frac{3}{2}$		1094,964
	10	12.042	0.0 - 8304.3	$2s^22p^5 - 2s^22p^4(^3P)3d$	$g^2 P^\circ - {}^4 D$	$\frac{3}{2} - \frac{1}{2}$		1094,964
	10	12.079	143.980 - 8422.1	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{1}D)3d$	$g^2 P^\circ - {}^2 S$	$\frac{1}{2} - \frac{1}{2}$		1094,964
	18	12.112	0.0 - 8256.3	$2s^22p^5 - 2s^22p^4(^3P)3d$	$g^2 P^\circ - {}^2 F$	3-5		1094,964
	15	12.130	0.0 - 8244.0	$2s^{2}2p^{5} - 2s^{2}2p^{4}({}^{3}P)3d$	$\mathbf{g}^{2}\mathbf{P}^{\circ} - {}^{4}\mathbf{P}$	$\frac{1}{2} - \frac{1}{2}$		1094,964
	8	12.157	0.0 - 8225.7	$2s^{2}2p^{5} - 2s^{2}2p^{4}({}^{3}P)3d$	$g^2 P^\circ - {}^4 P$	3 - 5		1094,964
	6	12.181	143.980 - 8353.5	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{3}P)3d$	$g^2 P^\circ - {}^2 P$	$\frac{1}{2} - \frac{3}{2}$		1094,964
		12.345	143.980 - 8244.0	2s ² 2p ⁵ - 2s ² 2p ⁴ ( ³ P)3d	g ² P° – ⁴ P	$\frac{1}{2} - \frac{3}{2}$	Q	1094
	9	12.927	0.0 - 7735.7	$2s^22p^5 - 2s^22p^4(^1D)3s$	$g^2 P^\circ - {}^2 D$	$\frac{3}{2} - \frac{5}{2}$		1094,964
	5	13.032	0.0 - 7673.3	$2s^22p^5 - 2s^22p^4(^3P)3s$	$g^2 P^\circ - {}^2 P$	3,-1,		1094,964
	6	13.075	0.0 - 7648.2	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{3}P)3s$	$g^2 P^\circ - {}^4 P$	3-3		1094,964
		13,135	0.0 - 7613.2	$2s^22p^5 - 2s^22p^4(^3P)3s$	$g^2 P^\circ - {}^4 P$	3-1		1094
	7	13.161	143.980 - 7742.2	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{1}D)3s$	$g^2 P^\circ - {}^2 D$	$\frac{1}{2} - \frac{3}{2}$		1094,964
	8	13.256	0.0 - 7543.8	$2s^22p^5 - 2s^22p^4(^3P)3s$	$g^2 P^\circ - {}^2 P$	$\frac{3}{2} - \frac{3}{2}$		1094,964
	5	13.282	143.980 - 7673.3	$2s^{2}2p^{5} - 2s^{2}2p^{4}(^{3}P)3s$	$g^2 P^\circ - {}^2 P$	$\frac{1}{2} - \frac{1}{2}$		1094,964
	10	13.309	0.0 - 7513.7	$2s^22p^5 - 2s^22p^4(^3P)3s$	$g^2 P^\circ - {}^4 P$	$\frac{3}{2} - \frac{5}{2}$		1094,716
		13.39	1202.211 - 8671. + K	2s2p ⁶ - 2s2p ⁵ ( ³ P [°] )3s	${}^{2}S - {}^{2}P^{\circ}$	$\frac{1}{2} - \frac{3}{2}$	P	375
	300	83.180	0.0 - 1202.211	$2s^22p^5 - 2s2p^6$	$g^2P^\circ - {}^2S$	3-1	P	1104,1091
	300	94.497	143.980 - 1202.211	2s ² 2p ⁵ - 2s2p ⁶	$g^2 P^\circ - {}^2 S$	$\frac{1}{2} - \frac{1}{2}$	Р	1104,1091

# NICKEL XXI (Ni²⁰⁺), Z = 28 Ground State 1s²2s²2p⁴(³P₂) ( 8 electrons) Ionization Potential [14 160 000] cm⁻¹; [1756] eV

Multiplet Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
10 20	8.775 8.802 8.849 8.886 8.960 9.016	128.290 - 11524. 128.290 - 11489. 0.0 - 11301. 128.290 - 11394. 212.190 - 11373. 0.0 - 11091.	$\begin{array}{l} 2s^22p^4-2s^22p^3(^2P^{\circ})4d\\ 2s^22p^4-2s^22p^3(^2P^{\circ})4d\\ 2s^22p^4-2s^22p^3(^2P^{\circ})4d\\ 2s^22p^4-2s^22p^3(^2P^{\circ})4d\\ 2s^22p^4-2s^22p^3(^2P^{\circ})4d\\ 2s^22p^4-2s^22p^3(^2S^{\circ})4d \end{array}$	$g^{3}P - {}^{3}D^{\circ}$ $g^{3}P - {}^{3}P^{\circ}$ $g^{3}P - {}^{3}D^{\circ}$ $g^{3}P - {}^{3}D^{\circ}$ ${}^{1}D - {}^{3}F^{\circ}$ $g^{3}P - {}^{3}D^{\circ}$	$ \begin{array}{r} 1 - 2 \\ 1 - 1 \\ 2 - 3 \\ 1 - 1 \\ 2 - 3 \\ 2 - 3 \end{array} $	Q	1094 1094 1094 716 1094 1094,716

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Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
		9.139	128.290 - 11070.	$2s^22p^4 - 2s^22p^3(^4S^\circ)4d$	$g^{3}P - {}^{3}D^{\circ}$	1 - 2		1094
	20	11.023	0.0 - 9071.2	$2s^{2}2p^{4} - 2s^{2}2p^{3}(^{2}P^{\circ})3d$	$g^{3}P - {}^{1}F^{\circ}$	2 - 3	0	716
	0	11.073	92.814 - 9123.7	$2s^22n^4 - 2s^22n^3(^2P^{\circ})$ 3d	$\sigma^3 \mathbf{P} = {}^1 \mathbf{P}^\circ$	0 - 1	ò	716
	20	11 123	0.0 - 8999.8	$2s^22n^4 - 2s^22n^3(^2P^2)$ 3d	$\sigma^{3}\mathbf{P} = {}^{3}\mathbf{P}^{\circ}$	2 - 1	ò	716
	20	11 150	128 200 - 9086 1	$2^{2}2^{2}p^{4} - 2^{2}2^{3}p^{3}({}^{2}\mathbf{P}^{0})^{3}d$	$a^{3}\mathbf{P} = {}^{1}\mathbf{D}^{9}$	1 2	à	716
	20	11.137	0.0 8034.6	$2s^2p = 2s^2p (1)su$	$g^{3}P^{-3}P^{2}$	1-2	Ŷ.	716
	30	11.203	0.0 - 8924.0	2s ⁻ 2p ⁺ - 2s ⁻ 2p ⁺ ( ⁺ P ⁻ )3d	g-P P	2-2	V	/10
		11.229	128.290 - 9033.8	$2s^22p^4 - 2s^22p^3(^2P^{\circ})^{3d}$	$g^{3}P - {}^{3}D^{\circ}$	1 - 2		1094
		11.239	0.0 - 8895.1	2s ² 2p ⁴ – 2s ² 2p ³ ( ² D ^o )3d	g`P – 'F°	2 - 3		1094
	30	11.262	212.190 - 9086.1	2s ² 2p ⁴ – 2s ² 2p ³ ( ² P°)3d	$^{1}\mathbf{D} - ^{1}\mathbf{D}^{\circ}$	2 – 2	Q	716
		11.272	128.290 - 8999.8	2s ² 2p ⁴ - 2s ² 2p ³ ( ² P°)3d	<b>g</b> ³ <b>P</b> – ³ <b>P</b> °	1-1		1094
		11.288	212.190 - 9071.2	$2s^22p^4 - 2s^22p^3(^2P^{\circ})3d$	${}^{1}D - {}^{1}F^{\circ}$	2 – 3		634
	40	11.302	0.0 - 8853.5	$2s^22p^4 - 2s^22p^3(^2D^\circ)3d$	$g^{3}P - {}^{3}D^{\circ}$	2 - 2		1094,716
		11.310	0.0 - 8850.3	$2s^22p^4 - 2s^22p^3(^2D^{\circ})3d$	g ³ P – ¹ P°	2 - 1		634
		11 318	0.0 - 8835 5	$2s^22p^4 = 2s^22p^3(^2D^2)^3d$	$a^3 \mathbf{P} = {}^3 \mathbf{D}^2$	2_3		1094
	214	11.316	0.0 8810.2	$2^{2}2p^{2} - 2^{2}2p^{2}(D) 3^{2}$		2-5		1074
	214	11.330	0.0 - 8819.3	$2s^{2}2p^{2} - 2s^{2}2p^{2}(D)$	g'P - P	2-2		1067
		11.345	0.0 - 8814.5	$2s^{2}2p^{3} - 2s^{2}2p^{3}(^{2}D^{3})3d$	g'P - 'P'	2 - 1		634
		11.416	0.0 - 8759.6	2s ² 2p ⁴ – 2s ² 2p ⁴ ( ² D ² )3d	g'P - 'F'	2 – 3		634
		11.435	128.290 - 8872.3	2s ² 2p ⁴ – 2s ² 2p ³ ( ² D°)3d	g''P – 'S°	1 – 1		634
		11.452	212.190 - 8944.3	2s ² 2p ⁴ - 2s ² 2p ³ ( ² P°)3d	$^{1}D - {}^{3}F^{\circ}$	2 - 2		634
		11.478	212.190 - 8924.6	2s ² 2p ⁴ - 2s ² 2p ³ ( ² P°)3d	$^{1}D - {}^{3}P^{\circ}$	2 – 2	1	1094
		11.517	212.190 - 8895.1	$2s^22p^4 - 2s^22p^3(^2D^\circ)3d$	${}^{1}D - {}^{1}F^{\circ}$	2 - 3	1	1094
		11.539	0.0 - 8666.3	$2s^22p^4 - 2s^22p^3(^4S^{\circ})3d$	$g^{3}P - {}^{3}D^{\circ}$	2-3		1094
		11.656	92 814 - 8672 1	$2s^22p^4 = 2s^22p^3(^4S^2)^3d$	$a^{3}P = {}^{3}D^{\circ}$	0-1		634
	20	11.691	212.190 - 8759.6	$2s^22p^4 - 2s^22p^3(^2D^\circ)3d$	¹ D - ³ F°	2 - 3	Q	716
			010 100 0/7/1					
	00	11.818	212.190 - 8674.1	$2s^{2}2p^{2} - 2s^{2}2p^{2}(-S^{2})3d$	D - D	2-2	V V	/16
		12.079	128.290 - 8407.1	$2s^{2}2p^{4} - 2s^{2}2p^{3}({}^{2}P^{2})3s$	g'P – 'P'	1 - 2		1094
	1	12.181	212.190 - 8421.8	$2s^22p^* - 2s^22p^*(^2P^*)3s$	'D – 'P°	2 – 1		1094
		12.208	0.0 - 8191.3	$2s^22p^4 - 2s^22p^3(^2D^\circ)3s$	$g^{3}P - {}^{3}D^{\circ}$	2 - 3		1094
		12.245	128.290 - 8294.9	$2s^22p^4 - 2s^22p^3(^2P^\circ)3s$	g ³ P - ³ P°	1 – 0		1094
		12.277	0.0 - 8145.3	$2s^22p^4 - 2s^22p^3(^2D^\circ)3s$	$g^{3}P - {}^{3}D^{\circ}$	2 – 2		1094
		12.370	128.290 - 8211.0	$2s^22p^4 - 2s^22p^3(^2D^\circ)3s$	g ³ P – ¹ D°	1-2		1094
		12.435	0.0 - 8035.0	$2s^22n^4 - 2s^22n^3(^4S^\circ)3s$	$\sigma^3 \mathbf{P} = {}^3 \mathbf{S}^\circ$	2 - 1		1094
	30	12 472	128 290 - 8145 3	$2s^2 2n^4 - 2s^2 2n^3 (^2D^2) 3s$	$a^{3}P = {}^{3}D^{2}$	1 - 2		1094 716
		12,502	212,190 - 8211.0	$2s^22p^4 = 2s^22p^3(^2D^2)3s$	יתי - חי	2_2		1094,710
		12 592	92 814 - 8035 0	$2s^2 2p^4 = 2s^2 2p^3 (4S^6) 3s^2$	a ³ D - ³ S°	0-1		1094
		12.656	128.290 - 8035.0	$2s^22p^4 - 2s^22p^3(4S^*)3s$	$g^{3}P - {}^{3}S^{\circ}$	1-1		1094
	50	(0.(2	0.0 1426.25		in in			
	50	09.02	0.0 - 1436.35	2s ² 2p ² - 2s ² 2p ²	g'P - 'P'	2-1		1091
	10	74.45	92.814 - 1430.35	$2s^{2}2p^{2} - 2s^{2}2p^{2}$	g'P - 'P'	0-1		1091
	4	76.45	128.290 - 1436.35	$2s^22p^4 - 2s^2p^3$	<b>g</b> ³ <b>P</b> - ⁴ <b>P</b> [*]	1-1	1	1091
	30	78.28	1125.98 - 2403.45	$2s2p^{\circ} - 2p^{\circ}$	³ P° – 'S	1-0		1091
	250	81.69	212.190 - 1436.35	$2s^22p^4 - 2s^2p^5$	¹ D – ¹ P°	2 – 1		1091
	250	88.81	0.0 - 1125.98	$2s^{2}2p^{4} - 2s^{2}p^{5}$	g ³ P - ³ P°	2 – 1		1091
	200	93.91	128.290 - 1193.14	$2s^22p^4 - 2s2p^5$	$g^{3}P - {}^{3}P^{\circ}$	1-0		1091
	375	95.85	0.0 - 1043.27	$2s^22n^4 - 2s^2n^5$	$\sigma^3 \mathbf{P} = {}^3 \mathbf{P}^{\circ}$	2_2		1091
	250	96 79	92 814 - 1125 98	$2e^{2}2n^{4}$ , $2e^{2}n^{5}$	a3D 3D°	0 1		1001
	110	97.13	406 75 - 1426 25	20 2p - 202p		0-1		1001
	150	100.22	129 200 1125 00	$25^{2}p^{-} - 252p^{-}$	S-P	0-1		1091
	250	100.23	1436.35 - 2403.45	$2s^{2}p^{5} - 2s^{2}p^{5}$ $2s^{2}p^{5} - 2p^{6}$	1 g P - 1 S	1 - 1 1 - 0		1091
				<b>r</b> - <b>r</b>				
	300	109.29	128.290 - 1043.27	$2s^{2}2p^{4} - 2s^{2}p^{5}$	$g^{3}P - {}^{3}P^{\circ}$	1 – 2		1091
	4	109.44	212.190 - 1125.98	$2s^22p^4 - 2s^2p^5$	${}^{1}D - {}^{3}P^{\circ}$	2 – 1		1091
	80	120.33	212.190 - 1043.27	$2s^22p^4 - 2s^2p^5$	¹ D – ³ P°	2 - 2		1091
		245.9	0.0 - 406.75	$2s^22p^4 - 2s^22p^4$	$g^{3}P - {}^{1}S$	2-0	F.P	375,1104
		359.1	128.290 - 406.75	$2s^22p^4 - 2s^22n^4$	$g^{3}P - {}^{4}S$	1-0	F.P	375,1120
		471.3	0.0 - 212.190	$2s^22p^4 - 2s^22p^4$	$g^{3}P - D$	2-2	F	1120
					• •	2-2	•	

#### NI XXI - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	1 - 1	Notes	References
		514.0 779.5 837.69 1077. 1192.	$\begin{array}{c} 212.190-406.75\\ 0.0-128.290\\ 92.814-212.190\\ 0.0-92.814\\ 128.290-212.190\end{array}$	$\begin{array}{r} 2s^22p^4-2s^22p^4\\ 2s^22p^4-2s^22p^4\\ 2s^22p^4-2s^22p^4\\ 2s^22p^4-2s^22p^4\\ 2s^22p^4-2s^22p^4\\ 2s^22p^4-2s^22p^4\\ \end{array}$	${}^{1}D - {}^{1}S$ $g^{3}P - g^{3}P$ $g^{3}P - {}^{1}D$ $g^{3}P - g^{3}P$ $g^{3}P - D$	$ \begin{array}{c} 2 - 0 \\ 2 - 1 \\ 0 - 2 \\ 2 - 0 \\ 1 - 2 \end{array} $	F,P F F,P F,P F,P	375,1104 1120 375,1104 375,1104 375,1104

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# NICKEL XXII (Ni²¹⁺), Z = 28 Ground State $1s^22s^22p^3({}^4S_{3/2})$ ( 7 electrons) Ionization Potential [15 280 000] cm⁻¹; [1894] eV

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	1 - 1	Notes	References
	140	10.791	0.0 - 9267.0	2s ² 2p ³ - 2s ² 2p ² ( ³ P)3d	g ⁴ S° - ⁴ P	$\frac{3}{2} - \frac{5}{2}$		1067
	20	10.820	400.12 - 9642.3	$2s^{2}2p^{3} - 2s^{2}2p^{2}(^{1}S)3d$	$^{2}P^{\circ} - ^{2}D$	$\frac{3}{2} - \frac{5}{2}$		716
	20	10.841	209.38 - 9426.0	$2s^{2}2p^{3} - 2s^{2}2p^{2}(^{1}D)3d$	$^{2}D^{\circ} - ^{2}D$	$\frac{5}{2} - \frac{5}{2}$	Q	716
		10.94	209.38 - 9350.2	2s ² 2p ³ - 2s ² 2p ² ( ³ P)3d	$^{2}\mathbf{D}^{\circ} - ^{2}\mathbf{D}$	$\frac{5}{2} - \frac{5}{2}$	P	877
	20	11.002	209.38 - 9300.3	$2s^{2}2p^{3} - 2s^{2}2p^{2}(^{3}P)3d$	${}^{2}D^{\circ} - {}^{2}F$	$\frac{5}{2} - \frac{7}{2}$	Q	716
		11.170	400.12 - 9350.2	$2s^22p^3 - 2s^22p^2(^3P)3d$	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{D}$	$\frac{3}{2} - \frac{5}{2}$	Q	634
	10	71.48	0.0 - 1398.94	$2s^{2}2p^{3} - 2s^{2}p^{4}$	$g^4S^\circ - {}^2P$	$\frac{3}{2} - \frac{3}{2}$		1091
	4	71.54	943.04 - 2340.89	$2s2p^4 - 2p_c^5$	${}^{4}\mathbf{P} - {}^{2}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{1}{2}$		1091
	30	72.52	157.52 - 1536.48	$2s^{2}2p^{3} - 2s^{2}p^{4}$	${}^{2}D^{\circ} - {}^{2}P$	$\frac{3}{2} - \frac{1}{2}$		1091
	4	74.37	0.0 - 1344.63	$2s^{2}2p^{3} - 2s^{2}p^{4}$	$g^{4}S^{\circ} - {}^{2}S$	$\frac{3}{2} - \frac{1}{2}$		1091
ļ	10	74.49	848.10 - 2190.55	$2s2p^4 - 2p^5$	$^{4}\mathbf{P} - ^{2}\mathbf{P}^{\circ}$	$\frac{5}{2} - \frac{3}{2}$		1091
	4	80.16	943.04 - 2190.55	$2s2p^4 - 2p^5$	${}^{4}\mathbf{P} - {}^{2}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		1091
	50	80.55	157.52 - 1398.94	$2s^22p^3 - 2s^2p^4$	$^{2}D^{\circ} - ^{2}P$	$\frac{3}{2} - \frac{3}{2}$		1091
	4	81.04	302.45 - 1536.48	$2s^{2}2p^{3} - 2s^{2}p^{4}$	$^{2}\mathbf{P}^{\circ} - ^{2}\mathbf{P}$	$\frac{1}{2} - \frac{1}{2}$		1091
	250	84.06	209.38 - 1398.94	$2s^22p^3 - 2s2p^4$	${}^{2}D^{\circ} - {}^{2}P$	$\frac{5}{2} - \frac{3}{2}$		1091
	110	84.24	157.52 - 1344.63	$2s^22p^3 - 2s^2p^4$	${}^{2}D^{\circ} - {}^{2}S$	$\frac{3}{2} - \frac{1}{2}$		1091
	30	85.02	0.0 - 1176.18	$2s^22p^3 - 2s^2p^4$	$g^4S^\circ - {}^2D$	$\frac{3}{2} - \frac{3}{2}$		1091
	50	85.86	1176.18 - 2340.89	$2s2p^4 - 2p^5$	$^{2}\mathbf{D} - ^{2}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{1}{2}$		1091
	250	88.00	400.12 - 1536.48	$2s^22p^3 - 2s^2p^4$	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{P}$	$\frac{3}{2} - \frac{1}{2}$		1091
	50	91.20	302.45 - 1398.94	$2s^22p^3 - 2s^2p^4$	$^{2}\mathbf{P}^{\circ} - ^{2}\mathbf{P}$	$\frac{1}{2} - \frac{3}{2}$		1091
	150	95.95	302.45 - 1344.63	$2s^22p^3 - 2s^2p^4$	${}^{2}P^{\circ} - {}^{2}S$	$\frac{1}{2} - \frac{1}{2}$		1091
	300	98.16	157.52 - 1176.18	$2s^22p^3 - 2s^2p^4$	$^{2}D^{\circ} - ^{2}D$	$\frac{3}{2} - \frac{3}{2}$		1091
	80	98.58	1176.18 - 2190.55	$2s2p^4 - 2p^5$	$^{2}D - ^{2}P^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		1091
	80	100.12	400.12 - 1398.94	$2s^{2}2p^{3} - 2s^{2}p^{4}$	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{P}$	$\frac{3}{2} - \frac{3}{2}$		1091
	300	100.60	209.38 - 1203.46	$2s^{2}2p^{3} - 2s^{2}p^{4}$	${}^{2}D^{\circ} - {}^{2}D$	$\frac{5}{2} - \frac{5}{2}$		1091
	150	101.31	1203.46 - 2190.55	$2s2p^4 - 2p^5$	${}^{2}D - {}^{2}P^{\circ}$	$\frac{5}{2} - \frac{3}{2}$		1091
	110	103.31	0.0 - 967.96	$2s^{2}2p^{3} - 2s^{2}p^{4}$	g ⁴ S° – ⁴ P	$\frac{3}{2} - \frac{1}{2}$		1091
	4	105.88	400.12 - 1344.63	$2s^{2}2p^{3} - 2s^{2}p^{4}$	${}^{2}P^{\circ} - {}^{2}S$	$\frac{3}{2} - \frac{1}{2}$		1091
	375	106.04	0.0 - 943.04	$2s^22p^3 - 2s^2p^4$	g ⁴ S° − ⁴ P	$\frac{3}{2} - \frac{3}{2}$		1091
ĺ	80	106.16	1398.94 - 2340.89	$2s2p^4 - 2p^5$	$^{2}\mathbf{P} - ^{2}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{1}{2}$		1091
	110	114.45	302.45 - 1176.18	$2s^22p^3 - 2s^2p^4$	$^{2}\mathbf{P}^{\circ} - ^{2}\mathbf{D}$	$\frac{1}{2} - \frac{3}{2}$		1091
	300	117.91	0.0 - 848.10	$2s^22p^3 - 2s^2p^4$	g ⁴ S° - ⁴ P	$\frac{3}{2} - \frac{2}{2}$		1091
1	30	118.21	1344.63 - 2190.55	$2s2p^4 - 2p^5$	$^{2}\mathbf{S} - ^{2}\mathbf{P}^{\circ}$	$\frac{1}{2} - \frac{3}{2}$		1091
	50	124.31	1536.48 - 2340.89	$2s2p^4 - 2p^5$	${}^{2}\mathbf{P} - {}^{2}\mathbf{P}^{\circ}$	$\frac{1}{2} - \frac{1}{2}$		1091
	30	124.48	400.12 - 1203.46	$2s^{2}2p^{3} - 2s2p^{4}$	$^{2}\mathbf{P}^{\circ} - ^{2}\mathbf{D}$	$\frac{3}{2} - \frac{5}{2}$		1091
	110	126.32	1398.94 - 2190.55	$2s2p^4 - 2p^5$	${}^{2}\mathbf{P} - {}^{2}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		1091
		249.9	0.0 - 400.12	$2s^22p^3 - 2s^22p^3$	$g^4S^\circ - {}^2P^\circ$	$\frac{3}{2} - \frac{3}{2}$	F,P	375,1091
		330.6	0.0 - 302.45	$2s^{2}2p^{3} - 2s^{2}2p^{3}$	$g^4S^\circ - {}^2P^\circ$	$\frac{3}{2} - \frac{1}{2}$	F,P	375,1091
		412.2	157.52 - 400.12	$2s^22p^3 - 2s^22p^3$	${}^{2}\mathbf{D}^{\circ} - {}^{2}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{3}{2}$	F,P	375,1120
		477.6	0.0 - 209.38	$2s^22p^3 - 2s^22p^3$	$g^4S^\circ - {}^2D^\circ$	$\frac{3}{2} - \frac{5}{2}$	F	1120
-							4 I	
		524.3	209.38 - 400.12	$2s^22p^3 - 2s^22p^3$	$^{2}D^{\circ} - ^{2}P^{\circ}$	$\frac{5}{2} - \frac{3}{2}$	F,P	375,1091

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#### NI XXII - Continued

Multiplet R	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
		689.9 1024. 1074. 1928.	157.52 - 302.45 302.45 - 400.12 209.38 - 302.45 157.52 - 209.38	$\begin{array}{c} 2s^22p^3-2s^22p^3\\ 2s^22p^3-2s^22p^3\\ 2s^22p^3-2s^22p^3\\ 2s^22p^3-2s^22p^3\\ 2s^22p^3-2s^22p^3\\ \end{array}$	${}^{2}D^{\circ} - {}^{2}P^{\circ}$ ${}^{2}P^{\circ} - {}^{2}P^{\circ}$ ${}^{2}D^{\circ} - {}^{2}P^{\circ}$ ${}^{2}D^{\circ} - {}^{2}D^{\circ}$	$\frac{\frac{3}{2} - \frac{1}{2}}{\frac{1}{2} - \frac{3}{2}}$ $\frac{\frac{3}{2} - \frac{3}{2}}{\frac{3}{2} - \frac{5}{2}}$	F,P F,P F,P F,P	375,1091 375,1091 375,1091 375,1091 375,1120

# NICKEL XXIII (Ni²²⁺), Z = 28 Ground State $1s^22s^22p^2({}^{3}P_0)$ ( 6 electrons) Ionization Potential [16 220 000] cm⁻¹; [2011] eV

Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	20	10.450	161.99 - 9739.7	$2s^22p^2 - 2s^22p3d$	$g^{3}P - {}^{3}D^{\circ}$	2 - 3	0	716
	10	10.49	324.64 - 9857.4	$2s^22p^2 - 2s^22p^3d$	${}^{1}D - {}^{1}F^{\circ}$	2 - 3	Q	716
		10.71	941.29 - 10277.7	$2s2p^{3} - 2s2p^{2}(^{4}P)3d$	³ D° – ³ F	3 - 4		877
	20	10.967	109.77 - 9227.7	$2s^22p^2 - 2s^22p^3s$	$g^{3}P - {}^{1}P^{\circ}$	1-1		716
	20	11.403	463.77 - 9227.7	$2s^{2}2p^{2} - 2s^{2}2p^{3}s$	$^{1}S - ^{1}P^{\circ}$	0 - 1	0	716
	30	12.693	1864.71 - 9739.7	$2p^4 - 2s^22p3d$	${}^{3}\mathbf{P} - {}^{3}\mathbf{D}^{\circ}$	2 - 3	Q	716
	10	74.07	109.77 - 1459.67	$2s^22p^2 - 2s^22p^3$	<b>g</b> ³ <b>P</b> – ¹ <b>P</b> °	1 - 1		1091
	4	78.21	586.10 - 1864.71	$2s2p^{3} - 2p^{4}$	⁵S° – ³P	2 – 2		1091
	10	79.99	0.0 - 1250.54	$2s^22p^2 - 2s^2p^3$	g ³ P – ³ S°	0 - 1		1091
	50	87.50	161.99 - 1304.59	$2s^22p^2 - 2s^22p^3$	$g^{3}P - {}^{1}D^{\circ}$	2 – 2		1091
	110	87.66	109.77 - 1250.54	$2s^22p^2 - 2s^2p^3$	$g^{3}P - {}^{3}S^{\circ}$	1 - 1		1091
	10	87.77	941.29 - 2080.63	$2s2p^{3} - 2p^{4}$	${}^{3}\mathbf{D}^{\circ} - {}^{1}\mathbf{D}$	3 – 2		1091
	80	88.11	324.64 - 1459.67	$2s^{2}2p^{2} - 2s^{2}2p^{3}$	¹ D - ¹ P°	2 - 1		1091
	30	90.49	894.24 - 1999.42	$2s2p^{3} - 2p^{4}$	${}^{3}D^{\circ} - {}^{3}P$	1 – 1		1091
	10	90.96	900.06 - 1999.42	$2s2p^{3} - 2p^{4}$	³ D° - ³ P	2 – 1		1091
	150	91.83	161.99 - 1250.54	$2s^22p^2 - 2s2p^3$	g ³ P – ³ S°	2 – 1		1091
	10	92.32	894.24 – 1977.49	$2s2p^{3} - 2p^{4}$	${}^{3}D^{\circ} - {}^{3}P$	1 – 0		1091
	10	92.75	0.0 - 1078.52	$2s^22p^2 - 2s2p^3$	$g^{3}P - {}^{3}P^{\circ}$	0 – 1		1091
	80	100.42	463.77 - 1459.67	$2s^22p^2 - 2s^22p^3$	¹ S – ¹ P°	0 – 1		1091
	30	100.50	109.77 - 1104.93	$2s^22p^2 - 2s^2p^3$	g ³ P - ³ P°	1 – 2		1091
	300	102.08	324.64 - 1304.59	$2s^22p^2 - 2s^2p^3$	¹ D - ¹ D°	2 – 2		1091
	4	102.50	1104.93 - 2080.63	$2s2p^{3} - 2p^{4}$	³ P° – ¹ D	2 – 2		1091
	10	103.07	894.24 - 1864.71	$2s2p^{3} - 2p^{4}$	³ D° - ³ P	1 – 2		1091
	110	103.23	109.77 - 1078.52	$2s^{2}2p^{2} - 2s^{2}2p^{3}$	<b>g</b> ³ <b>P</b> – ³ <b>P</b> °	1 – 1		1091
	50	103.67	900.06 - 1864.71	$2s2p^{3} - 2p^{4}$	³ D° - ³ P	2 - 2		1091
	30	104.70	109.77 - 1064.86	$2s^22p^2 - 2s2p^3$	g ³ P – ³ P°	1 – 0		1091
	375	106.02	161.99 – 1104.93	$2s^22p^2 - 2s^2p^3$	$g^{3}P - {}^{3}P^{\circ}$	2 – 2		1091
	4	107.00	1064.86 - 1999.42	$2s2p^{3} - 2p^{4}$	${}^{3}P^{\circ} - {}^{3}P$	0 – 1		1091
	150	108.27	941.29 - 1864.71	$2s2p^{3} - 2p^{4}$	³ D° – ³ P	3 – 2		1091
	10	109.06	161.99 - 1078.52	$2s^22p^2 - 2s^22p^3$	g ³ P - ³ P°	2 - 1		1091
	80	111.23	1078.52 - 1977.49	$2s2p^{3} - 2p^{4}$	${}^{3}P^{\circ} - {}^{3}P$	1 - 0		1091
	80	111.78	1104.93 - 1999.42	$2s2p^{3} - 2p^{4}$	³ P° ~ ³ P	2 – 1		1091
	200	111.86	0.0 - 894.24	$2s^22p^2 - 2s2p^3$	g ³ P - ³ D°	0 – 1		1091
	30	112.55	1459.67 - 2348.17	$2s2p^{3} - 2p^{4}$	¹ P° - ¹ S	1 - 0		1091
	110	126.54	109.77 - 900.06	$2s^22p^2 - 2s2p^3$	$g^{3}P - {}^{3}D^{\circ}$	1 – 2		1091
	10	127.21	1078.52 - 1864.71	$2s2p^{3} - 2p^{4}$	³ P° – ³ P	1 - 2		1091
	4	127.46	109.77 – 894.24	$2s^22p^2 - 2s2p^3$	g ³ P - ³ D°	1 - 1		1091
	110	128.30	161.99 - 941.29	$2s^{2}2p^{2} - 2s^{2}p^{3}$	g ³ P - ³ D°	2 - 3		1091
	200	128.87	1304.59 - 2080.63	$2s2p^{3} - 2p^{4}$	${}^{i}\mathbf{D}^{\circ} - {}^{1}\mathbf{D}$	2 – 2		1091
	10	131.60	1104.93 - 1864.71	$2s2p^{3} - 2p^{4}$	${}^{3}P^{\circ} - {}^{3}P$	2 - 2		1091
	30	133.54	1250.54 - 1999.42	$2s2p^{3} - 2p^{4}$	${}^{3}S^{\circ} - {}^{3}P$	1 – 1		1091
	10	137.55	1250.54 - 1977.49	$2s2p^{3} - 2p^{4}$	${}^{3}S^{\circ} - {}^{3}P$	1 - 0		1091

NI	XXIII	- Continued
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Multiplet Rel.	Int. λ _{vac} (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
	235.8	161.99 - 586.10	$2s^22p^2 - 2s^2p^3$	g ³ P - ⁵ S°	2 - 2	Р	375,1091
	282.5	109.77 - 463.77	$2s^22p^2 - 2s^22p^2$	$g^{3}P - {}^{1}S$	1-0	F,P	375,1091
	308.0	0.0 - 324.64	$2s^22p^2 - 2s^22p^2$	$g^{3}P - {}^{1}D$	0 - 2	F,P	375,1120
	331.4	161.99 - 463.77	$2s^22p^2 - 2s^22p^2$	$g^{3}P - {}^{1}S$	2 - 0	F,P	375,1120
	465.4	109.77 - 324.64	$2s^22p^2 - 2s^22p^2$	$g^{3}P - D$	1 - 2	F	1120
	614.8	161.99 - 324.64	$2s^22p^2 - 2s^22p^2$	$g^{3}P - D$	2 - 2	F	1120
	617.3	0.0 - 161.99	$2s^22p^2 - 2s^22p^2$	$g^{3}P - g^{3}P$	0 - 2	F,P	375,1120
	718.8	324.64 - 463.77	$2s^22p^2 - 2s^22p^2$	${}^{1}D - {}^{1}S$	2 - 0	F,P	375,1120
	911.0	0.0 - 109.77	$2s^22p^2 - 2s^22p^2$	$g^{3}P - g^{3}P$	0 - 1	F	1120
	1915.0	109.77 - 161.99	$2s^{2}2p^{2} - 2s^{2}2p^{2}$	$g^{3}P - g^{3}P$	1 - 2	F	1120

# NICKEL XXIV (Ni²³⁺), Z = 28 Ground State 1s²2s²2p(²P°_{1/2}) ( 5 electrons) Ionization Potential [17 190 000] cm⁻¹; [2131] eV

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Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
		9.69	0.0 - 10320.	2s ² 2p - 2s2p( ³ P°)3p	$g^2 P^\circ - {}^2 P$	$\frac{1}{2} - \frac{1}{2}$	Р	877
		9.74	163.950 - 10431.	$2s^{2}2p - 2s^{2}p(^{3}P^{\circ})^{3}p$	$g^2 P^\circ - {}^2 P$	$\frac{3}{2} - \frac{3}{2}$	P	877
	0	9.883	843.81 - 10951.	$2s2p^2 - 2s2p(^{1}P^{\circ})3d$	${}^{2}D - {}^{2}D^{\circ}$	$\frac{3}{2} - \frac{5}{2}$	Q	716
		9.90	0.0 - 10101.	$2s^{2}2p - 2s^{2}p(^{3}P^{\circ})^{3}p$	$g^2 P^\circ - {}^2 D$	$\frac{1}{2} - \frac{3}{2}$	P	877
		9.92	163.950 - 10244.	$2s^{2}2p - 2s^{2}p(^{3}P^{\circ})^{3}p$	$g^2 P^\circ - {}^2 D$	$\frac{3}{2} - \frac{5}{2}$	P	877
	2	9.933	884.25 - 10951.	2s2p ² - 2s2p('P°)3d	${}^{2}\mathbf{D} - {}^{2}\mathbf{D}^{\circ}$	$\frac{5}{2} - \frac{5}{2}$		1089
	15	9.966	610.08 + L - 10644. + L	2s2p ² - 2s2p( ³ P°)3d	⁴ P - ⁴ D°	$\frac{5}{2} - \frac{7}{2}$		1089
		10.00	884.25 - 10884.	2s2p ² – 2s2p( ¹ P°)3d	${}^{2}D - {}^{2}F^{\circ}$	$\frac{5}{2} - \frac{7}{2}$	P	877
		10.10	610.08 + L - 10511. + L	2s2p ² - 2s2p( ³ P°)3d	⁴ P – ⁴ P°	2 - 2	P	877
	20	10.195	1143.08 - 10951.	2s2p ² – 2s2p( ¹ P°)3d	$^{2}\mathbf{P} - ^{2}\mathbf{D}^{\circ}$	$\frac{3}{2} - \frac{5}{2}$	Q	716
	10	10.261	843.81 - 10581.	2s2p ² – 2s2p( ³ P°)3d	${}^{2}D - {}^{2}F^{\circ}$	3 - 2	Q	716
		10.35	884.25 - 10546.	$2s2p^2 - 2s2p(^3P^\circ)3d$	$^{2}\mathbf{D} - ^{2}\mathbf{D}^{\circ}$	$\frac{5}{2} - \frac{5}{2}$	P	877
	10	10.680	1143.08 - 10511.+L	2s2p ² - 2s2p( ³ P°)3d	² <b>P</b> – ⁴ <b>P</b> °	$\frac{3}{2} - \frac{5}{2}$	Q	716
	60	11.946	1872.97 - 10244.	$2p^{3} - 2s2p(^{3}P^{\circ})3p$	${}^{2}P^{\circ} - {}^{2}D$	$\frac{3}{2} - \frac{5}{2}$	Q	716
	50	87.50	0.0 - 1143.08	$2s^{2}2p - 2s^{2}p^{2}$	$g^2P^\circ - {}^2P$	$\frac{1}{2} - \frac{3}{2}$	i	1091
	4	88.54	0.0 - 1129.65	$2s^{2}2p - 2s^{2}p^{2}$	$\mathbf{g}^{2}\mathbf{P}^{\circ}-\mathbf{P}$	$\frac{1}{2} - \frac{1}{2}$		1091
	110	97.17	843.81 - 1872.97	$2s2p^2 - 2p^3$	$^{2}\mathbf{D} - ^{2}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		1091
	4	98.39	610.08 + L - 1626.44	$2s2p^2 - 2p^3$	${}^{4}\mathbf{P} - {}^{2}\mathbf{D}^{\circ}$	2 - 2	Q	1091
	10	101.13	884.25 - 1872.97	$2s2p^2 - 2p^3$	${}^{2}D - {}^{2}P^{\circ}$	$\frac{5}{2} - \frac{3}{2}$		1091
	300	102.11	163.950 - 1143.08	$2s^22p - 2s^2p^2$	$g^2 P^\circ - {}^2 P$	2 - 2		1091
	250	103.43	458.10+L - 1424.94+L	$2s2p^2 - 2p^3$	⁴ P – ⁴ S°	$\frac{1}{2} - \frac{2}{2}$		1091
	110	103.53	163.950 - 1129.65	$2s^{2}2p - 2s^{2}p^{2}$	$g^2 P^\circ - {}^2 P$	$\frac{1}{2} - \frac{1}{2}$		1091
	110	104.64	0.0 – 955.73	$2s^22p - 2s^2p^2$	$g^2 P^\circ - {}^2 S$	$\frac{1}{2} - \frac{1}{2}$		1091
	30	106.68	843.81 - 1781.17	$2s2p^2 - 2p^3$	$^{2}D - ^{2}P^{\circ}$	$\frac{2}{2} - \frac{1}{2}$		1091
	10	109.03	955.73 - 1872.97	$2s2p^2 - 2p^3$	² S - ² P°	$\frac{1}{2} - \frac{3}{2}$		1091
	50	113.14	541.08 + L - 1424.94 + L	$2s2p^2 - 2p^3$	*P - *S*	$\frac{2}{2} - \frac{2}{2}$		1091
	80	118.52	0.0 - 843.81	$2s^22p - 2s^2p^2$	$g^2P^\circ - {}^2D$	$\frac{1}{2} - \frac{3}{2}$		1091
	4	121.15	955.73 - 1781.17	$2s2p^2 - 2p^3$	$^{2}S - ^{2}P^{\circ}$	2 - 2		1091
	80	122.72	610.08 + L - 1424.94 + L	$2s2p^2 - 2p^3$	*P - *S*	$\frac{1}{2} - \frac{1}{2}$		1091
	10	127.78	843.81 - 1626.44	$2s2p^2 - 2p^3$	$^{2}D - ^{2}D^{\circ}$	$\frac{2}{2} - \frac{2}{2}$		1091
	10	134.53	1129.65 - 1872.97	$2s2p^2 - 2p^3$	$^{2}\mathbf{P} - ^{2}\mathbf{P}^{\bullet}$	$\frac{1}{2} - \frac{3}{2}$		1091
	50	134.73	884.25 - 1626.44	$2s2p^2 - 2p^3$	$^{2}D - ^{2}D^{\circ}$	2 - 2		1091
	10	135.47	843.81 - 1582.01	$2s2p^2 - 2p^3$	$^{2}D - ^{2}D^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		1091
	10	137.01	1143.08 - 1872.97	$2s2p^2 - 2p^3$	$^{2}\mathbf{P} - ^{2}\mathbf{P}^{\circ}$	$\frac{3}{2} - \frac{3}{2}$		1091
	50	138.80	163.950 - 884.25	$2s^{2}2p - 2s^{2}p^{2}$	$g^2 P^\circ - {}^2 D$	$\frac{1}{2} - \frac{5}{2}$		1091
	10	143.30	884.25 - 1582.01	$2s2p^2 - 2p^3$	² D – ² D°	$\frac{5}{2} - \frac{3}{2}$		1091

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NI XXIV - Continued

Multiplet Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in 10 ³ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
4	159.69 609.9	955.73 - 1582.01 0.0 - 163.950	$2s2p^2 - 2p^3$ $2s^22p - 2s^22p$	$\frac{{}^{2}\mathbf{S} - {}^{2}\mathbf{D}^{\circ}}{\mathbf{g}^{2}\mathbf{P}^{\circ} - \mathbf{g}^{2}\mathbf{P}^{\circ}}$	$\frac{1}{2} - \frac{3}{2}$ $\frac{1}{2} - \frac{3}{2}$	F	1091 1120

# NICKEL XXV (Ni²⁴⁺), Z = 28 Ground State $1s^22s^2(^1S_0)$ ( 4 electrons) Ionization Potential [18 510 000] cm⁻¹; [2295] eV

Aultiplet Re	el. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm $^{-1}$ )	Configurations	Terms	J - J	Notes	Reference
	2	9.194	419.19 - 11306.	1s ² 2s2p - 1s ² 2p3p	³ P° - ³ S	1 - 1	Q	1089
	0	9.215	419.19 - 11271.	$1s^22s2p - 1s^22p3p$	${}^{3}P^{\circ} - {}^{3}P$	1 – 2		643
	5	9.238	378.63 - 11206.	$1s^22s2p - 1s^22p3p$	${}^{3}P^{\circ} - {}^{3}P$	0-1	Q	1089
	11	9.297	549.98 - 11306.	$1s^22s2p - 1s^22p3p$	${}^{3}P^{\circ} - {}^{3}S$	2 – 1		1057
	16	9.306	549.98 - 11296.	$1s^22s2p - 1s^22p3p$	${}^{3}P^{\circ} - {}^{3}D$	2 - 3		1057
	12	9.316	419.19 - 11153.	$1s^22s2p - 1s^22p3p$	${}^{3}P^{\circ} - {}^{3}D$	1 – 2		1057
	15	9.340	0.0 - 10707.	$1s^22s^2 - 1s^22s^3p$	$g^{1}S - {}^{1}P^{\circ}$	0 - 1		1057
	30	9.355	378.63 - 11068.	1s ² 2s2p – 1s ² 2p3p	³ P° – ³ D	0 - 1		643
	8	9.39	0.0 - 10650.	$1s^22s^2 - 1s^22s^3p$	$g^1S - {}^3P^\circ$	0 – 1		1057
	10	9.407	848.10 - 11478.	$1s^22s2p - 1s^22s3s$	¹ P° – ¹ S	1-0		643
		9.471	848.10 - 11407.	$1s^22s^2p - 1s^22p^3p$	${}^{1}\mathbf{P}^{\bullet} - {}^{1}\mathbf{D}$	1 – 2	Р	619
	18	9.601	378.63 - 10795.	$1s^22s2p - 1s^22s3d$	${}^{3}P^{\circ} - {}^{3}D$	0 – 1		1057
	30	9.633	419.19 - 10800.	$1s^22s2p - 1s^22s3d$	³ P° - ³ D	1 - 2		1057
	30	9.695	848.10 - 11163.	1s ² 2s2p - 1s ² 2p3p	$^{1}\mathbf{P}^{\circ} - ^{1}\mathbf{P}$	1 – 1		643
	18	9.707	1154.73 – 11456.	1s ² 2p ² – 1s ² 2p3d	${}^{3}\mathbf{P} - {}^{3}\mathbf{P}^{\circ}$	1 - 2		1057
	45	9.744	549.98 - 10812.	1s ² 2s2p – 1s ² 2s3d	${}^{3}P^{\circ} - {}^{3}D$	2 – 3		1057
	20	9.753	549.98 - 10800.	$1s^22s2p - 1s^22s3d$	³ P° – ³ D	2 - 2		1057
	20	9.759	1208.29 – 11456.	$1s^{2}2p^{2} - 1s^{2}2p3d$	³ <b>P</b> - ³ <b>P</b> °	2 – 2		1057
	45	9.776	1208.29 - 11437.	$1s^22p^2 - 1s^22p3d$	${}^{3}P - {}^{3}D^{\circ}$	2 - 3		1057
	60	9.860	1379.65 – 11521.	$1s^22p^2 - 1s^22p3d$	¹ D - ¹ F°	2 – 3		1057
	30	9.873	1208.29 - 11343.	1s ² 2p ² - 1s ² 2p3d	${}^{3}P - {}^{3}D^{\circ}$	2 - 2		1057
	20	9.934	1208.29 - 11270.	1s ² 2p ² – 1s ² 2p3d	${}^{3}P - {}^{3}F^{\circ}$	2 – 3		643
	80	9.967	848.10 - 10878.	$1s^22s2p - 1s^22s3d$	¹ <b>P</b> [•] - ¹ <b>D</b>	1 - 2		643
	80	10.103	549.98 - 10449.	$1s^22s2p - 1s^22s3s$	${}^{3}P^{\circ} - {}^{3}S$	2 - 1		643
	10	10.276	1379.65 - 11110.	$1s^22p^2 - 1s^22p3s$	${}^{1}D - {}^{1}P^{\circ}$	2 - 1		643
	20	10.354	1048.75 – 10707.	$1s^22p^2 - 1s^22s3p$	${}^{3}\mathbf{P} - {}^{4}\mathbf{P}^{\circ}$	0 - 1	Q	716
	20	10.529	1611.52 – 11110.	$1s^22p^2 - 1s^22p3s$	¹ S – ¹ P°	0 - 1		643
	10	10.724	1379.65 – 10707.	$1s^22p^2 - 1s^22s3p$	$^{1}D - ^{1}P^{\circ}$	2 – 1	Q	716
	300	117.91	0.0 - 848.10	$1s^22s^2 - 1s^22s2p$	$g^{T}S - {}^{T}P^{\circ}$	0 - 1	[ ]	1091
	30	120.53	549.98 - 1379.65	$1s^22s^2p - 1s^22p^2$	${}^{3}\mathbf{P}^{\circ} - {}^{1}\mathbf{D}$	2 - 2		1091
	30	126.73	419.19 - 1208.29	$1s^22s2p - 1s^22p^2$	${}^{3}P^{\circ} - {}^{3}P$	1 - 2		1091
	200	128.85	378.63 - 1154.73	$1s^22s2p - 1s^22p^2$	³ P° – ³ P	0 – 1		1091
	10	130.99	848.10 - 1611.52	$1s^22s2p - 1s^22p^2$	¹ P° – ¹ S	1 – 0		1091
	10	135.95	419.19 - 1154.73	$1s^22s2p - 1s^22p^2$	${}^{3}P^{\circ} - {}^{3}P$	1 – 1		1091
	30	151.90	549.98 - 1208.29	$1s^22s2p - 1s^22p^2$	${}^{3}P^{\circ} - {}^{3}P$	2 - 2		1091
	4	158.84	419.19 – 1048.75	$1s^22s2p - 1s^22p^2$	${}^{3}\mathbf{P}^{\circ} - {}^{3}\mathbf{P}$	1 – 0		1091
	10	165.36	549.98 - 1154.73	$1s^22s2p - 1s^22p^2$	³ <b>P°</b> – ³ <b>P</b>	2 - 1		1091
	10	188.13	848.10 - 1379.65	$1s^22s2p - 1s^22p^2$	¹ P° – ¹ D	1 – 2		1091
		238.56	0.0 - 419.19	$1s^22s^2 - 1s^22s^2n$	$\sigma^1 S = {}^3 P^{\circ}$	0-1	р	375 1091

#### NICKEL XXVI (Ni²⁵⁺), Z = 28 Ground State $1s^22s(^2S_{1/2})$ ( 3 electrons) Ionization Potential 19 351 000 cm⁻¹; 2399.2 eV

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Multiplet	Rel. Int.	λ _{vac} (in Å)	Levels (in $10^3$ cm 3 )	Configurations	Terms	J - J	Notes	References
		6.811	0.0 - 14682.	1s ² 2s - 1s ² 4p	$g^2S - {}^2P^\circ$	$\frac{1}{2} - \frac{3}{2}$	Р	977
		6.821	0.0 - 14661.	$1s^{2}2s - 1s^{2}4p$	$g^2S - {}^2P^\circ$	$\frac{1}{2} - \frac{1}{2}$	P	977
		7.006	426.98 - 14700.	$1s^{2}2p - 1s^{2}4d$	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{D}$	1 - 3	P	977
		7.048	426.98 - 14615.	$1s^{2}2p - 1s^{2}4s$	${}^{2}P^{\circ} - {}^{2}S$	<u>1</u> - <u>1</u>	Р	977
		7.091	604.52 - 14707.	$1s^{2}2p - 1s^{2}4d$	${}^{2}P^{\circ} - {}^{2}D$	3-5	P	977
		7.138	604.52 - 14615.	$1s^22p - 1s^24s$	² <b>P°</b> – ² <b>S</b>	$\frac{1}{2} - \frac{1}{2}$	Р	977
	14	9.061	0.0 - 11036.	$1s^{2}2s - 1s^{2}3p$	$g^2S - {}^2P^\circ$	1-3		1057
	9	9.105	0.0 - 10983.	$1s^{2}2s - 1s^{2}3p$	$g^2S - {}^2P^\circ$	<u>1</u> - <u>1</u>		1057
	27	9.390	426.98 - 11077.	$1s^{2}2p - 1s^{2}3d$	${}^{2}P^{\circ} - {}^{2}D$	1-3		1057
	39	9.535	604.52 - 11092.	$1s^{2}2p - 1s^{2}3d$	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{D}$	3-5		1057
	9	9.55	604.52 - 11077.	$1s^{2}2p - 1s^{2}3d$	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{D}$	3-3		1057
	2	9.564	426.98 - 10880.	$1s^{2}2p - 1s^{2}3s$	$^{2}\mathbf{P}^{\circ}-^{2}\mathbf{S}$	$\frac{1}{2} - \frac{1}{2}$	Q	1089
	4	9.732	604.52 - 10880.	$1s^22p - 1s^23s$	² <b>P°</b> – ² <b>S</b>	3-1		1057
		165.42	0.0 - 604.52	$1s^{2}2s - 1s^{2}2p$	$g^2S - {}^2P^{\circ}$	1-3		730
	85	234.20	0.0 - 426.98	$1s^22s - 1s^22p$	$g^2S - {}^2P^\circ$	$\frac{1}{2} - \frac{1}{2}$		730

## NICKEL XXVII (Ni²⁶⁺), Z = 28 Ground State $1s^2({}^{1}S_0)$ ( 2 electrons) Ionization Potential 82 990 000 cm⁻¹; 10289.5 eV

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm ⁻¹ )	Configurations	Terms	J - J	Notes	References
		1.238	0.0 - 80745.	1s ² – 1s6p	$g^{1}S - {}^{3}P^{\circ}$	0 - 1	Р	728
		1.254	0.0 - 79762.64	$1s^2 - 1s5p$	$g^1S - {}^3P^{\circ}$	0 - 1	P	728
		1.283	0.0 - 77938.24	$1s^2 - 1s4p$	$g^{1}S - {}^{3}P^{\circ}$	0 - 1	P	728
		1.350	0.0 - 74076.25	$1s^2 - 1s3p$	g'S - P'	0 - 1	Р	728
		1.352	0.0 - 73985.01	$1s^2 - 1s3p$	$g^{i}S - {}^{3}P^{\circ}$	0 – 1	Р	728
	3	1.588	0.0 - 62961.52	$1s^2 - 1s2p$	$g^{1}S - P^{\circ}$	0 - 1	Р	856
		1.596	0.0 - 62644.18	1s ² - 1s2p	$g^1S - {}^3P^{\circ}$	0 - 1	Р	839
		1.603	0.0 - 62367.86	$1s^2 - 1s2s$	$g^{1}S - {}^{3}S$	0 – 1	F,P	1105

#### NICKEL XXVIII (Ni²⁷⁺), Z = 28 Ground State 1s( $^{2}S_{1/2}$ ) (1 electron) Ionization Potential 86 908 200 cm⁻¹; 10775.3 eV

Levels (in $10^3$ cm 1 )	Configurations	Terms	J - J	Notes	References
0.0 - 83456.7830	1s – 5p	${}^{2}S - {}^{2}P^{\circ}$	$\frac{1}{2} - \frac{3}{2}$	Р	1042
0.0 - 81513.5300	1s - 4p	${}^{2}S - {}^{2}P^{\circ}$	$\frac{1}{2} - \frac{3}{2}$	Р	1042
0.0 - 77315.6040	1s - 3p	${}^{2}S - {}^{2}P^{\circ}$	$\frac{1}{2} - \frac{3}{2}$	Р	1042
0.0 - 77247.1100	1s - 3p	² S – ² P°	$\frac{1}{2} - \frac{1}{2}$	Р	1042
0.0 - 65343.7700	1s - 2p	${}^{2}S - {}^{2}P^{\circ}$	$\frac{1}{2} - \frac{3}{2}$	Р	1042
0.0 - 65112.8100	1s - 2p	${}^{2}S - {}^{2}P^{\circ}$	$\frac{1}{2} - \frac{1}{2}$	P	1042
	Levels (in 10 ³ cm ⁻¹ ) 0.0 - 83456.7830 0.0 - 81513.5300 0.0 - 77315.6040 0.0 - 77247.1100 0.0 - 65343.7700 0.0 - 65112.8100	Levels (in $10^{3}$ cm 1 )Configurations $0.0 - 83456.7830$ $1s - 5p$ $0.0 - 81513.5300$ $1s - 4p$ $0.0 - 77315.6040$ $1s - 3p$ $0.0 - 77247.1100$ $1s - 3p$ $0.0 - 65343.7700$ $1s - 2p$ $0.0 - 65112.8100$ $1s - 2p$	Levels (in $10^{1}$ cm 1 )ConfigurationsTerms $0.0 - 83456.7830$ $1s - 5p$ $^{2}S - ^{2}P^{\circ}$ $0.0 - 81513.5300$ $1s - 4p$ $^{2}S - ^{2}P^{\circ}$ $0.0 - 77315.6040$ $1s - 3p$ $^{2}S - ^{2}P^{\circ}$ $0.0 - 77247.1100$ $1s - 3p$ $^{2}S - ^{2}P^{\circ}$ $0.0 - 65343.7700$ $1s - 2p$ $^{2}S - ^{2}P^{\circ}$ $0.0 - 65112.8100$ $1s - 2p$ $^{2}S - ^{2}P^{\circ}$	Levels (in 10 ³ cm 1 )ConfigurationsTermsJ - J0.0 - 83456.78301s - 5p $^{2}S - ^{2}P^{o}$ $\frac{1}{2} - \frac{3}{2}$ 0.0 - 81513.53001s - 4p $^{2}S - ^{2}P^{o}$ $\frac{1}{2} - \frac{3}{2}$ 0.0 - 77315.60401s - 3p $^{2}S - ^{2}P^{o}$ $\frac{1}{2} - \frac{3}{2}$ 0.0 - 77247.11001s - 3p $^{2}S - ^{2}P^{o}$ $\frac{1}{2} - \frac{3}{2}$ 0.0 - 65343.77001s - 2p $^{2}S - ^{2}P^{o}$ $\frac{1}{2} - \frac{3}{2}$ 0.0 - 65112.81001s - 2p $^{2}S - ^{2}P^{o}$ $\frac{1}{2} - \frac{1}{2}$	Levels (in $10^3$ cm 1 )ConfigurationsTermsJ - JNotes $0.0 - 83456.7830$ $1s - 5p$ $^2S - ^2P^\circ$ $\frac{1}{2} - \frac{3}{2}$ P $0.0 - 81513.5300$ $1s - 4p$ $^2S - ^2P^\circ$ $\frac{1}{2} - \frac{3}{2}$ P $0.0 - 77315.6040$ $1s - 3p$ $^2S - ^2P^\circ$ $\frac{1}{2} - \frac{3}{2}$ P $0.0 - 77247.1100$ $1s - 3p$ $^2S - ^2P^\circ$ $\frac{1}{2} - \frac{1}{2}$ P $0.0 - 65343.7700$ $1s - 2p$ $^2S - ^2P^\circ$ $\frac{1}{2} - \frac{3}{2}$ P $0.0 - 65112.8100$ $1s - 2p$ $^2S - ^2P^\circ$ $\frac{1}{2} - \frac{1}{2}$ P

#### NI XXVIII -- Continued

Multiplet Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	5.453	65118.9400 - 83456.7830	2s - 5p	$^{2}S - ^{2}P^{\circ}$	$\frac{1}{2} - \frac{3}{2}$	Р	1042
	5.519	65343.7700 - 83461.5951	2p - 5d	$^{2}P^{\circ} - ^{2}D$	3-5	Р	1042
	6.100	65118.9400 - 81513.5300	2s – 4p	² S – ² P°	$\frac{1}{2} - \frac{1}{2}$	P	1042
	6.181	65343.7700 - 81522.9289	2p – 4d	${}^{2}P^{\circ} - {}^{2}D$	$\frac{3}{2} - \frac{5}{2}$	Р	1042
	8.199	65118.9400 - 77315.6040	2s - 3p	${}^{2}S - {}^{2}P^{\circ}$	1 - 3	P	1042
ļ	8.337	65343.7700 - 77337.8641	2p - 3d	${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{D}$	3-5	P	1042
	8.337	65343.7700 - 77337.8641	2p - 3d	$^{2}\mathbf{P}^{\circ}-^{2}\mathbf{D}$	$\frac{3}{2} - \frac{5}{2}$	P	10

D. Magnetic Dipole Lines for Nickel Ions (Wavelengths, Classifications, and Transition Probabilities)

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#### D. Magnetic Dipole Lines for Nickel lons

[Excerpted from: V. Kaufman and J. Sugar, J. Phys. Chem. Ref. Data 15, 321 (1986)]

#### 1. introduction

The following tables, including the introductory comments, are excerpted from the above cited compilation of observed and predicted wavelengths of magnetic dipole lines arising within ground configurations of the type  $ns^2np^k$  (n=2 and 3, k=1 to 5). The compilation work was done by V. Kaufman and J. Sugar of the National Institute of Standards and Technology (formerly the National Bureau of Standards).

All measured lines that are correctly identified are included. Some are only tentatively classified by the authors, but appear to be reasonable on the basis of predictions along isoelectronic sequences.

Also included is a selected group of electric quadrupole lines (E2) that are frequently observed in  $ns^2np^2$  and  $ns^2np^4$  configurations; these are the  ${}^{1}D_2 - {}^{1}S_0$  transitions.

It will probably be difficult to observe the nsnp ( ${}^{3}P_{0,1,2} - {}^{1}P_{1}$ ) transitions in the Be and Mg isoelectronic sequences because the very large electric-dipole transition probability of the  $ns^{2} {}^{1}S_{0} - nsnp {}^{1}P_{1}$  resonant transition will tend to rapidly deplete the nsnp  ${}^{1}P_{1}$  level. Similarly, but to a lesser extent, the  ${}^{3}P_{0} - {}^{3}P_{1}$  transition can be expected to be weak because of the  $ns^{2} {}^{1}S_{0} - nsnp {}^{3}P_{1}$  transition. However, these magneticdipole transitions have been included for the sake of completeness.

Calculations of line strengths and transition probabilities have been made for all of these lines by both relativistic and non-relativistic methods. Preference has been given to the relativistic results. Calculations by both methods for the n=3 shell differ on the average by only  $5\%^{1}$ 

#### 2. Predicted Wavelengths

For the nickel ions, predicted values for the wavelengths of the M1 and E2 lines were obtained from the known energy levels by the Ritz principle of deriving wavelengths from energy differences. Their uncertainties are derived from the reported level uncertainties. The source of data is given in Sec. 7 below.

#### 3. Observed Wavelengths

The most common laboratory source generating copious forbidden lines is the tokamak, which contains a magnetically-confined, high-temperature plasma with an ion density similar to that of the solar corona. By injecting any impurity element, magnetic dipole lines of that element may be seen in stages of ionization determined by the plasma temperature. Most of the nickel data are from tokamak observations. The other wavelength data are from astronomical sources, including gaseous nebulae, stars and the solar corona.

The sources of observed data that have been credited are those providing the best measurements.

## 4. Predicted Transition Probabilities

In most cases multiconfiguration Dirac-Fock calculations of line strengths are available. These calculations do not generally converge for neutral and singly ionized atoms, but non-relativistic calculations have been made in every such case. Line strengths for the magneticdipole lines of the isoelectronic sequences of B I, C I, N I, and F I were taken from Cheng et al.² Those for the Al I, Si I, and P I sequences were taken from Huang.³⁻⁵ Those for the Cl I sequence, with a few exceptions, are from Huang et al.⁶ The relativistic calculations are not available for the Be, Mg, and S isoelectronic sequences. The transition probabilities for all magnetic-dipole lines of the Be-like, Mg-like, and S-like ions were therefore calculated in the manner described by Sugar and Kaufman.¹ These are non-relativistic calculations in intermediate coupling. They agree within a few percent with relativistic calculations in the n=3 sequences for which both are available.

Line strengths for the electric-quadrupole lines of  $2s^22p^k$  ( ${}^{1}D_2 - {}^{1}S_0$ ) [k=2] and [k=4] are for the carbon and oxygen sequences from Cheng *et al.*² The transition probabilities for these lines in the sulfur sequence,  $3s^{2}3p^{4}$ , are from Mendoza and Zeippen.⁷

Relations between transition probabilities  $A(s^{-1})$  and line strengths S are given explicitly as

$$A = \frac{2.697 \times 10^{13}}{\lambda^3 g} S(M1),$$
$$A = \frac{1.680 \times 10^{18}}{\lambda^5 g} S(E2),$$

where  $\lambda$  is the transition wavelength in Å and g is the 2J + 1 degeneracy of the upper level. S(M1) in Bohr magneton units ( $\mu_B$ ) and S(E2) in atomic units ( $ea_0^2$ ) are the magnetic-dipole and electric-quadrupole line strengths, respectively.

The magnetic-dipole transition rate in almost all cases is a few orders of magnitude greater than the electricquadrupole transition rate. The E2 rate has been added the M1 rate in those cases for which the former is greater than 1% of the latter. This is true only for some of the N I  $(2p^3)$  and P I  $(3p^3)$  sequence transitions. An asterisk following the transition rate in the tables shows where this occurs.

#### 5. Data Table Information

The tables contain the predicted and observed wavelengths and predicted transition probabilities for magnetic-dipole transitions within  $ns^2np^k$  (k = 1-5) and nsnpconfigurations for n = 2, 3. The electric quadrupole transition  ${}^{1}D_{2}$ - ${}^{1}S_{0}$  for k = 2, 4 is included because it is frequently observed. The data are presented in order of increasing wavelength. The columns from left to right in order of appearance contain the following information:

- Column No. Description
  - Wavelengths (observed and predicted) in Å below 20 000 Å, and in micrometers (μm) between 2 and 1000 μm. Wavelengths given without units are in Å. Wavelengths in vacuum are given below 2000 Å, in air between 2000 Å and 5 μm, and in vacuum above 5 μm. Each wavelength is followed by its uncertainty in parentheses. Tentative identifications are preceded by "T". E2 transitions are denoted by "Q".
  - 2 Transition probabilities (A) are written as a factor times 10 to a power. The power of ten follows the decimal factor. For example, 2.20 + 4 means  $2.20 \times 10^4$ . An asterisk following the transition probability indicates that the E2 rate for the transition is greater than 1% of the M1 rate and has been added to that value.
  - 3 Spectrum.
  - 4 Electronic configuration.
  - 5 Line classification. Lower level is given first.

Column No.

#### Description

- 6 Ionization energy in thousands of electron volts (keV).⁸⁻¹⁰
- 7 References for observed wavelengths. Definitions of symbols are given in Sec. 8, "References for Observed Wavelengths".

## 6. References to Text

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## 7. Reference for Energy Levels

Sugar, J., and Corliss, C. (1985), J. Phys. Chem. Ref. Data 14, Suppl. 2.

## 8. References for Observed Wavelengths

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## D-3

# Magnetic Dipole Lines for Nickel

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Wav Observed	elength Calculated	A (s ⁻¹ )	Spectrum	Config.	Classification	I.E. (keV)	Ref. (obs. H)
	212.81(16)	6.91 +4	Ni XXV	2s 2p	${}^{3}P_{0} - {}^{1}P_{1}$	2.30	
	232,89(11)	3.79 +4	Ni XXV	2s 2p	${}^{3}P_{1} - {}^{1}P_{1}$	2,30	
	249.94(19)	4.60 +4	Ni XXII	2s ² 2p ³	${}^{4}S_{3/2} - {}^{2}P_{3/2}$	1.89	
	282.4(3)	3.02 +5	Ni XXIII	25 ² 2p ²	${}^{3}P_{1} - {}^{1}S_{0}$	2.01	
	330.6(4)	7.80 +4	Ni XXII	$2s^2 2p^3$	${}^{4}S_{3/2} - {}^{2}P_{1/2}$	1.89	
	334.9(4)	2.21 +4	Ni XXV	2s 2p	${}^{3}P_{2} - {}^{1}P_{1}$	2.30	
	359.1(5)	3.31 +5	Ni XXI	$2s^2 2p^4$	${}^{3}P_{1} - {}^{1}S_{0}$	1.76	
	412.3(5)	1.20 +5	Ni XXII	2s ² 2p ³	$2_{D_{3/2}} - 2_{P_{3/2}}$	1.89	
465.4(3)	465.40(17)	4.15 +4	Ni XXIII	$2s^2 2p^2$	${}^{3}P_{1} - {}^{1}D_{2}$	2.01	HSCS
471.15(5)	471.14(6)	4.24 +4	Ni XXI	$2s^2 2p^4$	${}^{3}P_{2} - {}^{1}D_{2}$	1.76	W
477.6(3)	477.6(3)	4.48 +3	Ni XXII	$2s^2 2p^3$	$4s_{3/2} - 2D_{5/2}$	1.89	HSCS
	Q 514.0(8)	1.44 +2	Ni XXI	2s ² 2p ⁴	${}^{1}D_{2} - {}^{1}S_{0}$	1.76	
	524.3(9)	2.99 +4	Ni XXII	$2s^2 2p^3$	${}^{2}D_{5/2} - {}^{2}P_{3/2}$	1.89	
609.9(3)	609,9(3)	3.94 +4	Ni XXIV	2s ² 2p	${}^{2}P_{1/2} - {}^{2}P_{3/2}$	2.13	HSCS
614.8(3)	614.8(3)	3.71 +4	Ni XXIII	$2s^2 2p^2$	${}^{3}P_{2} - {}^{1}D_{2}$	2.01	HSCS
634.8(3)	634.8(3)	4.11 +4	Ni XXII	$2s^2 2p^3$	$4s_{3/2} - 2D_{3/2}$	1.89	HSCS
	689.8(1.5)	9.11 +3	Ni XXII	$2s^2 2p^3$	$2_{D_{3/2}} - 2_{P_{1/2}}$	1.89	
694.64(3)	694.64(3)	5.34 +4	Ni XX	2s ² 2p ⁵	${}^{2}P_{3/2} - {}^{2}P_{1/2}$	1.65	PSS
	Q 718.1(2.1)	2.37 +1	Ni XXIII	$2s^2 2p^2$	¹ D ₂ - ¹ S ₀	2.01	
	730.35(16)	5.37 +2	Ni XVII	3s 3p	${}^{3}P_{0} - {}^{1}P_{1}$	0.57	
	764.6(1.8)	2.87 +4	Ni XXV	2s 2p	${}^{3}P_{1} - {}^{3}P_{2}$	2.30	
	777.06(19)	3.30 +2	Ni XVII	3s 3p	${}^{3}P_{1} - {}^{1}P_{1}$	0.57	
779.5(3)	779.48(12)	4.14 +4	Ni XXI	2s ² 2p ⁴	${}^{3}P_{2} - {}^{3}P_{1}$	1.76	HSCS
911.0(3)	911.00(25)	2.07 +4	Ni XXIII	$2s^2 2p^2$	${}^{3}P_{0} - {}^{3}P_{1}$	2.01	HSCS
	928.76(27)	3.26 +2	Ni XVII	3s 3p	${}^{3}P_{2} - {}^{1}P_{1}$	0.57	
	1025.(5)	5.61 +3	Ni XXII	2s ² 2p ³	$2_{P_{1/2}} - 2_{P_{3/2}}$	1.89	
	1033.2(5)	2.50 +3	Ni XV	$3s^2 3p^2$	³ P ₁ - ¹ S ₀	0.46	
	1034.9(5)	7.17 +2	Ni XIV	3s ² 3p ³	⁴ S _{3/2} - ² P _{3/2}	0.43	
1174.72(5)	1174.720(7)	4.66 +2	Ni XIV	3s ² 3p ³	${}^{4}S_{3/2} - {}^{2}P_{1/2}$	0.43	SBT
1191.1(4)	1191.0(3)	1.01 +3	Ni XXI	2s ² 2p ⁴	${}^{3}P_{1} - {}^{1}D_{2}$	1.76	FBM
1277.23(1)	1277.231(18)	2.57 +3	Ni XIII	3s ² 3p ⁴	${}^{3}P_{1} - {}^{1}S_{0}$	0.38	SBT
1866.75(1)	1866.751(17)	8.27 +0*	Ni XIV	35 ² 3p ³	$4s_{3/2} - 2D_{5/2}$	0.43	SBT
1917.3(2)	1914.98(21)	1.32 +3	Ni XXIII	$2s^2 2p^2$	${}^{3}P_{1} - {}^{3}P_{2}$	2.01	Н
1928.7(3)	1929.(6)	1.03 +3	Ni XXII	$2s^2 2p^3$	$2D_{3/2} - 2D_{5/2}$	1.89	H
	1966.1(1.9)	5.97 +2	Ni XIV	3s ² 3p ³	$2_{D_{3/2}} - 2_{P_{3/2}}$	0.43	
	Q 1968.38(4)	1.16 +1	Ni XIII	3s ² 3p ⁴	${}^{1}D_{2} - {}^{1}S_{0}$	0.38	
	Q 2046.5(2.1)	1.34 +1	Ni XV	$3s^2 3p^2$	$^{1}D_{2} - ^{1}S_{0}$	0.46	
2085.51(5)	2085.51(3)	1.94 +2	Ni XV	3s ² 3p ²	${}^{3}P_{1} - {}^{1}D_{2}$	0.46	SBT
2125.50(2)	2125.500(23)	2.58 +2	Ni XIII	352 3p4	${}^{3}P_{2} - {}^{1}D_{2}$	0.38	SBT
2184.26(5)	2184.259(24)	1.63 +2	Ni XIV	3s ² 3p ³	⁴ S _{3/2} - ² D _{3/2}	0.43	SBT
	2321.6(2.7)	2.11 +2*	Ni XIV	3s ² 3p ³	$^{2}D_{5/2} - ^{2}P_{3/2}$	0.43	

# Magnetic Dipole Lines for Nickel - Continued

Wave Observed	length Calculated	A (s ⁻¹ )	Spectrum	Config.	Classification	I.E. (keV)	Ref. (obs. H)
	2467.(19)	1.23 +3	Ni XXV	2s 2p	³ P ₀ - ³ P ₁	2.30	
	2539,96(5)	1.59 +2	Ni XIV	3s ² 3p ³	${}^{2}D_{3/2} - {}^{2}P_{1/2}$	0.43	
2818.2(3)	2817.7(3)	5.72 +2	Ni XXI	2s ² 2p ⁴	${}^{3}P_{0} - {}^{3}P_{1}$	1.76	HSCS
	2818.01(6)	2.05 +2	Ni XV	3s ² 3p ²	${}^{3}P_{2} - {}^{1}D_{2}$	0.46	
3601.1(4)	3600.0(2.6)	1.93 +2	Ni XVI	3s ² 3p	${}^{2}P_{1/2} - {}^{2}P_{3/2}$	0.50	J
	3636.50(9)	1.84 +1	Ni XIII	3s ² 3p ⁴	${}^{3}P_{1} - {}^{1}D_{2}$	0.38	
4231.2(4)	4230.9(1.8)	2.37 +2	Ni XII	3s ² 3p ⁵	$2_{P_{3/2}} - 2_{P_{1/2}}$	0.35	J
T 4744.	4756.(10)	1.23 +2	Ni XVII	3s 3p	${}^{3}P_{1} - {}^{3}P_{2}$	0.57	Р
5115.8(4)	5115.81(10)	1.57 +2	Ni XIII	3s ² 3p ⁴	${}^{3}P_{2} - {}^{3}P_{1}$	0.38	J
6701.7(4)	6701.68(22)	5.65 +1	Ni XV	3s ² 3p ²	${}^{3}P_{0} - {}^{3}P_{1}$	0.46	J
8024.1(4)	8024.1(5)	2.27 +1	Ni XV	3s ² 3p ²	${}^{3}P_{1} - {}^{3}P_{2}$	0.46	J
	8690.(40)	1.11 +1	Ni XIV	3s ² 3p ³	$2_{P_{1/2}} - 2_{P_{3/2}}$	0.43	
	12150.(60)	1.00 +1	Ni XVII	3s 3p	${}^{3}P_{0} - {}^{3}P_{1}$	0.57	
	12815.0(1.2)	4.27 +0	Ni XIV	$3s^2 3p^3$	$2_{D_{3/2}} - 2_{D_{5/2}}$	0.43	
	19.3(4) μm	5.90 -3	Ni XIII	3s ² 3p ⁴	³ P ₁ - ³ P ₀	0.38	

E. Atomic Energy Levels of Nickel, Ni I through Ni XXVIII

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## E. Atomic Energy Levels of Nickel, Ni I through Ni XXVIII

[Excerpted from: J. Sugar and C. Corliss, J. Phys. Chem. Ref. Data 14, Suppl. 2 (1985)].

#### 1. Introduction

The following tables, including the introductory comments, are excerpted from the iron-period compilation of atomic energy levels by J. Sugar and C. Corliss (1985) of the Atomic Energy Levels Data Center at the National Institute of Standards and Technology (formerly the National Bureau of Standards).

Generally, only published papers have been used as sources of data. Unpublished data are included when they constitute a substantial improvement over material in the literature. For many of the higher ions the original papers do not give energy level values, but only classifications of observed lines. In these cases the level values have been derived from the given data.

All energy levels are given in units of  $cm^{-1}$ , beginning with a value of zero for the ground level. Ionization energies found in the literature are usually given in eV or  $cm^{-1}$ . The conversion factor, 8065.479(21)  $cm^{-1}/eV$ , given by Cohen and Taylor (1973), is used here. In a few cases where adequate data were available but the ionization energy had not been derived, this calculation was carried out. For a number of the ions, no suitable series are known. In these cases values obtained by Lotz (1967), by a method of successive differences along isoelectronic sequences, have been quoted. Although uncertainties are not provided with these extrapolated values, it is estimated that they are accurate to 0.2% by comparing them with recently determined values.

Nearly all of the data are based on observations of various types of laboratory light sources. However, the laboratory data are sometimes supplemented by data obtained from solar observations. This is particularly true where spin-forbidden lines are needed to establish the absolute energy of a system of excited levels and where parity-forbidden transitions between levels of a ground configuration are used to obtain accurate relative energies for the low levels. Whenever both solar data and equivalent laboratory data are available preference is generally given to the laboratory measurements.

When no observations are available to connect independent systems of levels, an estimate of the connecting energy is adopted. Those level values affected by the estimate are denoted by +x following the value. The value of x is the systematic error of the estimate.

Included under the heading "Leading Percentages" are the results of calculations that express the eigenvector percentage composition of levels (rounded to the nearest %) in terms of the basis states of a single configuration, or more than one configuration where configuration interaction has been included. First the percentage of the basis state corresponding to the level's name is given; next the second largest percentage together with the related basis state. Sometimes the leading percentage in an alternative coupling scheme is given. Generally, when the leading percentage is less than 40%, no name is given. When the first and second resultant terms are the same and sum to  $\geq 40\%$  the first name is given. When the first and second resultant terms are the same but have different parentages, and their share of the eigenvector composition sums to 40% or more, the level will be named as the higher percentage term. In cases where these percentages differ by one or two units (an insignificant difference), either term may be selected for the level name, and the lower percentage may appear first. For the unnamed level, the term symbol follows the percentage. The user should of course bear in mind that the percentages are model dependent, so that the results of different calculations can yield notably different percentages. In the case of Cr, the 1969 results by Roth are adopted. It was intended to use his new 1980 calculations as well, but it was found that the sum of percentages for a number of states exceeded 100 by significant amounts.

For configurations of equivalent *d*-electrons, several terms of the same LS type may occur. These are theoretically distinguished by their seniority number. In the present compilations they are designated in the notation of Nielson and Koster (1963). For example, in the  $3d^5$  configuration there are three ²D terms with seniorities of 1, 3, and 5. These terms are denoted as ²D1, ²D2, and ²D3, respectively, by Nielson and Koster. Martin, Zalubas, and Hagan (1978) give a complete summary of the coupling notations used here, tables of the allowed terms for equivalent electrons, etc.

The text for each ion does not include a complete review of the literature but is intended to credit the major contributions. In assembling the data for each spectrum the following bibliographies were used:

- i. Papers cited by Moore (1949, 1952)
- ii. C. E. Moore (1968, 1969)
- iii. L. Hagan and W. C. Martin (1972)
- iv. L. Hagan (1977)
- v. R. Zalubas and A. Albright (1980)
- vi. Card file of publications since June 1979 maintained by the NBS Atomic Energy Levels Data Center

#### He I isoelectronic Sequence

Spectra of K, Ca, Ti, and V were obtained by Aglitskii et al. (1974) with a laser-heated plasma in third and fifth orders of a crystal spectrograph. Reference lines of Mg XI and Al XII published by Flemberg (1942) were used, and an uncertainty of  $\pm 0.0005$  Å was reported for the lines of the He I isoelectronic sequence, which fall in the range of 2.3-3.6 Å. Flemberg's reference wavelengths were in x-units. The equivalence to Å that he used must be increased by 8 parts in 10⁵, according to the more recent conversion determined by Deslattes and Henins (1973). With this correction, the data of Aglitskii et al. deviate randomly from the calculated wavelengths of Safronova (1981) by  $\pm 0.0008$  Å.

In a beam-foil experiment the He-like argon spectrum was observed by Briand et al. (1983a). Their wavelengths for the  $1s^{2} {}^{1}S_{0} - 1s2p {}^{3}P_{1}^{\circ}$  and  ${}^{1}P_{1}^{\circ}$  transitions were 3.9693(3) Å and 3.9491(3) Å, in agreement with the calculated values by Safronova.

The 1s2s  ${}^{3}S_{1} - 1s2p$   ${}^{3}P_{2}^{\circ}$  transition has been measured in Ca XIX by Livingston (1983) and in Fe XXV by Buchet *et al.* (1982). The measured wavelengths are 466.78(8) Å for Ca and 271.04(10) Å for Fe. The corresponding energy differences are greater than those predicted by Safronova by 162(37) and 123(136) cm⁻¹, respectively, or 0.07% and 0.03% of the energy difference. A new calculation of these energies by Hata and Grant (1983) predicted values that were 60 cm⁻¹ lower in Ca and 154 cm⁻¹ lower in Fe than the observed values.

Because of the excellent agreement of Safronova's calculations with the best experimental data available and the paucity of these data, the compilation of this sequence was based on her results. Her calculated energies were quoted for the 1s2s and 1s2p levels of the He I isoelectronic sequence and for the principal ionization energies (with correction to the Rydberg for finite atomic mass). The observed  $1s2s {}^{3}S_{1} - 1s2p {}^{3}P_{2}^{\circ}$  intervals in Ca XIX mentioned above are incorporated in the respective level lists. For n = 3-5 the calculated binding energies reported by Ermolaev and Jones (1974) are subtracted from the binding energy of the ground state by Safronova to arrive at energy level values. The uncertainty in the calculated energy levels and the ionization energies is assumed conservatively to be 2 parts in 10⁴, corresponding to the deviations from the Aglitskii et al. (corrected) observations. (The deviation from the measurements in Ar is 1 part in 10⁴.) The uncertainties in energy differences for levels of the same n-value are estimated to be 2 parts in  $10^3$ . The deviation of the 1s2p ${}^{3}P_{1}^{\circ} - {}^{1}P_{1}^{\circ}$  intervals measured by Aglitskii et al. with resonance lines differ randomly from the calculated values of Safronova by 3%.

The singlet-triplet mixing coefficients for the 1*sup* ¹³P° states are quoted from Ermolaev and Jones.

#### H I Isoelectronic Sequence

No observations of 1s - np transitions have been sufficiently accurate to test the theoretical values. The best measurement available is for the 1s - 2p energies for Fe xxvI with an uncertainty of  $\pm 5000$  cm⁻¹, or 1 part in 10⁴, by Briand, Tavernier, and Indelicato (1983b). Erickson (1977) has calculated the absolute binding energies for each of the levels through n = 5 and for the ns and np states through n = 13. An improved calculation of the Lamb-shift effects was reported by Mohr (1983), who gave the energy separations among the n = 1 and 2 levels. Gould and Marrus (1983) have measured the Lamb-shift of the 2s 2S1/2 state of Ar XVIII, obtaining the value 1264(13) cm⁻¹. Their results agrees with the value 1275.8(0.8) cm⁻¹ calculated by Mohr and is three standard deviations lower than Erickson's value of  $1301(2) \text{ cm}^{-1}$ .

Mohr's results for the energy separations of n = 1 and 2 levels have been compiled, and Erickson's for n = 3-5 relative to the 2p  $^{2}P_{3/2}^{\circ}$  level. This increases Erickson's values for the levels, or, equivalently, increases the binding energy of the ground state (the ionization energy). Assuming that the uncertainty in these compiled values is mainly due to the error in the Lamb shift, the fractional error is taken as equal to the experimental fractional error in the Ar measurement. This contribution to the level values relative to the ground state is about 4 parts in 10⁶ for the iron period. This is about 10 times the error estimated by Mohr for his calculated 1s - 2p intervals. The corresponding intervals calculated by Erickson are lower than those of Mohr by about the same fractional amount.

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NiI

Z = 28

Ground state:  $1s^22s^22p^63s^23p^63d^84s^2{}^3F_4$ 

## Ionization energy = $61600 \pm 10 \text{ cm}^{-1} (7.6375 \pm 0.0012 \text{ eV})$

The analysis of this spectrum is by Russell (1929), with a few changes of interpretation taken from recent theoretical studies. No energy levels have been found since his work 50 years ago. He outlined the previous work in his paper and increased the number of classified lines from 622 to 1071. His line list extends from 1963-18 040 Å.

The spectrum was reobserved by Burns and Sullivan (1947, 1948) with a vacuum arc and a Fabry-Perot interferometer. Three decimal place wavelengths were measured from 2173-8968 Å. From these they derived the three decimal place energy levels with a level uncertainty of  $\pm 0.01$  cm⁻¹. Except for 10 level values retained from Russell, their values are given here. In the course of their work they measured about 400 lines not previously observed.

The five place g-values from the three lowest terms are from Childs, Fred, and Goodman (1966), Childs and Goodman (1968), and Childs and Greenebaum (1972). The three place g-values are from measurements of M.I.T. Zeeman patterns reported by Lindsley (1942). The remaining (two place) values are from Marvin and Baragar (1933) or Dijkstra (1937).

The percentage compositions of the J=2 levels of  $3d^{8}4s^{2}$  and  $3d^{9}4s$  were calculated with configuration interaction by Childs, Fred, and Goodman. Those of  $3d^{9}4p$ ,  $3d^{8}4s4p$ , and  $3d^{7}4s^{2}4p$  were calculated with configuration interaction by Roth (1980).

We derived the ionization energy from the three member 3d⁹ns series by means of a Ritz formula, giving the value 61 579 cm⁻¹. We added a correction of 21 cm⁻¹ obtained from comparisons with a corresponding longer ns-series in Cu I.

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	Russen,	, <b>n</b> . 19. (1929), P	-nys. Rev. <b>34</b> , 6	21.
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			N	li I				
Configuration	Term	J	Level (cm ⁻¹ )	8		Leading	g percentages	
$3d^8 4s^2$	<i>a</i> ³ F	4	0.000	1.24965				
		3	1 332.153	1.08280				
		2	2 216.519	0.66956	95	1	$^{1}D$	
$3d^9(^2\mathbf{D})4s$	a ³ D	3	204.786	1.33354				
		2	879.813	1.15105	91	9	$^{1}\mathbf{D}$	
		1	1 713.080	0.49804				
$3d^9(^2\mathrm{D})4s$	a ¹ D	2	3 409.925	1.01297	89	9	3 D	
$3d^8 4s^2$	b ¹ D	2	13 521.352	1.143	70	26	³ P	
$3d^{10}$	a ¹ S	0	14 728.847					
$3d^8 4s^2$	a ³ P	2	15 609 861	1 356	71	25	ID	
		1	15 734.018	1.497		20	D	
		Ō	16 017.317					
$3d^8 4s^2$	a ¹ G	4	22 102.349	0.99				
$3d^{8}({}^{3}\mathrm{F})4s4p({}^{3}\mathrm{P}^{\circ})$	$z^{5}D^{\circ}$	4	25 753.578	1.51	95			
· · · · · · · · · · · · · · · · · · ·		3	26 665.903	1.495	93			
		2	27 414.893	1.494	93			
		1	27 943.543	1.486	95			
		0	28 212.997		96			
Ni 1-Continued

Configuration	Term	J	Level (cm ⁻¹ )	8		Leading	g percentages
$3d^{8}({}^{3}\mathbf{F})4s4p({}^{3}\mathbf{P}^{\circ})$	z ⁵G°	6	27 260.891	1.32	100		
		5	27 580 411	1.276	81	16	° <b>7</b> ²
		4	28 068 091	1 171	82	13	• <b>T</b>
		3	28 578 046	0.945	87	9	5 <b>.</b>
		2	29 013.228	0.364	94	5	⁵ F°
18.3m. (	5	-					0.18/373-1.4 (370) 500
$d^{\circ}({}^{\circ}\mathbf{F})4s4p({}^{\circ}\mathbf{P}^{\circ})$	z 'F°	5	28 542.113	1.377	83	15	$3d^{\circ}({}^{\circ}\mathbf{F})4s4p({}^{\circ}\mathbf{P}^{\circ}){}^{\circ}\mathbf{G}^{\circ}$
		4	29 084.478	1.288	70	12	$3d^3(^2D)4p^3F^3$
	1	3	29 832.810	1.208	40	26	$3d^{\circ}(^{2}\mathrm{D})4p^{\circ}\mathrm{F}^{\circ}$
		2	30 163.140	0.985	76	6	$3d^{9}(^{2}\mathrm{D})4p^{3}\mathrm{D}^{\circ}$
		1	30 392.052	0.006	97		
$d^{9}(^{2}\mathbf{D})4p$	z ³ P°	2	28 569.210	1.485	91	4	$3d^{9}(^{2}D)4p^{3}D^{\circ}$
		1	29 500.690	1.426	86	5	$3d^{9}(^{2}D)4p^{3}D^{\circ}$
		ō	30 192.268		96		
$d^9(^2\mathbf{D})/d\mathbf{p}$	- ³ ₽°	3	90 900 700	1 096		97	$3d^{9}(^{2}\mathrm{D})4n^{3}\mathrm{D}^{9}$
a (D)4p	2 1	3	29 320.782	1.080	34	21	2 d ⁸ ( ³ F) / d = ( ³ Te) ⁵ Te
		4	29 481.020	1.287	74	13	$3a(r)4s4p(P))^{*}F$
		2	30 619.440	0.740	73	16	$3d^{\circ}(\mathbf{P}) 4s4p(\mathbf{P}) \mathbf{P}$
$d^{9}(^{2}\mathbf{D})4p$		3	29 668.918	1.300	30	³ D° 30	$3d^{8}({}^{3}\mathrm{F})4s4p({}^{3}\mathrm{P}^{\circ}){}^{5}\mathrm{F}^{\circ}$
2 - ⁹ ( ² D) / -	- 300	9	00 000 505	1.044		99	$3d^{8}({}^{3}\mathbf{F})/(a/n)({}^{3}\mathbf{P}^{2}))^{3}\mathbf{D}^{3}$
a ⁻ ( ⁻ D)4p	ZD	Z	29 888.202	1.044	33	22	$3a^{(\Gamma)}+3s^{(\Gamma)}+3s^{(\Gamma)}$
		1	30 912.838	0.552	51	38	3a(r)4s4p(r)
$3d^{8}({}^{3}\mathbf{F})4s4p({}^{3}\mathbf{P}^{\circ})$	z ³ G°	5	30 922.763	1.214	95	5	$({}^{3}\mathbf{F})({}^{3}\mathbf{P}^{\bullet}) {}^{5}\mathbf{G}^{\bullet}$
	1	4	30 979.789	1.052	79	13	$({}^{3}\mathbf{F})({}^{3}\mathbf{P}^{\bullet}) {}^{1}\mathbf{G}^{\bullet}$
		3	31 786.210	0.761	95		
$d^9(^2\mathbf{D})4p$	z ¹ F°	3	31 031.042	1.048	58	26	$3d^9(^2\mathrm{D})4p$ ³ F°
$d^9(^2\mathbf{D})4p$	z ¹ D°	2	31 441.665	1.060	62	13	$3d^{8}(^{3}\mathrm{F})4s4p(^{3}\mathrm{P}^{\circ})^{-1}\mathrm{D}^{\circ}$
$3d^{8}({}^{3}\mathbf{F})4s4p({}^{3}\mathbf{P}^{\circ})$	³ F°	4	32 973.414	1.222	77	13	$3d^{9}(^{2}D)4p^{3}F^{\circ}$
•	i	3	33 112 368	1,193	46	19	$3d^{8}({}^{3}F)4s4p({}^{3}P^{\circ}){}^{3}D^{\circ}$
		2	33 610.916	0.973	42	30	$3d^{8}({}^{3}\mathrm{F})4s4p({}^{3}\mathrm{P}^{\circ}){}^{3}\mathrm{D}^{\circ}$
$d^9(^2\mathbf{D})4p$	z ¹ P°	1	32 982.280	1.005	94		
	3-0-0						
$Bd^{("}(\mathbf{F})4s4p(\mathbf{P})$	y ^o D ^o	3	33 500.854	1.198	48	23	$3d^{\circ}(^{-}F)4s4p(^{-}P^{-})^{-}F^{-}$
		2	34 163.29	1.19	45	40	$3a^{\circ}(^{\circ}\mathbf{F})4s4p(^{\circ}\mathbf{P}^{\circ})^{\circ}\mathbf{F}^{\circ}$ $3a^{\circ}(^{\circ}\mathbf{P})4s4p(^{\circ}\mathbf{P}^{\circ})^{\circ}\mathbf{F}^{\circ}$
		1	34 400.374	0.511	62	33	3a ( D)4p D
$3d^{8}(^{3}F)4s4p(^{3}P^{\circ})$	z ¹ G°	4	33 590.159		79	14	( ³ F)( ³ P*) ³ G*
$3d^{8}({}^{3}\mathbf{F})4s4p({}^{3}\mathbf{P}^{\circ})$	y ¹ F°	3	35 639.148	1.013	81	8	( ³ F)( ³ P°) ³ F°
$3d^{8}({}^{3}\mathbf{F})4s4p({}^{3}\mathbf{P}^{\circ})$	y ¹ D°	2	36 600.805	1.013	75	16	$3d^{9}(^{2}D)4p^{-1}D^{\circ}$
$3d^{8}(^{3}P)4s4p(^{3}P^{\circ})$	⁵ P°	3	40 361.254		86	11	$(^{1}D)(^{3}P^{\bullet})^{-3}D^{\bullet}$
-		2	40 484.282		89	7	
$3d^{8}({}^{1}\mathrm{D})4s4p({}^{3}\mathrm{P}^{\circ})$	³ F°	4	42 585.296	1.346	52	36	( ³ P)( ³ P*) ⁵ D*
		3	42 767.900	1.218	66	19	$({}^{3}P)({}^{3}P^{\circ}) {}^{5}D^{\circ}$
		2	42 954.234	0.840	79	6	$(^{1}\mathbf{D})(^{3}\mathbf{P}^{\bullet})^{-3}\mathbf{D}^{\bullet}$
0.19/200.5	30		40 605 064	1.94			
3a"("D)5s	e D	3	42 000.904	1.34			
		2	42 190.021	1.085			
			44 112.192		1		

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Configuration	Term	J	Level (cm ⁻¹ )	g		Leading	g percentages
$3d^{8}({}^{1}\mathrm{D})4s4p({}^{3}\mathrm{P}^{\circ})$	³ D°	3	42 621.048		42	36	$({}^{3}F)({}^{1}P^{\circ}) {}^{3}D^{\circ}$
		2	42 653.723		66	15	
		1	42 656.317	1.320	77	10	
$3d^{8}(^{3}\mathrm{F})4s4p(^{1}\mathrm{P}^{\circ})$	³ G°	5	43 089.636	1.226	99		
		4	44 314.980	1.182	66	18	$\binom{{}^{3}\mathbf{P}}{{}^{2}\mathbf{P}}\binom{{}^{3}\mathbf{P}^{\bullet}}{{}^{1}\mathbf{P}^{\bullet}}\binom{{}^{5}\mathbf{D}^{\bullet}}{{}^{2}\mathbf{P}^{\bullet}}$
		3	44 565.10	1.044	55	24	(°F)('P°) °F°
$3d^{8}({}^{3}\mathrm{F})4s4p({}^{1}\mathrm{P}^{\circ})$	³ F°	4	43 258.792	1.247	62	19	$(^{3}\mathbf{F})(^{1}\mathbf{P}^{\circ})$ $^{3}\mathbf{G}^{\circ}$
		3	45 281.152	0.779	45	40	$({}^{1}\mathbf{P})({}^{1}\mathbf{P}^{\circ}){}^{3}\mathbf{G}^{\circ}$
		2	45 418.858	0.677	80	7	$({}^{3}F)({}^{3}P^{\circ}) {}^{3}D^{\circ}$
$d^{8}(^{1}\text{D})4s4p(^{3}\text{P}^{\circ})$	³ P°	1	43 464.019	1.390	64	20	$({}^{3}P)({}^{3}P^{\circ}) {}^{3}P^{\circ}$
		2	<i>43 933.428</i>	1.476	59	18	( ³ P)( ³ P°) ⁵ D°
$d^{8}({}^{3}F)4s4p({}^{1}P^{\circ})$		3	43 654.974	1.243	35	³ D° 34	( ³ P)( ³ P°) ⁵ D°
$3d^{8}(^{3}P)4s4p(^{3}P^{\circ})$	⁵ D°	3	44 206.185		40	26	( ³ F)( ¹ P°) ³ D°
$3d^9(^2\mathbf{D})5s$	e ¹ D	2	44 262.619	1.09			
$3d^{8}(^{3}P)4s4p(^{3}P^{\circ})$		4	44 336.10		38	⁵ D° 37	( ¹ D)( ³ P°) ³ F°
$Bd^{8}({}^{3}F)4s4p({}^{1}P^{\circ})$	³ D°	2	44 475.158	1.155	56	14	$(^{1}\mathbf{D})(^{3}\mathbf{P}^{\bullet})^{-3}\mathbf{D}^{\bullet}$
		1	45 122.460	0.566	69	13	$({}^{3}P)({}^{3}P^{\circ}) \; {}^{3}D^{\circ}$
$3d^{8}({}^{3}\mathbf{P})4s4p({}^{3}\mathbf{P}^{\circ})$	r ³ P°	2	46 522 965		66	21	$({}^{3}P)({}^{3}P') {}^{5}S'$
	~ .	1	47 208.228		67	20	$(^{1}D)(^{3}P^{*})^{3}P^{*}$
		0	47 686.625		69	28	$(^{1}D)(^{3}P^{\circ})^{3}P^{\circ}$
$3d^{8}(^{3}P)4s4p(^{3}P^{\circ})$	v ³ D°	3	47 030.148	1.331	93		
		2	47 139.392	1.209	72	8	$({}^{3}P)({}^{3}P^{\circ}) {}^{5}S^{\circ}$
		1	47 424.830	0.726	83	8	( ³ F)( ¹ P°) ³ D°
$3d^{8}(^{3}P)4s4p(^{3}P^{*})$	⁵ S°	2	47 328.85		67	12	( ³ P)( ³ P°) ³ P°
$3d^8 4s({}^4F)5s$	<i>e</i> ⁵ F	5	48 466.530	1.40			
		4	49 086.030	1.33			
		3	49 777.619	1.23			
		2	50 346.477	0.95			
$3d^{9}(^{2}\mathrm{D})5p$	1F°	3	48 671 9	0.20			
			40 07 1.0				
3d ⁹ ( ² D)5p	³ F°	4 2	48 715.2 50 03 <b>9</b> .18				
$3d^9(^2\mathrm{D})5p$	w ³ P*	2	48 735.308				
-		1	49 403.42				
		0	50 138.53				
$3d^{8}(^{3}P)4s4p(^{3}P^{*})$	¹ <b>P</b> *	1	48 817.6		89	3	$(^{1}D)(^{1}P^{\bullet})^{-1}P^{\bullet}$
3d ⁹ ( ² D)4d	e ^s S	1	48 953.344	1.92			
$3d^{8}(^{3}P)4s4p(^{3}P^{\circ})$	¹ <b>D</b> *	2	49 032.589		93	4	( ¹ D)( ³ P•) ³ D•
3d ⁹ ( ² D)4d	e ³ G	5	49 158.529	1.20			
		4	49 174.811	1.05			
		3	50 677 599	0.77	1		

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Configuration	Term	J	Level (cm ⁻¹ )	8		Leading	percentages
$3d^9(^2\mathrm{D})4d$	e ³ P	2 1 0	49 159.060 49 171.187 50 276.354	1.43 1.00			
$3d^{9}(^{2}D)5p$	¹ D°	2	49 185.146				
$3d^9(^2\mathrm{D})4d$	f ³ D	3 2 1	49 271.578 49 327.845 50 716.927	1.32 0.45			
$3d^9(^2\mathrm{D})4d$	e ³ F	3 4 2	49 313.851 49 332.643 50 834.435				
$3d^9(^2\mathrm{D})5p$	³D°	3 2 1	49 327.56 50 689.490 50 851.22				
$3d^9(^2D)5p$		3	50 142.8				
$3d^9(^2D)5p$	x ¹ P°	1	50 458.187				
$3d^8 4s({}^4\mathbf{F})5s$	f ³ F	4 3 2	50 466.172 51 306.085 52 040.568	1.27 1.08 0.67			
$3d^9(^2\mathbf{D})4d$	e ¹ P	1	50 536.742	1.54			
$3d^9(^2\mathrm{D})4d$	e ¹ G	4	50 706.310	1.02			
$3d^9(^2\mathrm{D})4d$	f ¹ D	2	50 754.137				
$3d^{8}({}^{1}\mathrm{G})4s4p({}^{3}\mathrm{P}^{\circ})$	u ³ F°	4 3 2	50 789.5 51 124.8 51 343.80		94 94 93	4 4	( ¹ D)( ³ P°) ³ F° ( ¹ D)( ³ P°) ³ F°
$3d^9(^2\mathrm{D})4d$	e ¹ F	3	50 832.039				
$3d^8 4s^2$	e ¹ S	0	51 457.285				
$3d^9(^2\mathbf{D})6s$	g ³ D	3 2 1	52 197.482 52 271.716 53 703.899				
$3d^{9}(^{2}\mathrm{D})6s$	g ¹ D	2	53 754.036				
$3d^8 4s({}^2\mathrm{F})5s$	g ³ F	4 3 2	54 237.136 54 251.353 55 873.78	1.27 1.00			
$3d^{9}(^{2}D)5d$	f ³ S	1	54 574.64				
$3d^9(^2\mathrm{D})5d$	f ³ G	5 4 3	54 659.759 54 667.928 56 172.704	1.03			
$3d^9(^2\mathrm{D})5d$	h ³ D	3 2	54 699.852 54 732.425				

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Configuration	Term	J	Level (cm ⁻¹ )	g	Leading percentages
$3d^{9}(^{2}\mathrm{D})5d$	h ³ F	4	54 761.346		
		3	54 772.940		
		2	56 274.516		
$3d^8 4s({}^2\mathrm{F})5s$	$f^{1}\mathbf{F}$	3	55 576.905	1.07	
$3d^{9}(^{2}\mathrm{D})5d$	f ¹ G	4	56 183.51		
$3d^9(^2\mathrm{D})5d$	g ¹ F	3	56 262.92		
$3d^8 4s({}^4\mathrm{F})4d$	e ³ H	6	56 624.668		
		5	57 677.649		
		4	58 518.11		
$3d^8 4s({}^4\mathrm{F})4d$	f ³ P	2	56 710.889		
		1	57 767.83		
		0	58 448.79		
$3d^8 4s({}^4\mathrm{F})4d$	<i>i</i> ³ F	4	56 766.523		
		3	<b>57 968.08</b>		
		2	58 629.84		
$3d^8 4s({}^4\mathbf{F})4d$	g ³ G	5	56 801.654		
		4	57 789.611		
		3	58 530.35		
$3d^{8} 4s({}^{4}\mathrm{F})4d$	<i>e</i> ⁵ P	3	56 821.553		
		2	57 586.7		
		1	58 525.507		
$3d^{8} 4s({}^{4}\mathrm{F})4d$	e ⁵ D	4	56 857.933		
		3	57 743.596		
$d^{8} 4s({}^{4}\mathrm{F}) 4d$	<i>e</i> ⁵ H	7	56 885.249	1.26	
		6	57 762.106		
		5	58 520.923		
		4	59 039.693		
		3	59 188.78		
$3d^8 4s({}^4\mathrm{F})4d$	e ⁵G	6	56 954.167		
		5 9	57 829.405		
		3 4	58 872 31		
		2	59 118.06		
$3d^8 4s({}^4F)4d$	f ⁵ F	5	56 973 707		
04 10(1)14	, .	4	57 810.494		
		3	58 588.168		
		2	58 992.52		
		1	59 226.03		
$3d^8 4s({}^4\mathrm{F})4d$	i ³ D	3	57 103.946		
$3d^8 4s({}^4F)6s$	g ⁵F	5	59 862.756		
Ni II ( ² D _{5/2} )	Limit		61 600		
$3d^8 4s({}^2\mathbf{F})4d$	<i>i</i> ³ F	4	61 832 47		

Configuration	Term	J	Level	8	Leading percentages
a 18 a 12 a 1	130		(cm ·)		
$3d^\circ 4s(F)4d$	h°G	5	61 843.28		
$3d^8 4s(^2\mathbf{F})4d$	f ³ H	6	61 957.517		
$3d^8 4s({}^4\mathrm{F})5d$	f⁵H	7	62 782.614		
$3d^{8} 4s({}^{4}\mathrm{F})5d$	<i>f</i> ⁵ G	6	62 808.03		
$3d^8 4s({}^4\mathrm{F})5d$	h ⁵F	5	62 815.34		
		1			E Contraction of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second seco

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Co 1 isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^9 {}^2D_{5/2}$ 

### Ionization energy = $146541.56\pm0.2$ cm⁻¹ ( $18.16898\pm0.00005$ eV)

This compilation is based on the very extensive analysis by Shenstone (1970, 1971) with recent unpublished additions by him to  $4d^85g$ . He has observed 4300 lines between 700 and 10 000 Å with a hollow cathode discharge and has established 320 even and 336 odd levels. The low configurations  $3d^84s$  and  $3d^74s^2$  are nearly complete. Series in  $3d^8ns$ , nd, nf, and ng were observed. About half of the levels of the complex configuration  $3d^74s4p$  are known. Shenstone gave no uncertainty estimate for his level values. We estimate that it is  $\pm 0.05$  cm⁻¹.

This work has been extended by Brault and Litzén (1983) with infrared observations above 10 000 Å. They found the  $3d^{8}({}^{3}F)6h$  configuration, and made corrections and additions to  $3d^{8}5f$  and  $3d^{8}6g$ . In  $3d^{8}5f$  the level 131122.28_{11/2} was replaced by 131094.02_{11/2}, two new levels 131115.15_{3/2} and 131131.15_{7/2} were added, and the designation of 131124.96_{7/2} was changed to  $3d^{8}({}^{3}F_{2})5f^{2}[3]^{*}_{7/2}$ . In  $3d^{8}6g$  a number of new levels were added and some previously reported were discarded. The levels and designations given below for  $3d^{8}6g$  and  $3d^{8}6h$  are from Brault and Litzén. The level uncertainties are limited to those of Shenstone's levels on which these new results are based. All percentages for these configurations are reported to be 99 or 100%, but were not given.

The Zeeman effect data are from observations at M.I.T. reported by Lindsley (1942).

The leading percentages given here for the levels of  $3d^84p$  were calculated by Roth (1969). Those for  $3d^85p$  and  $3d^74s4p$  are from Shadmi and Caspi (1972). These authors given percentage only for cases where the coupling is not pure. Repeating terms of the  $3d^7$  parent configuration are distinguished by alphabetic prefixes. In these cases the percentage includes the sum over all contributing seniority states.

We have calculated the compositions of  $3d^84s$ , 5s, 4d, 5d, 4f, 5f, 6f, 5g, 6g, and  $3d^74s^2$  and give the leading percentages.

Shenstone found the limits of the  $3d^8ns$  and nd series at 146 532.0 cm⁻¹ and of the ng series at 146 541.56 cm⁻¹. He has adopted the latter limit, which is used here.

#### References

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Lindsley, C. H. (1942), J. Opt. Soc. Am. 32, 387.
Roth, C. (1969), J. Res. Natl. Bur. Stand. 73A, 125.
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Shenstone, A. G. (1971), J. Res. Natl. Bur. Stand. 75A, 335.

			N	1 11				
Configuration	Term	J	Level (cm ⁻¹ )	8		Leading perc	entages	
$3d^9$	² D	5/2 3/2	0.00 1 506.94					
3d ⁸ ( ³ F)4s	⁴F	9/2 7/2 5/2 3/2	8 393.90 9 330.04 10 115.66 10 663.89	1.355 1.244 1.023 0.397	100 98 99 99	2 1 1	( ³ F) ² F ( ³ F) ² F ( ¹ D) ² D	
$3d^8(^3\mathrm{F})4s$	² F	7/2 5/2	13 550.39 14 995.57	1.141 0.866	98 98	2 1	( ³ F) ⁴ F ( ¹ D) ² D	
3d ⁸ ( ³ P)4s	۴P	5/2 3/2 1/2	23 108.28 24 788.20 24 835.93	1.428 2.667	54 78 100	46 22	( ¹ <b>D</b> ) ² <b>D</b>	
3d ⁸ ( ¹ D)4s	²D	³ / ₂ ⁵ / ₂	23 796.18 25 036.38	1.045 1.368	75 53	22 46	( ³ P) ⁴ P	
3d ⁸ ( ³ P)4s	²P	³ / ₂ ¹ / ₂	29 070.93 29 593.46	1.322 0.670	97 100	3	( ¹ D) ² D	
$3d^{8}({}^{1}\mathrm{G})4s$	²G	9/2 7/2	32 499.53 32 523.54	1.135 0.895	100 100			

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Configuration	Term	J	Level (cm ⁻¹ )	8		Leading	g percentages	
$\frac{1}{3d^{7} 4s^{2}}$	⁴ F	9/2	51 045.46		100			
		7/2	52 205.95		100			
		5/2	53 037.93		100			
		³ / ₂	53 601.19		100			
$3d^{8}({}^{3}\mathbf{F})4p$	4D°	7/2	51 557.85	1.420	94			
		5/2	52 738.45	1.365	93			
		3/2	53 634.62	1.186	94	4	( ³ P) ⁴ D°	
		1/2	54 176.26	-0.005	96			
$3d^{8}({}^{3}\mathrm{F})4p$	⁴ G°	9/2	53 365.17	1.156	67	23	( ³ F) ² G°	
		11/2	<i>53 496.49</i>	1.305	100			
		7/2	54 262.63	1.025	81	10	( ³ F) ⁴ F°	
		⁵ / ₂	55 018.71	0.616	94	5	$(^{3}F)$ ⁴ F°	
$3d^8({}^3F)4n$	4F°	9/2	54 557.05	1.26	80	19	$({}^{3}\mathbf{F}) {}^{2}\mathbf{G}^{\circ}$	
0a (1/4p		7/	55 117 89	1 184	76	10	$({}^{3}\mathbf{F}) {}^{2}\mathbf{F}^{\circ}$	
		5/2	56 075 96	0.985	97	6	$(^{3}F)$ ⁴ C°	
		3/2 3/2	56 424.49	0.412	95	0	(1) G	
9-18(317) 4-	200	9/	55 200 CE	1 159		20	( ³ E) 4C*	
$3d^{\circ}(\mathbf{T})4p$	G	$\frac{7}{7}$	33 299.03 56 371 / 1	1.152		32	$(\mathbf{r})$ G	
		72	<i>30 371.41</i>	0.940	84	8	( <b>'F</b> ) 'G	
$3d^{8}({}^{3}\mathbf{F})4p$	2 F°	7/,	57 080.55	1.154	81	11	$({}^{3}F) {}^{4}F^{\circ}$	
r r		Ĩ	58 4 <b>93</b> .21	0.946	74	20	$(^{3}\mathbf{F})^{-2}\mathbf{D}^{\circ}$	
$3d^{8}({}^{3}\mathbf{F})4n$	² D°	5/0	57 420.16	1.116	74	20	$({}^{3}\mathbf{F}) {}^{2}\mathbf{F}^{\circ}$	
ou ( I /ip		3/2 3/2	58 705.95	0.795	89	7	$(^{1}\mathbf{D})^{2}\mathbf{D}^{\circ}$	
$2d^8(^3\mathbf{D})4n$	4 <b>D</b> °	5/	66 571 94	1.48	73	20	( ¹ D) ² D°	
5 <i>a</i> ( <b>r</b> )4 <i>p</i>	1	$3_{1}^{2}$	66 579 71	1.550	79	19	$(^{1}\mathbf{D})^{2}\mathbf{P}^{*}$	
			67 031.02	2.331	85	11	$(^{1}D)^{2}P^{\circ}$	
228/1014-	25.	5/	67 691 61	0.960	84	8	( ³ P) ⁴ P°	
3a (D) 4p		$\frac{7^{2}}{7^{\prime}_{2}}$	68 131.21	1.200	86	9	$(^{3}P)$ $^{4}D^{\circ}$	
0.47.4.2	40	5/	67 880 16		100			
3a 4s	r	3/2	68 156 57		100	c	² <b>D</b>	
		1/2	68 709.76		98	2	1	
2-18(1D)4-	2 <b>D</b> °	3/	68 151 91	1.02	65	19	( ³ P) ⁴ P ^o	
3a ² ( ² D)4p	D	⁷² ⁵ / ₂	68 735.98	1.264	63 74	18	$(^{3}P)^{4}P^{\circ}$	
0.18.15.4	200		<u>CO 201 C2</u>	1 009			( ³ <b>D</b> ) ² <b>D</b> °	
$3d^{\circ}(D)4p$	² P ²	⁷ 2 3/	68 281.62 68 965 65	1.008	61	23	$(^{1}P)^{-}P$ $(^{1}D)^{-}D^{*}$	
		/2	00 303.03	1.000	04	15		
$3d^7 4s^2$	² G	⁹ / ₂	70 358.94		97	3	2 H	
		⁴ / ₂	71 457.74		100			
$3d^{8}({}^{3}\mathbf{P})4p$	4D°	⁵ / ₂	70 635.46	1.325	83	9	$\binom{^{3}\mathbf{P}}{^{2}\mathbf{D}^{\circ}}$	
-	1	3/2	70 706.77	1.190	91	4	$(^{a}\mathbf{F})^{4}\mathbf{D}^{\circ}$	
	1	1/2 7	70 748.70		95	4	$(^{3}F)$ $^{4}D^{\circ}$	
		¹ / ₂	70 778.12	1.385	87	9	('D) *F*	
$3d^{8}(^{3}\mathrm{P})4p$	² D°	⁵ / ₂	71 770.83	1.240	87	10	$\binom{^{3}P}{^{9}}$	
<b>T</b>		3/2	72 375.42	0.844	82	11	( ³ P) ² P°	
$3d^8(^3\mathbf{P})/r$	² P°	3/2	72 985 65	1.326	67	16	$({}^{1}\mathbf{D}) {}^{2}\mathbf{P}^{\bullet}$	
ou ( <b>r</b> 14p	1	1/2	73 903 25	1.039	70	24	$(^{1}\mathbf{D})^{2}\mathbf{P}^{\circ}$	
		12	10 000.40	1.000				

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Configuration	Term	J	Level (cm ⁻¹ )	g	Leading percentages			
$\overline{3d^7} \ 4s^2$	² P	3/2	73 893.73		85	8	² D2	
$3d^8(^3\mathrm{P})4p$	² S*	¹ / ₂	74 283.33		94	4	( ¹ D) ² P°	
$3d^8(^3\mathrm{P})4p$	⁴ S°	3/2	74 300.93		97			
$3d^8({}^1\mathrm{G})4p$	² H°	⁹ / ₂ ¹¹ / ₂	75 149.48 75 721.68	0.903 1.119	100 100			
$3d^8({}^1\mathrm{G})4p$	² F°	7/2 5/2	75 917.63 76 402.03	1.165	94 95	4	( ¹ D) ² F°	
$3d^7 4s^2$	²H	¹¹ / ₂ 9/ ₂	76 727.36 77 736.79		100 97	3	² G	
$3d^7 4s^2$	² D2	⁵ / ₂ 3/ ₂	77 332.47 78 955.45		77 72	23 18	² D1	
$3d^{8}({}^{1}\mathrm{G})4p$	²G°	7/2 9/2	79 823.03 79 923.88		99 100			
$3d^{\overline{i}}({}^{4}\mathrm{F})4s4p({}^{3}\mathrm{P}^{\circ})$	⁶ F°	$ \begin{array}{c}     11/2 \\     9/2 \\     7/2 \\     5/2 \\     3/2 \\     1/2 \end{array} $	86 343.21 86 870.03 87 538.09 88 128.56 88 582.01 88 881.59					
$3d^{7}({}^{4}\mathrm{F})4s4p({}^{3}\mathrm{P}^{\circ})$	⁶ D°	⁹ / ₂ 7/ ₂	88 171.88 89 100.49					
$3d^{7}({}^{4}\mathrm{F})4s4p({}^{3}\mathrm{P}^{\circ})$	⁶ G°	¹¹ / ₂ 9/ ₂ 7/ ₂ ⁵ / ₂	89 460.35 89 918.47 90 275.30 90 526.18?					
$3d^8({}^3{ m F})5s$	⁴F	9/2 7/2 5/2 3/2	91 800.05 92 325.85 93 390.06 94 067.14	1.350 1.188 1.02 0.392	100 61 88 99	39 12 1	( ³ F) ² F ( ³ F) ² F ( ¹ D) ² D	
$3d^7 4s^2$	2	⁵ /2 7/2	92 373.45 92 792.08		100 100			
$3d^{8}({}^{3}\mathrm{F})5s$	² F	7/2 5/2	93 528.44 94 729.25	1.166 0.865	61 87	<b>39</b> 12	4F	
$3d^7({}^4\mathrm{F})4s4p({}^3\mathrm{P}^\circ)$	4F°	9/2 7/2 5/2 3/2	94 283.94 94 705.93 95 332.53 95 893.76					
$3d^{7}({}^{4}\mathrm{F})4s4p({}^{3}\mathrm{P}^{\circ})$	⁴G°	¹¹ / ₂ 9/ ₂ 7/ ₂	94 396.74 95 017.71 95 573.39					

Ni II-Continued

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Configuration	Term	J	Level (cm ⁻¹ )	g		Leadin	g percentages
$3d^{7}({}^{4}\mathbf{F})4s4p({}^{3}\mathbf{P}^{\circ})$	⁴D°	⁷ / ₂ ⁵ / ₂ ³ / ₂ ¹ / ₂	96 535.87 97 273.83 97 799.66 98 122.63				
$3d^{7}({}^{4}\mathrm{F})4s4p({}^{3}\mathrm{P}^{\circ})$	² G°	9/2 7/2	98 276.70 99 844.13				
$3d^8({}^3\mathbf{F})4d$	4D	7/2 5/2 1/2 3/2	98 467.25 99 559.33 100 010.17 100 078.78		90 42 69 49	7 39 16 45	( ³ F) ⁴ F ( ³ F) ⁴ P ( ³ F) ⁴ P ( ³ F) ² P
$3d^{6}({}^{3}\mathbf{F})4d$	٩Þ	⁵ /2 1/2 3/2	98 561.22 100 845.41 100 490.95		57 66 73	40 26 12	( ³ P) ⁴ D ( ³ F) ⁴ D ( ³ F) ⁴ D
$3d^{8}({}^{3}\mathrm{F})4d$	4H	13/2 11/2 9/2 7/2	98 822.55 100 309.29 100 332.09 101 144.63		100 54 52 62	32 22 28	( ³ F) ² H ( ³ F) ² H ( ³ F) ⁴ G
$3d^8({}^3\mathbf{F})4d$	² H	¹¹ / ₂ 9/ ₂	98 969.44 101 357.20		47 55	45 19	( ³ F) ⁴ H
$3d^8({}^3\mathbf{F})4d$	²P	³ / ₂ 1/ ₂	99 040.75 101 246.16		44 77	29 18	( ³ F) ⁴ D ( ³ F) ⁴ P
$3d^{(3}\mathbf{F})4d$	⁴G	¹¹ / ₂ ⁵ / ₂	99 132.78 101 366.14		78 68	21 28	( ³ F) ² H ( ³ F) ⁴ F
3d ⁸ ( ³ F)4d	⁴F	9/2 7/2 3/2	99 154.81 100 592.98 101 258.01		63 40 89	31 27 8	( ³ F) ⁴ G ( ³ F) ⁴ H ( ³ F) ⁴ D
$3d^{*}({}^{3}\mathbf{F})4d$	²F	7/2 5/2	99 340.55 101 247.37		58 47	23 31	( ³ F) ⁴ F
$3d^{7}({}^{4}\mathrm{F})4s4p({}^{3}\mathrm{P}^{\circ})$	² F°	⁷ / ₂ ⁵ / ₂	99 418.61 100 609.01				
3d ⁸ ( ³ F)4d	²G	⁹ /2 7/2	99 442.86 101 740.27		45 72	21 13	( ³ F) ⁴ F ( ³ F) ⁴ G
$3d^{8}({}^{3}\mathbf{F})4d$		⁵ / ₂	100 389.52		42 ² F	25	( ³ F) ⁴ F
$3d^{8}({}^{3}\mathbf{F})4d$		7/2	100 475.82		34 ⁴ G	34	$({}^{3}F) {}^{2}F$
$3d^{8}({}^{3}\mathrm{F})4d$		⁹ / ₂	100 619.26		32 ² G	30	( ³ F) ⁴ G
$3d^{7}({}^{4}\mathrm{F})4s4p({}^{3}\mathrm{P}^{\circ})$	² D°	⁵ /2 ³ /2	101 754.80 102 742.74				
3d ⁸ ( ³ F)4d	² D	⁵ / ₂ ³ / ₂	103 025.58 103 663.50		85 90	9 4	( ³ F) ² F ( ¹ D) ² D

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Ni II-Continued

Configuration	Term	J	Level (cm ⁻¹ )	8		Lea	ding	percentages	
3d ⁸ ( ³ F)5p	⁴ D°	⁷ / ₂ ⁵ / ₂ ³ / ₂ ¹ / ₂	103 653.03 104 503.22 105 439.85 106 022.79						
$3d^8({}^3\mathrm{F})5p$	²G°	9/2 7/2	104 081.04 106 620.53		60 58	3 2	2 24	⁴G° ⁴G°	
$3d^8({}^3\mathbf{F})5p$	⁴G°	¹¹ / ₂ ⁷ / ₂ ⁹ / ₂ ⁵ / ₂	104 147.29 105 499.05 105 588.89 106 283.16		55 41	2 3	24 18	² G° ² G°	
3d ⁸ ( ³ F)5p	⁴ F°	9/2 5/2 3/2	104 298.23 105 668.78 106 369.30		53	2	24	⁴G°	
$3d^8(^3\mathbf{F})5p$		7/2	104 646.52		39	<b>⁴F°</b> 3	33	² F°	
$3d^8({}^3\mathbf{F})5p$	² F°	7/2 5/2	105 838.06 107 082.21		46	3	32	4 <b>F</b> °	
$3d^{8}({}^{3}\mathrm{F})5p$	² D°	5/2 3/2	105 861.19 107 142.12						
$3d^{7}({}^{4}\mathbf{P})4s4p({}^{3}\mathbf{P}^{\circ})$	⁶ D°	⁹ /2	105 981.50?						
$3d^{8}(^{1}\mathrm{D})5s$	² D	⁵ /2 3/2	106 007.89 106 133.14		80 87	2	20 9	( ³ P) ⁴ P ( ³ P) ² P	
$3d^{7}({}^{4}\mathrm{P})4s4p({}^{3}\mathrm{P}^{\circ})$	⁴S°	³ /2	107 737.81						
3d*( ³ P)5s	⁴₽	⁵ /2 3/2 1/2	108 368.05 108 548.61 108 763.32		80 94 98	2	20 5 2	( ¹ D) ² D ( ¹ D) ² D ( ³ P) ² P	
$3d^{7}({}^{4}P)4s4p({}^{3}P^{\circ})$	⁶ P°	3/2	109 038.84						
3d ⁷ ( ² G)4s4p( ³ P°)	4 <b>F</b> •	9/2 7/2 5/2 3/2	109 148.05 109 846.00 110 573.36 111 120.54						
3d ⁸ ( ³ P)5s	²P	³ / ₂ ¹ / ₂ 9/	109 269.83 109 675.72		90 98		7 2	( ¹ D) ² D ( ³ P) ⁴ P	
$2d^{7}(^{2}C)/adn(^{3}P^{\circ})$	40.	72	111 799 70						
3d ⁷ ( ⁴ F)4s4p( ¹ P [•] )	4G•	⁷² 11/2 9/2 5/2	112 422.19? 113 753.04 115 108.09		67 50	2	8 8	⁴₽° ²₽°	
$3d^{8}(^{1}\mathrm{D})4d$	²F	5/2 7/2	112 686.30 112 719.75		66 77	1	3 9	( ¹ D) ² D ( ³ P) ⁴ D	
$3d^8(^1\mathrm{D})4d$	² D	³ / ₂ ⁵ / ₂	112 906.93 113 407.31		62 55	2 2	<b>2</b> 5	( ³ P) ² D ( ¹ D) ² F	

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Configuration	Term	J	Level (cm ⁻¹ )	g		1	Leading	, percentages
$3d^8(^1\mathrm{D})4d$	²G	9/2 7/2	113 172.96 113 177 61		84		15 10	$({}^{3}P) {}^{4}F$ $({}^{3}P) {}^{2}F$
	»_	/2	113 111.01				10	(1) 1
$3d^{\circ}(^{1}\mathrm{D})4d$	°P	1/2 3/2	113 225.06 113 408.71		78		13 13	(°P) *D
$3d^{7}({}^{4}\mathrm{F})4s4n({}^{1}\mathrm{P}^{\circ})$	4 <b>F</b> °	9/2	113 391 95		63		34	4G•
ou (1) 101p(1)		5/2 5/2	115 120.00?		61		16	² F°
		3/2	115 592.25?		42		30	⁴D°
$3d^{8}(^{1}\mathrm{D})4d$	² S	¹ / ₂	113 623.10		85		10	( ³ P) ⁴ P
$3d^7$ 4s4p		⁷ / ₂	114 052.04		29	⁴G°	28	⁴ F°
$3d^{8}(^{3}\mathbf{P})4d$	⁴D	7/2	114 836.63		79		20	$(^{1}D)^{2}F$
		5/2	114 874.88		72		19	$({}^{1}\mathbf{D}) {}^{2}\mathbf{D}$
		3/2	114 942.42		79		11	$(^{1}D)^{2}P$
		1/2	114 970.19		87		12	( ¹ D) ² P
$3d^{7}(^{2}\text{H})4s4p(^{3}\text{P}^{\circ})$	⁴G°	11/2	114 858.88					
		⁹ / ₂	115 612.88					
		1/2	116 275.81					
		⁹ / ₂	116 754.93					
$3d^{7}(^{2}P)4s4p(^{3}P^{\circ})$	² D°	3/2	114 869.35		62			
		5/2	116 893.98		50		33	⁴ D°
$3d^{7}(^{2}G)4s4p(^{3}P^{\circ})$	² <b>F</b> °	⁷ / ₂	115 000.25		51		22	⁴ D°
$3d^8({}^1\mathrm{G})5s$	$^{2}G$	9/2	115 081.36		100			
		⁷ / ₂	115 085.36		100			
3d  4s4p	4D.	⁷ /2	115 209.85		55		18	² F°
$3d^7 4s4p$		⁵ /2	115 565.98		32	⁴D°	25	4F°
$3d^{8}(^{3}P)4d$	۴F	9/2	115 739.15		84		15	$(^{1}D)^{2}G$
• • • • • • • • • • • • • • • • • • •		7/2	115 827.12		82		8	
		5/2	115 956.71		68		13	$\binom{^{3}\mathbf{P}}{^{2}\mathbf{F}}$
		3/2	116 167.76		97		1	( ³ P) ⁴ P
		³ / ₂	115 785.06					
$3d^7 4s^2$	² D1	⁵ / ₂	115 870.28		77		23	² D2
$3d^{8}(^{3}\mathrm{P})4d$	$^{2}\mathbf{F}$	7/2	116 145.69		82		11	( ³ P) ⁴ F
$3d^{8}({}^{3}\mathrm{P})4d$		⁵ ∕₂	116 191.47		38	$^{2}\mathbf{D}$	24	( ³ P) ⁴ F
$3d^{8}(^{3}\mathrm{P})4d$	4P	1/2	116 261.81		86		11	$(^{1}D)^{2}S$
		3/2	116 312.34		85		8	$({}^{1}\mathbf{D}) {}^{2}\mathbf{P}$
		5/2	116 732.51		41		28	$(^{3}P)$ $^{2}D$
$3d^7 4s4p$	⁴D°	7/2	116 512.06					
$3d^{8}(^{3}P)4d$	² P	1/2	116 786.42		89		7	$({}^{1}\mathbf{D}) {}^{2}\mathbf{P}$
		3/2	116 838.33		91		4	$({}^{3}\mathbf{P}) {}^{2}\mathbf{D}$
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Ni II-Continued

Configuration	Term	J	Level (cm ⁻¹ )	8	Leading percentages			
3d ⁸ ( ³ F)6s	⁴F	9/2 7/2 5/2 3/2	116 833.15 117 074.70 118 314.82 119 100.06					<u></u>
$3d^7(a^2\mathrm{D})4s4p(^3\mathrm{P}^{\circ})$	⁴ F°	9/2 7/2	117 573.68 117 972.47					
$3d^{7}(^{2}\mathrm{P})4s4p(^{3}\mathrm{P}^{\circ})$		³ /2	117 662.11		37	4S.	12	² D°
$3d^8(^1\mathrm{D})5p$		³ /2	117 763.91		36	² D*	12	² P°
$3d^8(^1\mathrm{D})5p$	² D°	⁵ /2	117 872.78		65			
$3d^{7}(^{2}\mathrm{H})4s4p(^{3}\mathrm{P}^{\circ})$	² I°	¹¹ / ₂ ¹³ / ₂	118 248.98 119 010.21					
$3d^8({}^3\mathrm{F})6s$	²F	7/2 5/2	118 294.17 119 315.44					
$3d^8(^1\mathrm{D})5p$	² F°	5/2 7/2	118 379.11 118 563.39					
$3d^8(^1\mathrm{D})5p$		³ / ₂	118 442.81		37	² P°	35	² D°
$3d^8(^1\mathrm{D})5p$	² P°	¹ / ₂	118 <b>631.95</b>		50		29	3d ⁷ 4s4p ⁴ D°
$3d^8({}^3\mathrm{F_4})4f$	²[1]°	1/2 3/2	118 774.76 118 809.34?		100 87		13	² [2]°
$3d^{8}({}^{3}\mathrm{F_{4}})4f$	²[7]°	¹³ / ₂ ¹⁵ / ₂	118 8 <b>03</b> .82 118 848. <b>9</b> 2		100 100			
$3d^8({}^3\mathrm{F_4})4f$	²[2]°	⁵ /2 ³ /2	118 828.61 118 877.09		92 87		8 13	² [3]° ² [1]°
$3d^8({}^3\mathrm{F_4})4f$	²[3]°	7/2 5/2	118 874.11 118 897.94		97 92		3 8	² [4]° ² [2]°
$3d^8({}^3\mathrm{F}_4)4f$	²[6]°	¹¹ / ₂ 13/ ₂	118 892.99 118 893.24		99 100			
$3d^8({}^3\mathrm{F_4})4f$	² [4]°	9/2 7/2	118 914.34 118 923.20		99 97		3	² [3]°
$3d^8({}^3\mathrm{F_4})4f$	²[5]°	⁹ / ₂ ¹¹ / ₂	118 927.02 118 939.53		99 99			
$3d^8({}^3\mathrm{F})5d$	⁴D	7/2 1/2 3/2	119 656.25 121 111.90 121 115.59		84 48 44		13 30 34	⁴F ²P ²P
$3d^8({}^3\mathrm{F})5d$	4P	⁵ /2 1/2	119 665.29 121 925.16		67 51		30 43	⁴D ⁴D
3d ⁸ ( ³ F)5d	⁴H	¹³ / ₂ ¹¹ / ₂ ⁹ / ₂ ⁷ / ₂	119 773.60 121 180.55 121 190.34 122 047.29		100 59 59 77		30 27 18	²H ²H ⁴G

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Configuration	Term	J	Level (cm ⁻¹ )	8		1	eading	percentages
3 <i>d</i> *( ³ P)5p	⁴ P°	⁵ /2 ³ /2 ¹ /2	119 796.98 120 166.52 120 316.02		51 36		19 17	( ¹ <b>D</b> ) ² <b>D</b> °
3d ³ ( ³ F)5d	⁴G	¹¹ / ₂ 7/ ₂ 9/ ₂ 5/ ₂	119 833.00 121 240.90 121 294.67 122 144.99		53 42 43 59		34 30 25 35	⁴ H ² F ² G ⁴ F
$3d^8({}^3\mathrm{F})\bar{5}d$	²H	¹¹ / ₂ ⁹ / ₂	119 889.47 122 140.71		56 59		36 25	⁴G ⁴H
$3d^8({}^3\mathrm{F})5d$	² P	³ / ₂ ¹ / ₂	119 909.72 122 112.94?		59 65		18 26	⁴P ⁴P
3d ⁸ ( ³ F)5d	4F	9/2 7/2 3/2	119 913.33 121 317.89 122 084.79		59 41 62		34 30 26	⁴G ²G ⁴D
$3d^8({}^3\mathbf{F})\bar{b}d$	$^{2}\mathbf{F}$	7/2 5/2	120 002.86 122 175.42?		60 52		20 20	⁴ F ² D
$3d^8({}^3\mathbf{F})5d$	²G	9/2 7/2	120 044.95 122 270.05		58 61		23 18	⁴F ⁴G
$3d^{*(3}\mathbf{F})5d$		ō/2	120 144.17		37	² D	18	⁴D
$3d^*({}^3\mathbf{F}_3)4f$	²[1]°	¹ / ₂ ³ / ₂	120 189.55 120 199.18		60 88		40 12	² [0] [•] ² [2] [•]
$3d^{*}({}^{3}\mathbf{F}_{3})4f$	²[ <b>2</b> ]°	5/2 3/2	120 203.49 120 222.89		99 88		1 12	²[3]° ²[1]°
$3d^{\kappa}({}^{3}\mathbf{F}_{3})4f$	²[6]°	¹¹ / ₂ 13/ ₂	120 211.30 120 218.22		100 100			
$3d^{*}(^{3}\mathbf{F}_{3})4f$	²[3]°	7/2 5/2	120 250.17 120 271.97		98 99		1 1	² [4] [•] ² [2] [•]
$3d^8({}^3\mathbf{F}_3)4f$	²[4]°	7/2 9/2	120 268.81 120 281.11		98 97		1 3	² [3] [•] ² [5] [•]
$3d^{8}({}^{3}\mathrm{F}_{3})4f$	²[5]°	¹¹ / ₂ 9/ ₂	120 270.44 120 272.53		100 97		3	² [4]°
3d ⁸ ( ³ P)5p	4D.	7/2 5/2 3/2 1/2	120 903.31 121 325.09 121 385.80 121 561.06		81 63 54 83		27	²D*
$3d^{8}({}^{3}\mathrm{F}_{2})4f$	² [1]°	³ / ₂ ¹ / ₂	121 042.52 121 090.71		90 99		9	²[2]°
$3d^8({}^3\mathbf{P})5p$		³ /2	121 042.57		35	² <b>P°</b>	18	² D•
$3d^{8}({}^{3}\mathrm{P})5p$	² D°	⁵ /2	121 050.66		57		20	⁴D•
$3d^{8}({}^{3}\mathrm{F})6p$	⁴G°	11/2	121 120.37					

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Ni II-Continued

Configuration	Term	J	Level (cm ⁻¹ )	g	Leading percentages				
$\overline{3d^8({}^3\mathrm{F}_2)4f}$	² [5]°	¹¹ / ₂ 9/ ₂	121 120.88 121 125.41		99 99				
$3d^8({}^3\mathrm{F}_2)4f$	²[2]°	⁵ /2 ³ /2	121 14 <b>6</b> .98 121 161.81		94 90		5 9	² [3]° ² [1]°	
$3d^8({}^3\mathrm{F}_2)4f$	² [4]°	7/2 9/2	121 178.56 121 180.54		86 99		13	² [3]°	
$3d^8({}^3\mathrm{F}_2)4f$	²[3]°	7/2 5/2	121 192.32 121 194.14		86 94		13 5	² [4]° ² [2]°	
$3d^8({}^3\mathrm{F})5d$		⁵ /2	121 227.80		37	⁴D	36	² F	
$3d^8({}^1\mathrm{G})4d$	² I	¹¹ / ₂ ¹³ / ₂	121 437.68 121 476.56		100 100				
$3d^8(^3\mathbf{P})5p$	⁴ S°	3/2	121 456.30		43		23	² D°	
$3d^{7}(^{2}\mathrm{H})4s4p(^{3}\mathrm{P}^{\circ})$	²G°	9/2 7/2	121 692.55 121 862.57						
		³ / ₂	121 699.02						
$3d^8({}^3\mathbf{P})5p$		³ /2	121 800.34		32	² P°	28	² D°	
$3d^8({}^1\mathrm{G})4d$	²F	5/2 7/2	122 080.25 122 086.58		99 100				
$3d^8({}^3\mathrm{F})6p$	⁴ F°	⁹ /2	122 441.22						
$3d^{8}({}^{1}\mathrm{G})4d$	²H	⁹ / ₂ ¹¹ / ₂	122 790.41 122 821.63		100 100				
$3d^8({}^3F)6p$	⁴D°	7/2	122 812.97						
$3d^{8}({}^{1}\mathrm{G})4d$	²G	9/2 7/2	122 837.33 122 847.60		99 100				
$3d^{8}({}^{3}\mathrm{F})6p$	² G°	⁹ /2	123 434.60						
$3d^{7}(^{2}\text{H})4s4p(^{3}\text{P}^{\circ})$	² H°	9/2 11/2	124 652.00 125 003.41						
$3d^8({}^1\mathrm{G})5p$	²H°	9/2 11/2	126 679.98 126 857.97						
$3d^7(^4\mathrm{P})4s4p(^1\mathrm{P}^{\circ})$	4S.	³ /2	126 738.82						
$3d^{8}({}^{1}\mathrm{G})5p$	² F°	7/2 5/2	127 219.57 127 331.60						
3d ⁸ ( ³ F)7s	⁴F	9/2 7/2 5/2 3/2	127 867.13 127 991.56 129 294.51 130 135.19						
3d ⁸ ( ¹ G)5p	²G•	9/2 7/2	127 885.86 127 895.33						

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Configuration	Term	J	Level (cm ⁻¹ )	8	Leading percentages			
$3d^8({}^3\mathbf{F}_4)5f$	²[1]°	³ / ₂ ¹ / ₂	128 732.03 128 799.64		87 100	13	² [2]°	
$3d^8({}^3\mathrm{F}_4)5f$	²[2]°	⁵ /2 ³ /2	128 803.23 128 822.23		92 87	8 13	² [ <b>3</b> ]° ² [1]°	
$3d^8({}^3F_4)5f$	²[7]°	¹³ / ₂ ¹⁵ / ₂	128 818.41 128 827.05		100 100			
3d ⁸ ( ³ F ₄ )5f	²[3]°	7/2 5/2	128 827.15 128 853.87		97 92	8	² [2]•	
$3d^8({}^3\mathrm{F}_4)5f$	²[6]°	¹¹ / ₂ ¹³ / ₂	128 837.11 128 855. <b>60</b>		99 100			
$3d^8({}^3\mathrm{F_4})5f$	²[4]*	9/2 7/2	128 853.91 128 867.00		100 97			
$3d^{8}({}^{3}\mathrm{F}_{4})5f$	²[5]°	⁹ /2 ¹¹ /2	128 862.49 128 869.89		100 100			
$3d^{8}({}^{3}\mathrm{F}_{4})5g$	² [0]	¹ /2	128 937.47		100			
$3d^{8}({}^{3}\mathrm{F}_{4})5g$	² [1]	³ / ₂ ¹ / ₂	128 939.76 128 939.76		100 100			
$3d^8({}^3\mathrm{F_4})5g$	²[2]	5/2 3/2	128 944.36 128 944.36		100 100			
$3d^{8}({}^{3}\mathrm{F}_{4})5g$	² [8]	$^{17}_{15/2}$	128 946.17 128 946.15		100 100			
$3d^8({}^3\mathrm{F_4})5g$	² [3]	7/2 5/2	128 950.84 128 950.89		100 100			
$3d^8({}^3\mathbf{F}_4)5g$ .	² [4]	9/2 7/2	128 958.34 128 958.40		100 100			
$3d^8({}^3\mathrm{F_4})5g$	²[7]	15/ 13/2	128 960.74 128 960.74		100 100			
$3d^8({}^3\mathrm{F_4})5g$	² [5]	¹¹ / ₂ 9/ ₂	128 964.63 128 964.62		100 100			
$3d^8({}^3\mathrm{F_4})5g$	²[6]	¹³ / ₂ 11/ ₂	1 <b>28 966.5</b> 1 128 966.51		100 100			
3d ⁸ ( ³ F)7s	² F	7/2 5/2	129 271.72 130 236.26					
3d ⁸ ( ³ F)6d	4P	5/2 3/2 1/2	129 284.50 129 479.73 130 710.85					
3d ⁸ ( ³ F)6d	⁴D	7/2 5/2 3/2	129 297.91 129 842.33 130 942 30					

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Configuration	Term	J	Level (cm ⁻¹ )	g		Leading	g percentages
$3d^8(^3\mathrm{F})6d$	4H	¹³ / ₂ ¹¹ / ₂ ⁹ / ₂ ⁷ / ₂	129 367.91 129 396.04 130 757.51 131 637.10				
$3d^8(^3\mathbf{F})6d$	4F	9/2 7/2 5/2 3/2	129 419.58 129 474.27 130 730.53 131 620.45				
$3d^8({}^3\mathrm{F})6d$	⁴G	¹¹ / ₂ 9/2 7/ ₂ 5/ ₂	129 424.03 129 503.24 130 815.91 131 670.87				
$3d^7(^4\mathrm{P})4s4p(^1\mathrm{P}^\circ)$	4D.	7/2 5/2 3/2 1/2	129 782.07 129 988.05 130 331.78 130 570.42				
$3d^8({}^3\mathbf{F}_3)5f$	²[0]°	¹ /2	130 147.87	1	51	49	² [1]•
$3d^8({}^3\mathrm{F}_3)5f$	² [1]°	³ /2	130 174.03		88	11	² [2]°
$3d^8({}^3F_3)5f$	² [2]°	5/2 3/2	130 184.39 130 197.23		100 88	12	² [1]°
$3d^8({}^3F_3)5f$	² [6]°	¹¹ / ₂ 13/ ₂	130 184.61 130 187.81		100 100		
$3d^{8}({}^{3}\mathrm{F}_{3})5f$	²[5]°	¹¹ /2 9/2	130 205.62 130 206.90		100 98		
$3d^{8}({}^{3}\mathrm{F}_{3})5f$	²[3]°	⁷ /2 ⁵ /2	130 208.89 130 227.52		97 100		
$3d^8({}^3\mathrm{F}_3)5f$	² [4]°	9/2 7/2	130 215.50 130 225.87		98 97		
$3d^{8}({}^{3}\mathrm{F}_{3})5g$	² [1]	³ / ₂ ¹ / ₂	130 301.40 130 301.40		100 100		
$3d^8({}^3F_3)5g$	²[2]	⁵ /2 ³ /2	130 306.97 130 306.97		9;9 99		
$3d^8({}^3F_3)5g$	² [7]	¹⁵ / ₂ ¹³ / ₂	130 308.71 130 308.71		100 100		
$3d^8({}^3F_3)5g$	² [3]	7/2 5/2	130 314.07 130 314.07		99 99		
$3d^{8}({}^{3}F_{3})5g$	² [4]	⁹ / ₂ 7/ ₂	130 320.97 130 320.94		100 100		
$3d^8({}^3F_3)5g$	² [6]	¹¹ / ₂ ¹³ / ₂	130 321.73 130 321.73		99 99		
$3d^8({}^3\mathbf{F}_3)5g$	² [5]	¹¹ / ₂ ⁹ / ₂	130 324.72 130 324.72		100 100		
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Ni II-Continued

Configuration	Term	J	Level (cm ⁻¹ )	g		Leading	g percentages
$3d^8({}^3\mathbf{F})7p$	⁴ F°	⁹ /2	130 470.90				
$3d^8({}^3\mathrm{F})7p$	4D•	⁷ /2	130 480.55				
$3d^{8}({}^{3}\mathrm{F})7p$	⁴G°	11/2	130 661.32				
$3d^8(^3\mathrm{F})6d$	²P	³ / ₂ ¹ / ₂	130 691.35 131 655.83				
$\mathbf{3d^8(^3F)6d}$	²H	¹¹ / ₂ 9/ ₂	130 751.03 131 686.56				
$3d^8(^3\mathbf{F})6d$	²F	7/2 5/2	130 765.26 131 796.26				
$3d^8({}^3\mathbf{F})6d$	²G	9/2 7/2	130 801.33 131 750.73				
$\mathbf{B}d^{\mathbf{\theta}}(^{1}\mathbf{D})6s$	² D	⁵ /2 ³ /2	130 900.65 130 942.36				
$\mathbf{Bd}^{\mathbf{e}}(^{3}\mathbf{F})\mathbf{6d}$	² D	⁵ /2	131 032.01				
$3d^8({}^3\mathbf{F}_2)5f$	²[1]°	¹ /2 ³ /2	131 063.85 131 075.78		99 87	12	² [2]*
$3d^{s}(^{3}\mathbf{F}_{2})5f$	²[5]°	⁹ / ₂ ¹¹ / ₂	131 093.30 131 094.02		99 99		
$3d^8({}^3\mathbf{F}_2)5f$	²[2]*	5/2 7/2	131 103.18 131 115.15		91 89	8 10	²[3]°
$3d^{8}({}^{3}\mathbf{F}_{2})5f$	²[ <b>4</b> ]°	⁹ / ₂ ⁷ / ₂	131 115.28 131 131.15		99 66	33	² [3]*
$3d^{*}({}^{3}\mathbf{F}_{2})5f$	²[3]°	7/2 5/2	131 124. <b>9</b> 6 131 133.58		66 91	33 8	² [4] [•] ² [2] [•]
$3d^8({}^3\mathbf{F}_2)5g$	²[2]°	⁵ /2 3/2	131 211.85 131 211.85		99 99	1 1	$({}^{1}D_{2}) {}^{2}[2]$
$3d^8({}^3\mathbf{F}_2)5g$	²[6]*	¹³ / ₂ ¹¹ / ₂	131 218.56 131 218.56		99 99		
$3d^{8}({}^{3}\mathbf{F}_{2})5g$	²[3]°	7/2 5/2	131 222.98 131 222.98		99 99		
$3d^8({}^3\mathbf{F}_2)5g$	²[4]°	⁹ /2 7/2	131 232.83 131 232.83		99 99		
$3d^8({}^3\mathbf{F}_2)5g$	²[5]°	¹¹ / ₂ 9/ ₂	131 233.31 131 233.31		99 99		
$3d^{(2}G)4s4p({}^{1}P^{\circ})$	² H•	¹¹ / ₂ 9/2	131 424.32? 132 311.98?				
$3d^{7}({}^{4}\mathrm{P})4s4p({}^{1}\mathrm{P}^{\bullet})$	⁴ P°	$\frac{5}{2}$ $\frac{1}{2}$ $\frac{3}{2}$	131 834.94 132 120.70 132 225 15				

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131 928.77 132 729.48 132 869.16 132 818.16 132 912.15 132 927.97 132 982.51 133 001.47 133 014.08 133 031.00	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
132 729.48 132 869.16 132 818.16 132 846.53 132 912.15 132 927.97 132 982.51 133 001.47 133 014.08 133 031.00	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
132 818.16 132 846.53 132 912.15 132 927.97 132 982.51 133 001.47 133 014.08 133 031.00	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
132 912.15 132 927.97 132 982.51 133 001.47 133 014.08 133 031.00	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
132 982.51 133 001.47 133 014.08 133 031.00	84 16 $({}^{3}P_{2}) {}^{2}[1]^{\circ}$ 83 16 $({}^{3}P_{2}) {}^{2}[5]^{\circ}$
133 014.08 133 031.00	83 16 $({}^{3}\mathbf{P}_{2}) {}^{2}[5]^{\circ}$
	83 16 $({}^{3}P_{2}) {}^{2}[5]^{\circ}$
133 169.92 134 208.30	
133 190.19? 133 209.30 133 528.02 133 853.04	
133 443.89 133 613.99 133 857.73	
133 445.75 134 380.82	
133 625.96	
133 715.13 133 809.76 135 116.72 135 983.22	
133 734.98 133 735.26	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
133 850.83 133 973.33 134 156.28 134 283.76	
133 862.21 134 241.96	
133 903.00 134 053.05	$\begin{array}{cccc} 80 & 7 & ({}^{3}\mathbf{P}) \; {}^{2}\mathbf{D} \\ 69 & 16 & ({}^{1}\mathbf{D}) \; {}^{2}\mathbf{F} \end{array}$
133 922.91 133 929.88	$\begin{array}{cccc} 83 & 16 & ({}^{3}\mathbf{P})  {}^{4}\mathbf{F} \\ 84 & 11 & ({}^{3}\mathbf{P})  {}^{2}\mathbf{F} \end{array}$
133 954.85 134 067.76	82 8 ( ³ P) ² P 84 9 ( ³ P) ⁴ P
	$133 \ 031.00$ $133 \ 169.92$ $134 \ 208.30$ $133 \ 190.19?$ $133 \ 209.30$ $133 \ 528.02$ $133 \ 528.02$ $133 \ 528.02$ $133 \ 528.02$ $133 \ 528.02$ $133 \ 528.02$ $133 \ 528.02$ $133 \ 528.02$ $133 \ 528.02$ $133 \ 528.02$ $133 \ 528.02$ $133 \ 528.02$ $133 \ 557.73$ $133 \ 445.75$ $134 \ 380.82$ $133 \ 625.96$ $133 \ 715.13$ $133 \ 625.96$ $133 \ 715.13$ $133 \ 734.98$ $133 \ 734.98$ $133 \ 735.26$ $133 \ 735.26$ $133 \ 973.33$ $134 \ 283.76$ $133 \ 862.21$ $134 \ 283.76$ $133 \ 903.00$ $134 \ 053.05$ $133 \ 922.91$ $133 \ 922.91$ $133 \ 954.85$ $134 \ 067.76$

Ni II-Continued

Configuration	Term	J	Level (cm ⁻¹ )	8		Leading	g percentages	
$3d^8({}^3\mathbf{F}_4)6f$	²[7]°	¹³ / ₂ 15/ ₂	134 238.44 134 251.30		100 100		1	
$3d^8({}^3\mathbf{F}_4)6f$	² [1]*	³ /2	134 249.72		87	13	²[ <b>2</b> ]*	
$3d^{8}({}^{3}\mathrm{F_{4}})6f$	²[ <b>3</b> ]•	7/2 5/2	134 252.85 134 294.99		97 91	3 9	² [4] [•] ² [2] [•]	
$3d^{8}({}^{3}\mathrm{F_{4}})6f$	²[2]°	³ / ₂ ⁵ / ₂	134 254.69 134 256.05		87 91	13 9	² [1] [•] ² [3] [•]	
3d ⁸ ( ³ F ₄ )6f	²[ <b>4</b> ]°	7/2 9/2	134 262.07 134 271.5 <b>9</b>		97 100	3	²[3] <b>*</b>	
$3d^{8}({}^{3}\mathrm{F}_{4})6f$	²[6]°	¹³ / ₂ ¹¹ / ₂	134 267.20 134 274.62		100 99	1	²[5] <b>°</b>	
$3d^{8}({}^{3}\mathrm{F}_{4})6f$	²[5]°	¹¹ / ₂ 9/ ₂	134 281.66 134 286.38		99 100	1	²[6]*	
$3d^{8}({}^{3}\mathrm{F}_{4})6g$	² [0]	¹ /2	134 320.12		100			
$3d^8({}^3\mathrm{F_4})6g$	² [1]	¹ / ₂ ³ / ₂	134 321.35 134 321.36		100 100			
$3d^{8}({}^{3}\mathrm{F_{4}})6g$	²[ <b>2</b> ]	⁵ /2 ³ /2	134 323.86 134 323.88		100 100			
$3d^8({}^3F_4)6g$	²[8]	¹⁵ / ₂ ¹⁷ / ₂	134 325.08 134 325.14		100 100			
$3d^{e}({}^{3}F_{4})6g$	²[3]	7/2 5/2	134 327.52 134 327.58		100 100			
$3d^8({}^3F_4)6g$	² [4]	9/2 7/2	134 331.78 134 331.88		100 100			
$3d^{8}({}^{3}\mathrm{F}_{4})6g$	² [7]	$^{13}_{15/2}$	134 333.36 134 333.40		100 100			
$3d^{8}({}^{3}\mathrm{F}_{4})6g$	² [5]	¹¹ /2 9/2	134 335.47 134 335.49		100 100			
$3d^8({}^3F_4)6g$	² [6]	¹¹ / ₂ ¹³ / ₂	134 336.63 134 336.66		100 100			
$3d^8({}^3F_4)6h$	²[1]°	¹ / ₂ , ³ / ₂	134 3 <b>36.8</b> 1					
$3d^8({}^3\mathrm{F}_4)6h$	²[2]°	³ /2, ⁵ /2	134 338.35					
$3d^{8}({}^{3}\mathbf{F}_{4})6h$	²[9]°	¹⁷ / ₂ , ¹⁹ / ₂	134 339.71					
$3d^{8}({}^{3}\mathrm{F}_{4})6h$	²[3]°	⁵ / ₂ , ⁷ / ₂	134 34 <b>0</b> .42					
$3d^8({}^3F_4)6h$	²[4]°	⁷ / ₂ , ⁹ / ₂	134 342.69					
$3d^{8}({}^{3}\mathrm{F}_{4})6h$	²[8]°	¹⁵ /2, ¹⁷ /2	134 344.32					
$3d^{8}({}^{3}\mathrm{F_{4}})6h$	²[5]°	⁹ / ₂ , ¹¹ / ₂	134 344.87		1			
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Configuration	Term	J	Level (cm ⁻¹ )	8		Leading	percentages
$\overline{3d^8({}^3\mathrm{F}_4)6h}$	²[6]*	¹¹ / ₂ , ¹³ / ₂	134 346.30				
$3d^8({}^3\mathrm{F}_4)6h$	²[7]°	¹³ /2, ¹⁵ /2	134 346.34				
$3d^{8}({}^{3}\mathrm{F})7d$	⁴D	7/2 5/2	134 527.24 134 978 47				
		3/2 3/2	136 054.50		Í		
$3d^8({}^3\mathrm{F})7d$	⁴P	5/2 3/2	134 539.37 134 670.07				
$3d^{8}({}^{3}\mathrm{F})7d$	⁴H	¹³ / ₂	134 583.07				
		9/2 9/2	134 597.43				
		7/2	136 895.36?				
$3d^{8}({}^{3}\mathrm{F})7d$	⁴F	⁹ / ₂	134 607.37				
		1/2 5/	134 642.09				
		3/2 3/2	136 852.44				
$3d^{8}({}^{3}\mathrm{F})7d$	⁴G	11/2	134 614.55				
		9/2 7/	134 658.60				
		5/2 5/2	135 986.06				
$3d^{7}(^{2}\mathrm{F})4s4p(^{3}\mathrm{P}^{*})$	² D°	5/2	134 783.14				
		3/2	<i>134 964.78</i>				
$3d^{7}(^{2}P)4s4p(^{1}P^{\circ})$	² P°	1/2 3/	135 053.14				
		⁹ 2	135 382.53				
$3d^{8}({}^{3}\mathrm{F})8s$	² F	⁷ /2 5/2	135 100.45 136 050.53				
$3d^{7}(^{2}\mathbf{P})AeAn(^{1}\mathbf{P}^{\circ})$	20.	5/	195 958 99				
5a (1/434p(1)		3/2 3/2	135 258.52				
$3d^{8}({}^{3}\mathrm{F})8p$	4G•	⁹ / ₂	135 261.99				
		11/ ₂	135 338.01				
$3d^8({}^3P_2)4f$	² [4] [•]	7/2 9/2	135 400.67 135 435 26		46 83	37 16	$\binom{{}^{3}\mathbf{P}_{2}}{\binom{{}^{1}\mathbf{D}_{2}}{2}} \binom{{}^{2}[3]^{\circ}}{\binom{{}^{2}}{4}}$
2,1 ⁸ ( ³ D) / f	21910	7/	195 111 17			00	$(^{3}P_{-})^{2}[A]^{\circ}$
ou $(\mathbf{r}_2)$ 4/	[3]	5/2 5/2	135 444.47 135 461.55		46 71	38 14	$\binom{1}{2} \binom{2}{2} \binom{3}{3}$
		7/2	135 464.86				
$3d^8({}^3\mathrm{P}_2)4f$	² [2]*	3/2	135 493.26		82	13	$\binom{1}{2} D_2 \binom{2}{2} [2]^{\circ}$
2 2		5√2	135 512.92		71	12	$({}^{3}P_{2}) {}^{2}[3]^{\circ}$
$3d^8({}^3\mathrm{P}_2)4f$	² [5]*	¹¹ / ₂	135 538.61?		84	16	$\binom{1}{2} \binom{2}{5}^{\circ}$
		⁹ /2	135 580.25		84	16	$(\mathbf{D}_2) - [\mathbf{D}]^2$
		⁹ / ₂	135 558.80				
$3d^8({}^3F_3)6f$	²[1]°	1/2 3/2	135 599.00		59	41	² [0]° ² [2]°
		∛ ₂	135 619.91		86	14	[4]

Ni 11-Continued

Configuration	Term	J	Level (cm ⁻¹ )	g		Leading	g percentages	
$3d^8({}^3\mathbf{F}_3)6f$	²[6]°	¹¹ / ₂ 13/ ₂	135 606.20 135 606.30		100 100			
$3d^8({}^3\mathrm{F}_3)6f$	²[2]°	⁵ /2 3/2	135 618.08 135 623.59		100 85	14	² [1]°	
$3d^{8}(^{3}\mathbf{F}_{3})6f$	²[3]°	7/2 5/2	135 622.60 135 630.63		97 100	3	² [4]°	
$3d^8({}^3\mathbf{F}_3)6f$	²[5]°	9/2 11/2	135 628.41 135 645.10		96 100	4	² [4]•	
$3d^8({}^3\mathbf{F}_3)6f$	² [4]*	7/2 9/2	135 629.40 135 640.53		97 96	3 4	² [3]° ² [5]°	
$3d^8(^3P_2)4f$	²[1]°	3/2 1/2	135 652.93 135 670.49		84 84	16 16	$({}^{1}D_{2}) {}^{2}[1]^{\circ} ({}^{1}D_{2}) {}^{2}[1]^{\circ}$	
$3d^{8}({}^{3}\mathbf{F}_{3})6g$	²[1]	¹ / ₂ ³ / ₂	135 682.28 135 682.29		100 100			
$3d^{8}({}^{3}\mathbf{F}_{3})6g$	²[2]	³ /2 ⁵ /2	135 685.36 135 685.43		100 100			
$3d^8({}^3\mathrm{F}_3)6g$	²[7]	$^{13}_{15/2}$	135 686.63 135 686.67		100 100			
$3d^{8}({}^{3}\mathrm{F}_{3})6g$	²[3]	7/2 5/2	135 689.44 135 689.47		99 99			
$3d^{*}({}^{3}\mathbf{F}_{3})6g$	²[ <b>4</b> ]	9/2 7/2	135 693.38 135 693.45		100			
$3d^{*}(^{3}\mathbf{F}_{3})6g$	²[6]	¹¹ / ₂ ¹³ / ₂	135 694.01 135 694.04		100 100			
$3d^{*}({}^{3}F_{3})6g$	²[5]	¹¹ / ₂ 9/ ₂	135 695.63 135 695.64		100 100			
$3d^{8}({}^{3}\mathrm{F}_{3})6h$	²[3]*	⁵ /2, ⁷ /2	135 700.04					
$3d^8({}^3\mathbf{F}_3)6h$	²[8]°	¹⁵ / ₂ , ¹⁷ / ₂	135 700.68					
$3d^{8}({}^{3}\mathbf{F}_{3})6h$	² [4]*	⁷ / ₂ , ⁹ / ₂	135 703.44					
$3d^{8}({}^{3}F_{3})6h$	² [7]°	¹³ /2, ¹⁵ /2	135 704.83					
$3d^{8}({}^{3}\mathbf{F}_{3})6h$	² [5]°	⁹ / ₂ , ¹¹ / ₂	135 705.68					
$3d^8({}^3F_3)6h$	² [6]	¹¹ / ₂ , ¹³ / ₂	135 706.06					
$3d^{7}({}^{2}\mathrm{F})4s4p({}^{3}\mathrm{P}^{\circ})$	²G°	7/2 9/2	135 746.06 136 076.26					
$3d^{8}(^{3}P_{1})4f$	² [2] [•]	³ /2	135 746.13		93	4	$({}^{1}D_{2}) {}^{2}[2]^{\circ}$	
$3d^8({}^3\mathrm{P}_1)4f$	²[ <b>3</b> ]•	⁵ /2 7/2	135 849.41 135 879.41		100 100			

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percentages
( ¹ D) ² F ( ¹ D) ² D ( ¹ D) ² P ( ¹ D) ² P ( ¹ D) ² D
$\binom{{}^{1}D_{2}}{\binom{{}^{1}D_{2}}{2}} \binom{{}^{2}[5]^{*}}{[5]^{*}}$
$\binom{{}^{1}D_{2}}{({}^{3}F_{2})} \binom{{}^{2}[1]}{[2]}$
( ¹ D) ² G ( ³ P) ² F ( ³ P) ² D
$({}^{3}F_{2}) {}^{2}[3]^{*}$ $({}^{1}D_{2}) {}^{2}[4]^{*}$
² [4] [•] ² [2] [•]

Ni II-Continued

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Configuration	Term	J	Level (cm ⁻¹ )	8		1	Leading	percentages
3d ⁸ ( ³ F)8p	²G°	9/2 7/2	136 673.64 137 562.74					
$3d^8(^3\mathbf{P})5d$	⁴ P	1/2 5/2	136 725.33 136 960.75		82 58		12 37	( ¹ D) ² S ( ³ P) ² F
$3d^8(^{3}\mathbf{P})5d$		3/2	136 732.74		31	$^{2}\mathbf{D}$	31	( ³ P) ⁴ P
$3d^{8}(^{3}\mathbf{P})5d$		3/2	136 899.33		38	4F	37	⁴P
$3d^8({}^3\mathrm{F})7d$	² P	¹ / ₂	136 955.28					
3 <i>d</i> ⁸ ( ³ F)9 <i>s</i>	4F	9/2 7/2 5/2 3/2	137 188.58 137 236.28 138 575.69 139 456.75					
$3d^8(^3\mathbf{P})5d$	²P	1/2 3/2	137 211.93 137 278.22?		85 67		8 19	( ¹ D) ² P ( ³ P) ² D
$3d^8({}^3\mathrm{F_4})7f$	² [2]*	⁵ /2	137 519.23					
$3d^8({}^3\mathrm{F_4})7f$	²[7]°	15/2	137 519.63					
$3d^{8}({}^{3}\mathrm{F}_{4})7f$	²[3]°	7/2 5/2	137 523.51 137 526.73					
$3d^8({}^3\mathbf{F_4})7f$	²[6]°	¹³ / ₂ ¹¹ / ₂	137 529.37 137 535.83					
$3d^8({}^3\mathrm{F_4})7f$	²[4]°	9/2 7/2	137 531.18 137 535.96					
$3d^8({}^3\mathbf{F_4})7g$	² [8]	¹⁵ / ₂ 17/ ₂	137 568.00 137 568.02					
$3d^8({}^3\mathrm{F_4})7g$	²[ <b>6</b> ]	¹³ / ₂ ¹¹ / ₂	137 573.19 137 573.19					
$3d^8({}^3\mathrm{F_4})7g$	²[5]	¹¹ / ₂	137 575.14					
$3d^{8}({}^{3}\mathrm{F})8d$	⁴P	⁵ /2	137 706.71					
$3d^8(^3\mathrm{F})8d$	⁴D	7/2 5/2	137 707.26 138 014.53		ŗ			
$3d^8(^3\mathbf{F})8d$	⁴H	¹³ / ₂ ¹¹ / ₂	137 735.22 137 742.95					
$3d^8({}^3\mathrm{F})8d$	4F	9/2 7/2	137 753.87 137 776.55					
$3d^{8}({}^{3}\mathrm{F})8d$	⁴G	¹¹ / ₂ 9/ ₂	137 754.78 137 782.50?					
$3d^8({}^3\mathrm{F})9p$	⁴ F°	9/2	138 121.88					
$0 \sqrt{1/2} E (4 - 4 - (1 \mathbf{P}^{\circ}))$	² G°	9/2	1.38 4.95 84?					

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Configuration	Term	J	Level (cm ⁻¹ )	g	Leading percentages
3d ⁶ ( ³ F)9s	² F	7/2 5/2	138 563.71 139 492.10		
$3d^8(^3\mathbf{P})6p$	4D.	⁷ / ₂	138 841.00		
$3d^8({}^3\mathrm{F}_3)7f$	²[6]°	¹³ /2	138 888.93		
$3d^8({}^3\mathrm{F}_3)7g$	² [7]	¹⁵ /2	138 928.70		
$3d^{8}({}^{3}\mathrm{F})8d$	² H	¹¹ / ₂	139 103.05		
$3d^8({}^3\mathrm{F}_2)7g$	²[6]	¹³ /2	139 834.24		
3d ⁸ ( ¹ G)6s	²G	9/2 7/2	140 006.17 140 008.76		
Ni III ( ³ F ₄ )	Limit		146 541.56		

### Z = 28

Fe I isoelectronic sequence

Ground state: 1s²2s²2p⁶3s²3p⁶3d⁸ ³F₄

Ionization energy =  $283\ 800\pm 200\ \text{cm}^{-1}\ (35.19\pm 0.02\ \text{eV})$ 

This analysis has been made by Shenstone (1954) and extended by Garcia-Riquelme (1958) who has also provided unpublished results.

Shenstone's line list includes the range 600-3000 Å. The spectrum has been reobserved and extended by Garcia-Riquelme and Velasco (1955) in the range 2300-8600 Å.

Some of Shenstone's identifications in  $3d^{7}4p$  have been changed by Roth (1968) in his theoretical study. He calculated the percentage compositions of the  $3d^{7}4p$  terms.

The  $3d^8$  and  $3d^74s$  configurations have been studied theoretically by Shadmi (1962) and by Shadmi, Caspi, and Oreg (1969). The leading percentages of the  $3d^8$  levels are taken from Pasternak and Goldschmidt (1972).

Some changes in the  $3d^{7}4s$  ³P and ³D levels suggested by Shadmi (1962) and agreed to by Shenstone are incorporated in this compilation.

Garcia-Riquelme has provided new terms for the known configurations  $3d^8$ ,  $3d^74s$ , and  $3d^74p$  and has extended the analysis further with the discovery of terms from the configurations  $3d^64s^2$ ,  $3d^74d$ ,  $3d^75p$ ,  $3d^74f$ ,  $3d^75s$ ,  $3d^75d$ , and  $3d^75g$ . With her new measurements, she has determined values for all levels above the ground

configuration and has calculated percentage compositions for  $3d^{7}4d$ , 4f, 5p, 5d, and 5g. In a few cases, we have changed her designations to correspond with her percentages. The uncertainty of the level values is  $\pm 0.1$  cm⁻¹.

In all the calculations, the percentages for the two  ${}^{2}D$  states of  $3d^{7}$ , distinguished by seniority, include the sum of contributions from both states. They are distinguished by the prefixes A and B.

Her value for the ionization energy determined from the  $3d^{7}(^{4}F)ns$  (n = 4,5,6) series is quoted here.

#### References

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Shenstone, A. G. (1954), J. Opt. Soc. Am. 44, 749.

Configuration	Term	J	Level (cm ⁻¹ )	Leading percenta	gei
3d ⁶	³ F	4	0.0	100	
	-	3	1 360.7	100	
		2	2 269.6	99	
3 <i>a</i> ⁸	¹ D	2	14 031.6	88 16	۶P
3d ⁶	3P	2	16 661.6	84 16	¹ D
	-		16 977.8	100	2
		0	17 230.7	100	
3a ⁶	¹ G	4	23 108.7	100	
3 <i>d</i> ⁸	¹ S	0	52 532.0	100	
$3d^{7}({}^{4}\mathrm{F})4s$	5F	5	53 703.93		
	-	4	54 657.83		
		3	55 406.29		
		2	55 952.21		
		1	56 308.24		
$3d^{7}({}^{4}\mathrm{F})4s$	⁸ F	4	61 338 58		
	-	3	62 605.58		
		2	63 471.93		

Ni III

Ni III—Continued

Configuration	Term	J	Level (cm ⁻¹ )	Leading percentages	
$\frac{1}{3d^7({}^4\mathbf{P})4s}$	⁵ P	3	71 067.35		
	_	2	71 384.10		
		1	71 842.42		
$3d^{7}(^{2}G)4s$	³ G	5	75 123.65		
		4	75 646.61		
		3	76 237.25		
$3d^{7}(^{4}\mathrm{P})4s$	³ P	2	78 303.54	47 53 ( ² P) ³ P	
		1	78 482.43	52 35	
		0	78 657.55	48 46	
$3d^{7}(^{2}\mathrm{P})4s$	³ P	2	79 143.01	47 53 ( ⁴ P) ³ P	
		1	79 749.22	56 39	
		0	80 621.10	43 51	
$3d^7(^2G)4s$	¹ G	4	79 250.11		
$3d^7(^2\mathrm{H})4s$	³ H	6	81 686.80		
		5	82 193.80		
		4	82 826.40		
$3d^7(a^2D)4s$	³ D	3	82 172.60		
		1	82 277.26	54 41 $(^{2}P)$ ¹ P	
		2	83 033.45		
$(^2\mathbf{P})4s$	¹ P	1	84 604.10	48 40 $(a^{2}D)^{1}D$	
$3d^{7}(^{2}\mathrm{H})4s$	$^{1}\mathbf{H}$	5	85 834.20		
$3d^7(a^2D)4s$	$^{1}\mathbf{D}$	2	8 <b>6 64</b> 5.88		
$3d^{7}({}^{2}\mathrm{F})4s$	³ F	2	97 841.60		
		3	97 995.81		
		4	98 237.93		
$3d^{7}(^{2}\mathrm{F})4s$	¹ <b>F</b>	3	101 954.90		
$3d^{7}({}^{4}\mathrm{F})4p$	⁵ F°	5	110 212.80	94 5 ( ⁴ F) ⁵ G°	
-		4	110 371.35	$65$ 29 $({}^{4}\mathbf{F}) {}^{5}\mathbf{D}^{\circ}$	
		3	111 221.20	78 17 $({}^{4}\mathbf{F}) {}^{5}\mathbf{D}^{\circ}$	
		2	111 914.53	88 9 ( ⁴ F) ⁵ D*	
			112 401.65	96	
$3d^7({}^4\mathbf{F})4p$	5 <b>D</b> •	4	111 898.65	63 26 ( ⁴ F) ⁵ F*	
		3	112 935.43	73 13 $({}^{4}\mathbf{F}) {}^{5}\mathbf{F}^{\bullet}$	
			113 001.47	78 8 (°F) °G°	
		0	114 295.45	88 8 (1₽) ⁻ D ⁻ 91 8 ( ⁴ P) ⁵ D [•]	
2d ⁷ (4F)/-	50.	E	110 707 05		
ou ( <b>r</b> )4p	G	5	112 787.85		
		4	11.8 705 19	52 12 (TF)°G° 94 9 (415)5⊂•	
		3	114 110.20	רייים פון עריים פון אין אין אין אין אין אין אין אין אין אי	
		2	114 371.01	88 5 ( ⁴ <b>F</b> ) ⁵ <b>D</b> [•]	
$3d^7({}^4\mathbf{F})4p$	³ G•	5	115 272.26	87 19 ( ⁴ 17) 5 <u>0</u> .•	
		4	116 674.39	88 9 ( ⁴ F) ⁸ F [•]	
	1	0			

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Ni III-Continued

3100					
	4	116 191 09	85	10	( ⁴ F) ³ G°
r	3	117 250 80	83	8	$({}^{4}\mathbf{F}) {}^{3}\mathbf{G}^{*}$
	2	118 114.95	92	0	(1) U
350	9	110 715 05			(4E) 3E.
^o D ^o	3	118 /40.20	90	5	( F) F
	2	119 009.54	92		
	1	120 272.32	93		
³ D	1	121 192.93			
	2	121 411.60			
	3	121 802.45			
⁵S°	2	122 282.40	99		
$^{1}\mathbf{D}$	2	125 433.55			
5D.	2	129 913 10	82	7	( ⁴ <b>F</b> ) ⁵ D°
-	3	129 954 00	84	7	
	1	129 957 95	75	. 7	
	Ô	130 190 05	96	9	
	4	130 312.30	93	6	
³ S°	1	130 863.50	53	12	( ² P) ³ S°
3	-	101 500 50			2011
°H°	5	131 500.50	74	15	$({}^{*}G) {}^{*}H^{*}$
	4	132 156.50	61	28	( <b>*G</b> ) <b>*F</b> *
	6	132 168.60	96		
³ F°	4	131 7 <b>92.02</b>	41	33	$(^{2}G)^{3}H^{\circ}$
	3	133 158.50	78	11	( ² G) ³ G°
	2	134 231.90	94		
⁵ P°	2	132 818.26	45	21	( ² <b>P</b> ) ³ <b>P</b> [•]
-	3	133 095.89	71	19	$({}^{4}P) {}^{3}D^{\circ}$
	1	133 339.70	73	20	( ⁴ P) ³ S [•]
300	0	199 861 8	69	19	$(a^{2}D)^{3}P^{2}$
ľ	1	199 976 70	45	19	$({}^{4}\mathbf{P}) {}^{3}\mathbf{D}^{\circ}$
	$\frac{1}{2}$	133 642.58	43	19	$(^{2}P)^{3}D^{2}$
las					( ² C) ³ E ⁸
'G*	4	133 324.70	47	24	( <b>*G</b> ) * <b>F</b> *
³ D°	3	133 390.94	65	20	( ⁴ P) ⁵ P°
	2	133 500.97	42	37	( ⁴ P) ⁵ P°
	1	133 839.54	54	15	$(^{2}P)^{3}D^{\circ}$
3G.	5	133 692.00	78	19	( ² G) ¹ H [•]
J	3	134 334 79	70	16	$(^{2}\mathbf{G})$ ¹ $\mathbf{F}^{\circ}$
	4	134 414.77	73	14	$(^{2}G)$ ¹ G°
¹ H°	5	134 217.60	62	23	( ² G) ³ H°
150		195 000 00	-7		$(^{2}C)^{3}C^{2}$
. F	3	135 023.20	57	15	(0)0
³ P°	0	135 334.90	52	35	$(^{2}P)^{1}S^{\circ}$
	2	135 350.33	75	10	$(a^{2}D)^{3}P^{\circ}$
		100 000 70	79	11	$(^{2}\mathbf{P})$ $^{3}\mathbf{D}^{\circ}$
	³ D [•] ³ D ⁵ S [•] ¹ D ⁵ D [•] ³ S [•] ³ H [•] ³ F [•] ³ P [•] ¹ G [•] ³ D [•] ³ G [•] ¹ H [•] ¹ F [•] ³ P [•]	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3 $117 250.00$ 2 $118 114.95$ ³ D*       3 $118 745.25$ 1 $120 272.32$ ³ D       1 $121 192.93$ 2 $121 411.60$ 3 $121 802.45$ ⁵ S*       2 $122 282.40$ ¹ D       2 $125 433.55$ ⁵ D*       2 $129 913.10$ 3 $129 954.00$ $129 957.95$ 0 $130 190.05$ 4 $130 312.30$ ³ S*       1 $130 863.50$ ³ H*       5 $131 500.50$ 4 $132 156.50$ $6$ $3TF*$ 4 $132 168.60$ ³ F*       4 $131 792.02$ $3 133 158.50$ $2$ $134 231.90$ ⁵ P*       2 $132 864.8$ $1 1 33 339.70$ $2$ $133 642.58$ ¹ G*       4 $133 339.70$ ³ P*       0 $132 864.8$ $1 33 339.70$ $133 839.54$ ³ G*       5 $133 692.00$ $3 134 334.79$	3 $117 230.60$ $83$ $2$ $118 114.95$ $92$ $3$ $118 745.25$ $90$ $2$ $119 669.54$ $92$ $3$ $120 272.32$ $93$ $3$ $121 192.93$ $92$ $2$ $121 282.40$ $99$ $1$ $2$ $122 282.40$ $99$ $1$ $2$ $125 433.55$ $5$ $5$ $2$ $122 99.13.10$ $82$ $3$ $129 957.95$ $75$ $0$ $3$ $129 957.95$ $75$ $0$ $3$ $129 957.95$ $75$ $0$ $3$ $129 957.95$ $75$ $0$ $3$ $129 957.95$ $75$ $0$ $3$ $129 957.95$ $75$ $0$ $3$ $130 190.05$ $86$ $41$ $3$ $130 192.05$ $86$ $61$ $3$ $131 50.50$ $74$ $133 158.50$ $78$ $3$ $131 792.02$ $41$ $313 395.96$ $71$ <t< td=""><td>3       $117 200.60$ $83$ $82$ $82$ 3D*       3       $118 114.95$ $92$ $5$ 3D*       3       $118 745.25$ $90$ $5$ 3D       1       $121 92.93$ $92$ $93$ 3D       1       $121 192.93$ $93$ $92$ 5S*       2       $122 282.40$ $99$ $91$         D       2       $125 433.55$ $5$ $75$ 5D*       2       $129 957.95$ $75$ $7$ $1 30 190.05$ $86$ $8$ $4$ $130 190.05$ $86$ $8$ $4$ $130 190.05$ $86$ $8$ $4$ 3S*       1       $130 863.50$ $53$ $12$ 3H*       $5$ $191 500.50$ $61$ $28$ 3F*       $4$ $131 792.02$ $41$ $33$ 3P*       $2$ $132 88.80$ $96$ $78$ $11$ $133 339.70$ $73$ $20$ $73$ $20$ $373$ $20$ 3P*&lt;</td></t<>	3 $117 200.60$ $83$ $82$ $82$ 3 D*       3 $118 114.95$ $92$ $5$ 3 D*       3 $118 745.25$ $90$ $5$ 3 D       1 $121 92.93$ $92$ $93$ 3 D       1 $121 192.93$ $93$ $92$ 5 S*       2 $122 282.40$ $99$ $91$ D       2 $125 433.55$ $5$ $75$ 5 D*       2 $129 957.95$ $75$ $7$ $1 30 190.05$ $86$ $8$ $4$ $130 190.05$ $86$ $8$ $4$ $130 190.05$ $86$ $8$ $4$ 3 S*       1 $130 863.50$ $53$ $12$ 3 H* $5$ $191 500.50$ $61$ $28$ 3 F* $4$ $131 792.02$ $41$ $33$ 3 P* $2$ $132 88.80$ $96$ $78$ $11$ $133 339.70$ $73$ $20$ $73$ $20$ $373$ $20$ 3 P*<

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Configuration	Term	J	Level (cm ⁻¹ )	L	cading	percer	itages
$\frac{1}{3d^7(^2\mathbf{P})4p}$	³ D°	2	136 813.20	41		29	$(^{2}P)^{1}D^{\bullet}$
	_	3	136 967.00	77		8	$(a^2D)^3F^*$
		1	137 362.36	54		15	$(a^2D)^3D^*$
$3d^{7}(^{2}\mathrm{H})4p$	³ G*	5	137 020.20	94		5	$(^{2}\mathbf{F})^{3}\mathbf{G}^{*}$
· · · · · · ·		4	138 030.90	90		5	
		3	138 852.20	85		6	
$3d^7(^2\mathbf{P})4p$		2	137 631.60	24	⁸ D*	20	¹ D°
$3d^7(^2\mathrm{H})4p$	³ I•	6	137 391.30	74		25	$(^{2}H)^{-1}I^{\circ}$
		7	137 991.40	100			
		5	138 060.40	95			
$3d^7(^2\mathrm{P})4p$	¹ <b>S</b> *	0	138 146.48	61		39	( ⁴ P) ³ P°
$3d^{7}(a^{2}\mathrm{D})4p$	³ D°	3	138 487.40	79		11	$(a^{2}D)^{3}F^{\circ}$
-		1	138 979.20	50		27	$({}^{2}\mathbf{P})^{\mathbf{I}}\mathbf{P}^{\mathbf{o}}$
		2	1 <b>39</b> 253.70	63		10	( ² P) ³ D°
$3d^7(^2\mathrm{H})4p$	¹ I°	6	139 633.90	74		24	( ² H) ³ I°
$3d^7(a \ ^2\mathbf{D})4p$	³ F°	4	140 184.65	98			
		3	140 544.52	71		8	$(^{2}P)^{3}D^{\circ}$
		2	140 885.40	73		10	$(a {}^{2}D) {}^{3}D^{\circ}$
$3d^7(^2\mathbf{P})4p$	³ S*	1	140 885.15	67		8	$(^{2}\mathbf{P})^{1}\mathbf{P}^{*}$
$3d^7(^2\mathbf{P})4p$	¹ <b>P</b> *	1	141 414.10	49		17	$(a {}^{2}D) {}^{3}D^{\circ}$
$3d^{7}(^{2}\mathrm{H})4p$	³ H°	6	142 187.80	98			
		5	142 575.60	95			
		4	143 002.70	95			
$3d^7(a \ ^2\mathrm{D})4p$	¹ D°	2	142 433.95	46		29	( <i>a</i> ² D) ³ P°
$3d^7(a \ ^2D)4p$	³ P°	2	143 560.16	48		24	$(a^{2}D)^{1}D^{\circ}$
		1	144 624.55	67		11	$\binom{2\mathbf{P}}{2}$
		0	145 088.45	80		15	$(^{2}P)^{3}P^{\circ}$
$3d^7(a \ ^2\mathrm{D})4p$	¹ F°	3	143 864.80	73		16	( ² G) ¹ F°
$3d^{7}(^{2}\mathrm{H})4p$	¹ G°	4	144 153.00	70		27	( ² G) ¹ G°
$3d^7(a \ ^2\mathbf{D})4p$	¹ P°	1	145 <b>9</b> 50.15	88			
$3d^7(^2\mathrm{H})4p$	¹ H°	5	146 325.80	96			
$3d^{6} 4s^{2}$	⁵ D	4	153 256.35				
		3	154 170.37				
$3d^7(^2\mathbf{F})4p$	¹ D°	2	155 071.00	60		32	( ² F) ³ F°
$3d^{7}(^{2}\mathrm{F})4p$	³ G°	3	155 443.30	82		10	( ² F) ³ F°
		4	155 841.40	73		15	$(^{2}\mathbf{F})$ ³ F°
		5	156 808.70	94		5	$(^{2}H)$ ³ G°
$3d^{7}(^{2}\mathrm{F})4p$	³ F°	3	156 411.20	88		19	( ² F) ³ D°
		2	156 522.87	64		29	$(^{2}\mathbf{F})^{1}\mathbf{D}^{\circ}$
		4	156 972.08	50		28	$(^{2}\mathbf{F})$ ¹ <b>G</b> °

Ni III-Continued

Configuration	Term	J	Level (cm ⁻¹ )	Leadi	ing percen	itages
$3d^{7}({}^{2}\mathbf{F})4n$	³ D°	3	156 853.00	72	18	$(^{2}\mathbf{F})$ $^{3}\mathbf{F}^{\circ}$
····		2	157 154.27	85	8	$(^{2}\mathbf{F})^{-1}\mathbf{D}^{\circ}$
		1	157 235.16	93	5	$(b^2D)^3D^\circ$
$3d^{7}(^{2}\mathrm{F})4p$	¹ G°	4	157 375.42	65	32	( ² F) ³ F°
$3d^7(^2\mathbf{F})4p$	¹ F°	3	161 754.89	97		
$3d^7(b^2D)4p$	³ P°	2	176 487.10	99		
		1	176 583.20	98		
		0	176 736.40	99		
$3d^7(b^2\mathrm{D})4p$	³ F°	2	177 805.60	96		
		3	178 451.50	96		
		4	179 282.00	97		
$3d^{7}({}^{4}\mathrm{F})4d$	⁵ F	5	181 019.08	90	8	⁵G
		4	181 482.95	83	8	5n
		3	181 996.70	80	8	5 D
		2	182 387.83	87	5	5D
		1	183 035.25	95	2	D
$3d^{\hat{i}}(b^{2}\mathrm{D})4p$	¹ P°	1	181 203.4	95		
$3d^7(b^2\mathbf{D})4p$	¹ F°	3	181 658.4	97		
$3d^{7}({}^{4}\mathrm{F})4d$	⁵ G	6	181 840.00	96	4	⁵ H
		5	182 327.13	63	26	°G 3G
		4	183 041.45	71	13	°G 30
		3		81	4	50 50
		2	184 124.80	74	17	1
$3d^{7}({}^{4}\mathrm{F})5s$	⁵ F	5	181 998.15	99	14	³ F
			182 798.20	84	14	r
		3	183 012.07	93		
		1	184 220.35	97 99		
3d ⁷ ( ⁴ F) Ad	511	7	182 508 30	99		
3a ( r )4a	п	6	183 126 19	59	39	³ H
		5	183 904.88	80	14	³ H
		4	184 510.75	88	5	³ G
		3	184 944.95	81	17	³ G
$3d^{7}({}^{4}\mathrm{F})4d$	⁵P	3	182 524.69	83	9	⁵ D
		2	183 575.58	55	21	°G
		1	184 375.68	59	38	°D
$3d^7({}^4\mathbf{F})4d$	³ G	5	183 052.20	66	24	⁵ G
		4	183 859.72	74	16	"G
		3	184 346.50	74	15	Ч
$3d^{7}({}^{4}\mathrm{F})4d$	⁵ D	4	183 464.88	85	9	⁵ F
		3	184 518.20	64	13	3D
		2	185 067.15	55	25	°D 5D
		1	185 116.05	46	38	P
		0	185 147.23	98		

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Ni III-Continued

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Configuration	Term	J	Level (cm ⁻¹ )	Leadi	ng percen	tages
$\frac{1}{3d^{\hat{i}}(b^2\mathbf{D})4p}$	³ D°	1	183 717.00	95		
_		2	183 872.00	73	25	${}^{1}\mathbf{D}^{\circ}$
		3	184 723.10	96		
$3d^7({}^4\mathbf{F})4d$	³ D	3	183 839.47	71	14	5D
		2	184 623.54	66	15	
		1	185 543.70	82	12	
$3d^{7}({}^{4}{ m F})5s$	³ F	4	184 037.62	85	14	⁵ F
		3	185 248.15	93		-
		2	186 073.40	97		
$3d^{7}({}^{4}\mathbf{F})4d$	³ ਸ	6	184 166 57	60	97	5 <b>L</b> I
	1	5	184 805 62	80	15	11
		4	185 639.13	91	5	
9-37 (412) 4-3	312		107 071 00			( ² a) ³ 7
oa ( <b>r</b> )4a	r	4	187 351.88	86	5	('G) 'F
		3	188 140.54	84	6	
			188 622.87	85	6	
$3d^{7}({}^{4}\mathrm{F})4d$	³ P	2	187 493.38	87	5	( ⁴ P) ³ P
	-	1	188 542.82	90	6	
		0	189 056.90	91	6	
$3d^{7}({}^{4}\mathrm{F})5n$	⁵ ₽°	5	199 919 08	01	0	50.0
ou (I)op			900 076 95	51	8	50°
		3	200 070.55	49	42	ם זה,
		9	200 302.37	04	21	ט זית ⁵
		1	202 263.08	94	15 6	5D.
2-1-(412)5-	500	6	200 717 00			
3a ( 'r ) 5p	G	6	200 747.06	99		300
		5	201 033.08	48	43	°G°
		4	201 909.90	67	14	5 F*
		3	202 608.20	76	11	°F°
		2	203 020.07	78	10	°D•
$3d^7({}^4\mathbf{F})5p$	⁵ D°	4	200 935.60	54	29	⁵ F°
		3	201 829.46	60	19	⁵ F°
		2	202 487.82	71	17	⁵ G°
		1	202 898.94	92	6	⁵ F°
		0	203 078.46	98		
$3d^7({}^4\mathrm{F})5p$	³ F°	4	202 074.33	71	5	⁵ F°
		3	203 360.52	57	29	³ D°
		2	203 739.65	58	38	³ D°
$3d^{7}({}^{4}\mathrm{F})5p$	³ G*	5	909 195 84	54	44	⁵ C*
	<b>—</b>	4	203 197 33	75	10	ŭ
		3	203 976.35	85	15	
$3d^{7}({}^{4}\mathrm{F})5r$	30.	2	909 691 51			3774
ou ( 1 /op		2	202 024.31	62	30	3179
		1	204 242.07 204 677.95	57 98	38	- P
a 11/100 1 4	5					
3a ³ (°D)4s4p	"D"	4	204 404.12			
		3	204 714.93			
		2	205 062.51			
		1	205 327.00			
		0	205 466.00			

Ni III-Continued

Configuration	Term	J	Level (cm ⁻¹ )	Leadi	ing perce	ntages	
3d ⁶ ( ⁵ D)4s4p	⁵ F°	5 4 3 2	206 925.18 207 382.10 207 744.30 208 005.7				
3d ⁶ ( ⁵ D)4s4p	³ D°	3 2 1	212 312.5 213 016.8 213 490.0				
3d ⁶ ( ⁵ D)4s4p	³ F°	4 3 2	212 837.7 213 979.67 214 744.0				
$3d^7({}^4\mathrm{F}_{9/2})4f$	²[ ¹¹ ⁄ ₂ ]°	6 5	221 187.25 221 195.35	99 88	11	²[ ⁹ / ₂ ]°	
$3d^{7}({}^{4}\mathrm{F}_{9/2})4f$	²[ ⁹ ⁄ ₂ ]°	4 5	221 256.08 221 268.50	98 88	11	² [ ¹¹ / ₂ ]•	
$3d^{7}({}^{4}\mathbf{F}_{9/2})4f$	²[ ¹³ / ₂ ]°	7 6	221 286.78 221 292.92	99 99			
$3d^{7}({}^{4}\mathrm{F}_{9/2})4f$	²[ ⁷ ⁄ ₂ ]°	3 4	221 350.90 221 388.14	<del>99</del> 98			
$3d^7({}^4\mathrm{F}_{9/2})4f$	²[ ¹⁵ / ₂ ]°	8 7	221 433.20 221 444.15	99 99			
$3d^{7}({}^{4}\mathrm{F}_{7/2})4f$	²[%2]°	5 4	222 455.66 222 466.47	94 89	9	²[ ⁷ / ₂ ]°	
$3d^7({}^4\mathrm{F}_{9/2})4f$	²[ ⁵ / ₂ ]°	3	221 476.68	99			
$3d^{7}({}^{4}\mathrm{F}_{7/2})4f$	²[ ¹¹ / ₂ ]°	6 5	222 494.65 222 529.55	99 94			
$3d^7({}^4\mathrm{F}_{7/2})4f$	²[ ⁷ ⁄ ₂ ]°	3 4	222 516.60 222 547.50	97 89	10	²[%2]°	
$3d^{\hat{i}}({}^{4}\mathrm{F}_{7/2})4f$	²[ ⁵ ⁄ ₂ ]°	3 2	222 530.00 222 571.37	97 98			
$3d^7({}^4\mathrm{F}_{7/2})4f$	² [ ¹³ / ₂ ]°	7 6	222 596.30 222 599.70	99 99			
$3d^7({}^4\mathrm{F}_{5/2})4f$	²[ ⁷ ⁄ ₂ ]°	4 3	223 387.00 223 329.77	98 87	12	²[ ⁵ ⁄ ₂ ]°	
$3d^{\hat{\tau}}({}^{4}\mathrm{F}_{5/2})4f$	²[ ⁵ / ₂ ]°	3 2	223 406.81 223 375.18	85 97	12	²[ ⁷ / ₂ ]°	
$3d^{7}({}^{4}\mathrm{F}_{5/2})4f$	²[%]°	5 4	223 434.10 223 314.77	<del>99</del> 98			
$3d^{7}({}^{4}\mathrm{F}_{5/2})4f$	²[ ¹¹ / ₂ ]°	5 6	223 461.15 223 469.90	99 99			
$3d^{7}({}^{4}\mathrm{F}_{5/2})4f$	²[¾]°	2 1	223 481.25 223 491.34	<del>99</del> 99			
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Ni 111-Continued

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Configuration	Term	J	Level (cm ⁻¹ )	L	cading	percer	tages	
$3d^7({}^4\mathbf{F}_{3/2})4f$	² [ ⁵ / ₂ ]•	3	223 957.54	97				
		2	224 020.05	97				
$3d^{7}({}^{4}\mathbf{F}_{9/2})4f$	² [ ⁹ / ₂ ]°	4	223 989.02	99				
		5	224 020.91	99				
$d^{7}({}^{4}\mathrm{F})6\mathrm{s}$	5F	5	225 784.20	99				
	-	3	227 270.07	73		26	³ F	
		4	227 288.70	55		44	³ F	
		2	227 985.66	90		9	з́F	
2d ⁷ ( ⁴ F)5d	5F	5	225 918 35	70		90	۶G	
		4	226 118 80	15		20	5 0	
		1	228 042.24	53 62		34 24	⁵D	
7.1-2.	50						5	
$3d'(\mathbf{F})5d$	Ğ I	6	226 124.64	91		8	°H 3G	
		5	227 433.80	41		34	G 5 <del>5</del>	
		3	227 963.02	43		17	Ď	
		2	228 483.54	68		13	°F	
$3d^{7}({}^{4}\mathrm{F})6s$	³ F	4	226 290.44	55		44	⁵ <b>F</b>	
		3	228 290.97	73		26		
		2	229 036.43	90		9		
$3d^7({}^4\mathbf{F})5d$	⁵ H	7	226 380.36	99				
		6	227 649.28	60		33	${}^{3}H$	
		5	227 726.91	61		26	${}^{3}H$	
		4	228 434.45	76		10	³ H	
		3	228 955.36	55		42	³ G	
$3d^{7}({}^{4}\mathbf{F})5d$	⁵ p	3	226 532 85	51		30	⁵D	
		2	227 767 03	53		26	₹	
		1	228 329.40	42		31	${}^{5}D$	
3d ⁷ ( ⁴ F) 5d	³ C	Б	226 603 73	51		20	٥C	
bu (T)ou	U	4	220 005.15	51		30	5G	
		3	228 155.11	40		34 34	⁵H	
2-17(415)5-1	377	c	996 696 99	20			5	
ou ( <b>F</b> )od	п	5	220 080.28	66		31	Н	
		5 4	228 609.82 229 291.50	59 79		29 12		
9-17(415)5-2		0	000 858 80		300		5r	
3a ( 1 ) 5d		3	226 757.78	37	۰D	27	۰P	
$3d^{7}({}^{4}\mathrm{F})5d$	⁵ D	4	227 091.99	42		37	⁵ G	
		3	228 363.94	46		23	⁵ F	
		0	228 736.36	99				
		2	228 819.73	56		20	${}^{5}\mathbf{P}$	
		1	229 057.39	38		31	⁵ P	
$3d^{7}({}^{4}\mathrm{F})5d$		2	227 346.84	35	⁵ F	15	⁵ P	
$3d^{7}({}^{4}\mathrm{F})5d$	30	3	227 459 43	AD.		26	яč	
ou ( r /ou		2	228 273 49	40		10	50	
		1	228 879 50	62		18	5D	
		1	220 013.00	59		21	r	
$3d^7({}^4\mathbf{F})5d$		4	227 553.40	30	${}^{5}\mathbf{F}$	27	³ G	

Ni III-Continued

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Configuration	Term	J	Level (cm ⁻¹ )	Lead	ling percen	itages
$3d^7({}^4\mathrm{F})5d$	³ F	4 3 2	230 169.90 231 033.56 231 548.58	89 84 83	6 3 2	³ G ³ G ³ D
$3d^7({}^4\mathrm{F})5d$	³ P	2 1 0	230 219.9 231 309.0 231 761.8	87 93 97	7 3 2	( ⁴ F) ³ D ( ⁴ F) ³ D ( ⁴ P) ³ P
$3d^7({}^4\mathrm{F}_{9/2})5g$	² [ ¹⁵ / ₂ ]	8 7	244 262.75 244 267.15	97 93		
$3d^{7}({}^{4}\mathbf{F}_{9/2})5g$	² [ ¹¹ / ₂ ]	6 5	244 264.23 244 264.28	86 72	10 27	² [ ¹³ / ₂ ] ² [ ⁹ / ₂ ]
$3d^{7}({}^{4}\mathrm{F}_{9/2})5g$	² [ ¹³ / ₂ ]	7 6	244 289.88 244 290.37	94 86	13	² [ ¹¹ / ₂ ]
$3d^7({}^4\mathbf{F}_{9/2})5g$	²[ ⁹ ⁄ ₂ ]	4 5	244 306.13 244 306.20	53 71	46 27	² [ ⁷ / ₂ ] ² [ ¹¹ / ₂ ]
$3d^{7}({}^{4}\mathrm{F}_{9/2})5g$	² [ ¹⁷ / ₂ ]	9 8	244 343.23 244 343.20	99 98		
$3d^{7}({}^{4}\mathrm{F}_{7/2})5g$	² [ ¹³ / ₂ ]	6	245 471.20	87	11	² [ ¹¹ / ₂ ]
$3d^{7}({}^{4}\mathbf{F}_{7/2})5g$	² [ ¹¹ / ₂ ]	5 6	245 488.31 245 495.36	60 89	38 10	² [ ⁹ / ₂ ] ² [ ¹³ / ₂ ]
$3d^{7}({}^{4}\mathrm{F}_{7/2})5g$	² [ ¹⁵ / ₂ ]	7	245 528.40	96		
$3d^{7}({}^{4}\mathrm{F}_{7/2})5g$	²[%]	5 4	245 532.59 245 572.57	60 70	39 28	$2^{2}[1/_{2}]^{2}[7/_{2}]$
$3d^{\tilde{i}}({}^{4}\mathrm{F}_{5/2})5g$	²[%2]	4 5	246 364.86 246 376.24	96 55	42	² [ ¹¹ / ₂ ]
$3d^{7}({}^{4}\mathrm{F}_{5/2})5g$	²[ ¹³ / ₂ ]	6	246 385.97	97		
$3d^7({}^4{ m F}_{3/2})\bar{s}g$	²[%2]	4 5	246 938.98 246 954.87	72 58	26 40	² [ ⁷ / ₂ ] ² [ ¹¹ / ₂ ]
Ni IV ( ⁴ F _{9/2} )	Limit		283 800			

Ni IV

Z = 28

Mn I isoelectronic sequence

Ground state: 1s²2s²2p⁶3s²3p⁶3d⁷ ⁴F_{9/2}

Ionization energy =  $443\ 000\pm 2000\ \text{cm}^{-1}\ (54.9\pm 0.2\ \text{eV})$ 

The first work on Ni IV was reported by Poppe (1968), who found two quartets in the  $3d^7$  configuration and quartets and sextets from  $3d^{6}4s$  and  $3d^{6}4p$ . The sextets and quartets were connected by intercombinations found by Garcia-Riquelme (1968).

The present compilation is taken from an extension of the analysis by Poppe (1976). The  $3d^7 - 3d^64p$  array was observed in the region 390-710 Å and the  $3d^{6}4s - 3d^{6}4p$ array in the region 1210–1830 Å. All levels of  $3d^7$  have been found. The uncertainty of the level values is  $3 \text{ cm}^{-1}$ .

The leading percentages were calculated by D.

(1976). We use the designations of Nielson and Koster (see Introduction) to represent the seniorities.

The ionization energy was obtained by extrapolation by Lotz (1967).

### References

Garcia-Riquelme, O. (1968), Physica 40, 27. Lotz, W. (1967), J. Opt. Soc. Am. 57, 873. Poppe, R. (1968), Physica 40, 17. Poppe, R. (1976), Physica 81C, 351.

1 ne	leaunig	percentages	were	calculateu	бy	roppe	

<u>Ni IV</u>									
Configuration	Term	J	Level (cm ⁻¹ )	Lead	ing perce	ntages			
$\overline{3d^{7}}$	⁴ F	9/2 7/2 5/2 3/2	0.0 1 189.7 2 042.5 2 621.1	100 100 100 100					
$3d^7$	4P	⁵ /2 ³ /2 ¹ /2	18 118.6 18 366.8 18 958.4	100 93 97	7 3	² P ² P			
$3d^7$	²G	9/2 7/2	19 829.6 20 947.6	97 100	2	² H			
$3d^7$	²P	³ /2 ¹ /2	23 648.9 24 651.4	83 97	8 3	²D2 ⁴P			
$3d^7$	² H	¹¹ / ₂ 9/ ₂	26 649.1 27 677.6	100 98	2	²G			
$3d^7$	² D2	⁵ /2 3/2	27 096.5 28 777.7	77 72	23 18	²D1			
3d ⁷	²F	⁵ /2 7/2	43 437.5 43 858.6	100 100					
$3d^7$	² D1	³ /2 ⁵ /2	67 360.0 67 989.8	80 77	20 23	² D2			
3a ⁶ ( ⁵ D)4s	6D	9/2 7/2 5/2 3/2 1/2	110 410.6 111 195.8 111 763.3 112 151.9 112 379.3	100 100 100 100 100					
3a ⁶ ( ⁵ D)4s	4D	7/2 5/2 3/2 1/2	120 909.5 121 807.7 122 386.1 122 717.4	100 100 100 <b>99</b>					

Ni IV-Continued

$3d^{6}(^{3}P2)4s$	⁴ P	⁵ / ₂	138 446.2	62	37	( ³ P1) ⁴ P
		$\frac{3}{2}$	140 343.0 141 561.2	60 60	35 36	
$3d^{6}(^{3}\mathrm{H})4s$	4H	¹³ / ₂	139 289.4	100		
		¹¹ / ₂	139 619.2	98	2	( ³ G) ⁴ G
		9/2 7/2	139 886.7 140 140.9	94 96	3 2	(³G) ⁴G (³G) ⁴G
	410	9/	141 000 0	70	-	( ³ E1) 4E
3d ³ ( ³ F ² )4s	r	$\frac{1}{2}$	141 220.3	72	21	( f1) f
		$\frac{7}{5}$	141 577.2	74	20	
		3/2 3/2	141 852.0	80	20 19	
$3d^{6}(^{3}G)4s$	4G	11/2	144 815.1	71	28	$(^{3}H)^{2}H$
		9/2	145 702.2	76	18	$({}^{3}H)^{2}H$
		7/2	146 061.5	88	4	$({}^{3}F2) {}^{2}F$
		5/2	146 153.8	90	6	( ³ F2) ² F
$3d^{6}(^{3}\text{P2})4s$	² P	³ /2	145 192.1	60	36	( ³ P1) ² P
$3d^{6}(^{3}\mathrm{H})4s$	² H	¹¹ / ₂	145 962.5	71	27	( ³ G) ⁴ G
		9/2	146 194.3	78	17	
$3d^{6}({}^{3}\mathrm{F2})4s$	² F	7/2	147 635.9	69	19	$({}^{3}F1) {}^{2}F$
		⁵ / ₂	148 358.2	74	18	
3d ⁶ ( ³ G)4s	²G	⁹ / ₂	151 574.7	97	3	$(^{3}H)^{2}H$
		$\gamma_2$	152 343.7	95	4	$({}^{3}F2) {}^{2}F$
$3d^6(^3\mathrm{D})4s$	⁴D	³ / ₂	153 313.8	99		
		⁹ / ₂	153 338.8	98		
		$\frac{1}{2}$	153 349.4	99		
		'/ ₂	153 533.6	100		
$3d^{6}({}^{1}\mathbf{I})4s$	² I	¹³ /2	155 253.7	100		
		¹¹ / ₂	155 308.7	99		
$3d^{6}({}^{1}\text{G2})4s$	²G	9/2 7:	156 294.0	65	32	( ¹ G1) ² G
		'/ ₂	156 351.2	65	32	
$3d^{6}({}^{3}\mathbf{D})4s$	² D	3/2	159 498.5	94	4	$(^{1}D2)^{2}D$
		୬₂	159 818.4	96	2	
$3d^{6}({}^{1}\mathrm{F})4s$	² F	⁷ / ₂	171 406.0	98		
		%2	171 408.0	98		
$3d^6({}^5\mathrm{D})4p$	⁶ D°	9/2 7/2	175 569.5	98		(5D) 6E*
		72 54	175 869.1	96	2	$(\mathbf{D})\mathbf{r}$
		$\frac{7}{3}$	176 247.1	97		
		1/2 1/2	176 749.0	98 99		
9.46( ³ E1)/a	4F	3/2	179 583 0	80	20	( ³ F2) ⁴ F
3a ( <b>r</b> 1)48	L L	9/2	179 655 0	78	22	
		5/2	179 724.0	79	20	
		7/	179 792 0	78	20	

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Ni IV-Continued

Configuration	Term	J	Level (cm ⁻¹ )	L	eading perce	ntages
$\frac{1}{3d^6({}^5\mathrm{D})4p}$	⁶ F°	11/2	181 931.5	100		
		9/2	182 044.9	94	4	$({}^{5}D) {}^{4}F^{\circ}$
		7/2	182 125.6	93	3	( ⁵ D) ⁴ F°
		5/2	182 206.8	95	2	( ⁵ <b>D</b> ) ⁴ <b>D</b> [•]
		3/2	182 259.9	96	2	$({}^{5}\mathbf{D}) {}^{4}\mathbf{D}^{\circ}$
		1/2 1/2	182 288.4	97	-	(2)2
$3d^6({}^5\mathrm{D})4p$	⁶ P°	7/2	184 099.1	84	11	( ⁵ D) ⁴ D [•]
		5/2	185 505.3	88	9	
		3/2	186 441.4	94	4	
$3d^6({}^5\mathrm{D})4p$	⁴D°	7/2	185 890.0	83	13	( ⁵ D) ⁶ P°
		5/2	186 516.1	84	10	( ⁵ D) ⁶ P°
		³ / ₂	186 957.2	89	4	( ⁵ D) ⁶ P°
		1/2	187 225.7	93	3	( ⁵ D) ⁶ F°
$3d^{6}({}^{3}\mathrm{F1})4s$	$^{2}\mathbf{F}$	7/2	185 967.0	77	21	( ³ F2) ² F
		5/2	185 997.0	80	20	
$3d^6({}^5\mathrm{D})4p$	⁴F°	9/2	186 470.1	94	4	( ⁵ <b>D</b> ) ⁶ <b>F</b> °
-		7/2	187 570.3	95	3	( ⁵ D) ⁶ F°
		5/2	188 320.1	96	2	( ⁵ <b>D</b> ) ⁶ <b>F</b> [•]
		3/2	188 824.2	97		
$3d^{6}({}^{5}\mathrm{D})4p$	⁴₽°	5/2	190 830.3	97		
	ļ	3/2	191 618.2	98		
		1/2	192 033.5	98		
$3d^{6}({}^{1}\mathrm{G1})4s$	² G	9/2	190 864.7	66	33	$({}^{1}G2) {}^{2}G$
		7/2	190 932.8	66	33	
$3d^{6}({}^{3}\mathrm{P2})4p$	4S°	3/2	205 114.1	44	19	( ³ P2) ⁴ P°
$3d^{6}(^{3}\mathrm{H})4p$	4G°	11/2	206 005.3	68	21	( ³ F2) ⁴ G°
	-	9/2	206 340.9	51	28	(
		7/2	206 645.7	45	34	
		5/2	206 847.0	42	38	
$3d^{6}(^{3}\text{P2})4p$		⁵ /2	206 523.2	27	⁴ P° 23	( ³ P1) ⁴ P°
$3d^{6}({}^{3}\mathrm{H})4p$	4I°	11/2	206 740.7	51	35	( ³ H) ⁴ H°
		13/2	206 754.5	48	38	( ³ H) ⁴ H°
		9/2	208 046.8	46	19	( ³ H) ⁴ H°
		15/2	208 149.5	99		
$3d^{6}(^{3}\mathrm{H})4p$		⁹ /2	206 865.5	43	⁴ I° 37	⁴ H°
$3d^{6}(^{3}\mathrm{H})4p$	⁴H°	7/2	207 136.0	47	20	( ³ H) ² G°
		11/2	208 595.3	45	44	( ³ H) ⁴ I°
		13/2	208 631.3	51	40	$(^{3}H)$ ⁴ I°
$3d^{6}({}^{3}\mathrm{P2})4p$	۴P°	¹ / ₂	207 846.2	48	41	( ³ P1) ⁴ P°
$3d^{6}(^{3}\text{P2})4p$	² D°	∛₂	208 009.1	32	20	( ³ P1) ² D°
$3d^{6}(^{3}\text{P2})4p$		7/2	208 330.7	22	⁴ D° 19	( ³ F2) ⁴ F°
$3d^{6}(^{3}\text{P2})4p$		3/2	208 461.0	22	<b>⁴S°</b> 13	<b>⁴P°</b>

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Ni IV-Continued

Configuration	Term	J	Level (cm ⁻¹ )	Lea	ading perce	entages
$\frac{1}{3d^6(^3F2)4p}$	⁴ F°	⁵ /2	208 605.7	54	18	( ³ F1) ⁴ F°
	•	3/2	208 766.9	63	20	( <u>-</u> -, -
		9/2	208 933.6	49	18	
$3d^{6}(^{3}\text{P2})4p$	⁴D°	7/2	208 912.1	39	21	( ³ P1) ⁴ D°
		1/2	210 313.3	5 <b>9</b>	28	( ³ P1) ⁴ D°
$3d^6(^{3}\mathrm{H})4p$		⁹ / ₂	209 131.9	37	² G° 23	( ³ H) ⁴ H°
$3d^6(^{3}\mathrm{H})4p$		7/2	209 391.4	34	² G° 16	( ³ F2) ⁴ F°
$3d^6(^3\text{P2})4p$		³ / ₂	209 985.1	18	² D° 16	( ³ P2) ⁴ P°
$3d^{6}({}^{3}\mathrm{F2})4p$	⁴D°	7/2	210 121.8	49	10	( ³ F1) ⁴ D°
		⁵ / ₂	210 943.6	37	20	$({}^{3}P2) {}^{4}D^{\circ}$
		3/2	211 246.8	49	10	$(^{3}\mathbf{D})^{4}\mathbf{D}^{6}$
		¹ / ₂	211 351.7	67	12	(°F1) *D*
$3d^{6}(^{3}H)4p$	² I°	13/2	210 177.0	86	11	$({}^{3}H) {}^{4}I^{\circ}$
		11/2	210 987.5	88	4	
$3d^{6}({}^{3}\mathrm{F2})4p$		⁵ /2	210 590.6	24	⁴ D° 23	( ³ P2) ⁴ D°
$3d^{6}(^{3}\text{P2})4p$	}	3/2	211 027.6	20	⁴ D° 18	( ³ F2) ⁴ D°
3.d ⁶ ( ³ F2)/n	40.	9/	919 150 9	37	20	( ³ H) ⁴ G°
02 (T2)+p		11/2	212 207.0	53	17	
$3d^{6}({}^{3}\mathrm{F2})4p$		⁵ /2	212 275.9	24	² F° 19	( ³ F2) ⁴ G [•]
$3d^{6}({}^{3}\mathrm{F2})4p$		7/2	212 281.8	26	<b>4G*</b> 17	( ³ H) ⁴ G [•]
3d ⁶ ( ³ F2)4p		7/2	213 131.1	24	² F° 14	( ³ H) ⁴ G [•]
$3d^{6}({}^{3}G)4n$	4F°	9/0	213 408.6	57	25	( ³ G) ⁴ G [•]
5 <b>u</b> ( <b>u</b> / <b>p</b>	-	5/2	215 516.8	43	30	( ³ G) ⁴ G [•]
		3/2	215 541.3	68	15	( ³ D) ⁴ F°
$3d^{6}(^{3}\mathrm{H})4p$		5/2	213 412.1	28	<b>⁴G°</b> 18	( ³ F2) ⁴ G*
$3d^{6}({}^{3}\mathrm{G})4p$		11/2	213 606.9	31	<b>⁴G°</b> 30	² H•
$3d^{6}(^{3}\text{P2})4p$		¹ / ₂	213 640.2	31	² P° 23	( ³ P1) ² P*
$3d^{6}(^{3}\text{F2})4p$		⁹ /2	213 739.7	33	² G° 20	( ³ G) ² H [•]
$3d^{6}(^{3}\text{P2})4p$	² <b>P</b> *	3/2	214 055.8	50	33	( ³ P1) ² P*
$3d^{6}({}^{3}\mathrm{G})4p$	⁴G°	7/2	214 101.0	41	37	( ³ G) ⁴ F [•]
		11/2	214 316.8	47	21	$({}^{3}\mathbf{H}) {}^{2}\mathbf{H}^{\circ}$
		5/2	214 718.1	46	27	(°G) °F°
		9/2	214 910.5	40	16	(°H) ² H°
$3d^{6}(^{3}\text{F2})4p$		⁹ / ₂	214 587.4	21	² G• 16	( ³ H) ² H•
$3d^{6}(^{3}\text{F2})4p$	²G°	7/2	214 622.8	60	14	$({}^{3}F1) {}^{2}G^{*}$
$3d^{6}({}^{3}\mathrm{G})4p$		7/2	215 292.9	39	4 <b>G</b> • 33	( ³ G) ⁴ F•

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# E-42

Ni IV-Continued

Configuration	Term	J	Level (cm ⁻¹ )	L	cading	perce	ntages
3a ⁶ ( ³ G)4p	4H°	$ \begin{array}{c}     13_{2} \\     11_{2} \\     7_{2} \\     9_{4} \end{array} $	215 506.6 215 684.5 215 724.5	86 73 73		11 10 12	$({}^{3}H) {}^{4}H^{\circ}$ $({}^{3}H) {}^{2}H^{\circ}$ $({}^{3}H) {}^{4}H^{\circ}$ ${}^{3}H^{\circ}$
30 ⁶ ( ³ P2)42	² S*	1/2 1/2	215 736.1	73		9	$({}^{3}H)$ $({}^{3}H)$
		72	210 001.0	41		19	(11) 5
3d°(°F2)4p	² D•	³ / ₂ ³ / ₂	217 414.3 217 939.7	67 64		10 15	( ³ P2) ² D°
$3d^6(^3\mathrm{H})4p$	² H°	11/2	218 860.6	48		42	( ³ G) ² H°
$3d^6({}^3\mathrm{G})4p$	² F°	5/2 7/2	219 553.4 219 896.0	47 52		19 16	( ³ D) ² F°
$3d^{6}({}^{3}G)4p$	² H°	⁹ / ₂	219 765.0	43		39	( ³ H) ² H°
$3d^6({}^1\mathrm{I})4p$	² K°	¹³ / ₂ ¹⁵ / ₂	220 7 <b>6</b> 2.6 222 202.8	97 99		2	( ¹ <b>I</b> ) ² <b>I</b> •
$3d^6({}^3\mathrm{G})4p$	² G°	9/2 7/2	221 991.0 222 029.3	71 71		18 12	( ³ H) ² G°
3d ⁶ ( ³ D)4p	4 <b>P</b> •	5/2 3/2 1/2	222 333.3 222 662.9 223 225.4	87 74 66		3 8 13	( ³ P2) ⁴ P° ( ³ D) ² P° ( ³ D) ⁴ D°
$3d^{6}({}^{1}\mathrm{G2})4p$	²H°	9/2 11/2	222 705.5 225 758.5	44 36		17 27	( ¹ I) ² H* ( ¹ G1) ² H*
$3d^{6}({}^{1}I)4p$	² H°	¹¹ / ₂ 9/ ₂	222 993.3 225 903.7	53 61		<b>2</b> 5 15	( ¹ G2) ² H° ( ¹ G1) ² H°
$3d^6(^3\mathbf{D})4p$		¹ /2	223 785.4	33	⁴D•	26	( ³ D) ⁴ P°
3d ⁶ ( ³ D)4p	4 <b>F</b> •	5/2 7/2 9/2	224 021.3 224 824.9 225 096.4	58 47 73		17 12 11	( ³ G) ⁴ F° ( ¹ G2) ² G° ( ³ G) ⁴ F°
$3d^6(^3\mathrm{D})4p$		"∕₂	224 075.3	24	⁴ F°	10	( ¹ G2) ² F°
$3d^6(^3\mathrm{D})4p$		³ / ₂	224 174.0	30	⁴D°	30	( ³ D) ² P°
$3d^6({}^1\mathrm{G2})4p$	²G*	7/2 9/2	224 463.6 224 761.5	44 50		18 21	( ¹ G1) ² G°
$3d^6(^3D)4p$	4D.	⁵ / ₂ 7/ ₂	224 645.7 225 136.9	68 54		14 13	( ³ D) ⁴ F° ( ¹ G2) ² F°
$3d^6(^3\mathrm{D})4p$	² P*	3/2 1/2	224 936.9 224 996.5	41 40		41 36	( ³ D) ⁴ D°
$3d^{6}(^{1}\text{G2})4p$		⁵ / ₂	225 431.6	34	² F*	15	( ¹ G1) ² F°
$3d^6({}^1I)4p$	² I*	¹³ / ₂ ¹¹ / ₂	226 685.0 226 702.5	98 82		2 10	( ¹ I) ² K• ( ¹ I) ² H•
3d ⁶ ( ³ D)4p	²D*	3/2 5/2	227 181.1 227 549.4	76 86		7 3	( ¹ D2) ² P• ( ¹ F) ² D°

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Configuration	Term	J	Level (cm ⁻¹ )	L	ading	percer	ntages
$3d^6(^1\text{D2})4p$	² P°	³ / ₂ ¹ / ₂	228 214.2 232 897.0	34 40		23 27	( ¹ S2) ² P*
$3d^6(^{3}\mathrm{D})4p$	² F°	7/2 5/2	228 518.5 229 269.5	62 54		14 20	( ¹ D2) ² F*
$3d^{6}(^{1}\mathrm{S2})4p$		¹ / ₂	229 297.5	32	² <b>P</b> °	26	$(^{1}D2) ^{2}P^{\bullet}$
$3d^{6}(^{1}\text{D2})4p$		⁵ /2	231 091.8	31	² D°	17	$(^{1}D2)$ $^{2}F^{\circ}$
$3d^6(^1\text{D2})4p$	² D°	³ / ₂	231 742.0	62		12	( ¹ D1) ² D*
$3d^6(^1\text{D2})4p$		⁵ /2	232 272.7	30	² <b>D</b> *	25	² F°
$3d^{6}(^{1}\text{D2})4p$	² F°	⁷ / ₂	232 539.5	51		13	( ¹ D1) ² <b>F</b> °
$3d^{6}(^{1}\mathrm{S2})4p$		³ / ₂	234 019.5	37	² <b>P</b> °	24	( ¹ D2) ² P°
$3d^{6}({}^{1}\mathrm{F})4p$	²G°	⁷ / ₂ 9/ ₂	237 480.3 238 957.8	90 93		2 2	( ³ G) ² G* ( ¹ G2) ² G*
$3d^6({}^1\mathrm{F})4p$	² D°	⁵ /2 3/2	239 009.7 240 094.2	63 70		15 9	( ¹ D2) ² D°
$3d^{6}(^{3}\text{P1})4p$	⁴D°	¹ / ₂	241 172.4	37		37	( ³ F1) ⁴ D°
$3d^{6}({}^{3}\mathrm{F1})4p$	⁴D°	³ /2 5/2 7/2	241 540.0 241 817.9 241 939.0	35 43 50		32 29 23	( ³ P1) ⁴ D [•]
$3d^6({}^1\mathbf{F})4p$	² F°	5/2 7/2	243 520.1 243 542.0	83 82		4 4	( ¹ G2) ² F°
$3d^{6}({}^{3}\mathrm{F1})4p$	⁴G°	7/2 9/2 11/2	247 731.7 248 218.0 248 855.4	77 74 78		17 18 20	( ³ F2) ⁴ G*
3d ⁶ ( ³ P1)4p	4S°	³ /2	249 130.0	74		24	( ³ P2) ⁴ S°
$3d^{6}({}^{3}\mathrm{F1})4p$	² D°	³ /2 ⁵ /2	250 951.0 251 694.3	49 46		24 23	( ³ P1) ² D [•]
$3d^6({}^3\mathrm{F1})4p$	²G°	9/2 7/2	251 773.6 252 523.0	66 69		17 16	( ³ F2) ² G°
$3d^{6}(^{3}\text{P1})4p$	⁴ P°	⁵ /2	252 354.0	37		29	( ³ P2) ⁴ P°
$3d^{6}({}^{3}\mathrm{F1})4p$		3/2	252 975.4	32	⁴D°	23	( ³ P1) ⁴ D°
$3d^{6}({}^{3}\mathrm{F1})4p$		⁵ √2	253 326.2	26	⁴ F°	13	( ³ P1) ⁴ D°
3d ⁶ ( ³ F1)4p	⁴ F°	3/2 7/2 5/2 9/2	253 57 <b>9</b> .3 253 639.1 254 123.7 254 300.0	57 40 40 66		18 16 17 24	( ³ F2) ⁴ F° ( ³ P1) ⁴ D° ( ³ F1) ⁴ D° ( ³ F2) ⁴ F°
$3d^{6}({}^{3}\mathrm{F1})4p$		⁷ / ₂	254 663.4	26	⁴ F°	22	( ³ P1) ⁴ D [•]
$3d^{6}({}^{3}\mathrm{F1})4p$		³ / ₂	255 064.0	27	² D°	23	( ³ P1) ² D°
$3d^{6}({}^{3}\mathrm{F1})4p$		³ / ₂	255 064.0	27	² D°	23	$(^{3}P1) \ ^{2}D^{\circ}$

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# E-44

Configuration	Term	7	Level	T anding accounts and				
Configuration	Term		(cm ⁻¹ )	Leaung	percen	lages		
$\frac{1}{3d^6({}^3\mathrm{F1})4p}$	² F°	7/2	257 018.0	54	23	( ³ F2) ² F°		
		⁵ / ₂	257 406.4	66	25			
$3d^{6}({}^{1}\mathrm{G1})4p$	² H°	⁹ /2	258 672.8	59	33	( ¹ G2) ² H°		
		¹¹ / ₂	260 065.1	62	35			
$3d^{6}({}^{1}\mathrm{G1})4p$		⁷ /2	260 355.5	31 ² F°	23	( ¹ G1) ² G°		
$3d^{6}({}^{1}\mathrm{G1})4p$	² F°	⁵ /2	261 226.3	55	26	( ¹ G2) ² F°		
$3d^{6}({}^{1}\mathrm{G1})4p$	² G°	⁹ /2	262 275.5	64	27	( ¹ G2) ² G°		
		7/2	262 538.7	44	19			
$3d^{6}(^{1}\text{D1})4p$	² D°	3/2	282 179.5	79	17	( ¹ D2) ² D°		
		5/2	282 645.2	79	17			
Ni v ( ⁵ D ₄ )	Limit		443 000					

Cr 1 isoelectronic sequence

Ground state: 1s²2s²2p⁶3s²3p⁶3d⁶ ⁵D₄

Ionization energy =  $613500 \pm 500 \text{ cm}^{-1}$  (76.06  $\pm 0.06 \text{ eV}$ )

The  $3d^6-3d^54p$  transition array between 300 and 425 Å has been observed and analysed by Raassen, van Kleef, and Metsch (1976). They have found all but the high ¹S level of  $3d^6$  and 177 out of 214 levels of  $3d^54p$ . The uncertainty of the level values is about  $\pm 5$  cm⁻¹. They give the percentage compositions for these two configurations.

Raassen and van Kleef (1977) found 37 more levels of  $3d^{5}4p$  and observed and analysed the  $3d^{5}4s - 3d^{5}4p$  transition array between 990 and 1400 Å. They also found one term in each of the configurations  $3d^{5}5p$ ,  $3d^{3}4f$  and  $3d^{5}5f$ . They give the percentage compositions for the  $3d^{5}4s$  configuration.

Raassen and van Kleef derived the ionization energy from the two-member  $3d^{5}np$  and nf series. We have confirmed their value to within  $300 \text{ cm}^{-1}$  by recalculating the  $3d^{5}({}^{6}\text{S})nf$   ${}^{5}\text{F}$  series limit and assuming a value for  $n^{*}(5f) - n^{*}(4f)$  of 0.9952 taken from Zn II. Accordingly, we reduced their uncertainty estimate of  $\pm 3000 \text{ cm}^{-1}$  to  $\pm 500 \text{ cm}^{-1}$ .

#### References

Raassen, A. J. J., van Kleef, Th. A. M., and Metsch, B. C. (1976), Physica 84C, 133.

Raassen, A. J. J., and van Kleef, Th. A. M. (1977), Physica 85C, 180.

Configuration	Term	J	Levei (cm ⁻¹ )	.evel Leading per .m ⁻¹ )			
3d ⁶	⁵ D	4	0.0	100			
		3	889.7	100			
		2	1 489.9	100			
		1	1 871.5	100			
		0	2 057.6	100			
3 <b>d</b> ⁶	³ P2	2	26 153.0	62	38	³ P1	
		1	28 697.6	63	37		
		0	29 640.0	62	36		
3 <i>d</i> ⁶	³ H	6	27 111.2	99	1	¹ I	
		5	27 578.2	97	3	³ G	
		4	27 858.8	88	5	³ F2	
$3d^6$	³ F2	4	29 123.7	68	20	³ F1	
		3	29 570.8	75	20		
		2	29 899.2	80	20		
$3d^6$	³ G	5	33 256.5	97	3	³ Н	
	-	4	34 061.7	93	4	³ F2	
		3	34 416.4	96	4	³ F2	
3 <i>d</i> ⁶	¹ <b>I</b>	6	41 252.2	99	1	³ H	
$3d^6$	³ D	2	41 626.9	97	2	¹ D2	
	_	1	41 701.1	100	-		
		3	41 920.2	100			
3 <i>d</i> ⁶	¹ G2	4	42 208.1	65	33	¹ G1	
3 <i>d</i> ⁶	¹ S2	0	47 699.7	76	22	¹ <b>S</b> 1	
3 <b>d</b> ⁶	¹ D2	2	48 607.0	76	21	¹ D1	
3 <i>d</i> ⁶	¹ <b>F</b>	3	57 924.1	98	1	³ F1	

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Configuration	Term	J	Level (cm ⁻¹ )	Lead	ing percen	tages
3d ⁶	³ P1	0	66 737 8	64	36	³ P2
04		1	67 547.9	63	37	
		2	69 156.1	62	38	
$3d^6$	³ F1	2	68 632.1	80	20	³ F2
		4	68 718.7	77	22	
		3	68 854.7	78	20	
$3d^6$	¹ G1	4	77 899.5	66	34	¹ G2
$3d^6$	¹ D1	2	104 420.5	78	22	¹ D2
$3d^5(^6\mathrm{S})4s$	⁷ S	3	164 525.9	100		
$3d^5(^6\mathrm{S})4s$	⁵ S	2	178 019.8	100		
$3d^{5}({}^{4}\mathrm{G})4s$	⁵G	6	208 046.4	100		
		5	208 131.0	100		
		2	208 151.5	99	1	$({}^{2}F1) {}^{3}F$
	1	4	208 163.7	100		
		3	208 164.6	100		
$3d^{5}({}^{4}\mathrm{P})4s$	⁵ <b>P</b>	3	212 095.8	90	9	( ⁴ <b>D</b> ) ⁵ <b>D</b>
		2	212 253.4	91	8	
		1	212 455.7	96	4	
$3d^{5}({}^{4}\mathrm{D})4s$	⁵ D	4	216 189.9	99	1	$({}^{4}G){}^{3}G$
		0	216 305.7	98	2	$({}^{4}\mathbf{P}) {}^{3}\mathbf{P}$
		1	216 434.7	94	4	$({}^{4}\mathbf{P}) {}^{5}\mathbf{P}$
		2	216 590.5	91	8	( ⁴ <b>P</b> ) ⁵ <b>P</b>
		3	216 596.0	90	9	( ⁴ <b>P</b> ) ⁵ <b>P</b>
$3d^{5}({}^{4}\mathrm{G})4s$	³ G	5	217 048.7	100		
		3	217 101.0	99	1	$(^{2}F1)^{-1}F$
		4	217 129.1	99	1	( ⁴ D) ⁵ D
$3d^{5}({}^{4}\mathrm{P})4s$	³ P	2	221 087.6	88	9	( ⁴ D) ³ D
		1	221 429.0	92	6	
$3d^{5}({}^{4}\mathrm{D})4s$	³ D	3	225 200.7	99		
		1	225 545.1	94	6	( ⁴ P) ³ P
		2	225 616.5	90	9	( ⁴ <b>P</b> ) ³ <b>P</b>
$3d^{5}(^{2}\mathbf{I})4s$	³ I	6	229 408.8	99	1	$(^{2}H)^{3}H$
		5	229 413.0	99	1	$(^{2}H)$ ³ H
		7	229 440.6	100		
$3d^{5}(^{2}\text{D}3)4s$	³ D	3	232 545.9	55	19	$(^{2}F1)$ $^{3}F$
		2	232 655.6	50	17	$({}^{2}F1) {}^{3}F$
		1	232 910.8	50	34	( ⁴ <b>F</b> ) ⁵ <b>F</b>
$3d^{5}(^{2}\mathbf{I})4s$	¹ I	6	233 839.2	<b>9</b> 8	2	( ² H) ³ H
$3d^{5}({}^{4}\mathrm{F})4s$	⁵ <b>F</b>	5	234 082.1	98	2	$(^{2}G2)^{3}G$
	_	4	234 125.4	92	5	$(^{2}F1)^{3}F$
		3	234 275.2	89	8	$(^{2}F1)^{3}F$
		2	234 412.7	70	23	$(^{2}F1)^{3}F$
		1	235 116.5	65	27	$(^{2}D3)^{3}D$

Ni v-Continued

Configuration	Term	J	Level (cm ⁻ⁱ )	Lead	ing percer	ntages	
$\frac{1}{3d^5(^2\mathbf{F1})4s}$	³ F	4	235 420.6	92	6	( ⁴ <b>F</b> ) ⁵ <b>F</b>	
	_	2	235 736.5	36	23	$(^{2}D3)^{-3}D$	
		3	236 454.1	69	16	( ² D3) ³ D	
$3d^{5}(^{2}\text{D3})4s$	¹ <b>D</b>	2	239 107.7	55	23	( ² F1) ³ F	
$3d^{5}(^{2}\mathrm{F1})4s$	¹ <b>F</b>	3	240 193.8	83	6	( ² G2) ³ G	
$3d^{5}(^{2}\mathrm{H})4s$	³ H	4	240 959.6	71	24	( ² G2) ³ G	
		5	241 082.2	69	28	$(^{2}G2)$ $^{3}G$	
		6	241 773.6	97	2	$(^{2}I)^{-1}I$	
$3d^{5}(^{2}\text{G2})4s$	³ G	3	242 290.4	79	12	$({}^{4}\mathbf{F}) {}^{3}\mathbf{F}$	
				45	28	$({}^{4}F) {}^{9}F$	
		5	242 862.6	66	30	(*H) *H	
$3d^5(^6S)4p$	⁷ P°	2	242 837.0	99	1	( ⁶ S) ⁵ P°	
		3	243 608.5	98	2	("S) "P"	
		4	244 900.5	100			
$3d^{5}({}^{4}\mathbf{F})4s$	³ F	2	243 266.2	93	3	$({}^{2}F2) {}^{3}F$	
( - /		4	243 331.5	62	30	$(^{2}G2)$ ³ G	
		3	243 370.5	83	14	( ² G2) ³ G	
$3d^{5}(^{2}\mathrm{H})4s$	¹ H	5	246 240.9	96	4	( ² G2) ³ G	
$3d^{5}(^{2}\text{G2})4s$	¹ G	4	247 049.1	63	33	( ² F2) ³ F	
$3d^{5}({}^{2}\mathrm{F2})4s$	³ F	3	247 104.9	97	1	( ⁴ F) ⁵ F	
		2	247 165.0	96	3	$({}^{4}\mathbf{F}) {}^{3}\mathbf{F}$	
		4	247 281.8	63	<b>29</b>	$(^{2}G2)$ ¹ G	
$3d^{5}(^{2}$ <b>F2</b> ) $4s$	¹ F	3	251 654.9	<del>96</del>	2	( ⁴ F) ³ F	
$3d^{5}({}^{6}S)4p$	⁵ P°	3	253 862.7	96	2	( ⁶ S) ⁷ P°	
-		2	254 495.6	97	1	$(^{4}D) ^{5}P^{\circ}$	
		1	254 885.0	98	1	( ⁴ D) ⁵ P [•]	
$3d^{5}(^{2}S)4s$	³ S	1	253 905.2	100			
$3d^{5}(^{2}\text{D2})4s$	³ D	1	263 700.9	100			
	İ	2	263 735.7	99			
		3	263 805.8	99			
$3d^{5}(^{2}\text{D2})4s$	¹ D	2	268 273.9	99			
$3d^{5}(^{2}\text{G1})4s$	³ G	5	274 695.4	100			
		4	274 738.6	100			
		3	274 773.5	100			
$3d^{5}(^{2}\mathrm{G1})4s$	¹ G	4	279 199.5	100			
$3d^{5}({}^{4}\mathrm{G})4p$	⁵G°	2	284 215.5	92	4	( ⁴ G) ³ F°	
2		3	284 249.0	84	9	('G) 'H'	
		4	284 308.9	81	14	(G) "H"	
		5	284 402.5	80	14	(G) H	
		6	284 579.5	84	11	('G) 'H'	
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Ni v-Continued

Configuration	Term	J	Levei (cm ⁻¹ )	L	eading	perce	ntages
$3d^{5}({}^{4}\mathrm{G})4p$	⁵ H°	3	286 293.6	88		8	( ⁴ G) ⁵ G°
		4	286 706.6	82		12	$({}^{4}\mathbf{G}) {}^{5}\mathbf{G}^{*}$
		5	287 127.2	75		11	$({}^{4}G) {}^{5}F^{\circ}$
	1	6	287 645.9	86		13	( ⁴ G) ⁵ G°
		7	288 021.6	100		10	
$2d^{5}(4\mathbf{D})/n$	5 <b>D</b> °	1	987 755 5	69		90	⁴ 0° (1 ⁴ )
ou ( F)4p	D	2	987 789 1	03		10	$(\mathbf{D})$ $\mathbf{D}$
		0	290 262.0	45 64		18 19	$({}^{4}D) {}^{5}D^{\circ}$
$3d^{5}(^{4}C)/n$	5150	5	987 ODE 0	75		0	(4C) 5U°
(0)		1	207 300.3 000 161 6	15		10	$(4D)^{5}E^{9}$
		1	200 101.0	71		10	
			289 103.0	71		11	
		2	289 247.1	52		13	( <b>P</b> ) <b>D</b>
		3	289 298.0	40		32	(*P) [°] D°
$3d^5({}^4\mathrm{G})4p$		3	287 960.0	39	⁵ F°	25	( ⁴ P) ⁵ D°
$3d^5(^4\mathrm{P})4p$		2	288 877. <b>9</b>	38	⁵ S°	9	( ⁴ G) ⁵ F°
$3d^{5}({}^{4}\mathrm{P})4p$	⁵ P°	3	290 757.0	44		32	( ⁴ D) ⁵ P°
		2	291 390.0	58		26	
		1	291 541.7	71		15	
$3d^{5}({}^{4}\mathrm{G})4n$	³ F°	2	291 097 7	84		4	( ⁴ G) ⁵ G°
		3	291 328 5	21			$({}^{4}\mathbf{F}){}^{3}\mathbf{F}^{\circ}$
		4	291 554.6	88		4	$(^{4}\mathbf{F})^{3}\mathbf{F}^{\circ}$
2.15.40.1-	3110	c	201 201 /			•	(40) 5110
5a ('G)4p	п	0	291 091.4	93		3	
		5	292 353.4	94		2	$(^{2}\mathbf{G})^{*}\mathbf{H}^{*}$
		4	292 631.0	95		2	(1) ³ H [*]
$3d^{5}(^{4}\mathrm{P})4p$	³ P°	2	292 983.0	52		18	( ⁴ D) ³ P°
		1	293 420.0	53		18	
		0	293 867.0	65		20	
$3d^{5}(^{4}\mathrm{D})4p$	⁵ F°	1	293 833.8	73		17	( ⁴ G) ⁵ F°
		2	294 086.0	76		15	
		3	294 443.3	76		11	
		4	294 939.6	79		8	
		5	295 444.3	91		6	
$3d^{5}({}^{4}\mathbf{D})4p$	⁵ D°	3	296 574.0	51		18	( ⁴ <b>P</b> ) ⁵ <b>D</b> °
-		4	296 919.3	68		22	
		2	297 013.9	54		17	
		1	297 417 9	51		17	
		0	298 060.0	63		22	
$2d^{5}(4C)/n$	³ C*	3	906 017 1			0	( ⁴ ፑ) ³ ር°
<i>a</i> (G)4 <i>p</i>	G	0	290 841.1	90		2	
		4	290 897.0	91		2	
		Ð	296 932.9	92		2	('G') ' <b>F</b> ''
$3d^5({}^4\mathrm{P})4p$	${}^{3}\mathbf{D}^{\circ}$	3	297 418.1	60		14	( ⁴ <b>D</b> ) ⁵ <b>P</b> °
		2	297 842.5	57		18	
$3d^{5}({}^{4}\mathbf{D})4n$	⁵ P°	1	297 982 8	40		36	( ⁴ P) ³ D°
ou (D)+p		2	299 045.6	39		19	$(^{4}P)$ ⁵ P°
					300-		4
$d^{\circ}(^{\circ}P)4p$		1	298 600.6	30	°D°	29	(*D) ³ P*
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Configuration	Term	J	Level (cm ⁻¹ )	Leadi	ng percer	ntages
$Bd^{5}({}^{4}\mathrm{D})4p$	³ D°	3	298 972.3	43	15	( ⁴ P) ⁵ P°
		2	300 224.9	74	8	$({}^{4}\mathbf{F}) {}^{3}\mathbf{D}^{\circ}$
		1	300 563.3	65	17	( ⁴ <b>P</b> ) ³ <b>D</b> [•]
$Bd^{\bar{\mathfrak{d}}}({}^{4}\mathrm{D})4p$		3	300 201.0	36 ³ D°	31	( ⁴ D) ⁵ P°
$Bd^{5}({}^{4}\mathrm{D})4p$	³ F°	4	300 918.1	84	5	$(^{2}G2)^{3}F^{\circ}$
		3	301 470.2	76	8	$({}^{4}P) {}^{3}D^{\circ}$
		2	301 553.0	80	7	( ⁴ P) ³ D°
$Bd^{5}({}^{4}\mathrm{P})4p$	³ S°	1	303 249.5	91	3	( ⁴ D) ³ P*
$\mathbf{B}d^{\mathfrak{d}}(\mathbf{^{4}D})4p$	³ P°	0	305 386.9	72	22	( ⁴ P) ³ P°
		1	305 838.1	66	21	
		2	306 377.8	63	<b>2</b> 5	
$3d^{5}(^{2}\mathrm{I})4p$	³ K°	6	305 590.8	69	26	$(^{2}I)^{3}I^{\circ}$
		7	305 996.3	56	34	$(^{2}I)^{3}I^{\circ}$
		8	308 138.8	100		
$3d^{5}(^{2}\mathrm{I})4p$	³ I°	5	306 049.0	64	19	$\binom{2}{2}$ 1) ¹ H [•]
		6	307 399.7	53	26	$(^{2}\mathbf{I})^{3}\mathbf{K}^{\bullet}$
		7	308 317.3	62	38	$(^{2}I)$ ³ K [•]
$3d^{5}(^{2}\text{D1})4s$	³ D	3	306 962.9	77	23	( ² D3) ³ D
		2	307 025.2	77	23	
		1	307 105.1	76	23	
$3d^{5}(^{2}\text{D}3)4p$	³ F°	2	307 731.1	21	25	( ² F1) ³ F°
		3	308 592.0	37	23	
		4	310 212.6	39	25	
3d ⁵ ( ² I)4p	¹ H•	5	308 804.1	52	29	$(^{2}I)$ ³ I [•]
$3d^{5}(^{2}\text{D}3)4p$		2	308 943.0	29 ³ F°	21	¹ D*
$3d^{5}({}^{2}\mathrm{I})4p$	³ H°	6	309 264.0	73	17	$(^{2}I)$ $^{3}I^{\circ}$
		5	309 919.5	78	11	$(^{2}I)^{1}H^{\bullet}$
		4	309 952.5	79	5	( ² G2) ³ H*
$3d^5(^2\mathbf{I})4p$	¹ K°	7	309 743.6	91	5	( ² I) ³ K•
$3d^{5}(^{2}\mathrm{D1})4s$	¹ D	2	311 470.3	77	23	( ² D3) ¹ D
$3d^{5}(^{2}D3)/4n$	3 <b>D</b> •	2	211 066 5	40	15	$({}^{2}\mathbf{F}1) {}^{3}\mathbf{D}^{\circ}$
0a ( D0/4p		õ	313 577.3	66	20	( ² D1) ³ P [•]
$3d^{5}({}^{2}\mathrm{F1})4p$	¹ G°	4	312 008.3	43	12	( ² H) ¹ G*
$3d^{5}(^{2}\text{D}3)4p$		1	312 291.0	31 ³ P*	28	( ² D3) ³ D°
0.15/2101.)/-	300	9	910 169 9	49	20	( ² F1) ³ F°
oa (⁻r 1/4p	L G	5	312 403.3 314 702.2	43 70	20	( ⁴ <b>F</b> ) ⁵ <b>G</b> [•]
2.J ⁵ (4F)/r	50.0	2	319 778 9	78	9	( ² F1) ³ F*
ou (r)4p	U U	3	312 889 4	43	19	( ² D3) ⁸ D*
		4	313 281 3	72	5	$({}^{4}F) {}^{5}F^{\circ}$
			010 001.0			
		15	313 464 7	56	15	$({}^{2}F1) {}^{3}G^{\bullet}$

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Ni v-Continued

Configuration	Term	J	Level (cm ⁻¹ )	Leading percentages
$3d^{5}(^{2}\mathrm{F1})4p$		3	312 953.6	$33  {}^{3}D^{\circ}  31 \qquad ({}^{4}F) \; {}^{5}G^{\circ}$
$3d^{5}(^{2}\text{D}3)4p$		1	313 679.0	29 ${}^{3}D^{\circ}$ 27 $({}^{2}D3) {}^{3}P^{\circ}$
$3d^{5}(^{2}\text{D}3)4p$	³ D°	2	313 686.6	45 15 $(^{2}D1)^{3}D^{\circ}$
$3d^{5}({}^{2}\mathrm{F1})4p$		3	313 919.8	23 ${}^{3}D^{\circ}$ 22 $({}^{2}D3) {}^{3}D^{\circ}$
$3d^{5}({}^{2}\mathrm{F1})4p$		4	314 208.8	$30 \ {}^{3}F^{\circ} \ 30 \ ({}^{2}F1) \ {}^{3}G^{\circ}$
$3d^5(^2\mathrm{I})4p$	¹ I°	6	314 392.0	44 38 ( ⁴ F) ⁵ G°
$3d^{5}({}^{4}\mathrm{F})4p$	⁵ F°	3	314 562.8	61 25 $({}^{4}\mathbf{F}) {}^{5}\mathbf{D}^{\circ}$
-		4	314 599.2	39 21 $({}^{4}\mathbf{F}) {}^{5}\mathbf{D}^{\circ}$
		2	314 834.7	42 23 $({}^{4}\mathbf{F}) {}^{5}\mathbf{D}^{\circ}$
		1	315 152.8	74 9 $({}^{4}\mathbf{F}) {}^{5}\mathbf{D}^{\circ}$
		5	315 168.2	65 9 $({}^{4}F) {}^{5}G^{\circ}$
$3d^{5}(^{2}\text{F1})4p$	³ D°	1	315 300.7	51 19 ( ² D3) ¹ P°
$3d^{5}(^{2}\mathrm{F1})4p$		3	315 326.2	25 ${}^{3}G^{\circ}$ 14 $({}^{2}D3) {}^{1}F^{\circ}$
$3d^{5}(^{2}\text{F1})4p$		2	315 366.1	$32  {}^{3}D^{\circ}  18  ({}^{4}F)  {}^{5}F^{\circ}$
$3d^{5}(^{2}G2)4p$	³ H°	4	315 370.1	31 29 $(^{2}H)$ $^{3}H^{\circ}$
		5	323 908.6	36 28
		6	325 148.4	45 37
$3d^{\circ}(^{2}\mathrm{H})4p$	³ H°	5	315 990.5	$30$ $36$ $({}^{2}G2) {}^{3}H^{\circ}$
		6	317 327.3	3 <b>9 3</b> 5
		4	323 926.3	44 36
$3d^{5}(^{2}\text{D}3)4p$		4	316 068.8	20 ${}^{3}F^{\circ}$ 18 $({}^{2}F1) {}^{3}G^{\circ}$
$3d^{5}({}^{2}\mathrm{F1})4p$		2	316 165.4	$31 \ ^{3}F^{\circ} \ 17 \ (^{2}F1) \ ^{3}D^{\circ}$
$3d^{5}({}^{2}\mathrm{F1})4p$		3	316 280.3	19 ${}^{3}F^{\circ}$ 14 ( ${}^{2}D3$ ) ${}^{1}F^{\circ}$
$3d^5(^2\mathrm{H})4p$	³ G°	5	316 726.6	47 14 $(^{2}G2)$ ³ G [•]
$3d^{5}({}^{4}\mathrm{F})4p$	⁵ D°	4	316 744.0	44 24 $({}^{4}\mathbf{F}){}^{5}\mathbf{F}^{\circ}$
		3	317 232.0	39 17 $({}^{4}\mathbf{F}) {}^{5}\mathbf{F}^{\bullet}$
		0	317 462.3	88 7 $(^{2}D3)^{3}P^{\circ}$
		1	317 477.9	76 9 ( ⁴ F) ⁵ F°
		2	317 517.5	65 15 ( ⁴ F) ⁵ F°
$3d^5(^2\mathrm{H})4p$		4	316 887.8	36 $^{3}G^{\circ}$ 12 ( $^{2}F2$ ) $^{3}G^{\circ}$
$3d^{5}({}^{4}\mathrm{F})4p$		3	<b>3</b> 17 <b>376</b> .8	22 ${}^{5}D^{\circ}$ 20 $({}^{2}H) {}^{3}G^{\circ}$
$3d^5(^2\text{D}3)4p$	¹ P°	1	319 073.4	45 22 ( ² F1) ³ D [•]
$3d^{5}(^{2}\mathrm{H})4p$	3 ¹ °	5	319 076.2	85 6 ( ² H) ³ H°
		6	319 860.4	78 8 $(^{2}\text{H})^{1}\text{I}^{\circ}$
		7	320 783.1	95 2 $(^{2}I)^{3}I^{\circ}$
$3d^{5}(^{2}\text{G2})4p$		4	319 138.7	25 ${}^{1}G^{\circ}$ 18 $({}^{2}F1) {}^{1}G^{\circ}$

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B	Term	J	Level (cm ⁻¹ )	Leadi	ng percer	ntages
$3d^{5}({}^{4}\mathbf{F})4p$	³ G°	3	319 620 2	38	32	( ² G2) ³ G°
· - ·		5	319 652.7	65	15	(,
		4	319 899.1	57	15	
$d^{5}(^{2}\mathrm{F1})4p$	¹ D°	2	319 926.5	51	29	$(^{2}D3)$ $^{1}D^{\circ}$
$3d^{5}(^{2}\text{G2})4p$	³ F°	3	320 513.8	41	18	( ⁴ F) ³ G°
•		2	321 018.3	57	11	$({}^{4}F) {}^{3}F^{\circ}$
		4	321 056.4	54	13	( ² G2) ¹ G°
$3d^{5}({}^{2}\mathrm{F1})4p$	¹ F°	3	321 081.9	52	17	$(^{2}G2)$ $^{3}F^{\circ}$
$Bd^{5}(^{2}\mathrm{H})4p$	¹ I°	6	322 324.2	76	9	( ² H) ³ H°
$Bd^{5}({}^{4}\mathbf{F})4p$	³ D°	2	322 436.4	54	11	$({}^{2}F2) {}^{3}F^{\circ}$
•		3	322 617.6	50	10	$({}^{2}\mathbf{F2}) {}^{3}\mathbf{F}^{\circ}$
		1	322 984.5	79	7	( ⁴ D) ³ D°
$3d^{5}({}^{4}\mathrm{F})4p$	³ F°	4	322 820.8	60	28	( ² F2) ³ F°
		3	323 532.2	60	17	
		2	323 853.1	53	20	
$3d^{5}(^{2}\text{G2})4p$	³ G°	5	324 980.2	25	21	( ² F2) ³ G°
		3	325 211.9	30	29	
		4	325 222.9	27	28	
$3d^{5}(^{2}\mathrm{F2})4p$		4	325 558.6	32 ¹ G	13	$(^{2}G2)$ $^{1}G^{\circ}$
$3d^{5}(^{2}\mathrm{F2})4p$	³ F°	2	325 982.2	26	23	( ⁴ F) ³ F°
		3	326 029.9	48	13	
		4	326 876.3	44	14	
$3d^{5}(^{2}\text{G2})4p$	¹ H°	5	326 337.1	53	26	$(^{2}H)$ $^{1}H^{\circ}$
$3d^{5}(^{2}G2)4p$	¹ F°	3	326 739.0	58	6	$(^{2}G2)$ $^{3}G^{\circ}$
$3d^{5}(^{2}\mathbf{F}2)4p$	¹ <b>D</b> °	2	327 122.7	60	24	$(^{2}F2)$ $^{3}F^{\circ}$
$3d^{5}(^{2}\mathrm{H})4p$	¹ H*	5	327 356.6	63	29	$(^{2}G2)$ ¹ H°
$3d^5(^2\mathbf{F2})4p$	³ D°	1	329 462.3	55	21	$(^{2}S)^{3}P^{\circ}$
		2	329 776.3	70	12	$({}^{2}F1) {}^{3}D^{\circ}$
		3	329 872.9	47	12	( <b>*F</b> 2) <b>*G*</b>
$3d^{5}(^{2}\mathrm{F2})4p$	³G°	3	329 614.3	27	33	( ² H) ³ G°
		4	330 297.6	47	37	
		5	330 718.1	58	31	
$3d^5(^2\mathbf{S})4p$	³ P°	0	329 618.5	83	13	$\binom{^{2}\text{D2}}{^{^{2}\text{E2}}}$
		1	330 370.7	58	23	$(^{2}F2)^{3}D^{3}$
		2	331 678.2	74	16	(*D2) "P"
$3d^5(^2\mathrm{H})4p$	¹ G°	4	332 9 <b>9</b> 5.6	39	37	$(^{2}F2)$ $^{1}G^{\circ}$
	¹ P°	1	334 477.2	70	19	$(^{2}D2)$ $^{1}P^{\circ}$
$3d^5(^2\mathbf{S})4p$						

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Configuration	Term	J	Level (cm ⁻¹ )	Lead	ing percen	itages
$3d^5(^2\text{D2})4p$	³ F°	2 3	342 894.6 343 281.0	67 50	21 27	( ² D2) ³ D° ( ² D2) ³ D°
	2	4	344 911.2	92	5	( ² G2) ³ F [•]
$3d^{\circ}(^{2}\text{D2})4p$	°D°	1	343 478.2	89	2	$(^{2}D2)^{3}P^{\circ}$
		2	343 905.7	65	21	$(^{2}D2)$ $^{3}F^{0}$
		3	344 805.3	60	33	$(^{2}\text{D2})^{3}\text{F}^{4}$
$3d^5(^2\text{D2})4p$	¹ F°	3	345 936.1	72	12	$(^{2}G1)$ $^{1}F^{\circ}$
$3d^{5}(^{2}D2)4p$	³ P°	2	346 912.4	72	16	$(^{2}S)^{3}P^{\circ}$
00 ( D=) -p	_	Ō	346 920.2	85	14	
		1	346 959.5	76	15	
	1.					
$3d^{5}(^{2}\text{D2})4p$	¹ P*	1	348 477.9	72	17	$(^{2}S)$ ¹ P°
$3d^5(^2\text{D2})4p$	¹ D°	2	349 546.0	87	5	$(^{2}F2)$ $^{1}D^{\circ}$
$3d^{5}(^{2}\text{G1})4p$	³ H°	4	353 071.6	47	31	$({}^{2}G1) {}^{3}F^{\circ}$
		5	353 548.7	76	15	$(^{2}G1)^{3}G^{\circ}$
		6	354 989.6	98	2	$(^{2}I)$ ³ H°
0.15/201.1.	3100		959 917 1	-		(201) 3770
3a ⁻ (-GI)4p	r	4	303 347.1	50	40	$(^{2}C1)^{3}C^{2}$
		0	333 344.1	55	36	$(^{2}G1)^{3}G^{2}$
		2	355 150.0	90	6	$(\mathbf{D}\mathbf{I})$ <b>F</b>
$3d^{5}(^{2}\text{G1})4p$	³ G°	3	355 398.0	59	36	$({}^{2}G1) {}^{3}F^{\circ}$
<b>-</b>	_	4	355 765.2	80	9	$(^{2}G1)$ ³ F°
		5	356 036.3	78	18	( ² G1) ³ H°
$3d^{5}(^{2}\mathrm{G1})4p$	¹ H°	5	358 475.6	90	4	( ² G1) ³ G°
$3d^{\circ}(^{2}\text{G1})4p$	¹ G.º	4	358 760.0	93	2	( ² G1) ³ F°
$3d^{5}({}^{2}\text{G1})4p$	¹ F°	3	360 059.7	78	10	$(^{2}D2)$ $^{1}F^{\circ}$
$3d^{5}(^{2}\mathrm{P})4p$	³ P°	0	368 440.5	75	20	$(^{2}D1)^{3}P^{\circ}$
		1	368 749.7	73	21	•
		2	369 649.1	72	23	
$3d^{5}(^{2}\mathbf{P})4n$	³ D°	2	374 803 7	57	97	$(^{2}P)^{1}D^{\circ}$
ou (1/4p		1	374 828 1	90	5	
		3	376 471.6	89	7	$(^{2}D1)^{3}D^{\circ}$
$3d^5(^2\mathrm{P})4p$	¹ <b>D</b> °	2	377 059.1	49	33	( ² P) ³ D°
$3d^5(^2\mathrm{P})4p$	³ S*	1	378 555.0	90	7	( ² <b>P</b> ) ¹ <b>P</b> °
$3d^5(^2\mathrm{P})4p$	¹ P°	1	380 165.6	68	16	( ² D1) ¹ P°
$3d^{5}(^{2}\text{D1})4n$	³ F°	2	386 968 8	63	20	$(^{2}D3)^{3}F^{\circ}$
ou ( D1) .p	-	3	387 333.4	60	19	(20) 1
		4	388 698.9	72	22	
0. m/2	3754		000 01 0 1			(2 <b>D</b> a) 3 <b>D</b> a
$3d^{\circ}(^{*}D1)4p$	"D"		388 746.1	71	21	("D3) "D"
		2	389 571.8	60	18	
		3	390 478.2	60	18	
$3d^{5}(^{2}\text{D1})4p$	¹ D°	2	390 675.1	44	16	( ² P) ¹ D°

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Configuration	Term	J	Level (cm ⁻¹ )	Lead	ing percer	itages
$3d^{5}(^{2}\text{D1})4p$	³ P°	2	3 <b>9</b> 2 413.5	43	21	( ² P) ³ P°
$3d^{5}(^{2}\text{D1})4p$	¹ <b>F°</b>	3	<b>39</b> 2 <b>9</b> 57.1	69	21	( ² D3) ¹ F°
3d⁵( ⁶ S)5p	₂Ъ.	3 2 1	423 533 423 782 423 935			
3d⁵( ⁶ S)4f	⁵ F°	2 1 3 4 5	439 419 439 420 439 423 439 423 439 427 439 434			
3d ⁵ ( ⁶ S)5f	⁵ F•	5 4 3 1 2	502 124 502 133 502 137 502 143 502 143 502 148			
Ni VI ( ⁶ S _{5/2} )	Limit		613 500			

Ni v-Continued

V I isoelectronic sequence

Ground state: 1s²2s²2p⁶3s²3p⁶3d⁵⁶S_{5/2}

Ionization energy =  $870\ 000\pm 16\ 000\ cm^{-1}\ (108\pm 2\ eV)$ 

The resonance multiplet  $3d^{5}6S - 3d^{4}4p$  ⁶P[•] was identified by Kruger and Gilroy (1935). An extensive analysis of this spectrum was carried out by Raassen (1980), who reported all the presently known levels and their percentage compositions. The uncertainty in the level values is probably  $\pm 5$  cm⁻¹.

The ionization energy was obtained by extrapolation by Lotz (1967).

# References

**b**uilte

Kruger, P. G., and Gilroy, H. T. (1935), Phys. Rev. 48, 720.
Lotz, W. (1967), J. Opt. Soc. Am. 57, 873.
Raassen, A. J. J. (1980), Physica 100C, 404.

Ni VI							
Term	J	Level (cm ⁻¹ )	Lead	ling perce	ntages		
⁶ S	⁵ /2	0.0	100	•			
4G	11/2	41 920.9	100				
-	5/2	42 003.6	99		1	² F1	
	9/2	42 023.2	100		-		
	"∕₂	42 035.1	100				
4p	ь,	45 884.2	90		9	4D	
	8/2	46 104.4	92		7	_	
	1/2	46 324.8	97		8		
4D	7/2	50 331.0	99				
	1/2	50 643.5	97		8	4P	
	5/2	50 777.6	90		9	4P	
	8/2	50 780.5	92		7	⁴ P	
۶I	¹¹ / ₂	61 196.0	98		2	²H	
	¹⁸ / ₂	61 279.5	100				
²D3	⁵ √2	64 152.4	52		29	<b>2</b> F1	
	⁸ / ₂	65 173.5	71		22	2D1	
<b>²</b> F1	⁷ /2	67 085.1	98		8	<b>'F</b>	
4F	⁵ / ₂	68 444.9	51		89	<b>²F</b> 1	
	⁹ / ₂	68 551.2	95		4	<b>2</b> G2	
	7/2	68 801.7	94		4	<b>2F</b> 1	
	∛2	69 173.5	92		6	2D3	
	5∕2	69 447.0	47	<b>'</b> F	81	² <b>F</b> 1	
² H	9/2	72 908.8	74		24	² G2	
	¹¹ /2	73 756.6	98		2	²I	
² G2	7/2	74 627.7	98		1	<b>'</b> F	
	%_	75 441.7	72		25	ľΗ	
*F2	5/2	79 391.4	96		1	⁴F	
	∛₂	79 608.8	97		2		
	Term           *S           *G           *P           *D           *I           *D3           *F1           *F2	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	TermJLevel (cm ⁻¹ ) 6S ${}^5{}_2$ 0.0 4G ${}^{11}{}^1_{2}$ 41 920.9 ${}^5{}_2$ 4G ${}^{11}{}^1_{2}$ 41 920.9 ${}^5{}_2$ 72 42 003.6 	TermJLevel (cm ⁻¹ )Lead*S $\frac{5}{2}$ 0.0100*G $\frac{11}{2}$ 41 920.9100* $\frac{9}{2}$ 42 03.699 $\frac{9}{2}$ 42 035.1100*P $\frac{5}{2}$ 45 884.290 $\frac{9}{2}$ 42 035.1100*P $\frac{5}{2}$ 46 104.492 $\frac{9}{2}$ 46 324.897*D $\frac{7}{2}$ 50 331.099 $\frac{9}{2}$ 50 643.597 $\frac{9}{2}$ 50 777.690 $\frac{9}{2}$ 61 196.098 $\frac{11}{2}$ 61 196.098 $\frac{13}{2}$ 65 173.571*F1 $\frac{7}{2}$ 67 085.198*F2 $\frac{5}{2}$ 68 444.951 $\frac{9}{2}$ 69 173.592 $\frac{5}{2}$ 69 447.047*H $\frac{9}{2}$ 72 908.874*G2 $\frac{7}{2}$ 73 756.698*G2 $\frac{7}{2}$ 79 9991.498*G2 $\frac{7}{2}$ 79 991.498	Term         J         Level (cm ⁻¹ )         Leading perce 6S $5_2$ 0.0         100 4G ${}^{11}j_2$ 41 920.9         100 ${}^{5}j_2$ 42 003.6         99         92 ${}^{7}j_2$ 42 023.2         100         100 ${}^{4}P$ $5_{12}^{5}$ 42 023.2         100 ${}^{4}P$ $5_{12}^{5}$ 46 104.4         92 ${}^{4}D$ $7_{12}^{5}$ 50 331.0         99 ${}^{4}D$ $7_{12}^{5}$ 50 780.5         92 ${}^{5}D$ $50780.5$ 92         50 ${}^{5}D$ $50780.5$ 92         50 ${}^{11}j_2$ 61 196.0         98         91 ${}^{11}j_2$ 61 279.5         100         92 ${}^{5}D$ $5_{2}^{5}$ 65 173.5         71 ${}^{5}F1$ $7_{2}^{5}$ 68 444.9         51 ${}^{5}j_2$ 69 47.0         47 $47$ ${}^{5}j_2$ 69 447.0         47 $47$ ${}^{5}j_2$	Term         J         Level (cm ⁻¹ )         Leading percentages           *S $\frac{5}{2}$ 0.0         100           *G $\frac{11}{2}$ 41 920.9         100 $\frac{5}{2}$ 42 003.6         99         1 $\frac{5}{2}$ 42 003.1         100         100           *P $\frac{5}{2}$ 42 035.1         100           *P $\frac{5}{2}$ 45 884.2         90         9           *I $\frac{1}{2}$ 46 324.8         97         8           *D $\frac{7}{2}$ 50 331.0         99         9 $\frac{1}{2}$ 50 643.5         97         8           *D $\frac{7}{2}$ 50 780.5         92         7           *I $\frac{11}{2}$ 61 196.0         98         2           *J $\frac{1}{2}$ 67 085.1         98         3           *D $\frac{7}{2}$ 67 085.1         98         3           *J $\frac{6}{2}$ 99         95         4           *J         68 801.7         94         4         4           *J         69 173.5         92	

Ni VI—Continu	led
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Configuration	Term	J	Level (cm ⁻¹ )	Leading	; percentages	
3d ⁵	² S	1/2	86 532.1	100		
2.45	² D2	3/	96 461 2	100		
		5/2 5/2	96 566.5	99	1	² F2
$3d^5$	² G1	9/2	107 848.3	100		
		7/2	107 887.0	100		
$3d^5$	² <b>P</b>	³ /2	129 951.6	99	1	² D1
		1/2	130 025.9	100		
3 <i>d</i> ⁵	² D1	⁵ /2	140 922.2	77	23	² D3
		3/2	141 006.8	76	23	
$3d^{4}(^{5}D)4s$	⁶ D	¹ / ₂	295 882.7	100		
		3/2	296 198.1	100		
		⁹ / ₂	296 696.7	100		
		1/2	297 350.5	100		
		⁹ / ₂	298 130.5	100		
$3d^4(^5\mathbf{D})4s$	⁴ D	¹ / ₂	307 843.9	99		
		3/2	308 323.8	100		
		5/2	309 054.9	100		
		7/2	309 977.1	100		
3d ⁴ ( ³ P2)4s	4P	1/2	328 437.2	59	38	( ³ P1) ⁴ P
		3/2	330 001.6	60	38	
		5/2	332 344.8	61	38	
$3d^{4}(^{3}\mathrm{H})4s$	⁴H	7/2	329 486.2	97	2	( ³ G) ⁴ G
		9/2	329 754.2	96	3	( ³ G) ⁴ G
		11/2	330 141.0	97	2	( ³ G) ⁴ G
		¹³ / ₂	330 580.5	100		
$3d^{4}({}^{3}F2)4s$	4F	3/2	332 031.8	78	22	$({}^{3}F1) {}^{4}F$
		5/2	332 051.6	74	20	
		7/2	332 175.4	72	19	
		9/2	332 343.6	73	18	
$3d^{4}(^{3}G)4s$	⁴G	5%	335 384.5	91	5	( ³ F2) ⁴ F
		1/2	335 976.0	90	7	$({}^{3}\mathbf{F2}) {}^{4}\mathbf{F}$
	1	9/2	336 344.9	73	18	$(^{3}H)^{2}H$
		11/2	336 430.4	78	19	$(^{3}H)$ $^{2}H$
$3d^4({}^3P2)4s$	² P	¹ / ₂	336 404.8	59	38	$(^{3}P1)$ $^{2}P$
		3/2	339 260.1	60	37	
$3d^{4}(^{3}\mathrm{H})4s$	² H	⁹ / ₂	337 007.7	78	19	( ³ G) ⁴ G
		11/2	337 993.9	79	20	
$3d^{4}({}^{3}\mathrm{F2})4s$	² <b>F</b>	⁵ /2	339 482.4	76	20	$({}^{3}F1) {}^{2}F$
		7/2	339 335.8	70	17	
3.44( ³ G)4e	² G	7/0	343 052.0	90	6	$({}^{3}F2) {}^{2}F$
02 ( 07 13		9/2	343 842.6	96	2	$(^{3}H)^{2}H$
3d ⁴ ( ³ D)/e	ל⁴	7/2	343 999.6	99		
ou ( D/45		5/	344 203 5	98		
		/0				

Ni vI-Continued

Configuration	Term	J	Level (cm ⁻¹ )	Leading	percentages	
$3d^4({}^1\mathrm{G2})4s$	²G	⁹ / ₂ ⁷ / ₂	347 278.5 347 445.2	64 62	31 30	( ¹ G1) ² G
$3d^4({}^1I)4s$	² I	¹³ / ₂ ¹¹ / ₂	347 892.4 347 963.9	100 99	1	( ³ H) ² H
$3d^4(^3\mathrm{D})4s$	² D	5/2 3/2	351 033.0 351 304.0	99 98	1	( ¹ D2) ² D
$3d^4({}^1S2)4s$	² S	¹ / ₂	351 096.2	78	20	( ¹ S1) ² S
$3d^4(^1\text{D2})4s$	² D	⁵ /2 ³ /2	358 716.6 358 827.9	77 77	20 20	( ¹ D1) ² D
$3d^4({}^1\mathrm{F})4s$	² F	5/2 7/2	366 289.8 366 299.8	98 98	1 1	( ³ F1) ⁴ F
3d ⁴ ( ³ P1)4s	⁴ P	⁵ /2 3/2	374 843.9 376 343.7	61 60	38 38	( ³ P2) ⁴ P
$3d^4({}^3{ m F1})4s$	⁴F	9/2 3/2 7/2 5/2	375 673.0 375 870.8 375 927.1 375 949.8	81 78 79 78	19 22 20 21	( ³ F2) ⁴ F
3d ⁴ ( ⁵ D)4p	⁶ F°	$ \begin{array}{c} \frac{1}{2} \\ \frac{3}{2} \\ \frac{5}{2} \\ \frac{7}{2} \\ \frac{9}{2} \\ \frac{9}{2} \\ \frac{11}{2} \end{array} $	380 756.7 381 163.8 381 832.8 382 758.9 383 960.2 385 520.9	99 99 99 98 98 100	1 1 1 1	( ⁵ D) ⁴ D° ( ⁵ D) ⁴ F° ( ⁵ D) ⁴ F° ( ⁵ D) ⁴ F°
$3d^4({}^3\mathrm{F1})4s$	²F	7/2 5/2	382 677.1 382 889.1	80 78	19 21	( ³ F2) ² F
$3d^{4(5}D)4p$	6 <b>P</b> .	³ / ₂ ⁵ / ₂ ⁷ / ₂	383 557.8 383 739.8 384 096.5	91 94 98	6 4 1	( ⁵ D) ⁴ P° ( ⁵ D) ⁴ P° ( ⁵ D) ⁶ D°
$3d^4({}^5\mathrm{D})4p$	⁴ P°	1/2 3/2 5/2	384 747.4 386 157.3 389 760.4	68 55 55	29 33 42	( ⁵ D) ⁶ D°
$3d^4({}^5\mathrm{D})4p$	⁶ D°	5/2 1/2 3/2 7/2 9/2	387 849.9 388 918.6 389 214.0 389 243.4 389 883.2	54 71 64 94 88	38 29 35 4 10	( ⁵ D) ⁴ P° ( ⁵ D) ⁴ P° ( ⁵ D) ⁴ P° ( ⁵ D) ⁴ F° ( ⁵ D) ⁴ F°
$3d^4({}^1\mathrm{G1})4s$	²G	7/2 9/2	389 362.5 389 299.6	66 67	33 33	( ¹ G2) ² G
3d ⁴ ( ⁵ D)4p	4F°	³ /2 ⁵ /2 ⁷ /2 ⁹ /2	392 808.1 393 072.0 393 468.2 394 061.0	94 93 91 85	2 2 4 11	( ³ G) ⁴ F° ( ³ G) ⁴ F° ( ⁵ D) ⁶ D° ( ⁵ D) ⁶ D°

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Ni vi-Continued

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Configuration	Term	J	Level (cm ⁻¹ )	Leading	g perce	ntages	
$3d^4({}^5\mathrm{D})4p$	⁴ D°	¹ / ₂ ³ / ₂ ⁵ / ₂	400 962.1 401 280.9 401 720.9	96 96 96		1 1 1 1	( ³ D) ⁴ D°
		7/2	402 171.3	96		2	
$3d^{4}(^{3}\mathrm{H})4p$	⁴ H°	7/2 9/	411 669.4	74		20	( ³ G) ⁴ H°
		¹ / ₂ 11/ ₂	412 095.6	70 72		19 17	
		13/2	413 631.6	77		13	
$3d^4(^{3}\text{P2})4p$	⁴ D°	1/2 3	412 248.2	47		32	( ³ P1) ⁴ D°
		9/2 5/2	413 553.1	47		31	
		/2 5.	410 144.0	38		26	2
3d*(°F2)4p	'G'	$\frac{\eta_2}{\tau_1}$	415 382.0	40		23	( ³ G) ⁴ G°
		9/2	410 040.0	25		40	( ³ H) ⁴ G°
		11/2	420 623.4	58		22	$(^{3}H)$ $^{4}G^{\circ}$
3d ⁴ ( ³ H)4p	4I°	⁹ / ₂	415 754.3	45		11	$(^{3}H)$ ² G°
		11/2	417 164.1	63		14	( ³ H) ⁴ G [•]
		¹³ / ₂ 15/	418 553.6	90		8	$(^{\circ}H)$ "H"
		7 ₂	419 333.3	99		1	(1) <b>K</b>
$3d^{4}(^{3}\mathrm{H})4p$		⁹ / ₂	416 422.3	43	4I°	11	( ³ F2) ⁴ G*
$3d^4(^{3}\text{P2})4p$	⁴ P°	$\frac{1}{2}$	416 459.0	35		20	( ³ P1) ⁴ P°
		$\frac{3}{2}{5}$	418 491.4	45		25	
		/ ₂	420 308.9	90		28	<b>a</b>
3d ⁴ (3F2)4p	⁴D°	1/2	416 493.0	31		23	$({}^{3}P2) {}^{4}D^{\circ}$
		$\frac{1}{3}$	422 369.4	42		15 19	(°F1) *D* (°F1) *D*
		/2	422 431.2	31		12	
3d ⁴ (''H)4p		11/2	417 538.4	34	⁴G°	25	(*H) *I*
$3d^4(^{3}{ m H})4p$	² G°	7/2	417 717.7	38		16	( ³ F2) ² G°
		⁹ / ₂	418 368.8	32		18	
$3d^{4}({}^{3}\mathrm{F2})4p$		³ / ₂	418 713.4	28	⁴ F°	21	( ³ F2) ² D [•]
$3d^{4}(^{3}\mathrm{H})4p$		⁵ /2	419 390.5	30	⁴G°	26	( ³ F2) ⁴ G°
$3d^4({}^3F2)4p$		⁵ /2	419 844.7	39	⁴ F°	14	( ³ H) ⁴ G°
$3d^{4}(^{3}\mathrm{H})4p$	⁴G°	7/2	419 863.3	47		32	( ³ F2) ⁴ G°
$3d^4(^{3}\text{P2})4p$		1/2	419 961.5	23	⁴P°	18	( ³ P1) ² S°
2 - 4 ( ³ E 2 ) 4 -	450	7,	100 559 0	<b>C</b> 9			( ³ <b>F</b> 1) ⁴ <b>F</b> °
3a (12)4p	, r	9/2 9/2	420 335.2 420 835.3	58		13	( ³ G) ⁴ F [•]
3d ⁴ ( ³ P2)4p		³ / ₂	420 722.0	26	² P•	18	( ³ P2) ⁴ S [•]
$3d^{4}({}^{3}\mathrm{F2})4p$		⁵ /2	421 324.3	19	² D [•]	15	( ³ F2) ⁴ F*
$3d^4({}^3F2)4p$		3/2	421 607.2	24	⁴F°	20	( ³ F2) ² D [•]
3d ⁴ ( ³ F2)4p		5/2	421 8 <b>9</b> 4.0	15	² <b>D</b> •	14	( ³ F2) ⁴ D [•]
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Ni vI-Continued

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21 80 82 22 36 70 54 39 75 18	⁴ D° ² F° ² H°	20 6 11 16 20 20 18 39 14	$({}^{3}G) {}^{4}F^{\circ}$ $({}^{1}I) {}^{2}I^{\circ}$ $({}^{3}G) {}^{4}H^{\circ}$ $({}^{3}F2) {}^{4}D^{\circ}$ $({}^{3}G) {}^{4}H^{\circ}$ $({}^{3}H) {}^{4}H^{\circ}$ $({}^{3}H) {}^{2}H^{\circ}$ $({}^{3}H) {}^{2}H^{\circ}$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	80 82 22 36 70 54 39 75 18	² F° ² H°	6 11 16 20 20 18 39 14	( ¹ I) ² I° ( ³ G) ⁴ H° ( ³ F2) ⁴ D° ( ³ G) ⁴ H° ( ³ H) ⁴ H° ( ³ H) ² H° ( ³ H) ² H°
$3d^{4}({}^{3}G)4p \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad$	82 22 36 70 54 39 75 18	² F° ² H°	11 16 20 20 18 39 14	( ³ G) ⁴ H° ( ³ F2) ⁴ D° ( ³ G) ⁴ H° ( ³ H) ⁴ H° ( ³ H) ² H° ( ³ H) ² H°
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22 36 70 54 39 75 18	² F° ² H°	16 20 20 18 39 14	( ³ F2) ⁴ D° ( ³ G) ⁴ H° ( ³ H) ⁴ H° ( ³ H) ² H° ( ³ H) ² H°
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	36 70 54 39 75 18	² H°	20 20 18 39 14	( ³ G) ⁴ H [•] ( ³ H) ⁴ H [•] ( ³ H) ² H [•] ( ³ H) ² H [•]
$3d^{4}({}^{3}G)4p \qquad \begin{array}{c} {}^{4}H^{\circ} & {}^{7}\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!$	70 54 39 75 18	470.	20 18 39 14	( ³ H) ⁴ H° ( ³ H) ² H° ( ³ H) ² H°
$3d^{4}({}^{3}G)4p \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad$	54 39 75 18	410	18 39 14	$({}^{3}H) {}^{2}H^{\circ}$ $({}^{3}H) {}^{2}H^{\circ}$
$3d^{4}({}^{3}G)4p \qquad 7_{2} \qquad 425 567.6 \\ 13_{2} \qquad 426 451.9 \\ 7_{2} \qquad 423 645.8 $	39 75 18	410.0	39 14	(°H) ² H°
$3d^4({}^3G)4p$ $\frac{7}{2}$ 423 645.8	18	41210		$(^{3}H)$ ⁴ H°
			15	( ³ D) ² F°
$3d^4({}^{3}P2)4n$ $\frac{1}{2}$ 423.646.8	99	2 <b>P</b> •	18	( ³ F2) ⁴ D°
3d ⁴ ( ³ G)4n 3/ 499 710 5	25	- 4F°	10	$(^{3}F2)^{4}F^{\circ}$
	20	r	12	(12) 1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	52 39		15 16	( ³ F2) ⁴ F° ( ³ F2) ⁴ D°
$3d^4({}^3\mathrm{G})4p$ ${}^{3}\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!$	21	4F°	20	( ³ P2) ² P°
$3d^4({}^3F2)4p$ $7/_2$ 424 346.1	25	⁴D°	20	( ³ G) ⁴ F°
$3d^4({}^3G)4p$ ${}^{11}/_2$ 424 363.7	36	4H•	30	( ³ H) ² H°
$3d^4({}^{3}\text{P2})4p$ ${}^{2}\text{D}^{\circ}$ ${}^{3}\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!\!$	39		27	( ³ P1) ² D°
$3d^4({}^3\mathrm{F2})4p$ $5_{2}$ 427 096.5	26	² F°	20	( ³ P2) ² D [•]
$3d^4({}^{3}\text{P2})4p$ $5_{2}$ $427\ 342.2$	27	² D°	26	( ³ F2) ² F°
$3d^4({}^3\mathrm{F2})4p$ ${}^{7}\!\!/_2$ 427 575.0	24	² G°	13	( ³ F1) ² G
$3d^4({}^3G)4p$ $11/_2$ $427702.7$	38	² H°	21	( ³ G) ⁴ G°
$3d^{4}({}^{3}G)4p$ ${}^{9}_{2}$ 427 995.6	22	⁴G°	15	( ³ H) ⁴ G°
$3d^{4}({}^{3}G)4p$ $\frac{9}{2}$ 428 051.5	37	² H°	15	( ³ H) ² G°
$3d^{4}({}^{3}F2)4p$ ${}^{2}F^{\bullet}$ ${}^{7}\!\!\!/_{2}$ 428 221.4	46		32	( ³ G) ² F [•]
$3d^{4}({}^{3}G)4p$ ${}^{4}G^{\bullet}$ ${}^{5}_{/2}$ $428496.5$	50		29	$({}^{8}H) {}^{4}G^{\bullet}$
	45		20	( ³ H) ⁴ G [•] ( ³ C) ² H [•]
	43	400	25	(°G) °H°
$3a^{-}(^{+}G)^{4}p$ $\gamma_{2}$ 429 486.3	36	'G'	15	("G) "H"
$3d^{*}({}^{\circ}D)4p$ $4D^{\circ}$ $430898.8$ $3000710$	78		9 19	( ³ D) ² P° ( ³ D) ⁴ P°
$\frac{1}{7}$ $\frac{1}{2}$ $\frac{430}{430}$ $\frac{371.5}{912.6}$	09 77		6	( ⁸ D) ⁴ F°
5 ¹ / ₂ 432 295.7	46		33	( ³ D) ⁴ P [•]
$3d^4({}^{8}D)4p$ ${}^{4}P^{\bullet}$ ${}^{5/2}_{2}$ $431019.9$	56		32	( ⁸ D) ⁴ D•
	74		9	("D) "D"

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² I° ² F° ² G° ² P° ² H°	$ \begin{array}{c}     13_{1/2} \\     11_{1/2} \\     \overline{7}_{1/2} \\     \overline{5}_{1/2} \\     9_{1/2} \\     \overline{7}_{1/2} \\     1_{1/2} \\     3_{1/2} \\   \end{array} $	432 616.6 432 932.0 432 800.1 434 997.0 433 371.2 433 517.3 433 936 9	66 88 46 42 53 49	27 5 21 20 20	( ¹ I) ² K° ( ³ H) ² I° ( ¹ G1) ² F°
² F° ² G° ² P° ² H°	7/2 5/2 7/2 7/2 1/2 3/2	432 800.1 433 997.0 433 371.2 433 517.3 433 936 9	46 42 53 49	21 20 20	( ¹ G1) ² F°
r ² G° ² P° ² H°	¹ / ₂ ⁵ / ₂ ⁹ / ₂ ¹ / ₂ ¹ / ₂ ¹ / ₂ ³ / ₂	432 000.1 433 997.0 433 371.2 433 517.3	40 42 53 49	21 20 20	(01) F
² G [•] ² P [•] ² H [•]	9/2 7/2 1/2 3/2	433 371.2 433 517.3 433 936 9	53 49	20	
² P° ² H°	7/2 1/2 3/2	433 517.3 433 936 9	49		( ³ H) ² G°
² P° ² H°	¹ / ₂ 3/ ₂	133 936 9		17	
² H°	9/ ₂	400 000.0	. 37	33	( ³ D) ² P [•]
²H° ¦		440 168.6	30	16	
	⁹ / ₂ 11/ ₂	434 167.3 435 011 5	47 53	22 20	( ¹ G1) ² H°
4770	3	400 011.0		20	30 AT
*F*	9/2 5/	434 200.9	63	21	$(^{\circ}G)$ $\mathbf{F}^{\circ}$
	72	434 025.7	54	15	
	⁷ 2	435 116.2	65	1 <b>9</b>	
	⁹ / ₂	<i>435 459.4</i>	77	19	
² P°	3/2	434 995.8	54	26	$(^{1}S2)^{2}P^{\circ}$
	1/2	440 689.3	47	27	
² K°	¹³ / ₂	435 165.4	71	28	$({}^{1}\mathbf{I}) {}^{2}\mathbf{I}^{\circ}$
	15/2	436 550.3	99	1	( ³ H) ⁴ I°
² G°	7/2	437 919.7	45	29	( ¹ G1) ² G*
	⁹ / ₂	438 639.4	41	30	
² H°	¹¹ / ₂	440 038.7	70	10	$(^{3}G)$ $^{2}H^{\circ}$
	9/2	440 917.9	82	11	
² F°	7/2	441 216.1	65	11	$({}^{3}G) {}^{2}F^{\circ}$
	5/2	441 785.7	42	14	( ³ D) ² D°
	^ق /2	441 401.2	30	² D° 21	$(^{3}D)$ $^{2}F^{\circ}$
² D°	³ / ₂	442 620.7	53	13	( ¹ D2) ² D°
² D°	³ / ₂	444 252.2	40	22	( ³ D) ² D°
	5/2	444 784.2	24	26	
² F°	⁵ / ₂	446 061.2	44	11	$(^{1}D2)^{2}D^{\circ}$
	"/ ₂	446 863.8	47	31	('F) 'F"
² F°	⁵ / ₂	451 041.3	64	14	( ¹ D2) ² F°
	"/ ₂	451 859.4	47	27	
² <b>P</b> °	³ / ₂	451 622.9	65	13	$(^{1}D1) ^{2}P^{\circ}$
	¹ / ₂	451 642.0	72	14	
² G°	⁷ / ₂	453 983.0	86	5	$({}^{1}\mathbf{F}) {}^{2}\mathbf{F}^{\circ}$
	⁹ / ₂	455 890.5	92	4	$({}^{1}G2) {}^{2}G^{\circ}$
² D°	⁵ / ₂	456 815.6	53	17	$({}^{3}P1) {}^{2}D^{\circ}$
	3/2	458 772.2	49	14	( ³ F1) ⁴ F°
	<ul> <li>F</li> <li>²P*</li> <li>²K*</li> <li>²G*</li> <li>²F*</li> <li>²F*</li> <li>²F*</li> <li>²F*</li> <li>²P*</li> <li>²G*</li> <li>²D*</li> <li>²D*</li> </ul>	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\mathbf{F}^{\mathbf{r}}$ $7_{2}^{2}$ $434 \ 200.9$ $\frac{5}{2}_{2}$ $435 \ 455.7$ $\frac{7}{2}$ $435 \ 116.2$ $\frac{9}{2}$ $435 \ 459.4$ $^{2}\mathbf{P}^{\mathbf{r}}$ $\frac{3}{2}$ $434 \ 995.8$ $\frac{1}{2}$ $435 \ 165.4$ $\frac{1}{2}$ $437 \ 919.7$ $\frac{9}{2}$ $438 \ 639.4$ $^{2}\mathbf{G}^{\mathbf{r}}$ $\frac{7}{2}$ $437 \ 919.7$ $\frac{9}{2}$ $438 \ 639.4$ $^{2}\mathbf{H}^{\mathbf{r}}$ $\frac{9}{2}$ $440 \ 038.7$ $\frac{9}{2}$ $440 \ 038.7$ $\frac{9}{2}$ $440 \ 038.7$ $\frac{9}{2}$ $440 \ 037.9$ $^{2}\mathbf{F}^{\mathbf{r}}$ $\frac{7}{2}$ $441 \ 216.1$ $\frac{5}{2}$ $441 \ 252.2$ $441 \ 785.7$ $\frac{5}{2}$ $444 \ 620.7$ $2$ $^{2}\mathbf{D}^{\mathbf{r}}$ $\frac{3}{2}$ $444 \ 252.2$ $\frac{5}{2}$ $444 \ 620.7$ $2$ $^{2}\mathbf{D}^{\mathbf{r}}$ $\frac{3}{2}$ $444 \ 620.7$ $^{2}\mathbf{D}^{\mathbf{r}}$ $\frac{3}{2}$ $444 \ 620.7$ $^{2}\mathbf{D}^{\mathbf{r}}$ $\frac{3}{2}$ $444 \ 620.7$ $^{2}\mathbf{D}^{\mathbf{r}}$ $\frac{3}{2}$	$\mathbf{F}^{-}$ $\frac{7}{2}$ $\frac{434}{434}$ 200.9       63 $\frac{5}{2}$ $\frac{434}{434}$ 625.7       54 $\frac{7}{2}$ $\frac{435}{435}$ 459.4       77 $^{2}\mathbf{P}^{-}$ $\frac{9}{2}$ $\frac{434}{435}$ 459.4       77 $^{2}\mathbf{P}^{-}$ $\frac{9}{2}$ $\frac{434}{435}$ 459.4       77 $^{2}\mathbf{R}^{-}$ $\frac{19}{2}$ $\frac{435}{436}$ 550.3       99 $^{2}\mathbf{G}^{-}$ $\frac{7}{2}$ $\frac{437}{437}$ 919.7       45 $\frac{438}{92}$ $\frac{438}{440}$ 638.7       70 $\frac{9}{2}$ $\frac{440}{438}$ 639.4       41 $^{2}\mathbf{H}^{-}$ $\frac{9}{2}$ $\frac{440}{440}$ 038.7       70 $\frac{9}{2}$ $\frac{4410}{440}$ 917.9       82       22 $\frac{7}{2}$ $\frac{441}{441}$ 785.7       42       30 $^{2}\mathbf{D}^{-}$ $\frac{7}{2}$ $\frac{444}{441}$ 785.7       42 $\frac{9}{2}$ $\frac{444}{24}$ 620.7       53       30 $^{2}\mathbf{D}^{-}$ $\frac{7}{2}$ $\frac{444}{252.2}$ 40 $\frac{9}{2}$ $\frac{444}{252.2}$ 40       41 $^{2}\mathbf{P}^{-}$ $\frac{7}{2}$ $\frac{445}{456}$ 863.8       47 $^{2}\mathbf{P}^{-}$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$

NT:		<b>^</b>	A
<b>N1</b>	VI-	-L .O.T	nnuea

Configuration	Term	J	Level (cm ⁻¹ )	Lead	ling perce	entages	1
	⁴ F°	5/2	460 364.6	61		9	( ³ P1) ⁴ D°
		7/2	460 535.9	66		8	$({}^{3}F2) {}^{4}F^{\circ}$
		3/2	460 604.0	57		9	$({}^{3}F2) {}^{4}F^{\circ}$
		⁹ / ₂	461 118.3	83		10	$({}^{3}F2) {}^{4}F^{\circ}$
$3d^{4}(^{3}\text{P1})4p$	⁴ P°	3/2	461 437.8	30		14	( ³ P2) ⁴ P°
		^୬ ⁄ ₂	463 301.5	45		22	
$3d^4(^3\text{P1})4p$		⁵ /2	461 622.6	21	⁴D°	20	( ³ F1) ⁴ F°
$3d^4(^{3}\text{P1})4p$		7/2	462 443.1	32	⁴ D°	20	( ³ F1) ⁴ D°
$3d^4(^3\text{P1})4p$		³ / ₂	462 884.1	24	⁴P°	21	( ³ P1) ⁴ D°
$3d^{4}(^{3}\text{P1})4p$		1/2	462 903.6	31	⁴ P°	21	$({}^{3}P1) \; {}^{4}D^{\circ}$
$3d^{4}(^{3}\text{F1})4p$	⁴G°	5/2	464 027.8	44		23	$({}^{3}F1) {}^{2}F^{\circ}$
		⁹ / ₂	466 065.2	70		21	$({}^{3}F2) {}^{4}G^{\circ}$
		11/2	466 754.3	76		22	( ³ F2) ⁴ G°
$3d^4({}^3\mathrm{F1})4p$		7/2	464 807.8	35	⁴G°	32	( ³ F1) ² F°
$3d^4({}^1\mathrm{F})4p$		⁵ /2	465 552.7	25	² D°	19	( ³ P1) ² D°
$3d^4({}^1\mathbf{F})4p$		3/2	466 034.2	29	² <b>D</b> °	21	( ³ P1) ² D°
$3d^{4}({}^{3}\mathrm{F1})4p$		7/2	466 133.7	36	² F°	35	( ³ F1) ⁴ G°
$3d^4({}^3\mathrm{F1})4p$	² F°	⁵ / ₂	466 649.1	47		20	( ³ F1) ⁴ G°
$3d^4(^{3}\text{P1})4p$	4S°	³ / ₂	471 106.8	48		44	( ³ P2) ⁴ S°
$3d^4({}^3\mathrm{F1})4p$	⁴D°	7/2	472 497.3	47		17	$({}^{3}P1) {}^{4}D^{\circ}$
		3/2	473 292.4	48		18	$({}^{3}F2) {}^{4}D^{\circ}$
		3/2	473 656.4	48		19	$({}^{3}F2) {}^{4}D^{\circ}$
		1/2	473 727.6	51		20	$({}^{3}F2) {}^{4}D^{\circ}$
$3d^{4}(^{3}F1)4p$	² G°	9/2	472 579.5	72		20	( ³ F2) ² G°
•		$\gamma_2$	473 531.9	73		22	
$3d^4({}^3\mathrm{P1})4p$	² <b>P</b> °	3/2	472 833.0	61		27	( ³ P2) ² P°
-		$1\sqrt{2}$	473 869.5	59		26	
$3d^4({}^1\mathrm{G1})4p$		9/2	476 332.1	38	² H°	24	$(^{1}G1)$ $^{2}G^{\circ}$
$3d^4({}^1\mathrm{G1})4p$	² G°	7/2	476 935.6	52		32	$(^{1}G2)$ $^{2}G^{\circ}$
$3d^4({}^3\mathrm{P2})4p$	² S°	Ψ2	477 177.1	55		41	$(^{3}P1)$ $^{2}S^{\circ}$
$3d^4({}^1\mathrm{G1})4p$		⁹ / ₂	479 046.3	35	²G°	26	( ¹ G1) ² H°
$3d^4({}^1G1)4p$	² H°	11/2	479 481.8	65		31	$(^{1}G2)$ $^{2}H^{\circ}$
$3d^{4}({}^{1}\mathrm{G1})4p$	² F°	7/2	480 189.3	54		18	( ¹ G2) ² F°
-		5/2	480 724.2	57		19	
$3d^4({}^3\mathrm{F1})4p$	² <b>D</b> °	5/2	483 043.4	47		18	( ³ F2) ² D [•]
		3/2	483 480.9	45		21	$(^{3}P1)^{2}D^{\circ}$

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Ni	vi-	Con	tin	ued
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Ni vI—Continued											
Configuration	Term	J	Level (cm ⁻¹ )	Leading	g percentages						
$3d^4(^1\mathrm{D1})4p$	²₽°	³ / ₂ ¹ / ₂	498 773.0 500 275.2	75 75	15 16	( ¹ D2) ² P°					
$3d^{4}({}^{1}\mathrm{D1})4p$	² F°	⁵ /2 7/2	505 150.5 507 300.4	69 73	18 19	( ¹ D2) ² F°					
$3d^{4}({}^{1}\mathrm{D1})4p$	²D°	³ /2 5/2	511 217.4 512 113.2	72 71	26 25	( ¹ D2) ² D°					
$3d^{4}({}^{1}\mathrm{S1})4p$	²₽°	¹ / ₂ 3/ ₂	540 394.1 543 115.6	74 74	20 20	( ¹ S2) ² P°					
Ni VII ( ⁵ D ₀ )	Limit		870 000								

1 Same

Ti t isoelectronic sequence

Ground state:  $1s^22s^22p^63s^23p^63d^{45}D_0$ 

Ionization energy =  $1\,070\,000\pm16\,000\,\text{cm}^{-1}\,(133\pm2\,\text{eV})$ 

The  $3d^4 - 3d^34p$  transition array of this spectrum between 205 and 231 Å was observed and analysed by Phillips and Kruger (1938). Henrichs (1975) has revised that work from new observations and isoelectronic comparisons. His results are given here. The uncertainty of the level values is about  $\pm 10$  cm⁻¹.

The ionization energy was obtained by extrapolation by Lotz (1967).

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Henrichs, H. F. (1975), Astron. Astrophys. 44, 41. Phillips, L. W., and Kruger, P. G. (1938), Phys. Rev. 54, 839. Lotz, W. (1967), J. Opt. Soc. Am. 57, 873.

Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
$3d^4$	⁵ D	0	0	$3d^{3}({}^{4}\mathrm{F})4p$	⁵ F°	2	470 056
	_	1	279			3	471 096
		2	804			1	471 250
		3	1 520			4	472 067
		4	2 392			5	472 907
3P2	³ P2	0	30.077	$3d^3({}^4\mathrm{F})4p$	³ G°	3	476 258
	1	1	31 836			4	477 261
		2	34 555			5	478 534
3d ⁴ ³ H	³ н	4	31.672	$3d^3({}^4\mathrm{F})4p$	³ F°	2	479 950
ou -		5	32 286	-		3	481 091
	6	32 877			4	482 229	
9.74	310	2	24 247	$3d^{3}(^{4}P)4p$	⁵ P°	1	486 151
ou -	r2	3	34 317			2	487 207
		4	34 576			3	488 <b>665</b>
3.74	³ G	3	38 160	$3d^3(^2G)4p$	³ G°	3	493 743
04	U	4	38 746			4	495 087
		5	39 247			5	4 <b>9</b> 6 340
$3d^{3}({}^{4}\mathrm{F})4p$	3D°	1	467 015	$3d^3(^2\mathrm{H})4p$	³ G•	5	511 464
ou (1/1)		2	471 976	-		4	511 698
		3	473 360			3	511 991
$3d^{3}({}^{4}\mathrm{F})4p$	5D°	2	467 705	Ni VIII $({}^{4}F_{3/2})$	Limit		1 070 000
ou (1) m		3	468 690				
		1	469 175				
		4	469 844				

Ni vii

NI VIII

Z = 28

Sc I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^{34} F_{3/2}$ 

Ionization energy =  $1 \ 310 \ 000 \pm 16 \ 000 \ cm^{-1} (162 \pm 2 \ eV)$ 

Anderson and Mack (1941) observed and classified 132 lines between 163 and 189 Å in the  $3d^3 - 3d^24p$  transition array. The uncertainty in the level values is  $\pm 10$  cm⁻¹, which corresponds to an error of about 0.003 Å in the wavelengths.

The separation of the ⁴F and ⁴P terms in  $3d^3$  is confirmed by the calculations of Racah (1954). The doublet system has been questioned by Bowen (1960), on the basis of isoelectronic extrapolations, but the objection does not seem to be well substantiated.

The configurations  $3d^3$ ,  $3d^24s$ , and  $3d^24p$  have been calculated by Kancerevicius, Ramonas, and Uspalis (1976), using Hartree-Fock radial integrals.

The ionization energy was obtained by extrapolation by Lotz (1967).

# References

Anderson, E. E., and Mack, J. E. (1941), Phys. Rev. 59, 717. Bowen, I. S. (1960), Astrophys. J. 132, 1.

Kancerevicius, A., Ramonas, A., and Uspalis, K. (1976), Lietuvos Fizikos Rinkinys 16, 49.

Lotz, W. (1967), J. Opt. Soc. Am. 57, 873.

Racah, G. (1954), Bull. Res. Council Israel 3, 290.

Ni	VIII	

Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
$3d^3$	⁴ F	3/2	0	$3d^2({}^3\mathbf{F})4p$	⁴ D°	3/2	569 839
		5/2	1 012			1/2	570 353
		1/2	2 184			5/2	571 517
		9/2	3 721			7/2	573 327
$3d^3$	4P	¹ /2	23 261	$3d^2({}^3\mathbf{F})4p$	² F*	⁵ ∕2	570 546
		3/2	23 710			7/2	571 804
		5/2	24 669			-	
		-		$3d^2(^3\mathbf{F})4p$	² G°	7/2	581 337
$d^3$	² G	7/2	26 977			9/2	583 241
	<u> </u>	9/2	28 068			2	
		12	20000	$3d^{2}(^{3}P)4p$	4S.	3/2	587 305
³ ² D2	5/_	34 689			- 2		
	⁷ 2 3/	07 100	$3d^{2}(^{3}P)4p$	4D.	1/2	590 764	
	$\gamma_2$	35 120		_	3/2	592 175	
•3	2	9,	00 854			5/2	594 068
Sd ^o	Ъ	$\frac{9}{2}$	36 754			7/2	596 908
		·· ⁷ 2	37 475			-2	
2.3-	400	5,	505 101	$3d^{2}(^{3}P)4p$	4p•	4	596 770
$d^{2}(^{\circ}\mathbf{F})4p$	'G'	⁹ / ₂	565 124		-	3/2	596 905
		·/2	566 964			5/2	598 570
		⁹ / ₂	569 564			12	
		1 ¹ / ₂	572 969	$3d^2({}^1G)4p$	² G*	7/2	598 638
	-	9.			Ŭ	9/2	599 079
$3d^2({}^{\circ}\mathbf{F})4p$	*F°	<u> %</u> 2	565 388			12	000 0.0
		$\frac{3}{2}$	566 831	$3d^{2}({}^{1}G)Ap$	2H.	9/	613 117
	1	$\gamma_2$	568 746	002 ( CI ) +p		11/	615 795
		<b>9</b> /2	570 960			<b>'</b> 2	010720
$3d^2({}^3F)4p$	² D°	3/,	569 667	Ni IX $({}^{3}\mathbf{F}_{2})$	Limit		1 310 000
		5/2	571 845				

Ni IX

Z = 28

Ca I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^2 {}^3F_2$ 

Ionization energy =  $1560000 \pm 16000 \text{ cm}^{-1} (193 \pm 2 \text{ eV})$ 

The analysis of the  $3d^2 - 3d4f$  array was given by Alexander, Feldman, Fraenkel, and Hoory (1966). The levels are obtained from the improved measurements and corrected classifications by Even-Zohar and Fraenkel (1968). The uncertainty of the level values is about  $\pm 50$ cm⁻¹. The singlet system, the  ${}^{3}P_{2}$  of  $3d^{2}$ , and the  ${}^{3}D_{3}$  of 3d4f are based on an estimated value for the  $3d^{2}$  ¹D term by Alexander et al. The value of the systematic shift is expected to be a few hundred cm⁻¹.

Fawcett, Ridgeley, and Ekberg (1980) classified the transition array  $3p^{6}3d^2 - 3p^{5}3d^3$ . Their wavelength accuracy is given as  $\pm 0.007$  Å, giving a level uncertainty of  $\pm 30$  cm⁻¹.

The  $3d^{21}$ G term is based on a tentative identification of a coronal line at 7144 Å by Pryce (1964).

The ionization energy was obtained by extrapolation by Lotz (1967).

#### References

Alexander, E., Feldman, U., Fraenkel, B. S., and Hoory, S. (1966), J. Opt. Soc. Am. 56, 651.

Even-Zohar, M., and Fraenkel, B. S. (1968), J. Opt. Soc. Am. 58, 1420.
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Pryce, M. H. L. (1964), Astrophys. J. 140, 1192.

Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
$3p^6({}^1\mathbf{S})3d^2$	³ F	2 3	0 1 880	$3p^{5}(^{2}\mathbf{P}^{\circ})3d^{3}(^{2}\mathbf{H})$	¹ G°	4	716 110+x
		4	4 070	$3p^6({}^1\mathrm{S})3d4f$	³ F°	2	977 130
$3p^{6}({}^{1}\mathbf{S})3d^{2}$	¹ <b>D</b>	2	$21\ 900 + x$			3 4	977 680 978 740
$3p^{6}({}^{1}\mathbf{S})3d^{2}$	³ P	2	27 160 + x	$3p^6({}^1\mathrm{S})3d4f$	³ G°	3	983 700
$3n^6({}^1S)3d^2$	¹ C	4	35 808 + ~2			4	985 140
<i>Sp</i> ( <i>S</i> ) <i>Su</i>	G	4	55 656 + X :			5	985 940
$3p^{5}({}^{2}\mathrm{P}^{\circ})3d^{3}({}^{2}\mathrm{H})$	³ G°	3	601 300 601 000	$3p^{6}({}^{1}\mathrm{S})3d4f$	¹ D°	2	984 630+x
		5	608 530	$3p^{6}({}^{1}\mathrm{S})3d4f$	¹ F°	3	986 960+x
$3p^{5}(^{2}\mathbf{P}^{\circ})3d^{3}(^{2}\mathbf{G})$	¹ H°	5	640 360+x	$3p^6(^1S)3d4f$	³ D°	3	988 760+x
$3p^{5}({}^{2}\mathrm{P^{o}})3d^{3}({}^{4}\mathrm{F})$	³ F°	2	661 050	<b>Ni</b> x $({}^{2}D_{3/2})$	Limit		1 560 000
		3	664 080				
		4	667 080			:	1
$3p^{5}(^{2}\mathbf{P}^{\circ})3d^{3}(^{4}\mathbf{F})$	³ D°	1	709 210				
		3	711 510				
		2	711 520				

Ni 1X

K 1 isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^2 D_{3/2}$ 

Ionization energy =  $1.812\ 000\pm 56\ 000\ cm^{-1}\ (224.6\pm 0.7\ eV)$ 

Observations were first reported by Alexander, Feldman, and Fraenkel (1965), who identified the 3d - 4fand 5f doublets. The series was extended to 7f by Even-Zohar and Fraenkel (1968), who noted that the 6f and 7f terms may be perturbed by the  $3p^{5}3d4d$  configuration. Their levels are given here with an uncertainty of  $\pm 100$  $cm^{-1}$ . We find that the *nf* terms do not follow a regular Rydberg series.

Gabriel, Fawcett, and Jordan (1966) identified the  $3p^{5}3d^{2}({}^{3}F)^{2}D$  and  $({}^{3}F)^{2}F$  terms. The  ${}^{2}P$  term was added by Goldsmith and Fraenkel (1970). With new observations with a reported accuracy of ±0.003 Å, Ramonas and Ryabtsev (1980) determined the  $({}^{1}G)^{2}F$  and  $({}^{1}D)^{2}F$  terms and improved the level values. Their results are given for the  $3p^{5}3d^{2}$  levels and for the  $3p^{6}3d^{2}D$  ground term interval. They also obtained the  $3p^{6}4p$  term. Their level value uncertainty is  $\pm 10 \text{ cm}^{-1}$ .

The analysis of the 3p⁵3d 4s configuration is by Hoory, Goldsmith, Fraenkel, and Feldman (1970). These levels have an uncertainty of about  $\pm 50$  cm⁻¹.

The ionization energy was obtained by extrapolation by Lotz (1967).

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Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
3p ⁶ 3d	² D	³ /2 ⁵ /2	0 3 178	$3p^5 3d(^3F^\circ)4s$	⁴ F°	7/2 5/2	1 154 390 1 156 550
$3p^{5}({}^{2}\mathbf{P}^{\circ})3d^{2}({}^{1}\mathbf{G})$	² F°	5/2 7/2	505 283 509 751	$3p^5 3d(^3F^\circ)4s$	² F°	7/2 5/2	1 161 930 1 169 300
$3p^{5}({}^{2}\mathbf{P}^{*})3d^{2}({}^{1}\mathbf{D})$	² F°	7/2 5/2	522 391 540 725	$3p^5 3d(^3D^*)4s$	4D.	7/2 5/2	1 184 390 1 187 750
$3p^{5}(^{2}P^{\circ})3d^{2}(^{3}F)$	² <b>F</b> °	⁵ /2 7/2	625 091 634 583	$3p^5 3d({}^1\mathbf{F}^\circ)4s$	² F°	7/ ₂	1 198 260
$3p^{5}(^{2}P^{\circ})3d^{2}(^{3}P)$	² P°	1/2 3/2	684 552 689 365	$3p^\circ 3d(°D^\circ)4s$	² D°	3/2 5/2	1 203 270 1 206 410
$3p^{5}({}^{2}P^{\circ})3d^{2}({}^{3}F)$	² D°	5/2 3/2	692 890 693 404	3p ⁶ 5f	² F°	5/2 7/2	1 349 580 1 349 690
3p ⁶ 4p	² P°	1/2 3/2	773 647 779 600	3p ⁶ 6f	² F°	7/2 5/2	1 502 720 1 502 810
3p ⁶ 4f	² F°	5/2 7/2	1 093 360	3p ⁶ 7f	² F°	⁵ /2 7/2	1 617 890 1 618 310
$3p^{5} 3d(^{3}P^{\circ})4s$	²P°	¹ /2 1/2 3/	1 140 510	Ni XI ( ¹ S ₀ )	Limit		1 812 000

Ni x

法纳法

Ar I isoelectronic sequence

Ground state:  $1s^22s^22p^63s^23p^{6-1}S_0$ 

## Ionization energy = $2589000 \pm 8000 \text{ cm}^{-1} (321.0 \pm 1.0 \text{ eV})$

Swartz et al. (1976) identified the transition array  $3p^{5}3d - 3p^{5}4f$  in the region of 81-94 Å. With their classifications and the forbidden transitions within the  $3p^{5}3d$  configuration, identified in the solar corona by Svensson et al. (1974) and by Sandlin and Tousey (1979), these configurations were determined. The ¹P° term is from the laboratory observations of Even-Zohar and Fraenkel (1968). The uncertainty in the  $3p^{5}3d$  level values varies from  $\pm 10$  cm⁻¹ to  $\pm 100$  cm⁻¹ while that of the  $3p^{5}4f$  levels is  $\pm 100$  cm⁻¹.

The  $3p^{5}4s$  and 4d configurations are taken from observations of resonance lines by Even-Zohar and Fraenkel

between 60 and 80 Å. The level values are uncertain by about  $\pm 300$  cm⁻¹.

The ionization energy was obtained by extrapolation by Lotz (1967).

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Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
$3s^2 3p^6$	¹ S	0	0	$3s^2 3p^5 4d$	³ P°	1	1 571 310
$3s^2 3p^5 3d$	³ P°	0	469 310 472 950	$3s^2 3p^5 4d$	¹ P°	1	1 594 130
		2	480 770	$3s^2 3p^5({}^2\mathrm{P}^{\bullet}_{3/2})4f$	²[¾2]	1 2	1 701 800 1 704 300
$3s^2 3p^3 3d$	³ F*	4 3	493 060 496 950	$3s^2 3p^5({}^2\mathrm{P}^{\circ}_{3/2})4f$	²[ ⁹ ⁄ ₂ ]	5	1 706 400
$3s^2 3p^5 3d$	³ D°	3 1 2	527 220 534 810 539 070	$3s^2 3p^5(^2\mathbf{P}^{\bullet}_{3/2})4f$	² [ ⁵ / ₂ ]	3	1 708 300
$3s^2$ $3p^3$ $3d$	¹ D°	2	530 050	$3s^2 3p^5(^2P^{\circ}_{3/2})4f$	² [ ⁷ / ₂ ]	4	1 716 400
$3s^2 3p^5 3d$	'F°	3	543 040	$3s^2 3p^3({}^2\mathbf{P}^{\bullet}_{1/2})4f$	² [ ⁵ / ₂ ]	3 2	1 732 900 1 739 400
$3s^2 3p^5 3d$	¹ P°	1	673 850	$3s^2 3p^5({}^2\mathrm{P}^{\bullet}_{1/2})4f$	²[ ⁷ / ₂ ]	3 4	1 736 000 1 736 400
$3s^2 3p^5 4s$	³ P'	1	1 269 940	Ni XII ( ² P _{3/2} )	Limit	-	2 589 000
$3s^2 3p^5 4s$	¹ P*	1	1 292 110				

Ni vi

CI 1 isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^5 {}^{2}P_{3/2}^{\circ}$ 

Ionization energy =  $2\,840\,000\pm 16000\,\mathrm{cm}^{-1}\,(352\pm 2\,\mathrm{eV})$ 

Fawcett and Hatter (1980) observed the  $3s^23p^5 {}^{2}P^{\circ} - 3s 3p^6 {}^{2}S$  transitions at 295.321 Å and 317.475 Å with an accuracy of  $\pm 0.008$  Å, or a level uncertainty of  $\pm 10$  cm⁻¹.

The portion of the  $3p^43d$  configuration below 600 000 cm⁻¹ is taken from the study of coronal spectra by Edlén and Smitt (1978). Their level values are adjusted here to the calculated energies of Nussbaumer (1976), from which we adopted the value 454 000 for the  $({}^{3}P)^{4}D_{7/2}$  level. The value of "x" is estimated to be  $\pm 1000$  cm⁻¹. The higher  $3p^43d$  terms are from Goldsmith and Fraenkel (1970); the uncertainty is  $\pm 50$  cm⁻¹. The designations of the parent terms of  $3p^43d$  are taken from the calculations of Bromage, Cowan, and Fawcett (1977) for the isoelectronic spectrum Fe x.

The  $3p^44s$ ,  $3p^44d$ , and  $3p^44f$  terms are from the observations of Fawcett, Cowan, and Hayes (1972) near 70 Å and are uncertain by  $\pm 500$  cm⁻¹.

The ionization energy was obtained by extrapolation by Lotz (1967).

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Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
$\overline{3p^5}$	² P°	³ / ₂ ¹ / ₂	0 23 629	$3p^4(^3P)3d$	² D	⁵ / ₂ ³ / ₂	657 230 676 420
$3s3p^{6}$	² S	¹ / ₂	338 615	$3p^4(^3P)4s$	² P	³ /2 1/2	1 374 200 1 385 600
$3p^4(^{3}\mathbf{P})3d$	⁴D	7/2	454 000+x	$3p^{4}(^{1}D)4s$	² D	5/2	1 401 000
$3p^4(^{3}\mathrm{P})3d$	⁴F	9/2 7/2	485 570+x 492 750+x			³ / ₂	1 401 600
$3p^4(^3\mathbf{P})3d$	² F	7/2	513 290+x	$3p^{4}(^{3}P)4d$	4E°	9/2	
$3p^4({}^1\mathbf{D})3d$	² G	7/2 9/2	526 960 + x 527 230 + x	$3p^{4}(^{3}P)4f$ $3p^{4}(^{3}P)4f$	r ⁴G°	¹¹ /2	1 808 000 + x
$3p^4({}^1\mathbf{D})3d$	² F	7/2	$567\ 200+x$		2	⁹ / ₂	1 811 400+x
$3p^4(^1\mathbf{D})3d$	² S	1/2	622 840	$3p^4(^{1}D)4f$	² H°	11/2	1848400+x
$3p^4({}^3\mathbf{P})3d$	² P	3/2 1/2	648 670 657 290		Limit		2 040 000
		12					

Ni XII

# Ni xiii

Z = 28

S I isoelectronic sequence

Ground state:  $1s^22s^22p^63s^23p^{4} {}^{3}P_2$ 

#### Ionization energy = $3\,100\,000\pm 16\,000\,\mathrm{cm}^{-1}(384\pm 2\,\mathrm{eV})$

Svensson (1971) calculated the levels of the ground configuration with a stated accuracy of  $\pm 10-50$  cm⁻¹. From these he made the following classifications of solar coronal lines within this configuration:  ${}^{3}P_{2} - {}^{1}D_{2}$  at 2126.7 Å (in vac.) and  ${}^{3}P_{2} - {}^{3}P_{1}$  at 5115.8 Å (in air). New measurements of the coronal spectrum observed from Skylab by Sandlin, Brueckner, and Tousey (1977) provide the more accurate wavelength of  $2126.17 \pm 0.02$  Å for  ${}^{3}P_{2} - {}^{1}D_{2}$ , and a new line at 1277.23±0.01 Å for  ${}^{3}P_{1} - {}^{1}S_{0}$ . The transition array  $3s^23p^4 - 3s^3p^5$  from 267-308 Å was measured by Fawcett and Hatter (1980) with an uncertainty of  $\pm 0.008$  Å. Their line classifications were used to derive the  $3s^23p^4$  ³P₀ level and the ³P° and ¹P° terms of  $3s 3p^{5}$ .

The  $3s^2 3p^3 3d$  levels are from laboratory observations of Fawcett and Hayes (1972) between 155 and 305 Å and are uncertain by about  $\pm 50$  cm⁻¹.

The  $3p^{3}4d$  levels are from the observations of Fawcett, Cowan, and Hayes (1972) at 56 Å. The uncertainty is about  $\pm 500$  cm⁻¹. They also observed levels in  $3p^{3}4f$ , which are not connected with this system.

The ionization energy was obtained by Lotz (1967) by extrapolation.

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			P				
Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
$3s^2 3p^4$	³ P	2	0.0	$3s^2  3p^3 (^2\mathrm{D}^{\circ})  3d$	¹ D°	2	666 000
		0	20 060	$3s^2 3p^3(^2\mathrm{D}^\circ) 3d$	${}^{1}\mathbf{F}^{\circ}$	3	681 750
$3s^2 3p^4$	¹ D	2	47 032.9	$3s^2 3p^3 (^2D^\circ) 3d$	¹ <b>P</b> °	1	715 960
$3s^2 3p^4$	¹ S	0	97 836.2	$3s^2 3p^3 ({}^4S^\circ) 4d$	³ D°	3	1 767 700
$3s3p^{5}$	³ P°	2	330 215 344 156	$3s^2 3p^3(^2\mathrm{D}^\circ)4d$	¹ <b>D</b> °	2	1 820 400
$3s3p^5$	¹ P°	1	395 545	$3s^2 3p^3(^2\mathrm{D}^{\circ})4d$	${}^{1}\mathbf{F}^{*}$	3	1 827 000
$3s^2 3p^3(^2D^\circ)3d$	³ P°	2	609 200	Ni XIV $({}^{4}S_{3/2}^{\circ})$	Limit		3 100 000
$3s^2 3p^3 ({}^4S^\circ) 3d$	³ D°	3	634 000				
		2	644 660 649 900				

P 1 isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^3 {}^4S^{\circ}_{3/2}$ 

Ionization energy =  $3470000 \pm 16000 \text{ cm}^{-1}(430 \pm 2 \text{ eV})$ 

The levels of the  $3s^23p^3$  configuration are determined from identifications of solar coronal lines by Svensson (1971) and Sandlin, Brueckner, and Tousey (1977). The values are from wavelengths given in the latter paper reporting spectra observed by Skylab measured with an uncertainty of  $\pm 0.01$  Å, giving a level uncertainty of  $\pm 0.5$  cm⁻¹. The calculated value for  ${}^2P_{3/2}^{\circ}$  is from Svensson, with an estimated uncertainty of  $\pm 50$  cm⁻¹.

The  $3s^23p^3 - 3s^3p^4$  array in the range of 245–292 Å was measured by Fawcett and Hatter (1980) with an accuracy of  $\pm 0.008$  Å. Their classifications are used to derive the levels of  $3s^3p^4$  with an uncertainty of  $\pm 10$  cm⁻¹. The  $3s^23p^23d$  levels are from the observations of Fawcett and Hayes (1972) between 160 and 320 Å and are uncertain by about  $\pm 60$  cm⁻¹. The  $3p^24d$  levels are from the observations of Fawcett, Cowan, and Hayes (1972). The uncertainty is about  $\pm 500$  cm⁻¹.

The ionization energy was obtained by extrapolation by Lotz (1967).

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Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
$3s^2 3p^3$	⁴ S°	³ / ₂	0.0	$3s^2 3p^2(^1\mathrm{D})3d$	² D	3/2 5/2	632 280 634 430
$3s^2 3p^3$	² D*	³ /2 ⁵ /2	45 767.8 53 569.0	$3s^2 3p^2(^1\mathrm{D})3d$	² P	1/2 3/2	648 320 660 710+x
$3s^2 3p^3$	² P°	¹ / ₂ ³ / ₂	85 126.7 96 630+x	$3s^2 3p^2(^1\mathrm{D})3d$	² F	7/2	662 780
3s3p ⁴	⁴ P	⁵ /2 ³ /2	316 343 330 837	$3s^2 3p^2(^3\mathbf{P})3d$	² D	5/2 3/2	690 560+x 691 930
3s3p ⁴	² <b>D</b>	3/2 5/	391 916 295 567	3s ² 3p ² 4d	²P	³ /2	1 628 400
		12	020 001	$3s^2 3p^2 4d$	² D	⁵ /2	1 653 100
3s3p ⁴	² P	³ / ₂ ⁵ / ₂	447 765 452 850 + x	Ni xv ( ³ P ₀ )	Limit		3 470 000
$3s^2 3p^2({}^3\mathbf{P})3d$	⁴P	5/2 3/2 1/2	583 530 589 310 594 810				

Ni xiv

Ni xv

# Z = 28

Si I isoelectronic sequence

Ground state: 1s²2s²2p⁶3s²3p² ³P₀

Ionization energy =  $3740000 \pm 16000 \text{ cm}^{-1}(464 \pm 2 \text{ eV})$ 

The levels of the  $3s^23p^2$  configuration are determined from measurements of solar coronal lines and are uncertain by about  $\pm 0.5$  cm⁻¹. The ³P values are from Svensson's (1971) compilation and the ¹D value is from the measurement by Sandlin, Brueckner, and Tousey (1977) of spectra observed from Skylab.

The transition array  $3s^23p^2 - 3s^2p^3$  was observed in the range of 209-319 Å by Fawcett and Hatter (1980) with an accuracy of  $\pm 0.008$  Å. Their assignments are used to derive the levels of  $3s^2p^3$  with an uncertinaty of  $\pm 10$  cm⁻¹. The  $3s^23p^3d$  levels are from the analysis by Fawcett and Hayes (1972) based on observations between 170 and 320 Å; they are uncertain by about  $\pm 60$  cm⁻¹.

The 3p4s, 3p4d, and 3p4f levels are from the observations of Fawcett, Cowan, and Hayes (1972) and of

Kastner, Swartz, Bhatia, and Lapides (1978). The uncertainty is about  $\pm 500$  cm⁻¹.

The ionization energy was obtained by extrapolation by Lotz (1967).

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Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
$3s^2 3p^2$	³ P	0	0.0	3s² 3p3d	¹ <b>F</b> °	3	638 460
		2	27 376.5	$3s^2 3p4s$	³ P°	2	1 730 700
$3s^2 3p^2$	¹ D	2	62 852.1	3s² 3p4s	¹ <b>D</b> *	2	1 741 300
3s3p ³	³ D°	1	335 400	$3s^2 3p4d$	³ D°	2	2 018 400
		2	335 682	-		3	2 020 500
		3	340 794				
				$3s^2 3p4d$	³ F°	3	2 042 500
Bs3p ³	³ S°	1	478 010	-			
				$3s^2 3p4d$	¹ F°	3	2 053 000
Bs3p ³	¹ P°	1	509 211				
				$3s^2 3p4f$	¹ G	4	2 185 600
3s² 3p3d	³ P*	2	555 830				
		1	565 930	Ni XVI $({}^{2}P_{1/2}^{\bullet})$	Limit		3 740 000
3s² 3p3d	¹ D°	2	574 330				
3s² 3p3d	³ D*	1	582 760				
-		3	585 170				
		2	586 410				

NT: .....

Al I isoelectronic sequence

Ground state:  $1s^22s^22p^63s^23p^2P_{1/2}^{\circ}$ 

Ionization energy =  $4\,020\,000\pm 16\,000\,\mathrm{cm}^{-1}\,(499\pm 2\,\mathrm{eV})$ 

The observations of the transition array  $3s^{2}3p - 3s^{2}3p^{2}$ in the range 218-309 Å by Fawcett and Hatter (1980) provided the ²P ground term interval and the levels of  $3s^{2}3p^{2}$  with an accuracy of  $\pm 20 \text{ cm}^{-1}$ . An isoelectronic plot of the transition energy  $3s^{2}3p^{2}P_{1/2}^{n} - 3s^{2}3p^{2}D_{3/2}^{2}$  indicates that there is a misprint for the wavelength 288.165 Å. It should be 289.165 Å. The  $3s^{2}3d$  levels are from the line classifications near 200 Å of Fawcett and Hayes (1972). They estimate the wavelength uncertainty to be  $\pm 0.03$  Å ( $\pm 75$  cm⁻¹). The  $3s^{2}4d$  and 4f levels are from wavelengths near 50 Å classified by Fawcett, Cowan, and Hayes (1972) and are uncertain by  $\pm 300$  cm⁻¹. The ionization energy was obtained by extrapolation by Lotz (1967).

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Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
3s ² 3p	² P°	¹ / ₂ ³ / ₂	0 27 770	3s ² 3d	²D	3/2 5/2	539 870 543 170
<b>3s3p</b> ²	² <b>D</b>	³ /2 ⁵ /2	345 820 351 210	3s² 4d	² D	³ /2 5/2	2 119 400 2 121 100
3s3p ²	² S	¹ / ₂	417 450	3s ² 4f	² F°	7/2 5/2	2 228 500 2 228 600
3s3p ²	² P	1/2 3/2	448 170 457 910	Ni хvп ( ¹ S ₀ )	Limit	-	4 020 000

# Ni xvii

Z = 28

Mg 1 isoelectronic sequence

Ground state:  $1s^22s^22p^63s^{2-1}S_0$ 

Ionization energy =  $4\,606\,000\pm1000\,\mathrm{cm^{-1}}\,(571.08\pm0.12\,\mathrm{eV})$ 

Fawcett et al. (1966) classified lines in the range of 30-55 Å that are transitions among configurations 3s 3l - 3snl' for n > 3. These were remeasured with improved accuracy of  $\pm 0.01$  Å with some additional classifications by Feldman et al. (1971). The uncertainty of level values is  $\pm 1000$  cm⁻¹. The transition arrays  $3s 3p - 3p^2$  and 3s 3p - 3s 3d in the range of 210-302 Å were classified by Fawcett, Cowan, and Hayes (1972). Their measurement uncertainty is reported as  $\pm 0.02$  Å, giving a level uncertainty of  $\pm 30$  cm⁻¹. They also revised the classification of  $3s 3d^{-1}D_2 - 3s 4f^{-1}F_3^{\circ}$  and gave new measurements for the lines given in Fawcett et al. (1966) with an acccuracy of  $\pm 0.01$  Å. No intersystem lines were identified in these observations. We use the new measurements of Fawcett and Hatter (1980) for the array  $3s 3p {}^{3}P^{\circ} - 3p^{2} {}^{3}P$ . They estimate about the same level uncertainty as Fawcett et al. (1972) but give new values.

Finkenthal et al. (1982) identified the line  $3s^{2} {}^{1}S_{0} - 3s 3p {}^{3}P_{1}^{\circ}$  in a tokamak plasma at  $366.7 \pm 0.3$  Å, providing the connection between the triplet terms and the ground state. We use the solar flare measurement by Dere (1978) of  $366.80 \pm 0.03$  Å. The  $3s^{2} {}^{1}S_{0} - 3s 3p {}^{1}P_{1}^{\circ}$  transition was identified by Fawcett and Hayes (1972) at 249.180 $\pm 0.004$  Å; the wavelength was obtained from the

solar observations of Behring, Cohen, and Feldman (1972).

The 3p 3d - 3p 4f transition array has been observed at 55 Å by Kastner, Swartz, Bhatia, and Lapides (1978) but it is unconnected with the present configurations.

We derived the ionization energy from the three member 3snd ³D series. The 6*f* term does not follow the *nf* series quantum defect trend.

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Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
3s ²	¹ <b>S</b>	0	0	3s4d	³ D	1	2 494 100
						2	2 495 200
3s3p	³ P°	0	264 400			3	2 497 300
		1	272 630				
		2	293 650	3s4d	¹ D	2	2 499 400
3s3p	¹ P°	1	401 320	3 <b>p4s</b>	³ P°	2	2 542 800
3p ²	³ P	0	627 870	3s4f	³ F°	2	2 585 000
-		1	643 820		-	3	2 585 400
		2	669 500			4	2 585 700
3s3d	³ D	1	771 290	3s4f	¹ F°	3	2 601 600
		2	772 970				
		3	775 670	3s5p	¹ P°	1	3 234 300
3s3d	¹ <b>D</b>	2	864 600	3s5d	³ D	1.2	3 272 200
						3	3 272 900
3s4s	$^{3}S$	1	2 187 600			-	
				3s5f	³ F°	2,3,4	3 312 800
3s4p	¹ <b>P</b> *	1	2 333 400	3s6f	³ F°	4	3 721 600
				Ni XVIII ( ² S _{1/2} )	Limit		4 606 000

Ni XVII

Ni xviii

Z = 28

Na 1 isoelectronic sequence

Ground state:  $1s^22s^22p^63s^2S_{1/2}$ 

Ionization energy =  $4\,896\,200\pm500\,\,\mathrm{cm^{-1}}$  (607.06±0.06 eV)

The 3s - 3p doublet was reported by Fawcett and Hatter (1980); they measured the  ${}^{2}S_{1/2} - {}^{2}P_{3/2}^{\circ}$  at  $291.983 \pm 0.008$  Å and the  ${}^{2}S_{1/2} - {}^{2}P_{1/2}^{\circ}$  at  $320.56 \pm 0.03$  Å. The latter has been observed by Peacock, Stamp, and Silver (1984) in a tokamak plasma at 320.565±0.006 Å. Fawcett, Cowan, and Hayes (1972) measured the 3p - 3ddoublet with an uncertainty of  $\pm 0.02$  Å. Improved values are given by Edlén (1978). The uncertainty of these level values is  $\pm 10$  cm⁻¹.

Except for the 3d - 4f doublet measured by Edlén (1936), we obtained the *nf* terms from the 3d - nf measurements reported by Feldman et al. (1971). They also found the 4s, np(n = 4-6), and nd(n = 4-8) terms. Their measurement uncertainty of  $\pm 0.01$  Å gives an energy level uncertainty of  $\pm 1000$  cm⁻¹.

The 4f-5g doublet was found by Kononov et al. (1977) and confirmed by Edlén (1978) by using a polarization formula.

Feldman and Cohen (1967) identified the  $2p^63s - 2p^53s^2$ transitions at 14.37 Å and 14.10 Å with an uncertainty of ±0.01 Å.

The value for the ionization energy was derived by Edlén (1978) from core polarization theory applied to the nf series.

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			Ni	XVIII			
Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
$2p^6({}^1\mathbf{S})3s$	² S	1/2	0	$2p^6({}^1\mathbf{S})5g$	²G	7/2 9/2	3 473 000 3 473 300
$2p^{6}({}^{1}S)3p$	²P°	¹ / ₂ ³ / ₂	311 949 342 485	$2p^{6}({}^{1}\mathrm{S})6p$	² P*	1/2 3/2	3 839 400 3 843 200
$2p^{6}({}^{1}\mathbf{S})3d$	² D	³ / ₂ ⁵ / ₂	765 610 770 280	$2p^{6}(^{1}\mathbf{S})6d$	² D	³ / ₂ ⁵ / ₂	3 885 700 3 886 100
$2p^{6}({}^{1}S)4s$	² S	1/2	2 301 800	$2p^6({}^1\mathrm{S})6f$	² F°	5/2	3 905 800
$2p^{6}({}^{1}S)4p$	² P°		2 426 100 2 438 100	$2n^{6}({}^{1}S)7d$	2D	1/2 5/2	<i>3 906 100</i> 4 156 700
$2p^{6}(^{1}S)4d$	² D	³ / ₂ ⁵ / ₂	2 594 400 2 596 500	$2p^{6}(^{1}S)7f$	² F°	5/2 T	4 169 000
$2p^{6}({}^{1}S)4f$	² F°	⁵ / ₂ 7/ ₂	2 666 230 2 667 100	$2p^6({}^1\mathbf{S})8d$	2 D	³ /2	4 189 100 4 331 100
$2p^{6}({}^{1}S)5p$	² P°	¹ / ₂ ³ / ₂	3 352 400 3 358 100	$2p^{6}({}^{1}\mathbf{S})8f$	² F*	⁹ ∕₂ ⁷ ∕₂	4 331 300 4 <i>339 400</i>
$2p^6({}^1\mathrm{S})5d$	² D	³ / ₂ ⁵ / ₂	3 433 700 3 434 600	Ni xix ( ¹ S ₀ )	Limit		4 896 200
2 <b>p⁶(</b> ¹ <b>S</b> )5 <b>f</b>	² F°	5/2 7/2	3 469 100 3 469 400	2p ⁵ 3s ²	²₽°	³ /2 ¹ /2	6 959 000 7 092 000
					1		

Ne 1 isoelectronic sequence

Ground state:  $1s^22s^22p^{6}$  S₀

## Ionization energy = $12\,430\,000\pm10\,000\,\mathrm{cm}^{-1}\,(1541\pm1\,\mathrm{eV})$

Only resonance lines are classified by this system of energy levels. The first line identifications were made by Feldman, Cohen, and Swartz (1967), who reported transitions from the  $2p^{5}3s$ ,  $2p^{5}3d$  and  $2s2p^{6}3p$  configurations. To these were added terms of  $2p^{5}4d$  by Feldman and Cohen (1967). These were augmented by the work of Swartz, Kastner, Rothe, and Neupert (1971), who observed lines originating from  $2p^{5}4s$ ,  $2p^{5}5d$ , and  $2p^{5}6d$ .

The spectrum was reobserved by Gordon, Hobby, and Peacock (1980) in the range of 8-14 Å with a wavelength uncertainty of  $\pm 0.005$  Å. Their results, with a level value uncertainty of  $\pm 5000$  cm⁻¹, are quoted here. They include all the lines previously identified plus transitions from the ³P₁ state of  $2s^22p^54d$ , 5d, 6d, and the levels of  $2s2p^64p$ .

By means of a very low pressure laboratory light source (a tokamak), Klapisch, Bar Shalom, Schwob, Fraenkel, Breton, de Michelis, Finkenthal, and Mattioli (1978) observed the magnetic quadrupole transition from  $2p^{5}3s^{3}P_{2}^{\circ}$  to the ground state as well as the transitions from the J = 1 states of  $2p^{5}3s$  and  $2p^{5}3d$ . No uncertainty estimate is given, but it is presumably  $\pm 0.005$  Å, which would give a level uncertainty of  $\pm 3000$  cm⁻¹. We have assigned designations and given percentages to the  $2p^{5}3s$  and  $2p^{5}3d$  configurations based on our own calculations. Both *jj*- and *LS*-leading percentages are listed for the  $2p^{5}3s$  levels.

Kastner, Behring, and Cohen (1975) identified transitions between  $2p^{3}3p$  and  $2p^{5}4d$ , but there is no connection with the levels given here.

We derived the ionization energy from the  $2s^2 2p^5 nd^3 D_1$  series for n = 3-6.

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			<u> </u>			
Configuration	Term	J	Level (cm ⁻¹ )	Leadi	ng percentages	
$2s^2 2p^6$	¹ S	0	0			
$2s^2 2p^5({}^2\mathbf{P}^{\bullet}_{3/2})3s$	( ³ / ₂ , ¹ / ₂ )°	2 1	7 104 000 7 121 000	100 98	or 100 ³ P° or 53 ¹ P°	
$2s^2 2p^5({}^2\mathbf{P}^{\bullet}_{1/2})3s$	( ¹ / ₂ , ¹ / ₂ )°	1	7 257 400	98	or 53 ³ P°	
2s² 2p ⁵ 3d	³ P°	1	7 805 200	91	9 ³ D°	
$2s^2 2p^5 3d$	³ D*	1	7 901 400	67	28 ¹ P°	
$2s^2 2p^5 3d$	¹ <b>P</b> *	1	8 041 800	72	24 ³ D°	
2s2p ⁶ 3p	³ P*	1	8 621 400			
2s2p ⁶ 3p	¹ P°	1	8 666 300			
$2s^2 2p^5(^2\mathbf{P}^{\bullet}_{3/2})4s$	( ³ / ₂ , ¹ / ₂ )°	1	9 585 000			
$2s^2 2p^5(^2\mathbf{P}_{1/2}^*)4s$	$(\frac{1}{2},\frac{1}{2})^{\circ}$	1	9 725 000			
$2s^2 2p^5 4d$	³ P*	1	9 845 000			
$2s^2 2p^5 4d$	³ D•	1	9 891 000			

E-	•7	5

NI XIX—Continue	
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Configuration	Term	J	Level (cm ⁻¹ )	Leading percentages
$\frac{1}{2s^2 2p^5 4d}$	¹ <b>P°</b>	1	10 023 000	
$2s^2 2p^5 5d$	³ P°	1	10 797 000	
$2s^2 2p^5 5d$	³ D°	1	10 806 000	
$2s2p^6 4p$	³ P°	1	10 925 000	
$2s2p^6$ 4p	¹ P°	1	10 941 000	
$2s^2 2p^5 5d$	¹ P°	1	10 942 000	
$2s^2 2p^5 6d$	³ D°	1	11 301 000	
$2s^2 2p^5 6d$	¹ P°	1	11 436 000	
Ni xx ( ² P _{3/2} )	Limit		12 430 000	

NI xx

Z = 28

F 1 isoelectronic sequence

Ground state: 1s²2s²2p⁵ ²P^o_{3/2}

Ionization energy =  $13\,290\,000\pm 27\,000\,\mathrm{cm}^{-1}\,(1648\pm 3\,\mathrm{eV})$ 

The ground term splitting is from a magnetic dipole transition at 694.64 $\pm$ 0.03 Å observed in a tokamak discharge by Peacock, Stamp, and Silver (1984). This line was first reported by Hinnov et al. (1982). The  $2s2p^6$  configuration was determined from the resonance doublet  ${}^{2}P^{\circ}-{}^{2}S$  measured by Doschek et al. (1974) with an accuracy of  $\pm$ 0.02 Å, giving a level uncertainty for  $2s2p^{6}{}^{2}S$  of  $\pm$ 300 cm⁻¹.

The  $2p^5 - 2p^4 3s$  and  $2p^5 - 2p^4 3d$  arrays were analyzed by Boiko et al. (1978). The region was remeasured from 9-13 Å by Gordon, Hobby, and Peacock (1980) with an accuracy of  $\pm 0.005$  Å, giving a level value uncertainty of  $\pm 5000$  cm⁻¹. They identified additional lines of these arrays as well as the higher configurations  $2s 2p^{5} 3p$ ,  $2p^{4} 4d$ , and  $2p^{4} 4s$ . There results are given here. The ionization energy is an extrapolated value by Lotz (1967).

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NI XX							
Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
$2s^2 2p^5$	² P°	³ / ₂ ¹ / ₂	0 143 959	$2s^2 2p^4(^1\mathrm{D})3d$	² P	³ / ₂ ¹ / ₂	8 445 000 8 495 000
$2s2p^{6}$	² S	1/2	1 202 300	$2s^2 2p^4({}^1\mathbf{S}) 3d$	² D	³ /2	8 634 000
$2s^2 2p^4(^{3}P)3s$	² P	³ / ₂ ¹ / ₂	7 544 000 7 673 000	$2s2p^5(^3P^*)3p$	⁴D	³ / ₂	8 908 000
$2s^2 2p^4({}^3\mathbf{P})3s$	4P	5/2 1/2	7 514 000	$2s2p^5(^{3}\mathbf{P}^{\bullet})3p$	² D	⁵ / ₂ ³ / ₂	8 908 000 9 052 000
		3/2 3/2	7 648 000	$2s2p^5(^3\mathbf{P}^{\bullet})3p$	² P	³ / ₂ ¹ / ₂	8 962 000 8 978 000
$2s^2 2p^4({}^1\mathbf{D})3s$	² D	³ / ₂ ³ / ₂	7 736 000 7 742 000	$2s2p^5(^{3}P^{\circ})3p$	⁴ P	3/2	9 008 000
$2s^2 2p^4({}^1S)3s$	² S	¹ / ₂	7 949 000	$2s2p^5(^3\mathbf{P}^{\bullet})3p$	² S	¹ / ₂	9 092 000
$2s^2 2p^4(^3\mathbf{P})3d$	⁴P	1/2 3/2	8 226 000 8 244 000	$2s2p^{5}(^{1}\mathbf{P}^{\bullet})3p$	² D	³ / ₂ 5/ ₂	9 250 000 9 283 000
$2s^2 2p^4(^{3}P)3d$	² F	⁵ / ₂	8 256 000	$2s2p^5(^1P^*)3p$	² P	¹ / ₂ ³ / ₂	9 288 000 9 303 000
$2s^2 2p^4({}^3\mathbf{P})3d$	⁴D	¹ / ₂ ³ / ₂	8 304 000 8 329 000	$2s^2 2p^4(^{3}P)4s$	² P	³ /2	10 182 000
$2s^2 2p^4(^{3}P)3d$	² <b>P</b>	3/2	8 353 000	$2s^2 2p^4(^{3}P) 4s$	4P	3/2	10 317 000
$2s^2 2p^4(^{3}P)3d$	² D	⁵ /2	8 360 000	$2s^2 2p^4(^3\mathrm{P})4d$	² D	³ / ₂ , ⁵ / ₂	10 462 000
$2s^2 2p^4({}^1D)3d$	² S	¹ / ₂	8 423 000	$2s^2 2p^4(^{3}P)4d$	⁴ F	³ / ₂ , ⁵ / ₂	10 530 000
$2s^2 2p^4({}^1\mathrm{D})3d$	² D	⁵ /2 3/2	8 452 000 8 484 000	$2s^2 2p^4(^3\mathbf{P})4d$	⁴P	⁵ /2	10 576 000
	Ni xx—	Continued					
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-	Level	Configuration	Та				

E-77

Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
$\frac{1}{2s^2 2p^4(^3\mathbf{P})4d}$	² P	³ /2	10 581 000				
$2s^2 2p^4({}^1\mathbf{D}) 4d$	² D	⁵ /2 ³ /2	10 655 000 10 674 000				
$2s^2 2p^4({}^1\mathrm{D}) 4d$	² P	³ /2 ¹ /2	10 655 000 10 674 000				
$2s^2 2p^4({}^1\mathbf{D})4d$	²S	¹ /2	10 655 000				
$2s^2 2p^4({}^1\mathbf{D})4d$	² F	⁵ /2	10 677 000				
$2s^2 2p^4({}^1\mathrm{D})4d$	² D	⁵ /2	10 655 000				
$2s^2 2p^4({}^1S)4d$	2 D	³ /2	10 853 000				
Ni XXI ( ³ P ₂ )	Limit		13 290 000				

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Ni xxı

Z = 28

O I isoelectronic sequence

Ground state:  $1s^22s^22p^{4} {}^{3}P_2$ 

Ionization energy =  $14\ 160\ 000\pm 28\ 000\ cm^{-1}\ (1756\pm 4\ eV)$ 

The fine structure of the ³P ground term is determined from two magnetic dipole transitions,  ${}^{3}P_{2} - {}^{3}P_{1}$  at 779.5 Å and  ${}^{3}P_{0}-{}^{3}P_{1}$  at 2818.2 Å (in air), measured in a tokamak plasma by Hinnov et al. (1982) with an accuracy of  $\pm 0.3$  Å. A solar flare line at 471.15 Å was identified by Widing (1978) as the intersystem line  $2s^2 2p^{4} {}^{3}P_2 - {}^{1}D_2$ .

Doschek et al. (1974) analyzed the  $2s^22p^4 - 2s^22p^5$  array and Doschek et al. (1975) found the  $2p^{6}$  S₀. Lawson and Peacock (1980) remeasured these arrays from 69-120 Å and found several intercombination lines. Lawson and Peacock's data are used to obtain the  ${}^{1}S_{0}$  level of  $2s^{2}2p^{4}$ and the levels of  $2s 2p^5$  with an uncertainty of  $\pm 300$  cm⁻¹. Percentage compositions of these levels were provided by Kaufman and Sugar (1982), with configuration interaction between  $2s^22p^4$  and  $2p^6$ .

The spectral region from 8-11 Å was measured by Gordon, Hobby, and Peacock (1980) with an accuracy of  $\pm 0.005$  Å, giving a level uncertainty of  $\pm 6000$  cm⁻¹. They classified lines arising from the  $2p^{3}3s$ ,  $2p^{3}3d$ , and

2p³4d configurations in this range. Only a few lines are assigned to 2p³4d, two of which are assigned to six transitions each. We did not attempt to derive energy levels for this configuration.

The ionization energy is an extrapolated value by Lotz (1967).

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	Ni XXI					
Configuration	Term	J	Level (cm ⁻¹ )	Leading	; percentages	
$2s^2 2p^4$	³ P	2 0 1	0 92 810 128 290	87 73 100	13 27	¹ D ¹ S
$2s^2 2p^4$	¹ D	2	212 250	87	13	³ P
$2s^2 2p^4$	¹ S	0	406 800	71	27	³ P
$2s2p^5$	³ P°	2 1 0	1 043 300 1 126 000 1 193 100	100 95 100	5	¹ <b>P</b> *
2s2p ⁵	¹ <b>P</b> *	1	1 436 400	95	5	³ P°1
2p ⁶	¹ S	0	2 403 500	98	2	$2s^22p^{4-1}S$
$2s^2 2p^3 ({}^4S^\circ) 3s$	³ S*	1	8 035 000			
$2s^2 2p^3(^2D^{\circ})3s$	³ D*	1,2 3	8 146 000 8 191 000			
$2s^2 2p^3(^2D^{\bullet})3s$	¹ D°	2	8 212 000			
$2s^2 2p^3 (^2P^{\circ}) 3s$	³ P•	0 1 2	8 295 000 8 313 000 8 405 000			
$2s^2 2p^3(^2\mathbf{P}^{\bullet})3s$	¹ <b>P</b> *	1	8 422 000			

Lawson, K. D., and Peacock, N. J. (1980), J. Phys. B13, 3313.

			111 / / / /	
Configuration	Term	J	Level (cm ⁻¹ )	Leading percentages
$2s^2 2p^3 ({}^4\mathrm{S}^\circ) 3d$	³ D°	3	8 666 000	<u> </u>
$2s^2 2p^3(^2\mathrm{D}^\circ)3d$	³ D°	3	8 835 000	
$2s^2 2p^3(^2\mathrm{D}^\circ)3d$	³ P°	2	8 848 000	
$2s^2 2p^3(^2\mathrm{D}^\circ) 3d$	¹ F°	3	8 896 000	
$2s^2 2p^3(^2\mathbf{P}^\circ)3d$	³ F°	3	8 895 000	
$2s^2 2p^3(^2\mathbf{P}^\circ) 3d$	³ P°	2 1	8 924 000 9 000 000	
$2s^2 2p^3(^2\mathbf{P}^\circ) 3d$	³ D°	2	9 034 000	
$2s^2 2p^3(^2\mathbf{P}^\circ) 3d$	¹ F°	3	9 048 000	
$2s^2 2p^3 (^2\mathbf{P}^\circ) 3d$	¹ D°	2	9 048 000	
$2s^2 2p^3(^2\mathbf{P^*}) 3d$	¹ P°	1	11 086 000	
Ni XXII	Limit		14 160 000	

Ni xxI—Continued

Ni xxii

#### Z = 28

N I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^{34} S_{3/2}^{\circ}$ 

Ionization energy =  $15\,280\,000\pm30\,000\,\mathrm{cm}^{-1}\,(1894\pm4\,\mathrm{eV})$ 

Two magnetic dipole lines observed in a tokamak plasma by Hinnov, Suckewer, Cohen, and Sato (1982) connect the doublet and quartet systems:  $2s^22p^3$  ${}^{3}S_{3/2}^{\circ}-{}^{2}D_{3/2}^{\circ}$  at 634.8±0.3 Å and  ${}^{4}S_{3/2}^{\circ}-{}^{2}D_{5/2}^{\circ}$  at 477.6±0.3 Å. The earlier analysis of the  $2s^22p^3-2s2p^4$ array by Doschek, Feldman, Cowan, and Cohen (1974) was extended by Lawson and Peacock (1980) to include intersystem lines as well as the additional array  $2s2p^4-2p^5$ . Their measurements in the range 71-124 Å, reported with an uncertainty of ±0.03 Å, are used here to derive the energy levels, giving a level value uncertainty of ±400 cm⁻¹. The percentage compositions of the levels were provided by Kaufman and Sugar (1982). The ionization energy was obtained by Lotz (1967) by extrapolation.

#### References

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Hinnov, E., Suckewer, S., Cohen, S., and Sato, K. (1982), Phys. Rev. A25, 2293.

Kaufman, V., and Sugar, J. (1982), private communication.

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			N1	xxII		
Configuration	Term	J	Level (cm ⁻¹ )	Lesding	percentages	
2s ² 2p ³	4S.	⁸ /2	0	81	15	²P•
$2s^2 2p^3$	²D*	⁸ /2 ⁵ /2	157 530 209 380	70 100	16	²₽•
$2s^2 2p^8$	²P*	1/2 3/2	302 500 400 100	99 68	1 25	2p ⁵ ² P* 2p ³ ² D*
2s( ² S)2p ⁴ ( ³ P)	4P	⁵ /2 ⁸ /2 ¹ /2	848 100 943 000 968 000	96 97 92	4 2 8	$2s(^2S)2p^4(^1D)\ ^2D$ $2s(^2S)2p^4(^1D)\ ^2D$ $2s(^2S)2p^4(^1S)\ ^2S$
$2s(^{2}S)2p^{4}(^{1}D)$	²D	8/2 5/2	1 176 200 1 203 400	89 96	8 4	$2s(^{2}S)2p^{4}(^{3}P)$ $^{2}P$ $2s(^{2}S)2p^{4}(^{3}P)$ $^{4}P$
$2s(^{2}S)2p^{4}(^{1}S)$	² S	¹ /2	1 344 600	64	30	2s( ² S)2p ⁴ ( ³ P) ² P
$2s(^{2}S)2p^{4}(^{3}P)$	²P	8/2 1/2	1 399 000 1 536 500	91 70	9 28	$2s(^{2}S)2p^{4}(^{1}D)$ $^{2}D$ $2s(^{2}S)2p^{4}(^{1}S)$ $^{2}S$
2p ⁵	²P•	8/2 1/2	2 190 500 2 340 900	98 99	2 1	2s²2p³ ²₽•
Ni xxIII ( ⁸ P ₀ )	Limit		15 280 000			

NI XXIII

Z = 28

C 1 isoelectronic sequence

Ground state:  $1s^22s^22p^2$  ³P₀

Ionization energy =  $16220000 \pm 30000 \text{ cm}^{-1} (2011 \pm 4 \text{ eV})$ 

Four magnetic dipole lines observed in a tokamak discharge by Hinnov, Suckewer, Cohen, and Sato (1982) determine the ³P and ¹D levels of the ground configuration: the  $2s^22p^2$   ${}^{3}P_0-{}^{3}P_1$  at 911.0 Å,  ${}^{3}P_1-{}^{3}P_2$  at 1915.0 Å,  ${}^{3}P_2-{}^{1}D_2$  at 614.8 Å, and  ${}^{3}P_1-{}^{1}D_2$  at 465.4 Å. The uncertainty of these measurements is  $\pm 0.3$  Å.

The rest of the levels of  $2s^22p^2$ ,  $2s2p^3$ , and  $2p^4$  (except for  $2s2p^{35}S_2^{\circ}$ ) were derived from the lines observed and classified by Lawson and Peacock (1980) in the range of 74-128 Å. Their measurement uncertainty is  $\pm 0.03$  Å, giving a level value uncertainty of  $\pm 400$  cm⁻¹. Edlén (1984) has compared the known values of the  ${}^{5}S_2^{\circ}$  level in the isoelectronic sequence with the theoretical predictions. He concluded that the values given by Lawson and Peacock are inconsistent with the trend. We give Edlén's predicted value in brackets.

The percentage compositions of these levels were provided by Kaufman and Sugar (1982).

The ionization energy was obtained by Lotz (1967) by extrapolation.

#### References

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Kaufman, V., and Sugar, J. (1982), private communication.

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Configuration	Term	J	Level (cm ⁻¹ )	Leading	percentages	
$2s^2 2p^2$	³ P	0	0	87	12	$2s^22p^2$ ¹ S
		] 1	109 770	99	1	2p ^{4 3} P
		2	161 990	67	32	$2s^2 2p^2$ ¹ D
$2s^2 2p^2$	¹ D	2	324 640	67	32	⁸ P
$2s^2 2p^2$	¹ S	0	463 900	85	12	³ P
$2s(^{2}S)2p^{3}(^{4}S)$	⁵ S*	2	[ <i>586 890</i> ]	95	5	$2s(^{2}S)2p^{3}(^{2}P^{*})^{3}P^{*}$
$2s(^{2}S)2p^{3}(^{2}D)$	³ D•	1	894 100	81	15	$2s(^{2}S)2p^{3}(^{2}P^{\bullet})^{3}P^{\bullet}$
•	_	2	900 000	79	18	
		3	941 400	100		
$2s(^{2}S)2p^{3}(^{2}P)$	³ P*	0	1 064 900	100		
-		1	1 078 500	78	16	$2s(^{2}S)2p^{3}(^{2}D^{*})^{3}D^{*}$
		2	1 105 000	65	20	· •
$2s(^{2}S)2p^{3}(^{4}S)$	³ S*	1	1 250 500	74	19	$2s(^{2}S)2p^{8}(^{2}P^{*})$ $^{1}P^{*}$
$2s(^{2}S)2p^{3}(^{2}D)$	¹ <b>D</b> •	2	1 304 600	87	12	$2s(^{2}S)2p^{3}(^{2}P)$ ³ P [•]
$2s(^{2}S)2p^{3}(^{2}P)$	¹ P*	1	1 459 700	77	19	$2s(^{2}S)2p^{3}(^{4}S^{*})$ $^{3}S^{*}$
2p ⁴	⁸ P	2	1 864 700	85	14	$2n^{4}$ ¹ D
7	-	Ō	1 977 400	79	20	$2p^{4}$ ¹ S
		1	1 999 400	99	1	2s ² 2p ² ³ P
2 <b>p</b> ⁴	¹ D	2	2 080 600	86	14	\$P
2p ⁴	¹ S	0	2 348 200	77	20	⁸ P
Ni <b>XXIV</b> $({}^{2}P_{1/2}^{\bullet})$	Limit		16 220 000			

Ni XXIII

#### Ni xxiv

#### Z = 28

B 1 isoelectronic sequence

Ground state: 1s²2s²2p ²P^{*}_{1/2}

Ionization energy =  $17 190 000 \pm 34 000 \text{ cm}^{-1} (2131 \pm 4 \text{ eV})$ 

Hinnov, Suckewer, Cohen, and Sato (1982) observed the  $2s^22p$   ${}^{2}P_{1/2}-{}^{2}P_{3/2}$  magnetic dipole transition at 609.9±0.3 Å in a tokamak plasma. The levels of the  $2s2p^{2}$ and  $2p^{3}$  configurations are from the measurements and classifications of Lawson and Peacock (1980) in the range of 87-160 Å with a wavelength uncertainty of ±0.03 Å, giving a level value uncertainty of ±400 cm⁻¹. They identified the transition  $2s 2p^{2} {}^{4}P_{5/2}-2p^{3} {}^{2}D_{3/2}^{2}$  at 98.39 Å that connects the quartet and doublet systems. Edlén (1983) suggested that this identification is inconsistent with the intersystem connection found in a solar flare spectrum by Sandlin et al. (1976) for isoelectronic Fe XXII. Edlén proposes the value 98.282 Å for this line. The percentage compositions of these levels were provided by Kaufman and Sugar. Their calculation includes configuration interaction between  $2s^22p$  and  $2p^3$ .

The ionization energy was obtained by Lotz (1967) by extrapolation.

#### References

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Configuration	Term	J	Level (cm ⁻¹ )	Leading	percentages	
2s ² 2p	² P°	1/2 8/2	0 163 960	98 98	2 2	2p ³ ² P°
2s2p ²	ťΡ	1/2 3/2 5/2	458 100 541 000 610 000	94 99 91	5 1 9	² S ² D ² D
$2s2p^2$	²D	⁸ /2 5/2	843 700 884 100	93 91	7 9	2P 4P
2s2p ²	²P	1/2 3/2	955 700 1 143 100	66 93	30 6	² S ² D
2s2p ²	²S	¹ / ₂	1 129 600	64	34	² P
2p ⁸	4S•	8/2	1 424 900	84	11	² P•
2p ⁸	²D•	8/2 5/2	1 582 000 1 626 400	78 100	12	² P•
2p ⁸	²₽•	¹ /2 8/2	1 781 100 1 872 900	98 75	2 18	2s ² 2p ² P* 2p ^{8 2} D*
Ni <b>xxv</b> ( ¹ S ₀ )	Limit		17 190 000			

#### Ni xxiv

Ni xxv

Z = 28

Be 1 isoelectronic sequence

Ground state:  $1s^22s^2 {}^1S_0$ 

Ionization energy =  $18510000 \pm 37000 \text{ cm}^{-1} (2295 \pm 5 \text{ eV})$ 

The  $2s^2 {}^{1}S_0 - 2s 2p {}^{1}P_1^{\circ}$  resonance line was measured by Breton et al. (1979) at 117.90 Å in a tokamak plasma. Sandlin et al. (1976) tentatively identified a faint image at 238.82 Å in a solar flare spectrum as the  ${}^{1}S_0 - {}^{3}P_1^{\circ}$  line of the same array. This value is in good agreement with the prediction by Edlén (1983).

The  $2s 2p - 2p^2$  array was classified by Lawson and Peacock (1989). Their stated measurement accuracy is  $\pm 0.03$  Å, giving a level value uncertainty of  $\pm 400$  cm⁻¹. We give their results, although Edlén concludes from his isoelectronic study that some of the identifications are doubtful.

The line identifications establishing the levels of the n=3 shell were given by Fawcett, Ridgeley, and Hughes (1979). The wavelengths, given with an accuracy of

 $\pm 0.003$  Å, fall in the range of 9–10 Å. The level value uncertainty is  $\pm 4000$  cm⁻¹.

The ionization energy was obtained by extrapolation by Lotz (1967).

#### References

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Sandlin, G. D., Brueckner, G. E., Scherrer, V. E., and Tousey, R. (1976), Astrophys. J. 205, 147.

Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
s ²	¹ S	0	0	2s3d	¹ D	2	10 880 000
ls2p	³ P°	0	378 190	2 <b>p</b> 3 <b>p</b>	$^{3}D$	2	11 153 000
		1	418 720			3	11 296 000
		2	549 500				
				2p3d	³ F°	3	11 271 000
s2 <b>p</b>	¹ <b>P</b> °	1	848 100				
	1 -	-		2p3d	³ D°	2	11 283 000
$p^2$	³ P	0	1 048 300?		_	1	11 2 <b>9</b> 6 000
r		1	1 154 300			3	11 437 000
		2	1 207 800				
		_		2p3p	$^{3}P$	2	11 306 000
$p^2$	¹ <b>D</b>	2	1 379 600				
•				2p3p	$^{3}S$	1	11 306 000
$p^2$	¹ S	0	1 611 500				
•				2p3d	¹ <b>D</b> °	2	11 408 000
s3p	³ P°	1	10 650 000	-			
•				2p3d	³ P°	0-2	11 456 000
2s3p	¹ <b>P</b> °	1	10 707 000	-			
-		ĺ		2p3d	¹ <b>F</b> °	3	11 525 000
s3d	$^{3}D$	1	10 794 000				
		2	10 800 000	<b>Ni XXVI</b> $({}^{2}S_{1/2})$	Limit		18 510 000
		3	10 813 000				

Ni xxv

198

Ni xxvi

## Z = 28

Li 1 isoelectronic sequence

Ground state: 1s²2s ²S_{1/2}

Ionization energy =  $19351000 \pm 5000 \text{ cm}^{-1} (2399.2 \pm 0.6 \text{ eV})$ 

Edlén (1983) has given extrapolated values for the 2s - 2p transition wavelengths with an estimated uncertainty of  $\pm 0.01$  Å. He concludes that the solar identification for this transition by Sandlin et al. (1976) is incorrect. Edlén's results are given in brackets. Fawcett, Ridgeley, and Hughes (1979) determined the 3s, 3p, and 3d terms from observations at 9 Å of a laser-produced plasma. Their measurement uncertainty is  $\pm 0.01$  Å, giving a level value uncertainty of  $\pm 12000$  cm⁻¹.

From measurements of spark spectra at  $\sim 1.6$  Å, Safronova and Sidelnikov (1977) determined the levels above the ionization energy. No estimated uncertainty is given but wavelengths to four decimal places are reported. The designations are from Vainstein and Safronova (1978).

The ionization energy was calculated by Edlén (1979).

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Vainstein, L. A. and Safronova, U. I. (1978), At. Data Nucl. Data Tables 21, 49.

$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1s ² 2s	² S	¹ / ₂	0	$1s(^2S)2s2p(^3P^{\circ})$	² P°	1/2 3/2	62 516 000 62 617 000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1s² 2p	2 <b>P</b> *	¹ /2 ³ /2	[ 427 180] [ 604 680]	$1s(^{2}S)2p^{2}(^{3}P)$	⁴P	$\frac{3}{2}$	$62 697 000 \\ 62 783 000$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$1s^2 3s$	² S	¹ / ₂	10 880 000	$1s(^2\mathbf{S})2s2p(^1\mathbf{P}^{\bullet})$	² P°	1/2	62 755 000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	18 <i>3p</i>	r	3/2 3/2	11 036 000	$1s(^{2}S)2p^{2}(^{3}P)$	²P	1/2 3/2	62 997 000 63 210 000
Ji XXVII ( ${}^{1}S_{0}$ )       Limit       19 351 000 $1s({}^{2}S)2s2p({}^{3}P^{\circ})$ $7_{2}$ 63 085 0 $1s({}^{2}S)2s2p({}^{3}P^{\circ})$ $4P^{\circ}$ $\frac{1}{2}$ $62$ 193 000 $1s({}^{2}S)2p^{2}({}^{1}S)$ $2S$ $\frac{1}{2}$ $63$ 397 0 $1s({}^{2}S)2s2p({}^{3}P^{\circ})$ $\frac{4}{2}$ $\frac{62}{2}$ 228 000 $\frac{63}{2}$ 228 000 $\frac{1}{2}$ $\frac{63}{2}$ $\frac{63}{2}$	$1s^2  3d$	² D	³ / ₂ ⁵ / ₂	11 077 000 11 092 000	$1s(^2\mathbf{S})2p^2(^1\mathbf{D})$	² D	3/2 5/	63 008 000
$\frac{1}{s(^{2}S)2s2p(^{3}P^{\circ})} = \frac{^{4}P^{\circ}}{^{3}/_{2}} = \frac{^{1}/_{2}}{62\ 228\ 000} = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2}) = \frac{1}{2}(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}{2})^{-1}P(\frac{1}$	$i xxvii ({}^{1}S_{0})$	Limit		19 351 000	$1s(^{2}S)2p^{2}(^{1}S)$	² S	¹ / ₂	63 085 000
	$1s({}^{2}S)2s2p({}^{3}P^{*})$	⁴ P°	¹ / ₂ ³ / ₂	62 193 000 62 228 000			12	

Ni XXVI	
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Ni xxvii

Z = 28

He 1 isoelectronic sequence

Ground state: 1s² S₀

Ionization energy =  $82\,984\,000\pm16\,000\,\mathrm{cm}^{-1}\,(10\,288.8\pm2.0\,\mathrm{eV})$ 

Because of the excellent agreement of the calculated energies of the n=2 shell by Safronova (1981) with the few well-measured spectra in the He I sequence, we have compiled her results for the n=2 levels and for the ionization energy. Detailed comparisons are given in the Introduction. Levels of the n=3-5 shells are from the calculated binding energies by Ermolaev and Jones (1974) subtracted from Safronova's value for the binding energy of the ground state. We have assumed an uncertainty of 2 parts in 10⁴ for the excited levels relative to the ground state, and for the ionization energy. For differences between excited levels where  $\Delta n = 0$ , we assumed an uncertainty of 2 parts in 10³. Observations by Safronova and Sidelnikov (1977) place the  $1s_{2p}$  ¹P₁^o at 62 925 000 cm⁻¹ with an estimated uncertainty of  $\pm 20\ 000\ \text{cm}^{-1}$ .

Percentage compositions are from Ermolaev and Jones.

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Configuration	Term	J	Level (cm ⁻¹ )	Leading pe	rcentages		
1 <i>s</i> ²	¹ <b>S</b>	0	0				
1 <i>s</i> 2 <i>s</i>	³ S	1	[62 358 960]				
1 <i>s2p</i>	³ P°	0 1 2	[62 614 630] [62 637 380] [62 801 270]	89	11	1 <b>P*</b>	
1 <i>s</i> 2 <i>s</i>	¹ S	0	[62 637 200]				
1 <i>s</i> 2 <i>p</i>	¹ <b>P</b> °	1	[62 952 670]	89	11	³ P*	
1 <i>s</i> 3s	³ S	1	[73 903 340]				
1s3p	³ P*	0 1 2	[ <i>73 974 350</i> ] [ <i>73 979 340</i> ] [ <i>74 028 190</i> ]	88	12	¹ <b>P</b> *	
1 <i>s</i> 3s	¹ S	0	[73 976 370]				
1s3p	¹ <b>P</b> *	1	[74 070 580]	88	12	³ P•	
1 <i>s</i> 4 <i>s</i>	³ S	1	[77 900 890]				
1 <i>s</i> 4 <i>s</i>	۱S	0	[77 930 480]				
1s4p	3 <b>P</b> •	0 1 2	[77 930 500] [77 932 560] [77 953 220]	88	12	1 <b>₽</b> •	
1 <i>s</i> 4 <i>p</i>	¹ <b>P</b> *	1	[77 970 500]	88	12	³ P*	
1s5s	³ S	1	[79 740 940]				
1\$55	¹ S	0	[79 755 710]				

Ni xxvii

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	Ni	XXVII-	-Continued
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Configuration	Term	J	Level (cm ⁻¹ )	Leading percentages					
1 <i>s5p</i>	³ P°	0 1 2	[79 755 910] [79 756 970] [79 767 550]	87	13	¹ P°			
1s5p	¹ P°	1	[79 776 290]	87	13	³ <b>P°</b>			
Ni xxviii $({}^{2}S_{1/2})$	Limit		82 984 000						

## NI XXVIII

#### Z = 28

H 1 isoelectronic sequence

Ground state:  $1s^{2}S_{1/2}$ 

Ionization energy =  $86\,909\,400\pm500\,\,\mathrm{cm^{-1}}$  (10 775.48±0.06 eV)

No observations of this spectrum are reported. We give calculated values by Mohr (1983) for the n = 2 shell and by Erickson (1977) for n = 3 to 5 relative to the 2p ²P_{3/2} level. Further details are given in the Introduction. Relative to the ground state, the level uncertainty is estimated to be one part in 10⁶.

#### References

Erickson, G. W. (1977), J. Phys. Chem. Ref. Data 6, 831. Mohr, P. J. (1983), At. Data Nucl. Data Tables, 29, 453.

Configuration	Term	J	Level (cm ⁻¹ )	Configuration	Term	J	Level (cm ⁻¹ )
ls	² S	¹ / ₂	0	4f	² <b>F</b> *	5/2 7/2	[ <i>81 524 081</i> ] [ <i>81 528 784</i> ]
2р	² P°	¹ / ₂ ³ / ₂	[65 113 950] [65 344 939]	5 <b>p</b>	2 <b>P</b> *	$\frac{1}{2}$	[ <i>83 443 186</i> ] [ <i>83 457 952</i> ]
2s	²S	¹ /2	[65 119 814]	56	2 <b>S</b>	ړ بر	[83 443 585]
3р	² P°	¹ / ₂ ³ / ₂	[77 248 280] [77 316 770]	5d	² D	3/2 5/	[83 457 924]
38	² S	¹ /2	[77 250 120]	5f	² F°	12 5/2	[83 462 755]
3 <b>d</b>	² D	³ / ₂ ⁵ / ₂	[77 316 649] [77 339 033]		2-	7/2 7.	[83 465 165]
4 <i>p</i>	² <b>P</b> *	1/2 3/2	[ <i>81 485 832</i> ]	5g	-G	"/2 9/2	[83 465 160] [83 466 603]
4 <i>s</i>	² S	1/2 1/2	[81 486 610]		Limit		86 909 400
4 <i>d</i>	² D	³ / ₂ ⁵ / ₂	[81 514 646] [81 524 098]				
		-					

Ni xxvIII

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F. Atomic Transition Probabilities of Nickel, Ni I through Ni XXVIII

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# F. Atomic Transition Probabilities of Nickel

[Exerpted from: J. R. Fuhr, G. A. Martin, and W. L. Wiese, J. Phys. Chem. Ref. Data 17, Supplement 4 (1988)]

## 1. Introduction

The following tables, including the introductory comments, are excerpted from the above cited compilation of atomic transition probabilities by J. R. Fuhr, G. A. Martin, and W. L. Wiese of the Data Center on Atomic Transition Probabilities at the National Institute of Standards and Technology (formerly the National Bureau of Standards).

This is part of the third major critical compilation by the NBS Data Center on Atomic Transition Probabilities. A first tabulation¹ containing transition probabilities for about 4,000 spectral lines of the elements hydrogen through neon, atomic numbers Z = 1 through 10, including the neutral atoms as well as their various ions, was published in 1966. A second data volume² was issued in 1969, containing data for about 5,000 lines of the elements sodium (Z = 11) through calcium (Z = 20), again for all stages of ionization for which data were available. The data compilation work then continued with a series of smaller tables for the atoms and ions of the elements of the iron group, i.e., Sc and Ti³; V, Cr, and Mn⁴; Fe, Co, and Ni⁵; and the forbidden lines of all these elements.⁶ From the beginning, it has been the intention to integrate these smaller tabulations into a single volume for the iron-group elements, in updated and expanded form. Unexpectedly, a great deal of new data were generated for these elements during the past few years, often with much improved accuracy, so that the revisions and additions became very extensive. Thus it took a much longer time than anticipated to complete these largely new data tables, and the greatly expanded tabulations had to be split into two separate volumes. Nickel is included in a volume that contains the material on the elements Fe (Z = 26) through Ni (Z = 28), and a companion volume⁷ contains the material on Sc (Z = 21) through Mn (Z = 25).

In the present compilation, the scope and format of the earlier tabulations is maintained, i.e., critically evaluated atomic transition probabilities of allowed and forbidden discrete transitions of all stages of ionization are presented for which reliable data are available. Data are listed for at least the more prominent lines of each spectrum, even if some of these data are of low accuracy. Furthermore, transition-probability data are also presented for weaker transitions if the accuracy of these data has been estimated to be better than  $\pm 50\%$ 

The original literature is continually monitored by this NBS Data Center, and a master reference list is maintained from which all literature sources for this compilation have been taken.

### 2. Method of Evaluation

For the compilation of data on a critical basis, the central task is the evaluation of the data accuracy and the subsequent choice of the most accurate material. In order to accomplish this task in a consistent manner, general guideposts were established for each experimental and theoretical approach in earlier compilation work, and these criteria were maintained in this work. Specifically, each original literature source was judged by the following principal criteria:

- A general evaluation of the capabilities and reliability of the applied experimental or theoretical method.
- (2) The author's consideration of the major critical factors in his approach that enter into the results.
- (3) The degree of agreement and general consistency between the author's results and other reliable data.
- (4) The degree of fit of the data into established systematic trends and, if deviations exist, the reasons for such disagreements.
- (5) The author's estimate of his uncertainties.

The general evaluations of each experimental and theoretical method have been discussed in considerable detail in the introductions to previous tabulations.¹⁻⁶ Thus, these publications are to be consulted for further details. However, it should be pointed out that in this tabulation, particularly interesting situations are illustrated by providing comparison tables or graphs in the introductions to individual spectra.

With respect to error estimates, one should note that the theoretical literature sources, which provide a large part of the data, generally contain no error estimates, since no reliable assessment of the uncertainties introduced by the various approximations is possible. But even for the experimental papers, where error estimates may often readily be made, the statements by some authors are too imprecise and also incomplete, so that they are not particularly useful as presented. Sometimes only statistical measurement errors have been given, without allowance for systematic errors. It therefore became essential to judge each paper by the principal factors 1-4 listed above, in addition to utilizing the author's error estimate (point (5)) whenever appropriate.

#### 3. General Arrangement of the Tables

The same general arrangement of the tables is used as in earlier volumes,^{1,2} i.e., data are included which serve to identify the spectral lines, as well as the actual transition probabilities (and related quantities), accuracy estimates, and references to the sources of the compiled material. However, for most of the spectra of neutral and singly-ionized atoms of the iron-group elements, the transition array column was dropped. Instead, in order to identify the lower and upper levels of a transition, the level designation scheme of C. E. Moore⁸ was adopted, who affixed lower-case letters (a,b,c,...,x,y,z) to the term designations. This convention is also retained in the very recent tables of "Atomic Energy Levels" by J. Sugar and C. Corliss.⁹ In other special cases, the notation was adapted to the special coupling situations encountered in those spectra, as, for example, the  $J_1 i$  coupling encountered in Ne-like ions and  $J_{1j}$  and  $J_{1\ell}$  coupling for Ar-like ions.

Material pertaining to spectral-line identifications has been taken from the comprehensive wavelength tabulations of Reader and Corliss,¹⁰ Kelly,^{11,12} and Kelly and Palumbo,¹³ the multiplet tables of C. E. Moore,^{14,15} and the recent energy-level compilation of Sugar and Corliss⁹ (this last reference supersedes earlier compilations by Sugar and others^{16,17}). The wavelength and energylevel data from these sources have been supplemented by original literature data when needed in the course of preparing the transition-probability tables.

Wavelengths and energy levels which are the results of theoretical calculations, or which were either calculated from experimentally determined data or interpolated or extrapolated from data on similar (e.g., isoelectronic) species, are placed in square brackets in order to distinguish them from the usually more accurate experimental material. For each transition-probability table which contains a minimum of twenty distinct wavelength values, a "list of tabulated lines," has been provided, in ascending order of wavelength, of the spectral lines contained therein, along with an index to the multiplet number (or numbers) in which each is to be found. Wavelengths that are printed in italics in the transition-probability tables are not included in these line lists.

The uncertainties in the atomic transition-probability data are denoted by letters as follows:

- A., for uncertainties within 3 percent,
- B.. for uncertainties within 10 percent,
- C.. for uncertainties within 25 percent,
- D.. for uncertainties within 50 percent,
- E., for uncertainties greater than 50 percent.

The word *uncertainty* is used here with the connotation "estimated extent of the deviation from the true value." The estimation procedure is based on the evaluation of random errors as well as estimates of the maximum effect of possible systematic errors. Often, further distinctions were made in the uncertainty labels by assigning plus or minus signs to some transitions to indicate that these lines are estimated to be somewhat better or worse than similar lines. These should, therefore, be the first or last choice among similar transitions.

A summary of the abbreviations and special symbols used in the tables is given in Section 4. Included there for convenience are the relations between line and multiplet values in the case of LS coupling. In Table 1, the conversion factors are provided which have been used throughout this compilation to convert from transition probabilities to oscillator strengths and line strengths, and vice versa.

	1		
	Aki	fik	S
			$\frac{\text{E1}}{\frac{2.026_1 \times 10^{18}}{g_k \lambda^3}}$
			$\frac{1.679_9 \times 10^{18}}{g_k \lambda^5}$
Aki	1	$\frac{6.670_3\times10^{13}g_i}{g_k\lambda^2}$	$\frac{M1}{\frac{2.697_4 \times 10^{13}}{g_k \lambda^3}}$
			$\frac{M2}{\frac{6.626_5 \times 10^{12}}{g_k \lambda^5}}$
fu	$\frac{1.499_2 \times 10^{-16} \lambda^2 g_k}{g_i}$	1	E1 $\frac{303.7_{\delta}}{g_{l}\lambda}$
	E1 4.935 ₅ × $10^{-19} g_k \lambda^3$	E1	
S	E2 5.952 ₆ × $10^{-19} g_k \lambda^5$	$3.292_1 \times 10^{-3} g_i \lambda$	1
	M1 3.707 ₃ × $10^{-14} g_k \lambda^3$		
	M2 1.509 ₁ × 10 ⁻¹³ $g_k \lambda^5$		

TABLE 1. Conversion factors The factor in each box converts by multiplication the quantity above it into the one at its left.

The line strength (S) is given in atomic units; formulas and values for these quantities in SI units are as follows:

For E1 transitions,  $a_0^2 e^2 = 7.188_3 \times 10^{-59} \text{ m}^2 \text{ C}^2$ For E2 transitions,  $a_0^4 e^2 = 2.012_9 \times 10^{-79} \text{ m}^4 \text{ C}^2$ For M1 transitions,  $\mu_B^2 = (eh/4\pi m_e)^2 = 8.600_7 \times 10^{-47} \text{ J}^2 \text{ T}^{-2}$ For M2 transitions,  $\mu_B^2 a_0^2 = 2.408_5 \times 10^{-67} \text{ J}^2 \text{ m}^2 \text{ T}^{-2}$ .

where  $a_0$ , e,  $m_e$ , and h are the Bohr radius, electron charge, electron mass, and Planck constant, respectively, and  $\mu_B$  is the Bohr magneton.

The transition probability  $(A_{kl})$  is in units of  $s^{-1}$ , and the *f*-value is dimensionless. The wavelength  $(\lambda)$  is given in Angström units, and  $g_l$  and  $g_k$  are the statistical weights of the lower and upper level, respectively.

[Note: the definition of the line strength for E2 transitions, which is used by some authors, yields an S-value that is 50% higher than that employed here and in earlier NBS transition-probability compilations. Such line strengths have been multiplied by  $\frac{2}{3}$  before tabulating them here, and this fact is indicated in the short introductions to the pertinent data tables.]

For the atomic constants entering into the relations given in this table, the recommendations of the CODATA Task Group on Fundamental Constants (E. R. Cohen and B. N. Taylor, Rev. Mod. Phys. 59, 1121 (1987)) have been used. The 1987 values were not available at the time that most of the data was compiled for this publication; however, differences between these and the earlier (CODATA Task Group, 1973) values of the fundamental constants were utilized, which amount to only 0.002% or less for the E1 transitions and 0.05% or less for the M1, E2, and M2 (forbidden) transitions and have therefore not affected the tabulated data.

## 4. Key to Abbreviations and Symbols Used In the Tables

- 1. Symbols for indication of accuracy:
  - A..... uncertainties within 3 percent,
  - B..... uncertainties within 10 percent,
  - C..... uncertainties within 25 percent,
  - D..... uncertainties within 50 percent,
  - E ..... uncertainties greater than 50 percent.
- 2. Abbreviations appearing in the source column of allowed transitions:
  - ls = LS coupling rules applied
  - n ormalized to a scale different from that of the author (as explained in the introductory remarks to the pertinent spectrum).
  - *interp.* = derived by an interpolation technique, rather than taken directly from the literature.
- 3. Special symbols used in the wavelength and energy level columns:

The number in parentheses under the multiplet designation refers to the sequence number of Ref. 14 (Revised Multiplet Table). If letters "uv" are added, they refer to the sequence number of Ref. 15 (Ultraviolet Multiplet Table).

Numbers in italics indicate multiplet values, i.e., weighted averages of *line* values.

Numbers in square brackets indicate approximate calculated or extrapolated values.

#### Useful Relations

(A) Statistical weights:

The statistical weights are related to the inner quantum number  $J_L$  (for one-electron spectra:  $j_l$ ) of a level (i.e., initial or final state of a *line*) by

$$g_L = 2J_L + 1,$$

and to the quantum numbers of a term (initial or final state of a *multiplet*) by

$$g_M = (2L + 1)(2S + 1).$$

(The "multiplet" values  $g_M$  may also be obtained by summing over all possible "line" values  $g_L$ . S is the resultant spin.)

- (B) Relations between the strengths of allowed lines and the total multiplet strength:
  - 1. Line strength S:

$$S(i,k) = \sum_{J_k J_k} S(J_k J_k)$$

or

$$S$$
 (Multiplet) =  $\Sigma S$  (line)

- (k denotes the upper and i the lower term).
- 2. Absorption oscillator strength  $f_{ik}$ :

$$f_{ik}^{\text{multiplet}} = \frac{1}{\bar{\lambda}_{ik} \sum_{I_i} (2J+1)} \sum_{J_b J_k} (2J_i+1) \times \lambda(J_{i_b} J_k) \times f(J_{i_b} J_k).$$

The mean wavelength for the multiplet,  $\bar{x}_{ik}$ , may be obtained from the weighted energy levels. Often the wavelength differences for the lines within a multiplet are small, in which case the wavelength factors may be neglected.

3. Transition probability  $A_{kl}$ :

$$A_{kl}^{\text{multiplet}} = \frac{1}{(\bar{\lambda}_{kk})^3 \sum_{J_k} (2J_k + 1)} \sum_{J_k J_k} (2J_k + 1) \times \lambda(J_l, J_k)^3 \times A(J_l, J_k).$$

Relative strengths  $S(J_i, J_k)$  of the components of a multiplet are listed for the case of LS coupling in C. W. Allen, Astrophysical Quantities, 3rd ed. (The Athlone Press, London, 1973); H. E. White and A. Y. Eliason, Phys. Rev. 44, 753 (1933); I W. Shore and D. H. Menzel, Principles of Atomic Structure, p. 447 (John Wiley & Sons, Inc., New York, 1968); L. Goldberg, Astrophys. J. 82, 1 (1935) and 84, 11 (1936).

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## F - 6

# Nickel

# Niı

Ground State:  $1s^22s^22p^63s^23p^63d^84s^2 {}^3F_4$ 

Ionization Energy: 7.6375 eV =  $61600 \text{ cm}^{-1}$ 

## Allowed Transitions

#### List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
10/2 95	69	2192.28	28	2007 46	16	2220.26	10
1903.83	24	2182.38	20	2907.40	16	3320.20	70
1908.90	24 20	2185.91	57	2914.01	13	3322.31	79
1970.87	68	2190.22	57	2943.91	47	3357.01	37
1981.01	08	2191.21	80 67	2981.03	4/	3351.00	3
1990.25	08	2197.33	5/	2984.13	15	3301.33	39
1994.29	33	2201.59	85	2991.11	15	3302.80	44
2000.49	05	2212.15	2/ 59	2992.39	45	3303.70	//
2001.83	00	2220.71	28	2994.40	48	3300.10	9
2007.01	05	2221.94	57	3002.48	47	3307.88	41
2007.09	34 79	2230.90	5/	3003.02	4/	3309.30	0
2014.25	08	2244.46	53	3012.00	81	3371.99	8
2025.40	32	2251.48	53	3019.14	11	3374.22	37
2026.62	32	2253.57	52	3031.87	11	3380.57	78
2029.29	66	2254.81	25	3037.93	45	3380.89	8
2033.56	60	2258.15	50	3045.01	13	3391.04	5
2041.16	65	2259.56	56	3050.82	45	3392.98	40
2047.35	63	2261.42	24	3054.31	45	3409.58	5
2050.84	6/	2266.35	52	3057.64	47	3413.48	5
2052.04	30	2267.55	21	3064.62	47	3413.94	37
2052.45	30	2271.95	55	3080.75	47	3414.76	39
2053.91	29	2274.66	21	3097.12	11	3420.73	10
2055.50	32	2287.32	53	3099.11	14	3423.71	41
2059.92	61	2288.40	52	3101.56	45	3433.56	39
2060.20	61	2289.98	23	3101.88	80	3437.28	3
2062.37	32	2293.11	56	3105.46	13	3446.26	41
2063.42	65	2300.77	54	3107.71	13	3452.88	37
2064.39	61	2302.97	56	3114.12	46	3458.46	39
2069.52	64	2307.35	55	3129.30	13	3461.66	37
2082.87	32	2312.34	20	3134.11	45	3467.50	3
2085.37	62	2313.98	21	3145.12	8	3469.48	9
2085.57	90	2317.10	20	3145./1	11	3472.55	40
2088.98	01	2320.03	20	3159.52	11	3483.77	27
2089.09	31	2321.38	21	3105.51	42	3485.88	3/
2095.15	90	2324.05	25	3184.37	11	3492.96	38
2103.85	20	2323.79	20	3193.37	15	3498.19	7
2105.79	20	2325.90	10	2200.42	40	3500.85	2
2111.75	27	2343.34	19	3200.42	44	3502.00	3
2114.45	00 50	2340.03	19	3221.03	70	3507.09	3
2121.40	59	2347.51	18	3225.02	/9	3510.33	38
2124.80	89	2348.73	51	3220.98	8	3513.93	37
2125.02	28	2419.31	19	3232.93	8	3515.05	39
2128.41	51	24/0.88	1/	3234.05	42	3519.76	5
2129.90	58	2540.02	83	3235.75	11	3523.07	74
2147.80	20	2553.37	17	3243.05	43	3523.44	36
2151.93	29	2501.42	1/	3248.40	42	3524.54	38
2152.23	59	2090.48	82	3249.44	12	3527.98	6
2157.83	5/	2740.74	50	3250.74	79	3548.19	41
2158.31	57	2798.65	50	3271.11	44	3551.53	5
2161.04	58	2805.08	15	3282.69	8	3561.75	2
2166.15	58	2821.29	49	3286.94	39	3566.37	76
2173.54	84	2834.55	16	3310.20	77	3571.86	5
2174.48	57	2865.50	50	3315.66	43	3577.24	3

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			11		11
- 11	4729.28	193	5094.42	163	6105.78
	4731.81	162	5099.95	154	6108.12
	4732.47	193	5102.97	97	6111.06
	4740.17	123	5115.40	167	6119.78
	4752.43	138	5129.37	153	6128.99
	4756.52	122	5137.08	98	6130.17
	4758.42	172	5155.14	179	6133.95
1	4762.63	115	5155.76	182	6175.42
	4773.41	164	5157.99	128	6176.81
	4786.29	99	5176.57	181	6177.26
	4786.54	122	5179.14	175	6186.74
	4791.00	115	5187.82	161	6198.65
	4793.47	159	5197.17	176	6204.64
	4807.00	156	5220.31	131	6223.99
	4808.86	160	5262.83	130	6230.09
	4812.00	136	5265.71	142	6256.36
- 11	4914 67	122	5347 71	147	6271 76

Wavelength (Å)

No.

List of tabulated lines - Continued

No.

Wavelength (Å)

Wavelength (Å)

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4.03 6.83

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No.

3397 93         36         472.2.8         193         509.4.2         163         6105.7.8         206           3027.2.8         3         4721.8.1         162         5099.55         154         6105.7.8         200           3060.3.1         36         4740.17         123         5112.97         97         6111.06         189           3061.24         7         4756.52         122         5117.08         99         613.07         203           3012.47         7         4756.52         122         5117.08         99         613.07         203           3012.47         7         4756.52         122         5117.08         99         613.07         203           3020.02         3         4766.54         122         5179.14         175         6165.74         118           3060.24         2         4790.00         115         5179.72         161         6198.64         206         202.09         187           3064.07         488.846         160         522.63         131         623.09         187           3074.0.6         35         481.0.0         166         522.63         131         316.246.64         117 <t< th=""><th></th><th></th><th>1</th><th></th><th>l</th><th></th><th></th><th></th></t<>			1		l			
399770         38         473.47         193         5102.97         97         6111.06         189           3602.81         36         4702.47         193         5112.47         97         6111.06         189           3610.46         38         4702.47         123         5115.40         167         6119.78         200           3611.46         38         4702.43         138         515.76         182         613.35         188           360.02         3         4706.63         115         515.76         182         6175.42         196           364.44         6         4786.29         95         5175.77         181         6176.81         186           364.67         4         4786.48         122         5171.17         175         602.45         185           364.64         4         4786.42         122         5371.17         114         602.45.65         92           364.64         5         4872.00         135         537.47         147         6272.65         50           364.64         14         623.23         136         623.23         186         630.45         187           364.71         71<	3587.93	36	4729.28	193	5094.42	163	6105.78	206
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3597 70	38	4731.81	162	5099.95	154	6108.12	94
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3602.28	30	4732.47	103	\$102.97	97	6111.06	189
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3002.28	3	4732.47	193	5115.40	167	6110.79	200
30         30         47         7         475         138         12.9.7         133         611.3.17         203           3617.39         75         4735.42         112         515.3.6         198         613.3.17         203           3610.20         3         476.6.5         116         515.3.6         117         613.5.7.6         1181         613.5.7.6         1181         613.5.7.6         1181         613.7.6         1181         613.7.6         1181         613.7.6         1181         613.7.6         1185         1187.4         1185         1187.4         1185         1187.4         1185         1187.4         1185         1187.4         1185         1187.4         1185         1187.4         1185         1187.4         1185         1187.4         1185         1187.4         1187         1187         1187         1187.4         1187         1187.4         1187.4         1187         1187.4         1187.4         1187.4         1187         1187.4         1187.4         1187.4         1187.4         1187.4         1187.4         1187.4         1187.4         1187.4         1187.4         1177.5         1177.5         1177.5         1177.5         1177.5         1177.5         1177.5	3609.31	30	4/40.17	123	5115.40	167	0119.78	200
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3610.46	38	4752.43	138	5129.37	153	6128.99	91
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3612.74	7	4756.52	122	5137.08	98	6130.17	203
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	3619.39	75	4758.42	172	5155.14	179	6133.95	188
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	3620.02	3	4762.63	115	5155.76	182	6175.42	196
3441.6464766.29995176.571816177.261033660.9424791.001155187.821616186.741883670.4344734.771595197.171766204.641853674.06354807.001565220.311316223.091863674.15714808.861605262.83130623.091873688.4154812.001365265.71142625.63.6923722.49384814.621225347.71147627.7.651173739.81694815.921375353.421146314.661033795.57734821.142085388.351146514.661033795.33694831.181285424.651446527.60933792.342483.17995452.251436573.28201383.169704845.171325452.2610673.22201383.80714855.411355494.89100673.22201383.83.0714855.411365464.10171638.67202385.8071490.441355494.891906421.52209395.5770491.2071285496.491006532.89109397.57714855.411365464.101716584.67202385.87	3624.73	2	4773.41	164	5157.99	128	6176.81	186
$  \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	3641. <b>64</b>	6	4786.29	99	5176.57	181	6177.26	103
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3664.09	4	4786.54	122	5179.14	175	6186.74	188
ST0.4.3         4         479.47         199         S197.17         176         G204.64         185           S674.15         71         4601.86         160         S262.31         131         G23.09         186           S684.4         5         4812.00         136         S262.83         130         G23.09         187           S72.49         38         4814.62         122         S347.71         147         G27.56         117           S73.63.16         69         481.52         177         S353.42         114         G72.65         200           S75.97         73         4829.03         137         S392.37         205         6522.17         204           S775.57         73         4829.03         137         S392.37         205         6522.17         204           S775.57         73         4829.03         137         S392.37         105         6542.60         111           S775.41         7         4832.64         122         5435.87         114         6544.60         111           S775.7         1         4852.64         150         577         616         6414.60         200           S81.67	3669.24	2	4791.00	115	5187.82	161	6198.65	206
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3670.43	4	4793 47	159	5197.17	176	6204.64	185
3674.15         71         400.86         100         5362.85         130         6230.05         197           3684.15         71         401.20         16         5362.857         142         635.85         92           3772.49         38         481.62         122         5347.71         147         677.76         117           3778.23         2         4817.82         208         5371.35         214         631.661         203           3779.23         7         4820.03         177         5392.37         205         6322.17         204           3775.57         73         4820.03         177         5392.37         205         6322.17         204           3772.34         2         4831.48         212         543.87         114         634.661         111           3772.34         2         483.17         193         5452.25         143         637.02.8         201           387.14         70         484.51         193         5452.26         171         637.22         210           383.8.0         71         4853.41         135         546.40         171         634.67         202           383.8.0	3674.06	35	4807.00	156	5220 31	131	6223.99	186
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3674.00	71	4808.86	160	5262.83	130	6230.09	187
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	30/4.13	/1 6	4000.00	136	5265 71	142	6256.36	07
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3088.41	5	4812.00	130	5205.71	142	0250.50	92
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3722.49	38	4814.02	122	5347.71	14/	02/1./0	117
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3736.81	69	4815.92	137	5353.42	114	62/2.65	200
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3739.23	2	4817.82	208	5371.33	214	6314.66	111
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3749.05	1	4821.14	208	5388.35	114	6316.61	203
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3775.57	73	4829.03	137	5392.37	205	6322.17	204
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3783.53	69	4831.18	128	5424.65	114	6327.60	93
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3792.34	2	4838.64	212	5435.87	114	6364.60	111
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	3793.61	4	4843.17	99	5452.85	143	6370.38	134
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3807.14	72	4843.51	193	5453.26	190	6375.22	210
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3831 69	70	4845.17	132	5462.49	171	6378.26	201
352.831 $452.54$ 136 $5475.57$ 161 $641.60$ 200 $3385.87$ 1 $4900.97$ 122 $5476.91$ 104 $6421.52$ 209 $3346.19$ 1 $4900.97$ 122 $5476.91$ 104 $6421.52$ 209 $3946.19$ 1 $4900.97$ 122 $5476.91$ 104 $6421.52$ 209 $4009.98$ 150 $4913.97$ 138 $5504.12$ 165 $6586.33$ 109 $4027.67$ 184 $4918.36$ 167 $5514.80$ 170 $6598.59$ 204 $4033.96$ 150 $4925.58$ 142 $537.11$ 169 $6633.15$ 213 $4093.62$ 1 $4937.34$ 131 $5578.72$ 96 $6661.39$ 202 $4295.88$ 168 $4945.46$ 149 $5589.38$ 178 $6772.36$ 134 $433.165$ 101 $4946.04$ 149 $5589.38$ 178 $6772.36$ 134 $433.165$ 101 $4976.16$ 129 $5623.33$ 199 $6914.56$ 106 $4431.57$ 157 $4976.57$ 128 $593.74$ 179 $6850.48$ 152 $4410.52$ 119 $4976.16$ 129 $5623.33$ 199 $6914.56$ 106 $4431.57$ 157 $4976.57$ 128 $5640.02$ 217 $700.54$ 109 $4450.46$ 148 $995.65$ 147 $5622.66$ 177 $703.442$ 121 $440.52$ 118 $4995.65$ 147 $5642.66$ 177 $703.442$ 121 </td <td>3932.97</td> <td>1</td> <td>4852 56</td> <td>136</td> <td>5468 10</td> <td>171</td> <td>6384 67</td> <td>202</td>	3932.97	1	4852 56	136	5468 10	171	6384 67	202
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3852.07	71	4052.50	136	5475 57	161	6414.60	200
388.57         1         490.41         122         346.57         104         64.1.2         20           3946.19         1         490.41         135         549.489         190         642.20         100           3973.55         70         4913.07         138         5504.12         165         6558.59         204           4009.98         150         4913.97         138         5504.12         165         6558.59         204           4033.96         150         4925.58         167         553.480         170         6598.59         204           4033.96         150         4925.88         167         553.69         112         6663.19         202           4295.88         168         4945.46         147         5587.87         114         677.77         102           4331.65         101         4946.04         149         5589.38         178         6773.52         131           4405.21         119         4976.16         129         5623.33         199         6914.56         106           4410.32         119         4976.16         129         5638.82         177         7001.54         109           4430.33	3838.30		4033.41	130	5475.01	104	6421 52	200
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3885.87	1	4900.97	122	5470.91	104	6492 90	205
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3946.19	1	4904.41	135	5494.89	190	0482.80	110
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3973.55	70	4912.03	128	5499.41	100	6532.89	109
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4009.98	150	4913.97	138	5504.12	165	6586.33	109
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4027.67	184	4918.36	167	5514.80	170	6598.59	204
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4035.96	150	4925.58	142	5537.11	169	6635.15	213
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4093.62	1	4935.83	167	5553.69	112	6643.64	92
4295.88168 $4945.46$ 147 $5587.87$ 114 $6767.77$ 102 $4331.65$ 101 $4946.04$ 149 $5589.38$ 178 $6772.36$ 134 $4382.87$ 183 $4955.20$ 128 $5592.28$ 112 $6642.07$ 133 $4401.54$ 118 $4967.55$ 142 $5593.74$ 179 $6850.48$ 152 $4410.52$ 119 $4976.16$ 129 $5623.33$ 199 $6914.56$ 106 $4431.03$ 194 $4976.35$ 97 $5637.12$ 197 $6973.52$ 216 $4437.57$ 157 $4976.71$ 208 $5638.82$ 177 $7001.54$ 109 $4450.13$ 168 $4980.17$ 129 $5641.88$ 192 $7030.06$ 133 $4462.46$ 118 $4995.85$ 147 $5642.66$ 177 $7034.42$ 121 $4470.48$ 118 $4996.85$ 146 $5643.10$ 211 $7062.97$ 109 $4513.00$ 162 $4998.23$ 128 $5664.02$ 215 $7110.91$ 108 $4519.99$ 100 $5003.75$ 99 $5695.00$ 198 $7197.02$ 106 $4553.18$ 139 $5010.96$ 146 $579.55$ 95 $7220.99$ 220 $4567.42$ 126 $5012.46$ 128 $5748.34$ 94 $7286.56$ 127 $4604.99$ 122 $5035.77$ 180 $5749.28$ 166 $7291.45$ 107 $4606.23$ 124 $5035.37$ 144 $5756.08$ 113 $7341.45$	4200.46	120	4937.34	131	5578.72	96	6661.39	202
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4295.88	168	4945.46	147	5587.87	114	6767.77	102
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4331.65	101	4946.04	149	5589.38	178	6772.36	134
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4382.87	183	4953.20	128	5592.28	112	6842.07	133
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4401.54	118	4967.55	142	5593.74	179	6850.48	152
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4410 52	119	4976 16	129	5625.33	199	6914.56	106
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4431.03	104	4976 35	97	5637 12	197	6973.52	216
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4427 57	157	4976 71	208	5638 82	177	7001 54	109
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4450 12	157	4970.71	1200	5641 88	197	7030.06	133
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4450.15	110	4700.17	147	5642.66	177	7034.42	121
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4402.40	110	4995.05	146	5642.00	211	7062.97	109
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	44 /0.48	118	4990.03	140	5045.10	211	7110.01	109
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4513.00	102	4998.23	120	5004.02	215	7110.91	122
4551.24       195       5003.75       99       5093.00       198       7197.02       106         4553.18       139       5010.96       146       5709.55       95       7220.79       220         4567.42       126       5012.46       128       5711.91       112       7261.93       106         4600.37       122       5017.58       128       5748.34       94       7286.56       127         4606.23       124       5035.37       144       5754.68       113       7327.67       141         4633.03       123       5039.37       145       5760.85       190       7381.94       219         4666.99       148       5048.85       174       5805.23       192       7385.24       116         4666.99       148       5048.85       174       5847.00       93       7401.13       218         4666.22       122       5080.53       144       5996.74       204       7422.30       140         4686.22       122       5080.53       144       5996.74       204       7422.30       140         4698.39       193       5081.11       173       6007.31       91       7488.73       1	4519.99	100	5000.34	14/	5082.20	191	7122.24	105
4553.18 $139$ $5010.96$ $146$ $509.53$ $95$ $7220.19$ $220$ $4567.42$ $126$ $5012.46$ $128$ $5711.91$ $112$ $7261.93$ $106$ $4600.37$ $122$ $5017.58$ $128$ $5748.34$ $94$ $7286.56$ $127$ $4604.99$ $122$ $5032.75$ $180$ $5749.28$ $166$ $7291.45$ $107$ $4606.23$ $124$ $5035.37$ $144$ $5754.68$ $113$ $7327.67$ $141$ $4633.03$ $123$ $5039.37$ $145$ $5760.85$ $190$ $7381.94$ $219$ $4648.66$ $122$ $5042.20$ $137$ $5805.23$ $192$ $7385.24$ $116$ $4666.99$ $148$ $5048.85$ $174$ $5847.00$ $93$ $7401.13$ $218$ $4675.64$ $132$ $5079.96$ $105$ $5892.88$ $113$ $7414.51$ $106$ $4698.39$ $193$ $5081.11$ $173$ $6007.31$ $91$ $7481.49$ $217$ $4701.34$ $125$ $5082.35$ $136$ $6025.73$ $207$ $7488.73$ $158$ $4711.42$ $122$ $5085.49$ $136$ $6025.73$ $207$ $7488.73$ $158$ $4711.42$ $122$ $5088.96$ $155$ $6039.31$ $203$ $7714.32$ $106$ $4715.78$ $122$ $5088.96$ $155$ $6086.29$ $204$ $7788.94$ $106$	4551.24	195	5003.75	99	5095.00	198	/19/.02	100
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4553.18	139	5010.96	140	5/09.55	95	1220.79	220
4600.37       122       5017.58       128       5748.34       94       7286.56       127         4604.99       122       5032.75       180       5749.28       166       7291.45       107         4606.23       124       5035.37       144       5754.68       113       7327.67       141         4633.03       123       5039.37       145       5760.85       190       7381.94       219         4648.66       122       5042.20       137       5805.23       192       7385.24       116         4666.99       148       5048.85       174       5847.00       93       7401.13       218         4656.22       122       5080.53       144       5996.74       204       7422.30       140         4698.39       193       5081.11       173       6007.31       91       7481.49       217         4701.34       125       5082.35       136       6025.73       207       7488.73       158         4701.54       193       5084.08       155       6039.31       203       7714.32       106         4714.42       122       5085.49       136       6053.68       201       7727.66 <td< td=""><td>4567.42</td><td>126</td><td>5012.46</td><td>128</td><td>5711.91</td><td>112</td><td>7261.93</td><td>106</td></td<>	4567.42	126	5012.46	128	5711.91	112	7261.93	106
4604.99       122       5032.75       180       5749.28       166       7291.45       107         4606.23       124       5035.37       144       5754.68       113       7327.67       141         4633.03       123       5039.37       145       5760.85       190       7381.94       219         4648.66       122       5042.20       137       5805.23       192       7385.24       116         4666.99       148       5048.85       174       5847.00       93       7401.13       218         4675.64       132       5079.96       105       5892.88       113       7414.51       106         4686.22       122       5080.53       144       5996.74       204       7422.30       140         4698.39       193       5081.11       173       6007.31       91       7481.49       217         4701.34       125       5082.35       136       6025.73       207       7488.73       158         4701.54       193       5084.08       155       6039.31       203       7714.32       106         4714.42       122       5085.49       136       6053.68       201       7727.66 <t< td=""><td>4600.37</td><td>122</td><td>5017.58</td><td>128</td><td>5748.34</td><td>94</td><td>7286.56</td><td>127</td></t<>	4600.37	122	5017.58	128	5748.34	94	7286.56	127
4606.231245035.371445754.681137327.671414633.031235039.371455760.851907381.942194648.661225042.201375805.231927385.241164666.991485048.851745847.00937401.132184675.641325079.961055892.881137414.511064686.221225080.531445996.742047422.301404698.391935081.111736007.31917481.492174701.341255082.351366025.732077488.731584701.541935084.081556039.312037714.321064714.421225085.491366053.682017727.661514715.781225088.961556086.292047788.94106	4604.99	122	5032.75	180	5749.28	166	7291.45	107
4633.031235039.371455760.851907381.942194648.661225042.201375805.231927385.241164666.991485048.851745847.00937401.132184675.641325079.961055892.881137414.511064686.221225080.531445996.742047422.301404698.391935081.111736007.31917481.492174701.341255082.351366025.732077488.731584701.541935084.081556039.312037714.321064714.421225085.491366053.682017727.661514715.781225088.961556086.292047788.94106	4606.23	124	5035.37	144	5754.68	113	7327.67	141
4648.661225042.201375805.231927385.241164666.991485048.851745847.00937401.132184675.641325079.961055892.881137414.511064686.221225080.531445996.742047422.301404698.391935081.111736007.31917481.492174701.341255082.351366025.732077488.731584701.541935084.081556039.312037714.321064714.421225085.491366053.682017727.661514715.781225088.961556086.292047788.94106	4633.03	123	5039.37	145	5760.85	190	7381.94	219
4666.991485048.851745847.00937401.132184675.641325079.961055892.881137414.511064686.221225080.531445996.742047422.301404698.391935081.111736007.31917481.492174701.341255082.351366025.732077488.731584701.541935084.081556039.312037714.321064714.421225085.491366053.682017727.661514715.781225088.961556086.292047788.94106	4648.66	122	5042.20	137	5805.23	192	7385.24	116
4675.641325079.961055892.881137414.511064686.221225080.531445996.742047422.301404698.391935081.111736007.31917481.492174701.341255082.351366025.732077488.731584701.541935084.081556039.312037714.321064714.421225085.491366053.682017727.661514715.781225088.961556086.292047788.94106	4666.99	148	5048.85	174	5847.00	93	7401.13	218
4686.22         122         5080.53         144         5996.74         204         7422.30         140           4698.39         193         5081.11         173         6007.31         91         7481.49         217           4701.34         125         5082.35         136         6025.73         207         7488.73         158           4701.54         193         5084.08         155         6039.31         203         7714.32         106           4714.42         122         5085.49         136         6053.68         201         7727.66         151           4715.78         122         5088.96         155         6086.29         204         7788.94         106	4675 64	132	5079.96	105	5892.88	113	7414.51	106
4698.39         193         5081.11         173         6007.31         91         7481.49         217           4701.34         125         5082.35         136         6025.73         207         7488.73         158           4701.54         193         5084.08         155         6039.31         203         7714.32         106           4714.42         122         5085.49         136         6053.68         201         7727.66         151           4715.78         122         5088.96         155         6086.29         204         7788.94         106	4686 22	122	5080 53	144	5996.74	204	7422.30	140
4036.39         173         5001.11         173         6007.13         71         71         711         711           4701.34         125         5082.35         136         6025.73         207         7488.73         158           4701.54         193         5084.08         155         6039.31         203         7714.32         106           4714.42         122         5085.49         136         6053.68         201         7727.66         151           4715.78         122         5088.96         155         6086.29         204         7788.94         106	4608 20	102	5081 11	173	6007 31	91	7481 49	217
4701.34       125       5062.35       136       6025.73       207       7466.73       136         4701.54       193       5084.08       155       6039.31       203       7714.32       106         4714.42       122       5085.49       136       6053.68       201       7727.66       151         4715.78       122       5088.96       155       6086.29       204       7788.94       106	4098.39	195	5082.25	126	6025 72	207	7499 72	158
4701.54         193         5084.08         155         6039.31         203         7714.32         106           4714.42         122         5085.49         136         6053.68         201         7727.66         151           4715.78         122         5088.96         155         6086.29         204         7788.94         106	4701.34	125	5082.35	150	6020.13	207	7714 22	106
4714.42         122         5085.49         136         6053.68         201         7721.66         151           4715.78         122         5088.96         155         6086.29         204         7788.94         106	4701.54	193	5084.08	155	0039.31	203	7719.32	161
4715.78         122         5088.96         155         6086.29         204         7788.94         106	4714.42	122	5085.49	136	0053.68	201	//2/.00	151
	4715.78	122	5088.96	155	6086.29	204	7788.94	100

For this spectrum, we provide data for 465 spectral lines and have utilized four data sources.¹⁻⁴ Huber and Sandeman¹ measured relative oscillator strengths by using the anomalous dispersion (hook) method and obtained data for a few additional, weak resonance lines by employing the absorption technique. They normalized their relative f-values to an absolute scale by using lifetime measurements of Becker et al.,5 who used the zerofield level-crossing (Hanle) technique. Doerr and Kock² performed emission as well as hook measurements to determine relative oscillator strengths. The emission work was done with a hollow cathode discharge and a Fourier transform spectrometer for the data acquisition. The hook measurements were made in a high-temperature furnace. The absolute scale of Ref. 2 is based on lifetime data of Becker et al.⁶ who employed selective laser excitation. Another source is the work of Lennard et al.,³ who measured branching ratios in emission with a hollow cathode discharge and then normalized these data to beam-foil lifetimes, which they also determined. In addition, we utilized the data of Kostyk,4 who derived log gf-values from solar spectra.

Our accuracy ratings for the data of Ref. 1 directly reflect the authors' own uncertainty estimates. The authors considered uncertainties in the relative values due primarily to measurement errors in the distance between line and hook, and also took into account the number of measurements taken, plus the uncertainty in the absolute scale as given by Ref. 5. The accuracies of the absolute log gf-values of Ref. 1 vary between 20 and 85 percent, but they are generally in the 25-30% range.

In their paper, Doerr and Kock separate their data into three distinct sets. Their "basic set" is emission Avalues (or branching ratios) which they have normalized directly to the lifetimes of Ref. 6. We view these data as being the most reliable presently available and have assigned accuracies of "C+." The second set contains hook measurements for lines originating from lower levels of the basic set. The final set comprises emission lines starting from the same upper level as lines measured by the hook method. Because of the additional normalizations required for the second and third sets of data, they are not as reliable as the first, and we have reduced the accuracies accordingly. Refs. 1 and 2 have 105 lines in common, and for 91 of these, the *f*-values agree within  $\pm 50$  percent. The situation for strong lines (log gf > -1.0) is even better — data for 85 percent of these lines agree within  $\pm 25$  percent.

The third data source included in this compilation is the experiment by Lennard et al.3 Their beam-foil lifetimes are, on the average, about 20 percent longer than those of Ref. 5. When Refs. 2 and 3 are compared, considerable scatter is present for weak lines, and the f-values of Lennard et al. are much lower (by about 50 percent) than those of Doerr and Kock. Because of likely cascade problems in the beam-foil measurements, we have renormalized the data of Ref. 3 to the lifetimes of Ref. 5 whenever possible. Lennard et al. also provided transition probabilities for lines arising from high-lying upper levels not measured by the authors of Refs. 5 or 6. Thus, in these cases, we had to rely on the somewhat less accurate beam-foil lifetimes of Ref. 3 for the absolute scale, and we have lowered the accuracy ratings accordingly.

Another source we utilized is the paper by Kostyk.⁴ This author determined log gf-values for 175 lines from the central intensities of solar Fe I lines. We compared Refs. 2 and 4 and found that the f-values for 11 of 15 overlapping lines agree within  $\pm$  52 percent. There are no apparent systematic trends or shifts in scale. However, because of saturation effects in the sun, Kostyk's f-values for stronger lines (log gf > -1.5) are probably not as reliable. We have therefore reduced the accuracies for these lines to "D-."

In this compilation, we have given first priority to either Ref. 1 or 2, depending largely on the authors' own error estimates. For lines not covered by either Ref. 1 or 2, we included the normalized (or unnormalized) data of Lennard *et al.* Finally, for the remaining (generally weak) lines, we tabulated the log gf-values of Kostyk.

#### References

¹ M. C. E. Huber and R. J. Sandeman, Astron. Astrophys. 86, 95 (1980).

- ² A. Doerr and M. Kock, J. Quant. Spectrosc. Radiat. Transfer 33, 307 (1985).
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- ⁶ U. Becker, H. Kerkhoff, M. Schmidt, and P. Zimmermann, J. Quant. Spectrosc. Radiat. Transfer 25, 339 (1981).

Ni I: Allowed transitions

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No.	Multiplet	λ (Å)	$egin{array}{c} E_i \ ({f cm}^{-1}) \end{array}$	$E_k$ (cm ⁻¹ )	<b>g</b> i	g.	A _{ki} (10 ⁸ s ⁻¹ )	fix	<i>S</i> (at. u.)	log gf	Accu- racy	Source
1.	a ³ F - z ⁵ D° (1)											
		3946.19 3749.05 3832.87 3885.87 4093.62	1332.2 0.0 1332.2 2216.5 1332.2	26666 26666 27415 27944 25754	7 9 7 5 7	7 7 5 3 9	$2.1(-6)^{a}$ $2.7(-4)$ $2.0(-4)$ $4.1(-5)$ $9.0(-7)$	$\begin{array}{r} 4.8(-7) \\ 4.4(-5) \\ 3.1(-5) \\ 5.5(-6) \\ 2.9(-7) \end{array}$	4.4(-5) 0.0049 0.0028 3.5(-4) 2.8(-5)	-5.47 -3.40 -3.66 -4.56 -5.69	C- C- C- C C	1 1 1 1 1
2.	a ³ F - z ⁵ G° (2)											
		3624.73 3739.23 3792.34 3561.75 3669.24 3498.19	0.0 1332.2 2216.5 0.0 1332.2 0.0	27580 28068 28578 28068 28578 28578	9 7 5 9 7 9	11 9 7 9 7 7	$\begin{array}{c} 0.0026\\ 0.0024\\ 3.8(-4)\\ 0.0029\\ 0.0020\\ 1.1(-5) \end{array}$	$\begin{array}{c} 6.2(-4) \\ 6.4(-4) \\ 1.2(-4) \\ 5.6(-4) \\ 4.0(-4) \\ 1.6(-6) \end{array}$	$\begin{array}{c} 0.067\\ 0.055\\ 0.0072\\ 0.059\\ 0.034\\ 1.7(-4) \end{array}$	-2.25 -2.35 -3.24 -2.30 -2.55 -4.84	C E D+ C D+ C-	2 1 2 2 2 1
3.	a ³ F - z ⁵ F° (3)											
		3502.60 3602.28 3620.02 3437.28 3507.69 3577.24 3351.06 3467.50	0.0 1332.2 2216.5 0.0 1332.2 2216.5 0.0 1332.2	28542 29084 29833 29084 29833 30163 29833 30163	9 7 5 9 7 5 9 7 5 9 7	11 9 7 9 7 5 7 5	$\begin{array}{c} 0.0015\\ 0.0044\\ 4.3(-5)\\ 0.044\\ 0.0024\\ 1.6(-4)\\ 2.8(-5)\\ 0.012\\ \end{array}$	$\begin{array}{c} 3.3(-4)\\ 0.0011\\ 1.2(-5)\\ 0.0079\\ 4.4(-4)\\ 3.0(-5)\\ 3.7(-6)\\ 0.0015\\ \end{array}$	0.034 0.092 7.0(-4) 0.80 0.036 0.0018 3.7(-4) 0.12	$\begin{array}{r} -2.53 \\ -2.11 \\ -4.23 \\ -1.15 \\ -2.51 \\ -3.82 \\ -4.48 \\ -1.98 \end{array}$	C C D+ C C D+ D+ C	2 2 1,2 2 2 2 2 1,2
4.	a ³ F - z ³ P° (4)											
		3670.43 3664.09 3793.61	1332.2 2216.5 2216.5	28569 29501 28569	7 5 5	5 3 5	0.0061 0.020 0.0018	8.8(-4) 0.0024 4.0(-4)	0.075 0.15 0.025	-2.21 -1.92 -2.70	D+ D+ D+	2 2 2
5.	a ³ F - z ³ F° (5)	3480.0	971.8	29699	21	21	0.066	0.012	2.9	-0.60	с	1,2,3n
		3391.04 3571.86 3519.76 3409.58 3413.48 3551.53 3688.41	0.0 1332.2 2216.5 0.0 1332.2 1332.2 2216.5	29481 29321 30619 29321 30619 29481 29321	9 7 5 9 7 7 5	9 7 5 7 5 9 7	0.066 0.052 0.041 0.0037 0.038 0.0016 0.0045	$\begin{array}{c} 0.011\\ 0.0099\\ 0.0076\\ 5.0(-4)\\ 0.0047\\ 3.9(-4)\\ 0.0013\\ \end{array}$	1.1 0.81 0.44 0.050 0.37 0.032 0.078	$\begin{array}{r} -0.99 \\ -1.16 \\ -1.42 \\ -2.35 \\ -1.48 \\ -2.56 \\ -2.19 \end{array}$	C C+ C C C E D+	1,2 1 1,2 1 3n 2
6.	a ³ F - (°) ^b	•										
		3369.56 3527.98 3641.64	0.0 1332.2 2216.5	29669 29669 29669	9 7 5	7 7 7	0.18 0.0042 8.4(-5)	$\begin{array}{c} 0.024 \\ 7.9(-4) \\ 2.3(-5) \end{array}$	2.4 0.064 0.0014		C C D+	1,2 2 2
7.	a ³ F - z ³ D° (6)											
		3500.85 3483.77 3612.74	1332.2 2216.5 2216.5	29889 30913 29889	7 5 5	5 3 5	0.046 0.14 0.042	0.0061 0.016 0.0081	0.49 0.89 0.48	-1.37 -1.11 -1.39	C C C	1,2 1 1

Ni I: Allowed transitions - Continued

No.	Multiplet	λ (Å)	$E_i$ (cm ⁻¹ )	$E_k$ (cm ⁻¹ )	<b>g</b> i	g.	$A_{ki}$ (10 ⁸ s ⁻¹ )	fik	S (at. u.)	log gf	Accu- racy	Source
8.	a ³ F - z ³ G° (7)	3310.9	971.8	31166	21	27	0.050	0.010	2.4	-0.66	С	1,2
		3232.93	0.0	30923	9	11	0.073	0.014	1.3	-0.90	с	1,2
		3371.99	1332.2	30980	7	9	0.026	0.0057	0.44	-1.40	C	1
		3226.98	2216.5	30980	9	9	0.0023	3.5(-4)	0.034	-1.54 -2.50	D	1
		3282.69	1332.2	31786	7	7	0.0060	9.7(-4)	0.073	-2.17	С	2
		3145.12	0.0	31786	9	7	2.1(-4)	2.4(-5)	0.0023	-3.66	D+	2
9.	$a {}^{3}\mathbf{F} - z {}^{1}\mathbf{F}^{\circ}$ (8)											
		3221.65	0.0	31031	9	7	0.016	0.0019	0.18	-1.76	с	1,2
		3366.16	1332.2	31031	7	7	0.040	0.0068	0.53	-1.32	D+	2
		3469.48	2216.5	31031	5	7	0.013	0.0032	0.18	-1.80	С	1
10.	$a {}^{3}F - z {}^{1}D^{\circ}$ (9)						1					
		3320.26	1332.2	31442	7	5	0.049	0.0058	0.45	-1.39	С	1,2
		3420.73	2216.5	31442	5	5	9.9(-4)	1.7(-4)	0.0098	-3.06	D+	2
11.	a ³ F - ³ F°	3104.8	971.8	33171	21	21	0.0390	0.00564	1.21	-0.927	C+	2
		3031.87	0.0	32973	97	9	0.017	0.0024	0.21	-1.67	C+	2
		3145.71	2216.5	33611	5	5	0.0080	0.0012	0.086	-2.08 -2.27	$C_+$	2
		3019.14	0.0	33112	9	7	0.064	0.0069	0.61	-1.21	C+	2
		3097.12	1332.2	33611	7	5	0.033	0.0033	0.24	-1.63	C+	2
		3159.52 3235.75	1332.2	32973	5	9	3.0(-4) 6.4(-4)	5.7(-5) 14(-4)	0.0041	-3.40 -3.15	C+ C+	2
									0.0010			-
12.	a ³ F - z ¹ P° (10)											
		3249.44	2216.5	32982	5	3	0.0041	3.9(-4)	0.021	-2.71	C+	2
13.	a ³ F - y ³ D [•] (12)	3035.8	971.8	33903	21	15	0.0603	0.00596	1.25	-0.903	С	2
		2984.13	0.0	33501	9	7	0.066	0.0069	0.61	-1.21	C+	2
		3045.01	1332.2	34163	7	5	0.028	0.0028	0.20	-1.71	C	2
		3105.46 3107 71	2216.5	34409 33501	5	3	0.071	0.0062 19(-4)	0.32	-1.51 -2.87	D+ C+	2
		3129.30	2216.5	34163	5	5	0.0053	7.8(-4)	0.040	-2.41	D+	2
		3195.57	2216.5	33501	5	7	0.0058	0.0012	0.065	2.21	C+	2
14.	a ³ F - z ¹ G [•] (13)											
		3099.11	1332.2	33590	7	9	0.021	0.0038	0.27	-1.57	C+	2
15.	a ³ F - y ¹ F [•] (uv 1)											
		2805.08	0.0	35639	9	7	0.0088	8.0(-4)	0.067	-2.14	с	2
		2914.01	1332.2	35639	7	7	0.0058	7.3(-4)	0.049	-2.29	C	2
		<b>29</b> 91.11	2216.5	35639	5	7	0.0012	2.3(-4)	0.011	-2.94	D+	2

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Ni I: Allowed transitions - Continued

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No.	Multiplet	λ (Å)	$E_i$ (cm ⁻¹ )	$E_{k}$ (cm ⁻¹ )	<b>g</b> i	₿k	$A_{ki}$ (10 ⁸ s ⁻¹ )	fik	<i>S</i> (at. u.)	log gf	Accu- racy	Source
16.	a ³ F - y ¹ D° (uv 2)											
		2834.55 2907.46	1332.2 2216.5	36601 36601	7 5	5 5	0.0066 0.020	5.7(-4) 0.0025	0.037 0.12	-2.40 -1.90	D+ D+	2 2
17.	a ³ F - ⁵ P°											
		2476.88 2553.37 2561.42	0.0 1332.2 1332.2	40361 40484 40361	9 7 7	7 5 7	0.026 0.0060 0.0037	0.0018 4.2(-4) 3.7(-4)	0.14 0.025 0.022	-1.78 -2.53 -2.59	C D D	1 1 1
18.	a ³ F - ³ F°											
		2347.51	0.0	42585	9	9	0.22	0.018	1.3	-0.78	D-	1
19.	<i>a</i> ³ F - ³ D°											
		2345.54 2419.31	0.0 1332.2	42621 42654	9 7	7 5	2.2 0.20	0.14 0.012	9.9 0.69	0.11 -1.06	C E	1 1
20.	a ³ F - ³ G°											
		2320.03 2325.79 2312.34	0.0 1332.2 1332.2	43090 44315 44565	9 7 7	11 9 7	6.9 3.5 5.5	0.69 0.37 0.44	47 20 24	0.79 0.41 0.49	C C C	1 1 1
21.	a ³ F - ³ F°											
		2274.66 2313.98 2267.55	1332.2 2216.5 1332.2	45281 45419 45419	7 5 7	7 5 5	0.052 5.0 0.080	0.0040 0.40 0.0044	0.21 15 0.23	-1.55 0.30 -1.51	D- E D-	1 1 1
		2321.38	2216.5	45281	5	7	5.6	0.63	24	0.50	E	
22.	a ³ F - ³ P°											
		2346.63	1332.2	43933	7	5	0.55	0.033	1.8	-0.64	<b>D</b> –	1
23.	a ³ F − (*) ^b											
		2289.98	0.0	43655	9	7	2.1	0.13	8.7	0.06	С	1
24.	a ³ F - ⁵ D*											
		2261.42	0.0	44206	9	7	0.091	0.0054	0.36	-1.31	C	1
25.	a ³ F − (*) ^b											
		2254.81 2324.65	0.0 1332.2	44336 44336	9 7	99	0.096 0.18	0.0073 0.019	0.49 1.0	-1.18 -0.88	C D-	1 1
26.	a ³ F - ³ D°											
		2317.16 23 <b>2</b> 9.96	1332.2 2216.5	44475 45122	75	5 3	3.8 5.3	0.22 0.26	12 9.9	0.18 0.11	C C	1
27.	a ³ F - x ³ P° (uv 15)											
		2212.15 2221.94	1332.2 2216.5	46523 47208	7 5	5 3	0.058 0.22	0.0031 0.0096	0.16 0. <b>3</b> 5	-1.67 -1.32	D– D	1 1

Ni I: Allowed transitions - Continued

No.	Multiplet	λ (Å)	$E_i$ (cm ⁻¹ )	$E_k$ (cm ⁻¹ )	gi	gk	$A_{ki}$ (10 ⁸ s ⁻¹ )	fik	<i>S</i> (at. u.)	log gf	Accu- racy	Source
28.	$a^{3}\mathbf{F} - v^{3}\mathbf{D}^{\circ}$											
	(44 10)	2125.62 2182.38	0.0 1332.2	47030 47139	9 7	7 5	0.051 0.13	0.0027 0.0068	0.17 0.34	$-1.62 \\ -1.32$	C C	1
29.	<i>a</i> ³ F - ¹ F°											
		2053.91 2111.73 2151.93	0.0 1332.2 2216.5	48672 48672 48672	9 7 5	7 7 7	0.0075 0.065 0.032	3.7(-4) 0.0043 0.0031	0.022 0.21 0.11	-2.48 -1.52 -1.81	D C C	1 1 1 1
30.	a ³ F - ³ F°											
		2052.04 2052.45 2109.79	0.0 1332.2 1332.2	48715 50039 48715	9 7 7	9 5 9	0.097 0.032 0.015	0.0061 0.0014 0.0013	0.37 0.068 0.063	-1.26 -2.00 -2.04	C C C	1 1 1
31.	<i>a</i> ³ F - ¹ D°											
		2089.09 2128.41	1332.2 2216.5	49185 49185	7 5	5 5	0.097 0.056	0.0045 0.0038	0.22 0.13	$-1.50 \\ -1.72$	D C	1 1
32.	<i>a</i> ³ F - ³ D°											
		2026.62 2025.40 2055.50 2082.87 2062.37	0.0 1332.2 2216.5 1332.2 2216.5	49328 50689 50851 49328 50689	9 7 5 7 5	7 5 3 7 5	0.24 0.23 0.33 0.085 0.046	0.012 0.010 0.013 0.0056 0.0030	0.70 0.47 0.43 0.27 0.10	-0.98 -1.15 -1.20 -1.41 -1.83	C D- C C E	1 1 1 1
33.	a ³ F - ( [•] ) ^b											
		1994.29	0.0	50143	9	7	0.057	0.0027	0.16	-1.62	с	1
34.	a ³ F - u ³ F* (uv 23)						a 1					
		1968.90 2007.69	0.0 1332.2	50790 51125	9 7	9 7	0.045 0.090	0.0026 0.0054	0.15 0.25	$-1.63 \\ -1.42$	C C	1 1
35.	a ³ D - z ⁵ D° (15)											
		3674.06	204.8	27415	7	5	0.0027	3.8(-4)	0.033	-2.57	<b>D</b> -	1
36.	a ³ D - z ⁵ G° (16)											
		3587.93 3609.31 3523.44	204.8 879.8 204.8	28068 28578 28578	7 5 7	9 7 7	0.0026 0.0059 0.0027	$\begin{array}{c} 6.5(-4) \\ 0.0016 \\ 5.1(-4) \end{array}$	0.054 0.097 0.041	-2.34 -2.09 -2.45	C C D+	1,2 1,2 2
37.	a ³ D - z ⁵ F° (17)											
		3461.66 3452.88 3513.93 3374.22 3413.94 3485.88 3337.01	204.8 879.8 1713.1 204.8 879.8 1713.1 204.8	29084 29833 30163 29833 30163 30392 30163	7 5 3 7 5 3 7	9 7 5 7 5 3 5	0.27 0.098 0.011 0.015 0.022 0.013 8.3(-5)	0.062 0.025 0.0033 0.0025 0.0038 0.0024 9.9(-6)	5.0 1.4 0.11 0.19 0.21 0.081 7.6(-4)	-0.36 -0.91 -2.01 -1.76 -1.72 -2.15 -4.16	C+ C+ C- C D+ C D+	1 1 1,2 2 1,2 2

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Ni I: Allowed transitions - Continued

No.	Multiplet	λ (Å)	<i>Ei</i> (cm ⁻¹ )	$E_{k}$ (cm ⁻¹ )	<b>g</b> i	g.	$A_{ki}$ (10 ⁸ s ⁻¹ )	fu	S (at. u.)	log <i>gf</i>	Accu- racy	Source
38.	$a^{3}D - z^{3}P^{\circ}$	3529.0	731.5	29060	15	9	1.1	0.13	22	0.28	C+	1,2
	(18)											
		3524.54	204.8	28569	7	5	1.0	0.13	11	-0.03	С	1,2
		3492.96	879.8	29501	5		0.98	0.11	6.2	-0.27	C+	
		3610.35	879.8	28569	5	5	0.072	0.071	2.5	-1.15	$C_{+}$	1
		3597.70	1713.1	29501	3	3	0.14	0.027	0.96	-1.09	č	1,2
		3722.49	1713.1	28569	3	5	0.0080	0.0028	0.10	-2.08	D+	2
39.	a ³ D - z ³ F° (19)	3451.2	731.5	29699	15	21	0.596	0.149	25.4	0.349	С	1,2
		3414.76	204.8	29481	7	9	0.55	0.12	9.8	-0.06	с	1
		3515.05	879.8	29321	5	7	0.42	0.11	6.4	-0.26	С	1,2
		3458.46	1713.1	30619		5	0.61	0.18	6.3	-0.26	C+	1
		3433.30	204.8	29321 30619	5	5	0.17	0.031	0.45	-1.89		12
		3286.94	204.8	30619	7	5	0.0047	5.4(-4)	0.041	-2.42	č	1,2
40.	a ³ D - ( °) ^b											
		3392.98	204.8	29669	7	7	0.24	0.041	3.2	-0.54	C+	1
		3472.55	879.8	29669	5	7	0.12	0.031	1.8	-0.81	C+	1
41.	a ³ D - z ³ D° (20)											
		3446.26	879.8	29889	5	5	0.44	0.078	4.4	-0.41	C+	1
		3423.71	1713.1	30913	3	3	0.33	0.058	2.0	-0.76	С	1,2
		3367.88	204.8	29889	7	5	0.0019	2.3(-4)	0.018	-2.79	D+	2
		3040.19	1/10.1	29009	0	Э	0.029	0.0090	0.31	-1.57	D+	2
42.	a ³ D - z ³ G° (21)											
		3248.46	204.8	30980	7	9	0.0047	9.7(-4)	0.072	-2.17	c	1
		3234.65	879.8	31786	5	7	0.020	0.0045	0.24	-1.65	С	1,2
		3165.51	204.8	31786	7	7	4.3(4)	6.5(-5)	0.0048	3.34	D+	2
43.	a ³ D - z ¹ F° (22)											
		3243.05	204.8	31031	7	7	0.048	0.0075	0.56	-1.28	С	1,2
		3315.66	879.8	31031	5	7	0.053	0.012	0.67	-1.21	C+	1
44.	a ³ D - z ¹ D° (23)											
		3200.42	204.8	31442	7	5	0.0028	3.1(-4)	0.023	-2.66	С	2
		3271.11	879.8	31442	5	5	0.0086	0.0014	0.075	-2.16	С	1,2
		3362.80	1713.1	31442	3	5	0.0021	5.9(-4)	0.020	-2.75	D+	2
45.	<i>a</i> ³ D - ³ F°	3081.8	731.5	33171	15	21	0.841	0.168	25.5	0.400	C+	2
		3050.82	204.8	32973	7	9	0.60	0.11	7.6	-0.12	C+	2
		3101.56	879.8	33112	5	7	0.63	0.13	6.4	-0.20	C+	2
		3134.11	1713.1	33611	3	5	0.73	0.18	5.5 2.8	-0.27		2
		3054.31	204.8	336112	5	5	0.40	0.056	2.8	-0.55	C+	2
		2992.59	204.8	33611	7	5	0.054	0.0052	0.36		C+	2

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Ni I: Allowed transitions - Continued

No.	Multiplet	λ (Å)	$E_i$ (cm ⁻¹ )	$E_k$ (cm ⁻¹ )	<b>g</b> i	g k	$egin{array}{c} {m A}_{ki} \ (10^8~{ m s}^{-1}) \end{array}$	fik	S (at. u.)	log gf	Accu- racy	Source
46.	$\begin{array}{c} a \ ^{3}\mathbf{D} - \mathbf{z} \ ^{1}\mathbf{P}^{*} \\ (24) \end{array}$											
		3114.12 3197.11	879.8 1713.1	32982 32982	5 3	3 3	0.058 0.029	0.0050 0.0044	0.26 0.14	$-1.60 \\ -1.88$	C+ C+	2 2
47.	a ³ D - y ³ D° (uv 24)	3013.8	731.5	33903	15	15	0.982	0.134	19.9	0.302	C–	1,2
		3002.48	204.8	33501	7	7	0.80	0.11	7.5	-0.12	C+	2
		3003.62	879.8	34163	5	5	0.69	0.094	4.6	-0.33	D-	1
		3057.64	1713.1	34409			1.0	0.14	4.3	-0.37	D-	1
		2943.91	204.8	34163	5	5	0.11	0.0099	0.67	-1.16	C	
		2981.65	879.8	33501	5	7	0.28	0.022	1.1	-0.95		2
		3080.75	1713.1	34163	3	5	0.087	0.021	0.63	-1.21	C C	1.2
48.	$a {}^{3}D - z {}^{1}G^{\circ}$											-,-
	()	2994.46	204.8	33590	7	9	0.087	0.015	1.0	-0.98	C+	2
49.	a ³ D - y ¹ F° (uv 25)											
		2821.29	204.8	35639	7	7	0.049	0.0058	0.38	-1.39	с	1,2
50.	$a {}^{3}D - y {}^{1}D^{\circ}$ (uv 26)											
		2746.74	204.8	36601	7	5	0.017	0.0013	0.084	-2.03	С	1,2
		2798.65	879.8	36601	5	5	0.058	0.0068	0.31	-1.47	С	1,2
		2865.50	1713.1	36601	3	5	0.018	0.0037	0.11	-1.95	С	2
51.	a ³ D - ³ F°											
		2348.73	204.8	42768	7	7	0.22	0.018	0.97	-0.90	Е	1
52.	a ³ D - ³ G°											
		2266.35	204.8	44315	7	9	0.023	0.0023	0.12	-1.80	D-	1
		2258.40 2253.57	879.8 204.8	44565 44565	5 7	7	0.081	0.0089	0.34	-1.35 -0.99	D- C	1
53.	a ³ D - ³ F°											
		2251.48	879.8	45281	5	7	0.040	0.0043	0.16	-1.67	D	1
		2287.32	1713.1	45419	3	5	0.18	0.024	0.55	-1.14	D-	1
		2244.46	879.8	45419	5	5	0.38	0.029	1.1	-0.84	С	1
54.	a ³ D - ( [•] ) ^b											
		2300.77	204.8	43655	7	7	0.75	0.060	3.2	-0.38	С	1
55.	a ³ D - ⁵ D°											
		2307.35 2271.95	879.8 204.8	44206 44206	5 7	777	0.16 0.050	0.017 0.0038	0.66 0.20	-1.06 -1.57	C C	1 1

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No.	Multiplet	λ (Å)	$E_i$ (cm ⁻¹ )	$E_{k}$ (cm ⁻¹ )	<b>g</b> i	g.	$A_{ki}$ (10 ⁸ s ⁻¹ )	fu	<i>S</i> (at. u.)	log gf	Accu- racy	Source
56.	<i>a</i> ³ D - ³ D°											
		2293.11 2302.97 2258.15 2259.56	879.8 1713.1 204.8 879.8	44475 45122 44475 45122	5 3 7 5	5 3 5 3	0.38 0.45 0.17 0.20	0.030 0.036 0.0094 0.0091	1.1 0.81 0.49 0.34	-0.82 -0.97 -1.18 -1.34	C C C C	1 1 1 1
57.	a ³ D - x ³ P° (uv 36)	2166.2	731.5	<b>46</b> 881	15	9	1.1	0.046	4.9	-0.16	C–	1
		2158.31 2157.83 2174.48 2190.22 2197.35 2230.96	204.8 879.8 1713.1 879.8 1713.1 1713.1	46523 47208 47687 46523 47208 46523	7 5 3 5 3 3	5 3 1 5 3 5	0.69 0.41 0.89 0.30 0.78 0.052	0.034 0.017 0.021 0.021 0.057 0.0065	1.7 0.60 0.45 0.77 1.2 0.14	$-0.62 \\ -1.07 \\ -1.20 \\ -0.97 \\ -0.77 \\ -1.71$	C C E C C E	1 1 1 1 1 1
58.	a ³ D - v ³ D° (uv 37)											
		2161.04 2129.96 2147.80 2166.15 2220.71	879.8 204.8 879.8 879.8 1713.1	47139 47139 47425 47030 47139	5 7 5 5 3	5 5 3 7 5	0.13 0.042 0.47 0.066 0.082	0.0089 0.0020 0.020 0.0065 0.010	0.32 0.099 0.69 0.23 0.22	-1.35 -1.85 -1.01 -1.49 -1.52	С С С С С С С	1 1 1 1 1
<b>59</b> .	a ³ D - ⁵ S°											
		2121.40 2152.23	204.8 879.8	47329 47329	7 5	5 5	0.28 0.032	0.014 0.0022	0.67 0.078	-1.02 -1.96	C C	1
60.	a ³D − ³ F°	2033.56	879.8	50039	5	5	0.030	0.0019	0.062	-2.03	D-	1
61.	a ³ D - w ³ P° (uv 40)											
		2059.92 2060.20 2064.39 2088.98	204.8 879.8 1713.1 879.8	48735 49403 50139 48735	7 5 8 5	5 3 1 5	0.21 0.23 0.40 0.042	0.0097 0.0087 0.0086 0.0028	0.46 0.30 0.17 0.095	-1.17 -1.36 -1.59 -1.86	D- E D- D-	1 1 1 1
62.	a ³ D - ¹ P°	2085.37	879.8	48818	5	3	0.077	0.0030	0.10	-1.82	с	1
63.	<i>a</i> ³ D - ¹ D°						:					
64	a ³ D - ¹ D°	2047.35	204.8	49033	7	5	0.18	0.0082	0.39	-1.24	С	1
04.	u D D	2069.52 2105.85	879.8 1713.1	49185 49185	5 3	5 5	0.11 0.030	0.0071 0.0033	0.24 0.069		D– C	1 1
65.	a ³ D - ³ D*					_			0.07	1.00	6	
		2007.01 2000.49 2063.42 2041.16	879.8 879.8 879.8 1713.1	50689 50851 49328 50689	5 5 3	5 3 7 5	0.17 0.054 0.050 0.032	0.010 0.0020 0.0045 0.0033	0.35 0.064 0.15 0.067	-1.28 -2.01 -1.65 -2.00	C C D– D–	1 1 1 1

Ni I: Allowed transitions - Continued

No.	Multiplet	λ (Å)	$E_i$ (cm ⁻¹ )	$E_k$ (cm ⁻¹ )	<b>g</b> i	g _k	$A_{ki}$ (10 ⁸ s ⁻¹ )	fik	<i>S</i> (at. u.)	log gf	Accu- racy	Source
66.	a ³ D - ( °) ^b											
		2001.83 2029.29	204.8 879.8	$50143 \\ 50143$	7 5	7 7	0.073 0.023	0.0044	0.20 0.065	$-1.51 \\ -2.01$	C C	1
67	$a^{3}D = r^{1}P^{\circ}$	2020.20			Ū			0.0020		2.02		-
01.	(uv 45)											
		2050.84	1713.1	50458	3	3	0.076	0.0048	0.098	-1.84	Е	1
68.	a ³ D - u ³ F° (uv 47)											
		1976.87	204.8	50790 51125	7	9	1.1	0.080	3.7	-0.25	C	1
		2014.25	1713.1	51125	3	5	0.83	0.005	1.9	-0.40  -0.55	c	1
		1963.85	204.8	51125	7	7	0.11	0.0064	0.29	-1.35	C	1
		1981.61	879.8	51344	5	5	0.13	0.0078	0.25	-1.41	C	1
69.	<i>a</i> ¹ D - <i>z</i> ⁵ F° (30)											
		3783.53 3736.81	3409.9 3409.9	29833 30163	5 5	7 5	$\begin{array}{c} 0.033\\ 0.014 \end{array}$	0.0098 0.0029	0.61 0.18	$-1.31 \\ -1.84$	C E	1
70.	a ¹ D - z ³ P° (31)											
		3973.55	3409.9	28569	5	5	0.0038	8.9(-4)	0.058	-2.35	D+	2
		3831.69	3409.9	29501	5	3	0.015	0.0020	0.13	-2.00	С	1
71.	$a {}^{1}D - z {}^{3}F^{\circ}$ (32)											
		3858.30 3674.15	3409.9 3409.9	29321 30619	5 5	7 5	0.069 0.020	0.021 0.0041	1.4 0.25	-0.97 -1.69	C D+	1 2
72.	<i>a</i> ¹ D - (°) ^b											
		3807.14	3409.9	29669	5	7	0.043	0.013	0.83	-1.18	с	1
73.	a ¹ D - z ³ D° (33)											
		3775.57	3409.9	29889	5	5	0.042	0.0089	0.56	-1.35	с	1
74.	a ¹ D - z ³ G° (34)											
		3523.07	3409.9	31786	5	7	4.4(-4)	1.2(-4)	0.0067	3.24	D+	2
75.	$a {}^{1}D - z {}^{1}F^{\circ}$ (35)	3619.39	3409.9	31031	5	7	0.66	0.18	11.0	-0.04	с	1,2
76.	<i>a</i> ¹ D - <i>z</i> ¹ D° (36)	3566.37	3409.9	31442	5	5	0.56	0.11	6.3	- 0.27	с	1
77.	<i>a</i> ¹ D - ³ F°											
		3365.76 3310.20	3409.9 3409.9	33112 33611	5 5	7 5	0.054 0.0012	0.013 2.0(-4)	0.72 0.011	$-1.19 \\ -3.01$	C+ C+	2 2

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No.	Multiplet	λ (Å)	$E_i$ (cm ⁻¹ )	<i>E</i> ^{<i>k</i>} (cm ⁻¹ )	gi	g.	$A_{ki}$ (10 ⁸ s ⁻¹ )	fik	<i>S</i> (at. u.)	log gf	Accu- racy	Source
78.	<i>a</i> ¹ D - <i>z</i> ¹ P° (37)	3380.57	3409.9	32982	5	3	1.3	0.14	7.5	-0.17	C+	2
79.	a ¹ D - y ³ D ^o (39)											
		3322.31 3250.74 3225.02	3409.9 3409.9 3409.9	33501 34163 34409	5 5 5	7 5 3	0.058 0.022 0.093	0.014 0.0035 0.0087	0.74 0.19 0.46	-1.17 -1.76 -1.36	C+ C C	2 2 1,2
80.	a ¹ D - y ¹ F* (40)	3101.88	3409.9	35639	5	7	0.49	0.098	5.0	-0.31	с	1
81.	a ¹ D - y ¹ D° (41)	3012.00	3409.9	36601	5	5	1.3	0.18	9.0	-0.04	с	1,2
82.	a 1D - 5P°											
		2696.48	3409.9	40484	5	5	0.014	0.0015	0.067	-2.12	D-	1
83.	<i>a</i> ¹ D - ³ F°	2540.02	8409.9	12768	5	7	0.026	0.0035	0.15	-176	D	1
84.	a ¹ D - w ³ P° (uv 59)	2010.02	0400.0	42100	J	•	0.020	0.0000	0.15	-10	5-	1
		2173.54	3409.9	49403	5	3	0.15	0.0065	0.23	-1.49	Е	1
85.	<i>a</i> ¹ D - ¹ P°	2201.59	3409.9	48818	5	3	0.73	0.032	1.1	-0.80	С	1
86.	<i>a</i> ¹ D - ¹ D°	2191.21	3409.9	49033	5	5	0.046	0.0033	0.12	-1.78	E	1
87.	a ¹ D – ¹ D°	2183.91	3409.9	49185	5	5	0.12	0.0089	0.32	-1.35	D	1
88.	$a {}^{1}D - {}^{3}D^{\circ}$											
		2114.43	3409.9	50689	5	5	0.097	0.0065	0.23	-1.49	C	1
89.	a ¹ D - x ¹ P° (uv 63)	2124.80	3409.9	50458	5	3	0.38	0.016	0.54	-1.11	С	1
90.	a ¹ D - u ³ F° (uv 65)											
		2095.13 2085.57	3409.9 3409.9	51125 51344	5 5	7 5	0.11 2.6	0.010 0.17	0.35 5.8	-1.30 -0.07	E D-	1 1
91.	b ¹ D - z ⁵ F° (42)											
		6128.99 6007.31	13521 13521	29833 30163	5 5	7 5	1.2(-4) 1.7(-4)	9.4(-5) 9.4(-5)	0.0094 0.0093	-3.33 -3.33	D+ D	2 4
92.	b ¹ D - z ³ P° (43)											
		6643.64 6256.36	13521 13521	28569 29501	5 5	5 3	0.0015 0.0019	0.0010 6.6(-4)	0.11 0.068	2.30 2.48	D D	3n 3n

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No.	Multiplet	λ	$E_i$	E _k	<b>g</b> i	g.	A _{ki}	fik	s	log gf	Accu-	Source
		(Å)	(cm ⁻¹ )	(cm ⁻¹ )			(10 ⁸ s ⁻¹ )		(at. u.)		racy	
93.	$b {}^{1}D - z {}^{3}F^{\circ}$ (44)											
		6327.60 5847.00	13521 13521	29321 30619	5 5	7 5	1.7(-4) 2.4(-4)	1.4(-4) 1.2(-4)	0.015 0.012	-3.15 -3.21	E D+	3n 2
94.	b ¹ D – z ³ D° (45)											
		6108.12 5748.34	13521 13521	29889 30913	5 5	5 3	0.0013 3.7(-4)	7.1(-4) 1.1(-4)	0.071 0.010	-2.45 3.26	D+ D	2 4
95.	<i>b</i> ¹ D - <i>z</i> ¹ F° (46)	5709.55	13521	31031	5	7	0.0020	0.0014	0.13	-2.17	D+	2
96.	b ¹ D - z ¹ D° (47)	5578.72	13521	31442	5	5	9.8(-4)	4.6(-4)	0.042	-2.64	D+	2
<b>97</b> .	<i>b</i> ¹ D – ³ F°											
		5102.97 4976.35	13521 13521	33112 33611	5 5	7 5	8.8(-4) 4.3(-4)	4.8(-4) 1.6(-4)	0.040 0.013	$-2.62 \\ -3.10$	C+ C+	2 2
98.	b ¹ D - z ¹ P* (48)	5137.08	13521	32982	5	3	0.0086	0.0020	0.17	-1.99	C+	2
<b>99</b> .	b ¹ D - y ³ D [•] (50)											
		5003.75 4843.17 4786.29	13521 13521 13521	33501 34163 34409	5 5 5	7 5 3	6.0(-4) 2.9(-4) 7.4(-4)	$\begin{array}{c} 3.2(-4) \\ 1.0(-4) \\ 1.5(-4) \end{array}$	0.026 0.0080 0.012	-2.80 -3.30 -3.12	C+ D+ D+	2 2 2
100.	b ¹ D - y ¹ F° (51)	4519.99	13521	35639	5	7	6.1(-4)	2.6(-4)	0.020	-2.88	D+	2
101.	b ¹ D - y ¹ D* (52)	4331.65	13521	36601	5	5	0.0056	0.0016	0.11	-2.10	D+	2
102.	a ¹ S - z ³ P° (57)											
		6767.77	14729	29501	1	3	0.0033	0.0068	0.15	-2.17	D	3n
103.	a ¹ S - z ³ D* (58)											
		6177.26	14729	30913	1	3	1.8(-4)	3.2(-4)	0.0064	-3.50	D	4
104.	a ¹ S - z ¹ P° (59)	5476.91	14729	32982	1	3	0.095	0.13	2.3	-0.89	C+	2
105.	a ¹ S - y ³ D° (60)											
		5079.96	14729	34409	1	3	0.0015	0.0018	0.030	-2.75	D+	2

Ni I: Allowed transitions - Continued

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No.	Multiplet	λ (Å)	$E_i$ (cm ⁻¹ )	$E_{k}$ (cm ⁻¹ )	<b>g</b> i	g.	$A_{ki}$ (10 ⁸ s ⁻¹ )	fu	<i>S</i> (at. u.)	log gf	Accu- racy	Source
									a <b>-</b> 4	1.00		
106.	$\begin{array}{c}a \ {}^{3}\mathbf{P}-z \ {}^{3}\mathbf{P}^{\bullet}\\(62)\end{array}$	7481.3	15697	29060	9	9	0.0029	0.0024	0.54	-1.66	D	3n,4
		7714.32	15610	28569	5	5	0.0014	0.0013	0.16	-2.20	D	3n
		7261.93	15734	29501	3	3	8.4(-4)	6.7(-4)	0.048	-2.70	E	3n
		7197.02 6914.56	15610	29501 30192	5	3	9.0(-4)	4.2(-4)	0.050	-2.68 -2.27	D	3n 4
	Ĩ	7788.94	15734	28569	3	5	8.4(-4)	0.0013	0.097	-2.42	D	3n
		7414.51	16017	29501	1	3	0.0011	0.0027	0.066	-2.57	E	3n
107.	a ³ P – z ³ F° (63)											
		7291.45	15610	29321	5	7	3.0(-4)	3.3(-4)	0.040	-2.78	Е	3n
108.	a ³ P - ( [•] ) ^b											
		7110.91	15610	29669	5	7	2.0(-4)	2.1(-4)	0.025	-2.98	D	4
109.	a ³ P - z ³ D° (64)											
		7062.97	15734	29889	3	5	8.5(-5)	1.1(4)	0.0074	-3.50	Е	3n
		7001.54	15610	29889	5	5	6.0(-5)	4.4(-5)	0.0050	-3.66	E	3n
		6532.89	15734	30913	5	3	2.1(-4)	8.1(-5)	0.0034	-3.39	D	4
110.	<i>a</i> ³ P - <i>z</i> ¹ F° (66)											
		6482.80	15610	31031	5	7	5.3(-4)	4.7(-4)	0.050	-2.63	Е	3n
111.	a ³ P - z ¹ D° (67)											
		6314.66 6364.60	15610 15734	31442 31442	53	55	0.0057 3.5(-5)	0.0034 3.6(-5)	0.35 0.0022	-1.77 -3.97	D E	3n 3n
112.	a ³ P - ³ F°											
			15010	00110			0.0010	0.0011	0.10	0.97		9
		5711.91	15610	33611	3	5	0.0010	9.0(-4)	0.10	-2.21 -2.57	C+ C+	2
		5553.69	15610	33611	5	5	2.5(-4)	1.2(-4)	0.011	- 3.23	C+	2
113.	<i>a</i> ³ P - <i>z</i> ¹ P° (68)											
		5754.68	15610	32982	5	3	0.0031	9.4(-4)	0.089	-2.33	C+	2
		5892.88	16017	32982	1	3	0.0029	0.0045	0.087	-2.30		Z
114.	a ³ P - y ³ D° (70)											
		5587.87	15610	33501	5	7	0.0022	0.0014	0.13	-2.14	C+	2
		5424.65	15734	34163	3	5	7.7(-4)	5.7(-4)	0.030	-2.77	D+	2
		5388.35	16017	34409 34163	5	5	1.3(-4)	5.5(-5)	0.046	-2.59	D+	2
		5353.42	15734	34409	3	3	0.0012	5.3(-4)	0.028	-2.80	D+	2
		I			1	1	I		I	I	i	I

Ni I: Allowed transitions - Continued

No.	Multiplet	λ (Å)	$E_i$ (cm ⁻¹ )	$E_k$ (cm ⁻¹ )	<b>g</b> i	gı	$A_{ki}$ (10 ⁸ s ⁻¹ )	f ik	<i>S</i> (at. u.)	log gf	Accu- racy	Source
115.	a ³ P – y ¹ D*											
	(71)											
		4762.63 4791.00	15610 15734	36601 36601	5 3	5 5	0.0022 2.3(-4)	7.6(-4) 1.3(-4)	0.060 0.0063	2.42 3.40	D+ D+	2 2
116.	a ¹ G - y ¹ F° (84)	7385.24	22102	35639	9	7	0.0019	0.0012	0.26	-1.97	D	4
117.	z ⁵ D° – $e$ ³ D											
		6271.76	26666	42606	7	7	5.8(-4)	3.4(-4)	0.050	-2.62	D	4
118.	z ⁵ D° - e ⁵ F (86)											
		4401.54	25754	48467	9	11	0.38	0.13	17	0.08	D	3
		4470.48 4462.46	27415 27944	49778 50346	5	7 5	0.19 0.17	0.080 0.084	5.9 3.7	$ -0.40 \\ -0.60$	D- D-	4 4
119.	z ⁵ D° – e ³ F (88)											
		4410.52	26666	49333	7	9	0.032	0.012	1.2	-1.08	D-	4
120.	z ⁵ D° - f ³ F (89)											
		4200.46	26666	50466	7	9	0.018	0.0062	0.60	-1.36	D-	4
121.	z ⁵ G° - e ³ D (97)											
		7034.42	28578	42790	7	5	0.0026	0.0014	0.23	-2.01	D	4
122.	z ⁵ G° – e ⁵ F (98)											
		4714.42	27261 27580	48467 49086	13	11	0.46	0.13	26 11	0.23	D D	3
		4604.99	28068	49778	9	7	0.23	0.057	7.8	-0.29	D-	4
		4600.37 4786 54	29013 27580	50745 48467	5	3	0.26	0.049	3.7 11		D-	4
		4756.52	28068	49086	9	9	0.15	0.051	7.2	-0.34	D-	4
		4715.78	28578	49778		7	0.20	0.065	7.1 9 5	-0.34	D-	4
		4000.22	29013	48467	9	11	0.14	0.040	0.32	-1.70	E E	4
i		4814.62	29013	49778	5	7	0.0086	0.0042	0.33	-1.68	D	4
123.	z ⁵ G° - e ³ G (99)											
		4740.17 4633.03	28068 27580	49159 49159	9 11	11 11	0.0034 7.8(-4)	0.0014 2.5(-4)	0.20 0.042	$-1.90 \\ -2.56$	E E	3 3
124.	z ⁵ G° - f ³ D (100)											
		4606.23	29013	50717	5	3	0.10	0. <b>020</b>	1.5	-1.00	D-	4

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Ni I: Allowed transitions - Continued

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| No. | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | ₿k | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fu | <i>S</i>
(at. u.) | log gf | Accu-
racy | Source |
|------|---|---|---|---|------------------------|------------------------|--|---|--------------------------------|---|---------------------------|-----------------------|
| 125. | z <sup>5</sup> G° – e <sup>3</sup> F
(101) | | | | | | | | | | | |
| | | 4701.34 | 28068 | 49333 | 9 | 9 | 0.020 | 0.0067 | 0.93 | -1.22 | D_ | 4 |
| 126. | z <sup>5</sup> G* - f <sup>3</sup> F
(102) | | | | | | | | | | | |
| | | 4567.42 | 28578 | 50466 | 7 | 9 | 0.0014 | 5.6(-4) | 0.058 | -2.41 | D | 4 |
| 127. | z <sup>5</sup> F° - e <sup>3</sup> D
(109) | | | | | | | | | | | |
| | | 7286.56 | 30392 | 44112 | 3 | 3 | 0.0025 | 0.0020 | 0.14 | -2.22 | D | 4 |
| 128. | z <sup>5</sup> F° – e <sup>5</sup> F
(111) | | | | | | | | | | | |
| | | 5017.58
4998.23
5012.46
4953.20
4912.03 | 28542
29084
29833
30163
30392 | 48467
49086
49778
50346
50745 | 11
9
7
5
3 | 11
9
7
5
3 | 0.20
0.049
0.11
0.12
0.15 | 0.076
0.018
0.041
0.043
0.053 | 14
2.7
4.8
3.5
2.6 | -0.08
-0.78
-0.54
-0.67
-0.80 | D
D-
D-
D-
D- | 3
4
4
4
4 |
| | | 4831.18
5157.99 | 29084
29084 | 49778
48467 | 9 | 11 | 0.16
0.0059 | 0.042
0.0029 | 6.0
0.44 | -0.42
-1.59 | D-
E | 4 |
| 129. | z <sup>5</sup> F° – e <sup>8</sup> G
(112) | | | | | | | | | | | |
| | | 4976.16
4980.17 | 29084
29084 | 49175
49159 | 9
9 | 9
11 | 0.013
0.19 | 0.0050
0.086 | 0.73
13 | -1.35
-0.11 | D–
D | 4
3 |
| 130. | z <sup>5</sup> F° – e <sup>3</sup> P | | | | | | | | | | | |
| | | 5262.83 | 30163 | 49159 | 5 | 5 | 5.7(-4) | 2.3(-4) | 0.020 | -2.93 | Е | 3 |
| 131. | z <sup>5</sup> F° – e <sup>3</sup> F
(114) | | | | | | | | | | | |
| | | 4937.34
5220.31 | 29084
30163 | 49333
49314 | 9
5 | 9
7 | 0.12
0.017 | 0.045
0.0098 | 6.6
0.84 | -0.39
-1.31 | D-
D- | 4
4 |
| 132. | z <sup>5</sup> F° – f <sup>3</sup> F
(115) | | | | | | | | | | | |
| | | 4675.64
4845.17 | 29084
29833 | 50466
50466 | 9
7 | 9
9 | 0.0062
0.0016 | 0.0020
7.2(-4) | 0.28
0.080 | -1.74
-2.30 | D
D | 4
4 |
| 133. | z <sup>3</sup> P° - e <sup>3</sup> D
(126) | | | | | | | | | | | |
| | | 7122.24
7030.06
6842.07 | 28569
28569
29501 | 42606
42790
44112 | 5
5
3 | 7
5
3 | 0.21
0.0050
0.016 | 0.22
0.0037
0.011 | 26
0.43
0.75 | 0.04
-1.73
-1.48 | D-
D
D- | 4
4
4 |
| 134. | z <sup>3</sup> P° - e <sup>1</sup> D
(127) | | | | | | | | | | | |
| | | 6370.38
6772.36 | 28569
29501 | 44263
44263 | 5
3 | 5
5 | 0.0038
0.030 | 0.0023
0.035 | 0.24
2.3 | -1.94
-0.98 | D
D- | 4
4 |

Ni I: Allowed transitions -- Continued

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| No. | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_{k}
(cm <sup>-1</sup>) | g i | Øk | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|------|---|---|---|---|-----------------------|-----------------------|--|--|----------------------------------|---|------------------|------------------|
| 135. | $z {}^{3}P^{\circ} - e {}^{3}S$
(129) | | | | | | | | | | | |
| | | 4904.41 | 28569 | 48953 | 5 | 3 | 0.62 | 0.14 | 11 | -0.17 | D- | 4 |
| 136. | z <sup>3</sup> P° - e <sup>3</sup> P
(130) | | | | | | | | | | | |
| | | 4855.41
5082.35
4852.56
4812.00
5085.49 | 28569
29501
28569
29501
29501 | 49159
49171
49171
50276
49159 | 5
3
5
3
3 | 5
3
3
1
5 | 0.57
0.25
0.080
0.095
0.017 | 0.20
0.096
0.017
0.011
0.011 | 16
4.8
1.4
0.52
0.55 | $\begin{array}{r} 0.00 \\ -0.54 \\ -1.07 \\ -1.48 \\ -1.48 \end{array}$ | D
D
D
E | 3
4
4
3 |
| 137. | z <sup>3</sup> P° - f <sup>3</sup> D
(131) | | | | | | | | | | | |
| | | 4829.03
5042.20
4815.92 | 28569
29501
28569 | 49272
49328
49328 | 5
3
5 | 7
5
5 | 0.19
0.14
0.0093 | 0.094
0.088
0.0032 | 7.4
4.4
0.26 | $-0.33 \\ -0.58 \\ -1.79$ | D-
D-
D | 4
4
4 |
| 138. | z <sup>3</sup> P° – e <sup>1</sup> P
(132) | | | | | | | | | | | |
| | | 4752.43
4913.97 | 29501
30192 | 50537
50537 | 3
1 | 3
3 | 0.20
0.22 | 0.067
0.23 | 3.1
3.8 | -0.70
-0.63 | D-
D- | 4 |
| 139. | z <sup>3</sup> P° – e <sup>1</sup> S
(135) | | | | | | | | | | | |
| 140. | z <sup>3</sup> F° – e <sup>3</sup> D | 4553.18 | 29501 | 51457 | 3 | 1 | 0.070 | 0.0073 | 0.33 | -1.66 | D | 4 |
| | (139) | 7422.30 | 29321 | 42790 | 7 | 5 | 0.18 | 0.10 | 18 | -0.14 | D | 4 |
| 141. | $z {}^{3}F^{\circ} - e {}^{1}D$ (140) | | | | | | | | | | | |
| 142. | $z^{3}F^{*} - e^{5}F$ | 7327.67 | 30619 | 44263 | 5 | 5 | 0.0042 | 0.0034 | 0.41 | -1.77 | D | 4 |
| | (141) | 5265.71
4925.58
4967.55 | 29481
29481
30619 | 48467
49778
50745 | 9
9
5 | 11
7
3 | 0.0037
0.059
0.024 | 0.0019
0.017
0.0054 | 0.29
2.5
0.44 | -1.77
-0.82
-1.57 | E
D-
D | 3
4
4 |
| 143. | $z {}^{3}F^{\circ} - e {}^{3}S$ | | | | | | | | | | | |
| | | 5452.85 | 30619 | 48953 | 5 | 3 | 0.016 | 0.0044 | 0.39 | -1.66 | D | 4 |
| 144. | z <sup>3</sup> F* - e <sup>3</sup> G
(143) | | | | | | | | | | | |
| | | 5080.53
5035.37 | 29481
29321 | 49159
49175 | 9
7 | 11
9 | 0.32
0.57 | 0.15
0.28 | 23
32 | 0.13
0.29 | D
D- | 3
4 |
| 145. | z <sup>3</sup> F° – e <sup>3</sup> P
(142) | | | | | | | | | | | |
| | | 5039.37 | 29321 | 49159 | 7 | 5 | 0.037 | 0.010 | 1.2 | -1.15 | Е | 3 |
Ni I: Allowed transitions - Continued

| No. | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | g. | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fu | S
(at. u.) | log gf | Accu-
racy | Source |
|---------------|---|--|----------------------------------|----------------------------------|------------------|------------------|--|------------------------------------|----------------------------|----------------------------------|------------------|------------------|
| 146. | $z^{3}F^{\circ} - f^{3}D$ (144) | | | | | | | | | | | |
| | (111) | 4996.85
5010.96 | 29321
29321 | 49328
49272 | 7
7 | 5
7 | 0.056
0.051 | 0.015
0.019 | 1.7
2.2 | -0.98
-0.87 | D-
D- | 4
4 |
| 147. | $z {}^{3}F^{\circ} - e {}^{3}F$
(145) | | | | | | | | | | | |
| | | 5000.34
4945.46
4995.65
5347.71 | 29321
30619
29321
30619 | 49314
50834
49333
49314 | 7
5
7
5 | 7
5
9
7 | 0.14
0.083
0.0078
0.0030 | 0.053
0.030
0.0038
0.0018 | 6.1
2.5
0.43
0.16 | -0.43
-0.82
-1.58
-2.04 | D
D
D
D | 4
4
4
4 |
| 148. | z <sup>3</sup> F° – f <sup>3</sup> F
(146) | | | | | | | | | | | |
| 149. | $z^{3}F^{\circ} - e^{1}F$
(148) | 4666.99 | 30619 | 52041 | 5 | 5 | 0.063 | 0.020 | 1.6 | -0.99 | D- | 4 |
| | | 4946.04 | 30619 | 50832 | 5 | 7 | 0.020 | 0.010 | 0.84 | -1.29 | D- | 4 |
| 150. | z <sup>3</sup> F° - g <sup>3</sup> F
(150) | | | | | | | | | | | |
| | | 4009.98
4035.96 | 29321
29481 | 54251
54251 | 7
9 | 7
7 | 0.0086
0.0048 | 0.0021
9.0(-4) | 0.19
0.11 | -1.84
-2.09 | E
E | 3
3 |
| 151. | (°) <sup>b</sup> – e <sup>3</sup> D | | | 10000 | | - | 0.11 | 0.007 | 17 | 0.17 | | |
| 1 52 . | (°) <sup>b</sup> - e <sup>1</sup> D | 7727.66 | 29669 | 42606 | | | 0.11 | 0.097 | 17 | -0.17 | D- | 4 |
| | | 6850.48 | 29669 | 44263 | 7 | 5 | 0.0023 | 0.0011 | 0.18 | -2.10 | D | 4 |
| 153. | (°) <sup>6</sup> – e <sup>3</sup> P | 5129.37 | 29669 | 49159 | 7 | 5 | 0.12 | 0.033 | 4.0 | -0.63 | D | 3 |
| 154. | (°) <sup>b</sup> - f <sup>3</sup> D | | | | | | | | | | | |
| 155 | (°) <sup>b</sup> - e <sup>3</sup> F | 5099.95 | 29669 | 49272 | 7 | 7 | 0.29 | 0.11 | 13 | -0.10 | D- | 4 |
| 100. | | 5084.08
5088.96 | 29669
29669 | 49333
49314 | 777 | 9
7 | 0.31
0.017 | 0.15
0.0065 | 18
0.77 | 0.03
-1.34 | D-
D- | 4 |
| 156. | (°) <sup>b</sup> - <i>f</i> <sup>8</sup> F | | | | | | | | | | | |
| 157. | (°) <sup>b</sup> − g <sup>3</sup> D | 4807.00 | 29669 | 50466 | 7 | 9 | 0.073 | 0.033 | 3.6 | -0.64 | D- | 4 |
| | | 4437.57 | 29669 | 52197 | 7 | 7 | 0.028 | 0.0082 | 0.84 | -1.24 | D | 4 |
| 158. | $z {}^{3}D^{\circ} - e {}^{1}D$
(157) | | | | | | | | | | | |
| | | 7488.73 | 30913 | 44263 | 3 | 5 | 0.0012 | 0.0017 | 0.13 | -2.29 | D | 4 |

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Ni I: Allowed transitions -- Continued

| No. | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | gi | g, | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | <i>S</i>
(at. u.) | log gf | Accu-
racy | Source |
|------|---|--------------------|------------------------------|------------------------------|--------------|-------------|--|-------------------------|----------------------|------------------|---------------|--------|
| | | | | | | | | | | | | |
| 159. | z <sup>3</sup> D° - e <sup>5</sup> F
(158) | | | | | | | | | | | |
| | | 4793.47 | 29889 | 50745 | 5 | 3 | 0.0062 | 0.0013 | 0.10 | -2.19 | D | 4 |
| 160. | z <sup>3</sup> D° - e <sup>3</sup> G
(160) | | | | | | | | | | | |
| | | 4808.86 | 29889 | 50678 | 5 | 7 | 0.016 | 0.0078 | 0.62 | -1.41 | D- | 4 |
| 161. | z <sup>3</sup> D° – e <sup>3</sup> P
(159) | | | | | | | | | | | |
| | | 5187.82
5475.57 | 29889
30913 | 49159
49171 | 5
3 | 5
3 | 0.0061
0.0059 | 0.0025
0.0026 | 0.21
0.14 | $-1.91 \\ -2.10$ | E
D | 3
4 |
| 162. | z <sup>3</sup> D° - f <sup>3</sup> F
(163) | | | | | | | | | | | |
| | | 4731.81
4513.00 | 30913
29889 | $52041 \\ 52041$ | 3
5 | 5
5 | 0.084
0.022 | 0.047
0.0068 | 2.2
0.50 | $-0.85 \\ -1.47$ | D-
D- | 4
4 |
| 163. | <i>z</i> <sup>3</sup> D° - <i>e</i> <sup>1</sup> P
(164) | | | | | | | | | | | |
| | | 5094.42 | 30913 | 50537 | 3 | 3 | 0.071 | 0.028 | 1.4 | -1.08 | D- | 4 |
| 164. | $z {}^{3}D^{\circ} - e {}^{1}F$
(167) | | | | | | | | | | | |
| | | 4773.41 | 29889 | 50832 | 5 | 7 | 0.012 | 0.0059 | 0.46 | -1.53 | D | 4 |
| 165. | z <sup>3</sup> G° – e <sup>5</sup> F
(175) | | | | | | | | | | | |
| | | 5504.12 | 30923 | 49086 | 11 | 9 | 0.0044 | 0.0016 | 0.32 | | D | 4 |
| 166. | <i>z</i> <sup>3</sup> G° – <i>e</i> <sup>3</sup> G
(176) | | | | | | * | | | | | |
| | | 5499.41
5749.28 | 30980
31786 | 49159
49175 | 9
7 | 11
9 | 6.2(-4)
0.0023 | 3.4(-4)
0.0015 | 0.056
0.19 | -2.51 - 1.99 | E
D | 3
4 |
| 167. | z <sup>3</sup> G° - f <sup>3</sup> F
(177) | | | | | | | | | | | |
| | | 5115.40
4918.36 | 30923
30980
31786 | 50466
51306
52041 | 11
9
7 | 9
7
5 | 0.22
0.23
0.24 | 0.071
0.064
0.064 | 13
9.3
7.2 | -0.11
-0.24 | D-
D- | 4 |
| 168. | z <sup>3</sup> G° – g <sup>3</sup> F
(178) | 4700.00 | 31700 | 92041 | 1 | Э | 0.24 | 0.004 | 1.0 | 0.35 | D- | 4 |
| | | 4295.88
4450.13 | 30980
31786 | 54251
54251 | 9
7 | 7
7 | 0.17
0.0082 | 0.037
0.0024 | 4.7
0.25 | $-0.48 \\ -1.77$ | D
E | 3
3 |
| 169. | <i>z</i> <sup>1</sup> F° - <i>e</i> <sup>5</sup> F
(188) | | | | | | | | | | | |
| | | 5537.11 | 31031 | 49086 | 7 | 9 | 0.0015 | 9.0(-4) | 0.12 | -2.20 | D | 4 |

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| F-2 | 25 |
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Ni I: Allowed transitions - Continued

| No. | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | g i | g | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fu | <i>S</i>
(at. u.) | log gf | Accu-
racy | Source |
|------|---|--------------------|------------------------------|------------------------------|------------|--------|--|------------------|----------------------|----------------|---------------|--------|
| 170. | $z^{1}F^{\circ} - e^{3}P$ | | | | | | | | | | | |
| | (100) | 5514.80 | 31031 | 49159 | 7 | 5 | 0.0045 | 0.0015 | 0.19 | -1.99 | Е | 3 |
| 171. | z <sup>1</sup> F° - e <sup>3</sup> F
(192) | | | | | | | | | | | |
| | | 5462.49
5468.10 | 31031
31031 | 49333
49314 | 7
7 | 9
7 | 0.029
0.0078 | 0.017
0.0035 | 2.1
0.44 | -0.93
-1.61 | D–
D | 4 |
| 172. | z <sup>1</sup> F° – f <sup>3</sup> F
(193) | | | | | | | | | | | |
| | | 4758.42 | 31031 | 52041 | 7 | 5 | 0.0046 | 0.0011 | 0.12 | -2.11 | D | 4 |
| 173. | <i>z</i> <sup>1</sup> F <sup>•</sup> - <i>e</i> <sup>1</sup> G
(194) | 5081.11 | 31031 | 50706 | 7 | 9 | 0.57 | 0.29 | 33 | 0.30 | D- | 4 |
| 174. | z <sup>1</sup> F* – e <sup>1</sup> F
(195) | 5048.85 | 31031 | 50832 | 7 | 7 | 0.16 | 0.060 | 6.9 | -0.38 | D- | 4 |
| 175. | $z {}^{1}D^{\circ} - e {}^{5}F$
(202) | | | | | | | | | | | |
| | | 5179.14 | 31442 | 50745 | 5 | 3 | 0.028 | 0.0068 | 0.58 | -1.47 | D- | 4 |
| 176. | $z {}^{1}D^{\circ} - e {}^{3}G$ (204) | | | | | | | | | | | |
| | | 5197.17 | 31442 | 50678 | 5 | 7 | 0.023 | 0.013 | 1.1 | -1.19 | D- | 4 |
| 177. | $z {}^{1}D^{\circ} - e {}^{3}P$ (203) | | | | | | | | | | | |
| | | 5642.66
5638.82 | 31442
31442 | 49159
49171 | 5
5 | 5
3 | 0.0040
0.013 | 0.0019
0.0038 | 0.18
0.35 | -2.02
-1.72 | E
D | 3
4 |
| 178. | $z {}^{1}D^{\circ} - f {}^{3}D$
(205) | | | | | | | | | | | |
| | | 5589.38 | 31442 | 49328 | 5 | 5 | 0.031 | 0.014 | 1.3 | -1.14 | D- | 4 |
| 179. | $z {}^{1}D^{\circ} - e {}^{3}F$
(206) | | | | | | | | 5 | | | |
| | | 5593.74
5155.14 | 31442
31442 | 49314
50834 | 5
5 | 75 | 0.044
0.11 | 0.029
0.045 | 2.7
3.8 | -0.84
-0.65 | D
D | 4 |
| 180. | $z {}^{1}D^{\circ} - f {}^{3}F$ (207) | | | | | | | | | | | |
| | | 5032.75 | 31442 | 51306 | 5 | 7 | 0.020 | 0.011 | 0.89 | -1.27 | D- | 4 |
| 181. | $z {}^{1}D^{\circ} - f {}^{1}D$
(209) | 5176.57 | 31442 | 50754 | 5 | 5 | 0.18 | 0.073 | 6.2 | -0.44 | D- | 4 |
| 182. | $\begin{array}{c} z \ {}^{1}\mathrm{D}^{\circ} - e \ {}^{1}\mathrm{F} \\ (210) \end{array}$ | 5155.76 | 31442 | 50832 | 5 | 7 | 0.29 | 0.16 | 14 | -0.09 | D- | 4 |
| 183. | z <sup>1</sup> D° – g <sup>3</sup> F | | | | | | | | | | | |
| | | 4382.87 | 31442 | 54251 | 5 | 7 | 0.015 | 0.0060 | 0.44 | -1.52 | Е | 3 |

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Ni I: Allowed transitions - Continued

| No. | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | $\frac{E_k}{(\mathrm{cm}^{-1})}$ | g i | g. | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|---------------|---|--------------------|------------------------------|----------------------------------|------------|---------|--|----------------|---------------|----------------|---------------|--------|
| | | | | | | | | | | | | |
| 184. | $z {}^{1}D^{\circ} - g {}^{1}F$ | 4027.67 | 31442 | 56263 | 5 | 7 | 0.13 | 0.046 | 3.0 | -0.64 | D | 4 |
| 185. | <sup>3</sup> F° – <i>e</i> <sup>5</sup> F | | | | | | | | | | | |
| | | 6204.64 | 32973 | 49086 | 9 | 9 | 0.014 | 0.0082 | 1.5 | -1.13 | D | 4 |
| 186. | ${}^{3}F^{\circ} - e^{-3}G$ | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | 6176.81
6223.99 | 32973
33112 | 49159
49175 | 97 | 11
9 | 0.047
0.020 | 0.033
0.015 | 6.0
2.1 | -0.53
-0.99 | D
D- | 3
4 |
| 187. | ${}^{3}F^{\circ} - e^{-3}P$ | | | | | | | | | | | |
| | | | | | | | | | | | _ | |
| | | 6230.09 | 33112 | 49159 | 7 | 5 | 0.019 | 0.0079 | 1.1 | -1.26 | E | 3 |
| 188. | ${}^{3}F^{\circ} - f^{3}D$ | | | | | | | | | | | |
| | | 6133.95 | 32973 | 49272 | 9 | 7 | 0.0037 | 0.0016 | 0.30 | -1.83 | D | 4 |
| | | 6186.74 | 33112 | 49272 | 7 | 7 | 0.027 | 0.016 | 2.2 | -0.96 | D- | 4 |
| 189. | ${}^{3}F^{\circ} - e {}^{3}F$ | | | | | ł | | | | | | |
| | | | 00070 | 10000 | | | 0.007 | | | | _ | |
| | | 6111.06 | 32973 | 49333 | 9 | 9 | 0.027 | 0.015 | 2.7 | -0.87 | D- | 4 |
| 190. | ${}^{3}F^{\circ} - f^{3}F$ | | | | | | | | | | | |
| | | 5494.89 | 33112 | 51306 | 7 | 7 | 0.022 | 0.0099 | 1.3 | -1.16 | D- | 4 |
| | | 5453.26 | 32973 | 51306 | 9 | 7 | 0.010 | 0.0036 | 0.58 | -1.49 | D- | 4 |
| | | 5760.85 | 33112 | 50466 | 1 | 9 | 0.035 | 0.023 | 3.0 | -0.80 | D- | 4 |
| 191. | ${}^{3}F^{\circ} - e {}^{1}G$ | | | | | | | | | | | |
| | | 5682.20 | 33112 | 50706 | 7 | 9 | 0.078 | 0.048 | 6.3 | -0.47 | D- | 4 |
| 100 | 3129 - 112 | | | | | | | | | | | |
| 192. | F - e F | | | | | | | | | | | |
| | | 5641.88
5805.23 | 33112
33611 | 50832 | 7 | 7 | 0.025 | 0.012 | 1.6 | -1.07 | D- | 4 |
| | | 0000.20 | 33011 | 00002 | 1 3 | ' | 0.005 | 0.040 | 4.4 | -0.64 | D – | 4 |
| 193. | $^{3}\mathbf{F}^{\circ} - g \ ^{3}\mathbf{F}$ | | | | | | | | | | | |
| | | 4701.54 | 32973 | 54237 | 9 | 9 | 0.14 | 0.045 | 6.3 | -0.39 | D | 4 |
| | | 4729.28 | 33112
32973 | 54251
54251 | 9 | | 0.027 | 0.0090 | 0.98 | -1.20 | E | 3 |
| | | 4732.47 | 33112 | 54237 | 7 | 9 | 0.093 | 0.040 | 4.4 | -0.55 | D- | 4 |
| | | 4843.51 | 33611 | 54251 | 5 | 7 | 0.044 | 0.021 | 1.7 | -0.97 | D | 3 |
| 1 94 . | <sup>3</sup> F° - f <sup>3</sup> G | | | | | | | | | | | |
| | | 4431.03 | 33611 | 56173 | 5 | 7 | 0.041 | 0.017 | 1.2 | -1.07 | D- | 4 |
| 105 | 3778 6177 | | | | | | | | | | | |
| 195. | $\mathbf{F}^{*} - f^{*}\mathbf{F}'$ | | | | | | | | | | | |
| | | 4551.24 | 33611 | 55577 | 5 | 7 | 0.061 | 0.026 | 2.0 | -0.88 | D- | 4 |
| 1 96 . | $z^{1}P^{\circ} - e^{3}P$ (217) | | | | | | | | | | | |
| | (211) | | | | | | | | | | | |
| | | 6175.42 | 32982 | 49171 | 3 | 3 | 0.17 | 0.098 | 6.0 | -0.53 | D- | 4 |

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Ni I: Allowed transitions - Continued

| No. | Multiplet | λ
(Å) | $\frac{E_i}{(\mathrm{cm}^{-1})}$ | E_k (cm <sup>-1</sup>) | gi | gı | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | <i>S</i>
(at. u.) | log gf | Accu-
racy | Source |
|------|---|--|----------------------------------|----------------------------------|------------------|------------------|--|-----------------------------------|--------------------------|------------------------------|----------------------|------------------|
| 197. | $z^{1}P^{\circ} - f^{3}D$
(218) | | | | | | | | | | | |
| | | 5637.12 | 32982 | 50717 | 3 | 3 | 0.11 | 0.050 | 2.8 | -0.82 | D- | 4 |
| 198. | $z {}^{1}P^{\circ} - e {}^{1}P$
(220) | 5695.00 | 32982 | 50537 | 3 | 3 | 0.17 | 0.082 | 4.6 | -0.61 | D | 4 |
| 199. | $z {}^{1}P^{\circ} - f {}^{1}D$ (221) | 5625.33 | 32982 | 50754 | 3 | 5 | 0.084 | 0.067 | 3.7 | -0.70 | D- | 4 |
| 200. | y <sup>3</sup> D° – e <sup>5</sup> F
(244) | | | | | | | | | | | |
| | | 6414.60
6272.65
6119.78 | 33501
34409
34409 | 49086
50346
50745 | 7
3
3 | 9
5
3 | 0.011
0.0059
0.027 | 0.0086
0.0058
0.015 | 1.3
0.36
0.90 | 1.22
1.76
1.35 | D-
D
D- | 4
4
4 |
| 201. | y <sup>3</sup> D° - e <sup>3</sup> G
(247) | | | | | | | | | | | |
| | | 6378.26
6053.68 | 33501
34163 | 49175
50678 | 7
5 | 9
7 | 0.023
0.022 | 0.018
0.017 | 2.7
1.7 | -0.89
-1.07 | D-
D- | 4
4 |
| 202. | y <sup>3</sup> D° – e <sup>3</sup> P
(246) | | | | | | | | | | | |
| | | 6384.67
6661.39 | 33501
34163 | 49159
49171 | 7
5 | 5
3 | 0.024
0.013 | 0.011
0.0054 | 1.6
0.59 | -1.13
-1.57 | E
D | 3
4 |
| 203. | y <sup>3</sup> D° - f <sup>3</sup> D
(248) | | | | | | | | | | | |
| | | 6130.17
6316.61
6039.31 | 34409
33501
34163 | 50717
49328
50717 | 3
7
5 | 3
5
3 | 0.065
0.0042
0.0057 | 0.037
0.0018
0.0019 | 2.2
0.26
0.19 | -0.96
-1.90
-2.03 | D–
D
D | 4
4
4 |
| 204. | y <sup>3</sup> D° - e <sup>3</sup> F
(249) | | | | | | | | | | | |
| | | 6598.59
6086.29
6322.17
5996.74 | 34163
34409
33501
34163 | 49314
50834
49314
50834 | 5
3
7
5 | 7
5
7
5 | 0.023
0.11
0.016
0.032 | 0.021
0.098
0.0097
0.017 | 2.8
5.9
1.4
1.7 | 0.98
0.53
1.17
1.06 | D-
D-
D-
D- | 4
4
4
4 |
| 205. | y <sup>3</sup> D° - f <sup>8</sup> F
(250) | | | | | | | | | | | |
| | 9700 ID | 5392.37 | 33501 | 52041 | 7 | 5 | 0.022 | 0.0068 | 0.85 | -1.32 | D- | 4 |
| 206. | y °D' – e 'P | 6105.78 | 34163 | 50537 | 5 | 3 | 0.0058 | 0.0020 | 0.20 | -2.01 | D | 4 |
| 207. | $y^{3}D^{\circ} - f^{1}D$ | 6198.65 | 34409 | 50537 | 3 | 3 | 0.0046 | 0.0026 | 0.10 | -2.10 | U | 4 |
| | (201) | 6025.73 | 34163 | 50754 | 5 | 5 | 0.0064 | 0.0035 | 0.34 | -1.76 | D | 4 |

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Ni I: Allowed transitions - Continued

| No. | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | $\frac{E_k}{(\mathrm{cm}^{-1})}$ | gi | g∗ | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|--------------|--|-------------------------------|------------------------------|----------------------------------|-------------|-------------|--|--------------------------|--------------------|-------------------------|---------------|-------------|
| 208. | y <sup>3</sup> D* – g <sup>3</sup> F
(254) | | | | | | | | | | | |
| | | 4821.14
4976.71
4817.82 | 33501
34163
33501 | 54237
54251
54251 | 7
5
7 | 9
7
7 | 0.045
0.016
0.070 | 0.020
0.0083
0.024 | 2.2
0.68
2.7 | -0.85
-1.38
-0.77 | D
E
D | 4
3
3 |
| 209. | z <sup>1</sup> G° – e <sup>3</sup> G
(258) | | | | | | | | | | | |
| | | 6421.52 | 33590 | 49159 | 9 | 11 | 0.0074 | 0.0056 | 1.1 | -1.30 | Е | 3 |
| 210. | z <sup>1</sup> G° - f <sup>3</sup> D | | | | | | | | | | | |
| | | 6375.22 | 33590 | 49272 | 9 | 7 | 0.0020 | 9.7(-4) | 0.18 | -2.06 | D | 4 |
| 211. | z <sup>1</sup> G° - f <sup>3</sup> F
(259) | | | | | | | | | | | |
| | | 5643.10 | 33590 | 51306 | 9 | 7 | 0.017 | 0.0064 | 1.1 | -1.24 | D- | 4 |
| 212. | z <sup>1</sup> G° - g <sup>3</sup> F
(260) | | | | | | | | | | | |
| | | 4838.64 | 33590 | 54251 | 9 | 7 | 0.22 | 0.060 | 8.6 | -0.27 | D | 3 |
| 213. | y <sup>1</sup> F° - e <sup>1</sup> G
(264) | 6635.15 | 35639 | 50706 | 7 | 9 | 0.025 | 0.022 | 3.3 | -0.82 | D- | 4 |
| 214. | γ <sup>1</sup> F° – g <sup>3</sup> F | | | | | | | | | | | |
| | | 5371.33 | 35639 | 54251 | 7 | 7 | 0.16 | 0.070 | 8.7 | 0.31 | D | 3 |
| 215. | y <sup>1</sup> D° - g <sup>3</sup> F
(272) | | | | | | | | | | | |
| | | 5664.02 | 36601 | 54251 | 5 | 7 | 0.11 | 0.074 | 6.9 | -0.43 | D | 3 |
| 216. | <sup>3</sup> F° - <i>i</i> <sup>3</sup> D | | | | | | | | | | | |
| | | 6973.52 | 42768 | 57104 | 7 | 7 | 0.025 | 0.018 | 3.0 | -0.89 | D- | 4 |
| 217 | <sup>3</sup> С° <i>– е</i> <sup>3</sup> Н | | | | | | | | | | | |
| 211. | u t n | 7491 40 | 44915 | 57070 | | 1.1 | 0.070 | 0.079 | 10 | 0.10 | D | |
| | 0 | 1481.49 | 44010 | 01010 | 9 | 11 | 0.070 | 0.072 | 10 | -0.19 | D- | 4 |
| 218. | <sup>3</sup> F° – <i>i</i> <sup>3</sup> F | | | | | | | | | | | |
| | | 7401.13 | 43259 | 56767 | 9 | 9 | 0.089 | 0.073 | 16 | -0.18 | D- | 4 |
| 219 . | ³F° − g <sup>3</sup> G | | | | | | | | | | | |
| | | 7381.94 | 43259 | 56802 | 9 | 11 | 0.097 | 0.097 | 21 | -0.06 | D- | 4 |
| 220. | ${}^{3}\mathbf{F}^{\circ} - i \; {}^{3}\mathbf{D}$ | | | | | | | | | | | |
| | | 7220.79 | 43259 | 57104 | 9 | 7 | 0.058 | 0.035 | 7.5 | -0.50 | D- | 4 |

<sup>a</sup> The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied. <sup>b</sup> The LS-coupling designation of this term was not provided in the NBS energy level compilation (J. Sugar and C. Corliss, J. Phys. Chem. Ref. Data 14, Suppl. 2 (1985)), so we have accordingly omitted it from this work.

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Forbidden Transitions

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|
| 1077.0 | 10 | 0.07.70 | | 7464.00 | | 01101 | 0 |
| 1977.2 | 13 | 6437.70 | 11 | 7464.39 | 4 | 31191 | 8 |
| 2030.2 | 6 | 6489.61 | 11 | 7507.44 | 9 | 39513 | 8 |
| 2080.6 | 18 | 6604.30 | 11 | 7908.30 | 9 | 45182 | 20 |
| 2635.2 | 22 | 6730.25 | 11 | 7929.70 | 16 | 47868 | 20 |
| 2788.8 | 24 | 6787.00 | 11 | 7989.9 | 3 | 58917 | 8 |
| 2798.5 | 24 | 6941.63 | 4 | 8111.97 | 16 | 75046 | 1 |
| 4523.16 | 5 | 7002.02 | 4 | 8194.57 | 16 | 82794 | 19 |
| 4565.4 | 12 | 7130.24 | 11 | 8201.77 | 2 | 113040 | 1 |
| 4710.7 | 12 | 7193.97 | 11 | 8466.38 | 9 | 119980 | 7 |
| 4813.27 | 5 | 7218.7 | 10 | 8832.31 | 15 | 148100 | 7 |
| 5027.34 | 5 | 7243.99 | 4 | 8843.42 | 2 | 352890 | 23 |
| 5348.3 | 17 | 7393.71 | 2 | 9887.18 | 14 | 805210 | 23 |
| 6404.46 | 4 | 7395.79 | 4 | 11650 | 21 | | |

List of tabulated lines

For this spectrum, we have utilized the work by Garstang,<sup>1</sup> who calculated M1 and E2 transition probabilities for lines arising from the three lowest configurations: $3d^84s^2$, $3d^94s$, and $3d^{10}$. Garstang included limited configuration interaction in his calculations. As is usually the case, the data for electric quadrupole transitions are

expected to be less accurate than those for magnetic dipole transitions.

Reference

<sup>1</sup>R. H. Garstang, J. Res. Nat. Bur. Stand., Sect. A 68, 61 (1964).

| No. | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | g i | g k | Type of
transition | $egin{array}{c} A_{ki} \ (\mathbf{s}^{-1}) \end{array}$ | S
(at. u.) | Асси-
гасу | Source |
|-----|---|---------------------|------------------------------|------------------------------|-------------|-------------|-----------------------|---|-------------------------|---------------|-------------|
| 1. | a <sup>3</sup> F - a <sup>3</sup> F | | | | | | | | | | |
| | | [75046]
[113040] | 0.0
1332.2 | 1332.2
2216.5 | 9
7 | 7
5 | M1
M1 | 0.062
0.025 | 6.8
6.7 | C+
C+ | 1
1 |
| 2. | a <sup>3</sup> F - b <sup>1</sup> D
(1F) | | | | | | | | | | |
| | | 7393.71
8201.77 | 0.0
1332.2 | 13521
13521 | 9
7 | 5
5 | E2
M1 | 0.0056
0.39 | 0.37
0.040 | E
D | 1
1 |
| | | 8843.42 | 2216.5 | 13521 | 7
5
5 | 5
5
5 | E2
M1
E2 | $7.6(-4)^{a}$
0.17
2.0(-4) | 0.084
0.022
0.032 | E
D
E | 1
1
1 |
| 3. | a <sup>3</sup> F - a <sup>1</sup> S | | | | | | | | | | |
| | | [7989.9] | 2216.5 | 14729 | 5 | 1 | E2 | 1.8(-4) | 0.0035 | E | 1 |

Ni I: Forbidden transitions

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| Ni 1: | Forbidden | transitions | — Continued |
|-------|-----------|-------------|-------------|
| | | | |

| No. | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | g i | g∗ | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|---|---|---|---|----------------------------|---------------------------------|--|---|--|---------------------------------|---------------------------------|
| 4. | a <sup>3</sup> F - a <sup>3</sup> P
(2F) | | | | | | | | | | |
| | | 6404.46
6941.63
7243.99
7002.02
7395.79 | 0.0
1332.2
2216.5
1332.2
2216.5 | 15610
15734
16017
15610
15734 | 9
7
5
7
5 | 5
3
1
5
5
3 | E2
E2
E2
M1
E2
M1 | 0.032
0.025
0.031
0.15
0.0056
0.0022 | 1.0
0.72
0.37
0.0095
0.28
9.9(-5) | E
E
D
E
D | 1
1
1
1
1
1 |
| | | 7464.39 | 2216.5 | 15610 | о
5
5 | 3
5
5 | E2
M1
E2 | 0.0090
0.039
4.0(-4) | 0.0030
0.028 | D
E | 1 1 1 |
| 5. | a <sup>3</sup> F - a <sup>1</sup> G
(3F) | | | | | | | | | | |
| | | 4523.16 | .0.0 | 22102 | 9
9 | 9
9 | M1
E2 | 0.32
2.2(-4) | 0.0099
0.0022 | D
E | 1 |
| | - | 4813.27 | 1332.2 | 22102 | 7
7 | 9
9 | M1
E2
F2 | $\begin{array}{c c} 0.16 \\ 3.8(-6) \\ 3.0(-4) \end{array}$ | 0.0060 | D
E
F | 1 |
| 6. | a <sup>3</sup> F - e <sup>1</sup> S | 5027.34 | 2210.5 | 22102 | 5 | 5 | E2 | 3.0(-4) | 0.0052 | Ľ | 1 |
| | | [2030.2] | 2216.5 | 51457 | 5 | 1 | E2 | 0.17 | 0.0034 | Е | 1 n |
| 7. | <i>a</i> <sup>3</sup> D - <i>a</i> <sup>3</sup> D | | | | | | | | | | |
| | | [148100]
[119980] | 204.8
879.8 | 879.8
1713.1 | 7
5 | 53 | M1
M1 | 0.0070
0.021 | 4.2
4.0 | C+
C+ | |
| 8. | a <sup>3</sup> D - a <sup>1</sup> D | [91101] | 204.9 | 2400.0 | 7 | 5 | M1 | 0.079 | 0.44 | D | 1 |
| | | [31191]
[39513]
[58917] | 879.8
1713.1 | 3409.9
3409.9
3409.9 | 5
3 | 5
5
5 | M1
M1
M1 | 0.0062
0.011 | 0.44
0.071
0.42 | D
D
D | 1
1 |
| 9. | a <sup>3</sup> D - b <sup>1</sup> D
(4F) | | | | | | | | | | |
| | | 7507.44
7908.30
8466.38 | 204.8
879.8
1713.1 | 13521
13521
13521 | 7
5
3 | 5
5
5 | E2
E2
E2 | 0.014
0.017
4.5(-4) | 0.99
1.6
0.058 | E
E
E | 1
1
1 |
| 10. | a <sup>3</sup> D - a <sup>1</sup> S | | | | | | | | | | |
| 11. | a <sup>3</sup> D - a <sup>3</sup> P
(5F) | [7218.7] | 879.8 | 14729 | 5 | 1 | E2 | 0.068 | 0.79 | E | 1 |
| | | 6437.70
6604.30
6489.61
6730.25
6787.00
7130.24
7193.97 | 204.8
879.8
204.8
879.8
879.8
1713.1
1713.1 | 15734
16017
15610
15734
15610
15734
15610 | 7
5
7
5
3
3 | 3
1
5
3
5
3
5 | E2
E2
E2
E2
E2
E2
E2
E2
E2
E2 | 0.092
0.19
0.074
0.012
0.018
0.053
0.0093 | 1.8
1.4
2.5
0.30
0.77
1.7
0.53 | E
E
E
E
E
E
E | 1
1
1
1
1
1
1 |
| 12. | <i>a</i> <sup>3</sup> D - <i>a</i> <sup>1</sup> G | | | | | | | | | | |
| | | [4710.7]
[4565.4] | 879.8
204.8 | 22102
22102 | 5
7 | 9
9 | E2
E2 | 0.080
7.9(-4) | 0.99
0.0084 | E
E | 1
1 |

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| | F | - | 3 | 1 |
|--|---|---|---|---|
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Ni 1: Forbidden transitions - Continued

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| No. | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | $\frac{E_k}{(\mathrm{cm}^{-1})}$ | g i | g. | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | <i>S</i>
(at. u.) | Accu-
racy | Source |
|-------------|---|--|------------------------------|----------------------------------|------------|--------|-----------------------|---------------------------------------|----------------------|---------------|------------|
| | | | | | | | | | | | |
| 13. | <i>a</i> <sup>3</sup> D - <i>e</i> <sup>1</sup> S | | | | | | | | | | |
| | | [1977.2] | 879.8 | 51457 | 5 | 1 | E2 | 8.3 | 0.15 | Е | 1 n |
| 14. | <i>a</i> <sup>1</sup> D - <i>b</i> <sup>1</sup> D
(6F) | 9887.18 | 3409.9 | 13521 | 5 | 5 | E2 | 0.012 | 3.4 | Е | 1 |
| 15. | <i>a</i> <sup>1</sup> D - <i>a</i> <sup>1</sup> S
(7F) | 8832.31 | 3409.9 | 14729 | 5 | 1 | E2 | 0.31 | 9.9 | Е | 1 |
| 16. | <i>a</i> <sup>1</sup> D - <i>a</i> <sup>3</sup> P
(8F) | | | | | | | | | | |
| | | 8194.57 | 3409.9 | 15610 | 5 | 5 | E2 | 0.024 | 2.6 | Е | 1 |
| | | 8111.97 | 3409.9 | 15734 | 5 | 3 | E2
E2 | 4.7(-4)
11(-5) | 0.029 | E | 1 |
| | | 1929.10 | 5409.9 | 10017 | J | 1 | 142 | 1.1(-5) | 2.1(-4) | | - |
| 17. | <i>a</i> <sup>1</sup> D – <i>a</i> <sup>1</sup> G | [5348.3] | 3409.9 | 22102 | 5 | 9 | E2 | 0.44 | 10 | E | 1 |
| 18. | a <sup>1</sup> D – e <sup>1</sup> S | [2080.6] | 3409.9 | 51457 | 5 | 1 | E 2 | 82 | 1.9 | Е | 1 n |
| 19 . | <i>b</i> <sup>1</sup> D - <i>a</i> <sup>1</sup> S | [82794] | 13521 | 14729 | 5 | 1 | E2 | 2.9(-4) | 670 | Е | 1 |
| 20. | b <sup>1</sup> D - a <sup>3</sup> P | | | | | | | | | | |
| | | [47868] | 13521 | 15610 | 5 | 5 | M 1 | 0.072 | 1.5 | D | 1 |
| | | [45182] | 13521 | 15734 | 5 | 3 | M1 | 0.063 | 0.65 | D | 1 |
| 21. | <i>b</i> <sup>1</sup> D - <i>a</i> <sup>1</sup> G | [11650] | 13521 | 22102 | 5 | 9 | E 2 | 4.1(-4) | 0.47 | Е | 1 |
| 22. | b <sup>1</sup> D – e <sup>1</sup> S | [2635.2] | 13521 | 51457 | 5 | 1 | E2 | 9.4 | 0.71 | Е | 1n |
| 23. | a <sup>3</sup> P - a <sup>3</sup> P | | | | | | | | | | |
| | | [805210]
[352890] | 15610
15734 | 15734
16017 | 5
3 | 3
1 | M1
M1 | 3.2(-5)
0.0012 | 1.9
2.0 | C+
C+ | 1
1 |
| 24. | a <sup>3</sup> P - e <sup>1</sup> S | | | | | | | | | | |
| | | [2 788.8]
[2 798.5] | 15610
15734 | 51457
51457 | 5
3 | 1
1 | E2
M1 | 2.9
5.3 | 0.29
0.0043 | E
D | ln
1n |

"The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

Co Isoelectronic Sequence

Ground State: 1s<sup>2</sup>2s<sup>2</sup>2p<sup>6</sup>3s<sup>2</sup>3d<sup>9</sup> <sup>2</sup>D<sub>5/2</sub>

Ionization Energy: $18.16898 \text{ eV} = 146541.56 \text{ cm}^{-1}$

Allowed Transitions

List of tabulated lines

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|
| 1751 09 | 1 | 9174 67 | Б | 2264 46 | q | 2275 42 | 19 |
| 2034.05 | 6 | 2174.07 | 4 | 2270.21 | 3 | 2387.76 | 10 |
| 2053.30 | 6 | 2184.61 | 4 | 2278.77 | 13 | 2394.52 | 11 |
| 2080.85 | 7 | 2188.05 | 3 | 2287.09 | 13 | 2410.74 | 9 |
| 2090.10 | 6 | 2201.41 | 4 | 2296.55 | 12 | 2412.27 | 2 |
| 2093.56 | 6 | 2206.72 | 4 | 2297.14 | 2 | 2413.04 | 10 |
| 2125.12 | 5 | 2210.38 | 4 | 2297.49 | 2 | 2416.13 | 11 |
| 2125.91 | 4 | 2216.48 | 3 | 2298.27 | 12 | 2433.56 | 10 |
| 2128.58 | 6 | 2220.40 | 14 | 2303.00 | 2 | 2437.89 | 10 |
| 2138.58 | 4 | 2222.96 | 3 | 2316.04 | 2 | 2510.87 | 9 |
| 2158.74 | 4 | 2224.36 | 12 | 2326.45 | 2 | 2545.90 | 9 |
| 2161.22 | 5 | 2224.86 | 3 | 2334.58 | 11 | 2630.27 | 8 |
| 2165.55 | 4 | 2226.33 | 3 | 2356.40 | 13 | | |
| 2169.10 | 4 | 2253.85 | 3 | 2367.39 | 2 | | |

For this spectrum, we have chosen the f-value data of Bell et al.,<sup>1</sup> as normalized by Lawler and Salih.<sup>2</sup> Bell et al. determined relative oscillator strengths in emission with a wall-stabilized arc operated in argon and small admixtures of nickel carbonyl. All observations were performed photoelectrically, and digital data processing techniques were employed. Since the measured lines are located in the near ultraviolet, the intensity calibrations presented a special problem, which was solved by utilizing the continuous emission of a hydrogen arc operated at well-diagnosed plasma conditions. Lawler and Salih measured radiative lifetimes of twelve levels of Ni II by the laser-induced fluorescence technique. They then used these lifetimes to convert the data of Ref. 1 to an absolute scale.

The f-values tabulated here are consistently 60 percent lower than those published in our earlier NBS compilation,<sup>4</sup> which utilized the data of Bell *et al.* on an absolute basis. The most probable reason for this difference lies in the method with which Bell *et al.* determined their absolute scale. In the absence of reliable lifetime data, they utilized local thermodynamic equilibrium (LTE) relations to tie their Ni II f-value scale to that of Ni I, which they had determined on an absolute scale. Recent LTE studies in stabilized arcs showed however that at the electron densities of their experiment, LTE conditions are not yet achieved, so that this normalization procedure is not applicable. Therefore, in this compilation, we have tabulated the data and accuracy estimates of Lawler and Salih, whenever available. For lines not covered by Ref. 2, we normalized the data of Ref. 1 (which should be quite reliable on a *relative* scale). This normalization consisted of subtracting 0.21 from the original log gf-values of Ref. 1.

For two lines, we did not use Ref. 1 as the original data source. For the 2326.45 Å line, Lawler and Salih found that the branching ratio of Ref. 1 was inconsistent with other measured and calculated data. We therefore used Lawler and Salih's recommended transition probability for this line. The log gf-value for the 1751.92 Å line was determined from the semi-empirical scaled Thomas-Fermi-Dirac calculations of Kurucz and Peytremann.<sup>3</sup> For this line, the branching ratio of Ref. 3 was adjusted to the lifetime of the $3d^{8}({}^{3}F)4p$ ${}^{2}F_{7/2}^{\circ}$ level, as measured by Lawler and Salih.

References

- <sup>1</sup>G. D. Bell, D. R. Paquette, and W. L. Wiese, Astrophys. J. 143, 559 (1966).
- <sup>2</sup>J. E. Lawler and S. Salih, Phys. Rev. A 35, 5046 (1987).
- <sup>3</sup>R. L. Kurucz and E. Peytremann, Smithsonian Astrophysical Observatory Special Report 362 (1975).
- <sup>4</sup>J. R. Fuhr, G. A. Martin, W. L. Wiese, and S. M. Younger, J. Phys. Chem. Ref. Data 10, 305 (1981).

| F | 3 | 3 |
|---|---|---|
|---|---|---|

Ni II: Allowed transitions

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | <i>E</i> <sup><i>k</i></sup> (cm <sup>-1</sup>) | gi | 8x | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|--|---|--|---|--|--|--|--|---|---|---|---|--|
| 1. | 3d <sup>9</sup> -
3d <sup>8</sup> (<sup>3</sup> F)4p | <sup>2</sup> D - <sup>2</sup> F° | | | 1 | | | | | | | | |
| | | | 1751.92 | 0 | 57081 | 6 | 8 | 0.48 | 0.029 | 1.0 | -0.75 | с | 3n |
| 2. | 3d <sup>8(3</sup> F)4s-
3d <sup>8(3</sup> F)4p | 4F - 4D° | | | | | | | | | | | |
| | | | 2316.04
2303.00
2297.14
2297.49
2367.39 | 8394
9330
10116
10664
9330 | 51558
52738
53635
54176
51558 | 10
8
6
4
8 | 8
6
4
2
8 | 2.88
2.9
2.70
3.0
0.074 | 0.185
0.17
0.142
0.12
0.0062 | 14.1
11
6.46
3.6
0.39 | $ \begin{array}{r} 0.268 \\ 0.14 \\ -0.068 \\ -0.32 \\ -1.30 \end{array} $ | B
C
B
B
B | 1n
1n
1n
1n
1n |
| | | | 2326.45 | 10664 | 53635 | 4 | 4 | 0.33 | 0.027 | 0.82 | -0.97 | D | 2 |
| 3. | | ⁴F - ⁴G° | 2412.21 | 10110 | 01000 | 0 | 0 | 0.0024 | 2.0(-4) | 0.013 | -2.18 | | 111 |
| | | | 2216.48
2270.21
2264.46
2253.85
2222.96
2224.86
2226.33 | 8394
9330
10116
10664
8394
9330
10116 | 53496
53365
54263
55019
53365
54263
55019 | 10
8
6
4
10
8
6 | 12
10
8
6
10
8
6 | 3.4
1.56
1.43
1.98
0.98
1.55
1.3 | 0.30
0.151
0.147
0.226
0.073
0.115
0.097 | 22
9.01
6.56
6.71
5.3
6.74
4.3 | $\begin{array}{r} 0.48\\ 0.081\\ -0.056\\ -0.043\\ -0.14\\ -0.036\\ -0.24\end{array}$ | B
B
C+
B
B
B | 1n
1n
1n
1n
1n
1n
1n |
| | | | 2188.05 | 9330 | 55019 | 8 | 6 | 0.057 | 0.0031 | 0.18 | -1.61 | C+ | 1 n |
| 4. | | <sup>4</sup> F - <sup>4</sup> F° | 2171.3 | 9355 | 55395 | 28 | 28 | 3.14 | 0.222 | 44.4 | 0.793 | C+ | 1n |
| | | | 2165.55
2169.10
2175.15
2184.61
2125.91
2138.58
2158.74
2210.38
2206.72
2201.41 | 8394
9330
10116
10664
8394
9330
10116
9330
10116
10664 | 54557
55418
56075
56424
55418
56075
56424
54557
55418
56075 | 10
8
6
4
10
8
6
8
6
4 | 10
8
6
4
8
6
4
10
8
6 | 2.4
1.58
1.77
2.90
0.050
0.177
0.35
0.39
1.66
1.3 | 0.17
0.111
0.126
0.207
0.0027
0.00910
0.016
0.036
0.162
0.14 | 12
6.37
5.39
5.97
0.19
0.513
0.70
2.1
7.04
4.1 | $\begin{array}{c} 0.23 \\ -0.050 \\ -0.123 \\ -0.081 \\ -1.57 \\ -1.138 \\ -1.01 \\ -0.54 \\ -0.013 \\ -0.25 \end{array}$ | C
B
B
B
B
C+
C
C
B
B | 1n
1n
1n
1n
1n
1n
1n
1n
1n |
| 5. | | ⁴F - ²G° | | | | | | | | | | | |
| | | | 2125.12
2174.67
2161.22 | 9330
9330
10116 | 56371
55300
56371 | 8
8
6 | 8
10
8 | 0.064
1.43
0.20 | 0.0043
0.127
0.019 | 0.24
7.26
0.80 | $-1.46 \\ 0.006 \\ -0.95$ | C
B
C | 1n
1n
1n |
| 6. | | ${}^{4}\mathbf{F} - {}^{2}\mathbf{F}^{\circ}$ | | | | | | | | | | | |
| | | | 2053.30
2034.05
2093.56
2128.58
2090.10 | 8394
9330
9330
10116
10664 | 57081
58493
57081
57081
58493 | 10
8
8
6
4 | 8
6
8
8
6 | 0.025
0.023
0.065
0.248
0.070 | 0.0013
0.0011
0.0043
0.0225
0.0069 | 0.086
0.057
0.24
0.944
0.19 | $-1.90 \\ -2.07 \\ -1.47 \\ -0.870 \\ -1.56$ | B
C
C+
B
C | 1n
1n
1n
1n
1n |
| 7. | | <sup>4</sup> F – <sup>2</sup> D° | 2080 85 | 10664 | 58706 | 4 | 4 | 0.080 | 0 0052 | 0.14 | -1.68 | C | 1n |
| 0 | | 2F = 4D* | 2000.00 | 1004 | 00100 | | 1 | 0.000 | 0.0002 | | 1.00 | | |
| 0. | | r - D | 2630.27 | 13550 | 51558 | 8 | 8 | 0.0068 | 7.1(-4) | 0.049 | -2.25 | с | 1 <i>n</i> |

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Ni II: Allowed transitions - Continued

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | g i | 84 | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | f ik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|--|----------------------------------|--|----------------------------------|----------------------------------|------------------|-------------------|--|-------------------------------------|------------------------------|--|------------------|----------------------|
| 9. | | ²F − ⁴G° | | | | | | | | | | | |
| | | | 2510.87
2545.90
2410.74 | 13550
14996
13550 | 53365
54263
55019 | 8
6
8 | 10
8
6 | 0.58
0.156
0.010 | 0.069
0.0202
6.5(-4) | 4.5
1.02
0.042 | -0.26
-0.916
-2.28 | B
B
D | 1n
1n
1n |
| 10. | | <sup>2</sup> F - <sup>4</sup> F° | | | | | | | | | | | |
| | | | 2437.89
2387.76
2433.56
2413.04 | 13550
13550
14996
14996 | 54557
55418
56075
56424 | 8
8
6
6 | 10
8
6
4 | 0.54
0.159
0.073
0.083 | 0.060
0.0136
0.0065
0.0048 | 3.9
0.855
0.31
0.23 | -0.32
-0.964
-1.41
-1.54 | C
B
B
B | 1n
1n
1n
1n |
| 11. | | <sup>2</sup> F - <sup>2</sup> G° | 2402.8 | 14170 | 55776 | 14 | 18 | 2.23 | 0.248 | 27.5 | 0.541 | C+ | 1 <i>n</i> |
| | | | 2394.52
2416.13
2334.58 | 13550
14996
13550 | 55300
56371
56371 | 8
6
8 | 10
8
8 | 1.70
2.1
0.80 | 0.183
0.25
0.065 | 11.5
12
4.0 | 0.165
0.17
-0.28 | B
C
C | 1n
1n
1n |
| 12. | | <sup>2</sup> F - <sup>2</sup> F° | 2297.3 | 14170 | 57686 | 14 | 14 | 3.94 | 0.312 | 33.0 | 0.640 | C+ | 1 <i>n</i> |
| | | | 2296.55
2298.27
2224.36
2375.42 | 13550
14996
13550
14996 | 57081
58493
58493
57081 | 8
6
8
6 | 8
6
6
8 | 1.98
2.8
0.32
0.66 | 0.157
0.22
0.018
0.074 | 9.47
10
1.0
3.5 | $\begin{array}{c} 0.098 \\ 0.12 \\ -0.85 \\ -0.35 \end{array}$ | B
C
C
B | 1n
1n
1n
1n |
| 13. | | <sup>2</sup> F – <sup>2</sup> D° | 2284.3 | 14170 | 57934 | 14 | 10 | 2.97 | 0.166 | 17.5 | 0.367 | с | 1 <i>n</i> |
| | | | 2278.77
2287.09
2356.40 | 13550
14996
14996 | 57420
58706
57420 | 8
6
6 | 6
4
6 | 2.8
2.8
0.28 | 0.16
0.15
0.023 | 9.8
6.6
1.1 | $0.12 \\ -0.06 \\ -0.85$ | c
c
c | 1n
1n
1n |
| 14. | 3d <sup>8</sup> (<sup>3</sup> P)4s
3d <sup>8</sup> (<sup>1</sup> D)4p | <sup>4</sup> P - <sup>2</sup> F° | | | | | | | | | | | |
| | | | 2220.40 | 23108 | 68131 | 6 | 8 | 2.3 | 0.23 | 9.9 | 0.13 | с | 1 <i>n</i> |

"The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

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فتنت

Nin

Forbidden Transitions

| List | of ta | bula | ted 1 | lines |
|------|-------|------|-------|-------|
|------|-------|------|-------|-------|

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|
| 1020.9 | 7 | 5132.6 | 6 | 7413 33 | 22 | 17646 | 2 |
| 3074 11 | 26 | 5269 16 | 12 | 7612.7 | 9 | 18953 | 18 |
| 3076.1 | 26 | 5274 27 | 6 | 7694.6 | 5 | 19388 | 2 |
| 3223 1 | 26 | 5275.83 | 12 | 8033.5 | 5 | 20487 | 2 |
| 3378 55 | 20 | 5281.46 | 6 | 8303.23 | 22 | 20805 | 14 |
| 3439 29 | 24 | 5431.39 | 6 | 8703.9 | 10 | 21014 | 14 |
| 3559.86 | 24 | 5703.64 | 12 | 8896.1 | 7 | 23079 | 2 |
| 3627 35 | 24 | 5711.46 | 12 | 9377.33 | 21 | 23343 | 14 |
| 3993.1 | 25 | 6007.1 | 9 | 9757.4 | 10 | 23606 | 14 |
| 4025.3 | 23 | 6365.1 | 9 | 9885.74 | 21 | 23688 | 2 |
| 4033.0 | 23 | 6441.3 | 8 | 9956.6 | 10 | 24779 | 18 |
| 4143.17 | 11 | 6467.3 | 5 | 10460 | 7 | 29106 | 2 |
| 4147.30 | 11 | 6668.16 | 22 | 10618 | 16 | 51850 | 15 |
| 4201.2 | 25 | 6700.2 | 9 | 10645 | 16 | 59510 | 13 |
| 4248.8 | 25 | 6791.5 | 5 | 10718.16 | 21 | 66342 | 1 |
| 4285.3 | 23 | 6794.2 | 5 | 10921.07 | 21 | 69177 | 4 |
| 4294.1 | 23 | 6813.6 | 5 | 11360 | 10 | 80610 | 19 |
| 4310.46 | 11 | 6848.4 | 8 | 11455 | 20 | 96151 | 17 |
| 4314.92 | 11 | 6910.8 | 9 | 11616.88 | 21 | 100780 | 17 |
| 4326.2 | 23 | 6955.8 | 9 | 12323 | 7 | 106790 | 2 |
| 4461.54 | 11 | 7054.2 | 5 | 12779 | 21 | 127250 | 2 |
| 4466.33 | 11 | 7078.0 | 5 | 12924 | 16 | 145330 | 15 |
| 4485.2 | 25 | 7102.84 | 8 | 13353 | 20 | 182360 | 2 |
| 4573.45 | 11 | 7255.8 | 5 | 13396 | 20 | 402820 | 15 |
| 4628.0 | 23 | 7307.7 | 9 | 16766 | 14 | | |
| 5064.2 | 6 | 7379.57 | 22 | 17245 | 18 | | |

For this ion, we have selected the data of Nussbaumer and Storey,<sup>1</sup> who calculated M1 and E2 transition probabilities for transitions within the $3d^9$ and $3d^84s$ configurations. These comprise the 17 energetically lowest levels of this spectrum. Nussbaumer and Storey included the $3d^9$, $3d^84s$, and $3d^84d$ configurations as the basis of their calculations, and they derived radial wavefunctions by using adjustable Thomas-Fermi potentials. These authors also applied additional empirical corrections to their coupling coefficients, so that their calculated eigenenergies are in close agreement with observed energy levels. Accuracies for M1 transitions within the same term should be quite good—within 25 percent or better. However, data for other magnetic dipole transitions, as well as for all electric quadrupole transitions, are necessarily much less reliable.

Reference

<sup>1</sup>H. Nussbaumer and P. J. Storey, Astron. Astrophys. 110, 295 (1982).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | 8k | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|----------------------------------|-----------|----------|------------------------------|---------------------------|------------|----|-----------------------|---------------------------------------|---------------|---------------|--------|
| 1. | 3d <sup>9</sup> -3d <sup>9</sup> | ²D - ²D | [66342] | 0 | 1507 | 6 | 4 | M1 | 0.0554 | 2.40 | C+ | 1 |

Ni II: Forbidden transitions

Ni II: Forbidden transitions - Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | gi | ₿ĸ | Type of
transition | $egin{array}{c} A_{ki} \ (\mathbf{s}^{-1}) \end{array}$ | S
(at. u.) | Accu-
racy | Source |
|-----|--|---|--|--|---|---|--|--|--|---|----------------------------|--|
| 2. | 3d <sup>8</sup> (<sup>3</sup> F)4s ~
3d <sup>8</sup> (<sup>3</sup> F)4s | 4F - 4F | | | | | | | | | | |
| | | | [106790]
[127250]
[182360] | 8394
9330
10116 | 9330
10116
10664 | 10
8
6 | 8
6
4 | M1
M1
M1 | 0.0271
0.0276
0.0105 | 9.79
12.7
9.44 | C+
C+
C+ | 1
1
1 |
| 3. | | ⁴ F – <sup>2</sup> F | | | | | | -
- | | | | |
| | | | [19388]
[17646]
[23688]
[20487]
[29106]
[23079] | 8394
9330
9330
10116
10116
10664 | 13550
14996
13550
14996
13550
14996 | 10
8
6
6
4 | 8
6
8
6
8
6 | M1
M1
M1
M1
M1
M1 | 0.087
0.0028
0.0055
0.0072
0.014
0.029 | 0.19
0.0034
0.022
0.014
0.10
0.079 | D
D
D
D
D
D | 1
1
1
1
1
1 |
| 4. | | <sup>2</sup> F - <sup>2</sup> F | | | | | | | | | | |
| | | | [69177] | 13550 | 14996 | 8 | 6 | M 1 | 0.0471 | 3.47 | C+ | 1 |
| 5. | 3d <sup>8</sup> (<sup>3</sup> F)4s-
3d <sup>8</sup> (<sup>3</sup> P)4s | 4 F − 4P | | | | | | | | | | |
| | | | [6794.2]
[6467.3]
[6791.5]
[7255.8]
[6813.6]
[7054.2]
[7694.6] | 8394
9330
10116
9330
10116
10664
10116 | 23108
24788
24836
23108
24788
24836
23108 | 10
8
6
8
6
6
4
4
6
6
4
4
6
6
4
4
6
6
6
4
4
6
6
6
6
6
6
6
6
6
6
6
6
6 | 6
4
2
6
6
4
4
2
2
6
6
6 | E2
E2
E2
M1
E2
M1
E2
M1
E2
M1
E2
M1 | $ \begin{array}{c} 0.0046 \\ 0.0062 \\ 0.0049 \\ 0.16 \\ 0.0010 \\ 0.092 \\ 0.0035 \\ 5.5(-4)^a \\ 0.0060 \\ 0.014 \\ 1.6(-4) \\ 0.007 \end{array} $ | 0.24
0.17
0.084
0.014
0.072
0.0043
0.12
1.4(-5)
0.12
0.0014
0.015
0.2014 | EEEEEEEEEE | 1
1
1
1
1
1
1
1
1
1
1
1
1
1 |
| | | | [8033.5] | 10664 | 23108 | 444 | 4 4 6 | M1
E2
M1
F2 | $\begin{array}{c c} 0.027\\ 9.6(-4)\\ 0.010\\ 1.2(-5)\end{array}$ | 0.0014
0.041
0.0012 | EEE | 1 1 1 1 |
| 6. | | <sup>4</sup> F - <sup>2</sup> P
(9F) | | | | - | ľ | EZ | 1.0(-0) | 0.0010 | E | Ĩ |
| | | | [5064.2]
[5132.6]
5274.27
-
5281.46 | 9330
10116
10116
10664 | 29071
29593
29071
 | 8
6
6
4 | 4
2
4
4
2 | E2
E2
M1
E2
M1 | $\begin{array}{c c} 0.0013 \\ 4.5(-4) \\ 0.012 \\ 1.7(-4) \\ 0.0013 \end{array}$ | $\begin{array}{c} 0.010 \\ 0.0019 \\ 2.6(-4) \\ 0.0017 \\ 1.4(-5) \end{array}$ | E
E
E
E | 1
1
1
1
1 |
| | | | 5431.39 | 10664 | 29071 | 4
4
4 | 2
4
4 | E2
M1
E2 | $5.7(-5) \\ 0.0019 \\ 4.3(-5)$ | $\begin{array}{c c} 2.8(-4) \\ 4.5(-5) \\ 4.8(-4) \end{array}$ | E
E
E | 1
1
1 |
| 7. | | ²F - 4P | | | | | | | | | | |
| | | | [8896.1]
[10460] | 13550
13550 | 24788
23108 | 8
8
8 | 4
6
6 | E2
M1
E2 | $\begin{array}{c} 4.5(-5) \\ 0.076 \\ 3.2(-6) \\ 0.0068 \end{array}$ | 0.0060
0.019
0.0014 | E
E
E | 1
1
1 |
| | | | [10209] | 14996 | 24/88 | 6
6 | 4
4
6 | E2
M1 | 0.0068
1.3(5)
0.082 | 0.0011
0.0034
0.034 | E
E
E | 1
1 |

Ni II: Forbidden transitions - Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_{k}
(cm <sup>-1</sup>) | gi | g. | Type of
transition | A ki
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|--|--|----------------------------------|-------------------------------|--------------------------------|-------------------|------------------|----------------------------|---|--------------------------------------|------------------|------------------|
| 8. | | <sup>2</sup> F – <sup>2</sup> P
(13F) | | | | | | | | | | |
| | | | [6441.3]
[6848.4]
7102.84 | 13550
14996
14996 | 29071
29593
29071 | 8
6
6
6 | 4
2
4
4 | E2
E2
M1
E2 | 0.031
0.029
0.0079
0.0026 | 0.82
0.52
4.2(-4)
0.11 | E
E
E
E | 1
1
1
1 |
| 9. | 3d <sup>8</sup> (<sup>3</sup> F)4s –
3d <sup>8</sup> (<sup>1</sup> D)4s | ⁴F – ² D | | | | | | | | | | |
| | | | [6007.1]
[6910.8]
[6365.1] | 8394
9330
9330 | 25036
23796
25036 | 10
8
8
8 | 6
4
6
6 | E2
E2
M1
E2
M1 | 0.0074
0.0012
0.19
0.0018 | 0.21
0.045
0.011
0.067 | E
E
E
E | 1
1
1
1 |
| | | | [6700.2] | 10116 | 25036 | 6
6
6 | 4
6
6 | M1
E2
M1
E2 | 0.38
5.8(-4)
0.0078
3.3(-4) | 0.029
5.2(-4)
0.016 | E
E
E | 1
1
1 |
| | | | [7612.7]
[6955.8] | 10664
10664 | 23796
25036 | 4
4
4 | 4
4
6
6 | M1
E2
M1
E2 | $\begin{array}{c c} 0.18 \\ 1.4(-4) \\ 0.0077 \\ 3.6(-5) \end{array}$ | 0.012
0.0085
5.8(-4)
0.0021 | E
E
E | 1
1
1 |
| 10. | | ² F − ²D | | | | | | | | | _ | - |
| | | | [9757.4]
[8703.9] | 13550
13550 | 23796
25036
″ | 8
8
8 | 4
6
6 | E2
M1
E2 | $\begin{array}{c} 6.0(-5) \\ 0.089 \\ 4.3(-5) \end{array}$ | 0.013
0.013
0.0077 | E
E
E | 1
1
1 |
| | | | [11360]
[9956.6] | 14996
14996 | 23796
*
25036 | 6
6
6 | 4
4
6 | M1
E2
M1 | 0.057
2.6(-5)
0.062 | 0.012
0.012
0.014 | E
E
E | 1
1
1 |
| 11. | 3d <sup>8</sup> (<sup>3</sup> F)4s-
3d <sup>8</sup> (<sup>1</sup> G)4s | <sup>4</sup> F - <sup>2</sup> G
(10F) | | | | | | | | | | |
| | | | 4147.30
4310 46 | 8394
,
,
,
,
, | 32500
32524 | 10
10
8 | 10
10
8 | M1
E2
M1 | 0.32
1.2(4)
0.16 | 0.0085
0.0010
0.0038 | E
E
E | 1 |
| | | | 4143.17 | 8394
9330 | 32524
32500 | 10
10
8 | 8
8
10 | M1
E2
M1 | 0.0096
1.0(-5)
0.073 | 2.0(-4)
5.8(-5)
0.0022 | E
E
E | 1
1
1 |
| | | | 4461.54 | 10116 | 32524 | 866 | 10
8
8 | E2
M1
E2
F2 | $\begin{array}{c} 2.1(-4) \\ 0.099 \\ 1.2(-4) \\ 1.3(-4) \end{array}$ | 0.0019
0.0026
0.0010 | E
E
E | 1 1 1 1 |
| 12. | | ² F − ²G | 4573.45 | 10664 | 32524 | 4 | 8 | E2 | 4.6(-4) | 0.0014 | E | 1 |
| | | (14F) | 5711.46 | 14996 | 32500 | 6 | 10 | E2 | 5.9(-4) | 0.021 | Е | 1 |
| | | | 5275.83
5703.64 | 13550
14996 | 32500
 | 8
8
6 | 10
10
8 | M1
E2
M1 | 0.082
0.0040
0.042 | 0.0045
0.097
0.0023 | E
E
E | 1
1
1 |
| | | | 5269.16 | 13550 | 32524 | 6
8
8 | 8
8
8 | E2
M1
E2 | 0.0020
0.12
2.5(-4) | 0.057
0.0052
0.0048 | E
E
E | 1
1
1 |

Ni II: Forbidden transitions - Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | gi | g⊧ | Type of
transition | $\begin{array}{c} A_{ki} \\ (\mathbf{s}^{-1}) \end{array}$ | S
(at. u.) | Accu-
racy | Source |
|-----|--|---|--|----------------------------------|----------------------------------|------------------|-------------------|----------------------------|---|-------------------------------------|------------------|------------------|
| 13. | 3d <sup>8</sup> (<sup>3</sup> P)4s−
3d <sup>8</sup> (<sup>3</sup> P)4s | 4P - 4P | | | | | | | | | | |
| | | | [59510] | 23108 | 24788 | 6 | 4 | M 1 | 0.0192 | 0.600 | C+ | 1 |
| 14. | | <sup>4</sup> P - <sup>2</sup> P | | | | | | | | | | |
| | | | [16766] | 23108 | 29071 | 6 | 4 | M1
F2 | 0.080
2 2(5) | 0.056 | D | 1 |
| | | | [20805]
[23343]
[21014]
[23606] | 24788
24788
24836
24836 | 29593
29071
29593
29071 | 4
4
2
2 | 2
4
2
4 | M1
M1
M1
M1
M1 | 0.0078
0.021
0.0061
0.0014 | 0.0052
0.040
0.0042
0.0027 | D
D
D
D | 1
1
1
1 |
| 15. | 3d <sup>8</sup> (<sup>3</sup> P)4s -
3d <sup>8</sup> (<sup>1</sup> D)4s | 4P - 2D | | | | | | | | | | |
| | | | [145330]
[51850]
[402820] | 23108
23108
24788 | 23796
25036
25036 | 6
6
4 | 4
6
6 | M1
M1
M1 | 0.0051
0.069
1.9(-4) | 2.3
2.1
2.0 | E
E
E | 1
1
1 |
| 16. | 3d <sup>8</sup> (<sup>3</sup> P)4s -
3d <sup>8</sup> (<sup>1</sup> G)4s | 4P - 2G | | | | | | | | | | |
| | | | [10645]
[12924]
[10618] | 23108
24788
23108 | 32500
32524
32524
* | 6
4
6
6 | 10
8
8
8 | E2
E2
M1
E2 | $\begin{array}{c} 2.9(-4) \\ 3.7(-5) \\ 8.0(-6) \\ 3.8(-5) \end{array}$ | 0.24
0.064
2.8(-6)
0.024 | E
E
E
E | 1
1
1
1 |
| 17. | 3d <sup>8</sup> (<sup>1</sup> D)4s-
3d <sup>8</sup> (<sup>3</sup> P)4s | ²D - ⁴P | | | | | | - | | | | |
| | | | [100780]
[96151] | 23796
23796 | 24788
24836 | 4
4 | 4
2 | M1
M1 | 0.012
0.0085 | 1.8
0.56 | E
E | 1
1 |
| 18. | | <sup>2</sup> D - <sup>2</sup> P | | | | 1 | | | | | | |
| | | | [24779] | 25036 | 29071 | 6 | 4 | M1
E2 | 0.0059
2.1(-6) | 0.013 | E | 1 |
| | | | [17245] | 23796 | 29593 | 4 | 2 | M1
E2 | 0.077
2.1(-6) | 0.029 | E | 1 |
| | | | [18953] | 23796 | 29071 | 4 | 44 | M1
E2 | 0.073 | 0.074 0.087 | E | 1 |
| 19. | $3d^{8(^{1}D)4s} - 3d^{8(^{1}D)4s}$ | <sup>2</sup> D - <sup>2</sup> D | | | | | | | | | | |
| | | | [80610] | 23796 | 25036 | 4 | 6 | M 1 | 0.00163 | 0.190 | C+ | 1 |
| 20. | 3d <sup>*</sup> (<sup>1</sup> D)4s-
3d <sup>8</sup> (<sup>1</sup> G)4s | <sup>2</sup> D - <sup>2</sup> G | | | | | | | | | | |
| | | | [13396]
[11455]
[13353] | 25036
23796
25036
″ | 32500
32524
32524 | 6
4
6
6 | 10
8
8
8 | E2
E2
M1
E2 | 9.8(-5)3.2(-4)2.3(-6)1.2(-5) | 0.25
0.30
1.6(-6)
0.024 | E
E
E
E | 1
1
1
1 |

Ni II: Forbidden transitions - Continued

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | gi | g× | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|--|---|---------------------|------------------------------|------------------------------|-------------|-------------|-----------------------|--|---------------------------|---------------|-------------|
| 21. | 3d <sup>9</sup> -3d <sup>8</sup> (<sup>3</sup> F)4s | <sup>2</sup> D - <sup>4</sup> F
(1F) | | | | | | | | | | |
| | | | [12779]
10718.16 | 1507
0 | 9330
9330 | 4 | 8
8 | E2
M1 | 2.1(-5)
6.4(-4) | 0.034
2.3(-4) | E
E | 1 |
| | | | 11616.88 | 1507 | 10116 | 6
4 | 8
6 | E2
M1 | 7.8(-4)
9.3(-4) | 0.53
3.2(-4) | E | 1 |
| | | | 9885.74 | 0 | 10116 | 4
6 | 6
6 | E2
M1 | 2.7(-4)
1.2(-4) | 0.20
2.6(-5) | E
E | 1 |
| | | | ,
10921.07 | 1507 | 10664 | 6
4 | 6
4 | E2
M1 | 1.6(-5)
7.7(-4) | 0.0054
1.5(-4) | E
E | 1 |
| | | | 9377.33 | ,0 | 10664 | 4
6
6 | 4
4
4 | E2
M1
E2 | $ \begin{array}{c c} 6.1(-5) \\ 1.3(-5) \\ 7.5(-5) \end{array} $ | 0.023
1.6(-6)
0.013 | E
E
E | 1
1
1 |
| 22. | | <sup>2</sup> D - <sup>2</sup> F
(2F) | | | | | | | | | | |
| | | | 8303.23
7379.57 | 1507
0 | 13550
13550 | 4
6
6 | 8
8
8 | E2
M1
E2 | 0.013
3.7(-4)
0.23 | 2.4
4.4(-5)
24 | E
E
E | 1
1
1 |
| | | | 7413.33 | 1507 | 14996 | 4 | 6 | M1
E2 | 3.3(-5)
0.18 | 3.0(-6) | E
E | 1 |
| | | | 6668.16
, | _0 | 14996 | 6
6 | 6
6 | M1
E2 | 6.2(-4)
0.098 | 4.1(-5)
4.6 | E
E | 1
1 |
| 23. | 3d <sup>9</sup> -3d <sup>8</sup> (<sup>3</sup> P)4s | ²D - 4P | | | | | | | | | | |
| | | | [4326.2] | 0 | 23108 | 6 | 6 | M1 | 0.0025 | 4.5(-5) | E | 1 |
| | | | [4294.1] | 1507 | 24788 | 4 | 4 | M1 | 0.0013 | $1.5 \\ 1.5(-5) \\ 0.99$ | E | 1 |
| | | | [4033.0] | .0 | 24788 | 46 | 4 | M1
F2 | 0.0033 | 3.2(-5) | E | 1 |
| | | | [4285.3] | 1507 | 24836 | 4 | 2 | M1
F2 | 0.0010 | 5.8(-6) | E | 1 |
| | | | [4628.0] | 1507 | 23108 | 4 | 6 | M1
F2 | 1.9(4) | 4.2(-6) | E | 1 |
| | | | [4025.3] | 0 | 24836 | 6 | 2 | E2 | 2.9(-4) | 3.6(-4) | Ē | 1 |
| 24. | | $^{2}D - ^{2}P$
(5F) | | | | | | | | | | |
| | | | 3378.55
3439.29 | 0 | 29593
29071 | 6
6 | 24 | E2
M1
F2 | 4.1
5.7(-4) | 2.1
3.4(-6) | E
E | 1 |
| | | | 3559.86 | 1507 | 29593 | 4 | 2 | M1
E2 | 0.0011 | 3.7(-6) | E | 1 |
| | | | 3627.35 | 1507 | 29071 | 4 | 4
4 | M1
E2 | 0.0014
2.8 | 9.9(-6)
4.2 | E
E | 1 |
| 25. | 3d <sup>9</sup> -3d <sup>8</sup> (<sup>1</sup> D)4s | <sup>2</sup> D - <sup>2</sup> D | | | | | | | | | | |
| | | | [3993.1] | 0 | 25036 | 6 | 6 | M1 | 0.0022 | 3.1(-5) | E | 1 |
| | | | [4485.2] | 1507 | 23796 | 4 | 4 | M1 | 8.4(-4) | 1.9
1.1(-5) | E | 1 |
| | | | [4201.2] | 0 | 23796 | 4
6 | 4 | M1 | 0.30 | 1.3
1.6(-5) | E | 1 |
| | | | 4248.8] | 1507 | 25036 | 4 | 4
6 | M1 | 0.0015 | 2.1
2.6(-5) | E | 1 |
| | | | | | | 4 | 0 | EZ | 0.17 | 0.64 | E | 1 |

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Ni II: Forbidden transitions -- Continued

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | g⊾ | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|--|---|---------------------------------|------------------------------|---------------------------|-------------|--------------|-----------------------|---------------------------------------|--------------------|---------------|-------------|
| 26. | 3d <sup>9</sup> -3d <sup>8</sup> (<sup>1</sup> G)4s | <sup>2</sup> D - <sup>2</sup> G
(6F) | | | | | | | | | | |
| | | | [3076.1]
[3223.1]
3074.11 | 0
1507
0 | 32500
32524
32524 | 6
4
6 | 10
8
8 | E2
E2
E2 | 4.6
3.5
0.35 | 7.5
5.8
0.46 | E
E
E | 1
1
1 |

"The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

Ni III

Fe Isoelectronic Sequence

Ground State: 1s<sup>2</sup>2s<sup>2</sup>2p<sup>6</sup>3s<sup>2</sup>3p<sup>6</sup>3d<sup>8</sup> <sup>3</sup>F<sub>4</sub>

Ionization Energy: $35.19 \text{ eV} = 283800 \text{ cm}^{-1}$

Allowed transitions

For this spectrum, we have chosen the calculations of Biemont<sup>1</sup> and of Kurucz and Peytremann.<sup>2</sup> Biemont obtained radial wavefunctions by means of the scaled Thomas-Fermi method and calculated individual line strengths in intermediate coupling. Similarly, Kurucz and Peytremann used a semiempirical scaled Thomas-Fermi-Dirac approach with very limited configuration interaction. Generally the agreement between Refs. 1 and 2 was good, particularly for strong lines: 63% of the log gf-values for common lines agreed within ± 50 percent. In this compilation, we have included only those lines showing 50 percent or better agreement between Refs. 1 and 2.

As in the case of Fe III, we were able to assess the reliability of Kurucz and Peytremann's (or Biemont's) absolute scale by comparing their theoretical branching ratios to beam-foil lifetime data of Andersen *et al.*<sup>3</sup> This comparison supports the adopted scale: for the z <sup>3</sup>G<sub>3</sub><sup>°</sup> state (the only level measured by Andersen *et al.* for Ni III) the inverse sum of the transition probabilities, $(\Sigma A_{kl})^{-1}$, taken from Ref. 2 is only 17 percent higher than the corresponding beam-foil lifetime.

References

- <sup>1</sup>E. Biemont, J. Quant. Spectrosc. Radiat. Transfer 16, 137 (1976).
- <sup>2</sup>R. L. Kurucz and E. Peytremann, Smithsonian Astrophysical Observatory Special Report 362 (1975).
- <sup>3</sup>T. Andersen, P. Petersen, and E. Biemont, J. Quant. Spectrosc. Radiat. Transfer 17, 389 (1977).

| Ni Ш: | Allowed | transitions |
|-------|---------|-------------|
|-------|---------|-------------|

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_{k}
(cm <sup>-1</sup>) | g i | g. | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fu | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|---|----------------------------------|--|---|--|-------------------------|-------------------------|--|--|--------------------------------|---|-----------------------|--|
| 1. | 3d <sup>7</sup> (4F)4s-
3d <sup>7</sup> (4F)4p | ⁵F – ⁵F° | | | | | | | | | | | |
| | | | 1769.64
1794.90
1791.64
1786.93
1782.75 | 53704
54658
55406
55952
56308 | 110213
110371
111221
111915
112402 | 11
9
7
5
3 | 11
9
7
5
3 | 6.2
2.7
2.5
2.5
3.8 | 0.29
0.13
0.12
0.12
0.12
0.18 | 19
6.9
5.0
3.5
3.2 | $0.50 \\ 0.07 \\ -0.08 \\ -0.22 \\ -0.27$ | D
D
D
D
D | 1,2
1,2
1,2
1,2
1,2 |
| 2. | | ⁵F – ⁵D° | | | | | | | | | | | |
| | | | 1724.52 | 56308 | 114295 | 3 | 1 | 6.7 | 0.10 | 1.7 | 0.52 | D | 1,2 |
| 3. | | ⁵ F – ⁵G° | | | | | | | | | | | |
| | | | 1692.51
1709.90
1719.46
1722.28
[1666.6] | 53704
54658
55952
56308
53704 | 112788
113141
114110
114371
113705 | 11
9
5
3
11 | 13
11
7
5
9 | 7.9
6.3
6.0
5.9
0.038 | 0.40
0.34
0.37
0.44
0.0013 | 25
17
10
7.5
0.078 | 0.64
0.49
0.27
0.12
-1.84 | D
D
D
D
D | 1,2
1,2
1,2
1,2
1,2
1,2 |
| 4. | | <sup>3</sup> F ~ <sup>3</sup> G° | | | | | | | | | | | |
| : | | | 1854.15
1849.54 | 61339
62606 | $115272 \\ 116674$ | 9
7 | 11
9 | 5.4
5.3 | 0.34
0.35 | 19
15 | 0.49
0.39 | D
D | 1,2
1,2 |
| 5. | | <sup>3</sup> F - <sup>3</sup> F° | | | | | | | | | | | |
| | | | 1823.06
1830.01
1830.08 | 61339
62606
63472 | 116192
117251
118115 | 9
7
5 | 9
7
5 | 5.6
4.6
5.0 | 0.28
0.23
0.25 | 15
9.7
7.5 | 0.40
0.21
0.10 | D
D
D | 1,2
1,2
1,2 |
| 6. | | <sup>3</sup> F – <sup>3</sup> D° | | | | | | | | | | | |
| | | | 1741.96
1752.43
1760.56 | 61339
62606
63472 | 118745
119670
120272 | 9
7
5 | 7
5
3 | 5.7
5.5
6.5 | 0.20
0.18
0.18 | 10
7.3
5.2 | 0.26
0.10
-0.05 | D
D
D | 1,2
1,2
1,2 |

Ni III

Forbidden Transitions

List of tabulated lines

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|
| 1989 6 | 5 | 6000.2 | 3 | 7889.9 | 2 | 73472 | 1 |
| 2596.6 | 8 | 6401.5 | 3 | 8499.6 | 2 | 109990 | 1 |
| 2787.0 | 11 | 6533.8 | 3 | 11014 | 7 | 316170 | 9 |
| 2811.8 | 11 | 6682.2 | 3 | 15507 | 10 | 395310 | 9 |
| 4326.2 | 4 | 6797.1 | 3 | 31250 | 6 | | |
| 4596.8 | 4 | 6946.4 | 3 | 33933 | 6 | | 1 |
| 4797.3 | 4 | 7124.8 | 2 | 38012 | 6 | | |

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n + 4

Ner-a

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4

inter Sheef For this spectrum, we have selected the data of Garstang,<sup>1</sup> who calculated M1 and E2 transition probabilities for lines arising between levels of the $3d^8$ configuration. Garstang's single configuration approximation should be fairly reasonable, since levels of the $3d^8$ configuration are generally well removed from those of the nearest neighboring configuration— $3d^74s$. His calculated energy levels are also in close agreement with observed energy levels. The $3d^8$ 'S level, however, is close to some levels of the $3d^74s$ configuration. Nevertheless, we feel that configuration interaction should still play a

minor role, since there are no nearby J=0 levels within the $3d^74s$ configuration. Accuracies for M1 transitions between levels of the same term should be 25 percent or better. However, data for other magnetic dipole transitions, as well as for all E2 transitions, are much less reliable.

Reference

<sup>1</sup>R. H. Garstang, Mon. Not. R. Astron. Soc. 118, 234 (1958).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | g. | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|---------------------|---------------------------------|----------|------------------------------|---------------------------|------------|----|-----------------------|---------------------------------------|---------------|---------------|--------|
| 1. | $3d^{8}$ - $3d^{8}$ | <sup>3</sup> F – <sup>3</sup> F | | | | | | | | ; | | |
| | | | [73472] | 0 | 1361 | 9 | 7 | M 1 | 0.065 | 6.7 | C+ | 1 |
| | | | [109990] | 1361 | 2270 | 7 | 5 | M 1 | 0.027 | 6.7 | C+ | 1 |
| 2. | | <sup>3</sup> F - <sup>1</sup> D | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | [7124.8] | 0 | 14032 | 97 | 5 | E2 | 0.0045 | 0.25 | E | 1 |
| | | | [1009.9] | 1301 | 14032 | | 5 | E2 | $5.4(-4)^{a}$ | 0.044 | E | 1 |
| | | | [8499.6] | 2270 | 14032 | 5 | 5 | M1 | 0.21 | 0.024 | E | 1 |
| | | | | • | , | 5 | 5 | E2 | 1.9(-4) | 0.025 | Е | 1 |
| 3. | | <sup>3</sup> F – <sup>3</sup> P | | | | | | | | | | |
| | | | [6000.2] | 0 | 16662 | 9 | 5 | E2 | 0.050 | 1.2 | Е | 1 |
| | | | [6401.5] | 1361 | 16978 | 7 | 3 | E2 | 0.038 | 0.73 | E | 1 |
| | | | [6682.2] | 2270 | 17231 | 5 | 1 | E2 | 0.046 | 0.36 | Е | 1 |
| | | | [6533.8] | 1361 | 16662 | 7 | 5 | M1 | 0.11 | 0.0057 | E | 1 |
| | | | [6797.1] | 2270 | 169/8 | 5 | 3 | M1
F2 | 0.0028 | 9.8(5) | E
F | 1 |
| | | | [6946.4] | 2270 | 16662 | 5 | 5 | M1 | 0.022 | 0.0014 | E | 1 |
| | | | | , | , | 5 | 5 | E2 | 7.2(-4) | 0.035 | Ē | 1 |
| 4. | | <sup>3</sup> F - <sup>1</sup> G | | | | | | | | | | |
| | | | [4326.2] | 0 | 23109 | 9 | 9 | M1 | 0.35 | 0.0095 | Е | 1 |
| | | | | - | - | 9 | 9 | E2 | 2.7(-4) | 0.0022 | Е | 1 |
| | | | [4596.8] | 1361 | 23109 | 7 | 9 | M1 | 0.18 | 0.0058 | E | 1 |
| | | | [4797.3] | 2270 | 23109 | 5 | 9 | E2 | 3.9(-4) | 0.0053 | Е | 1 |
| 5. | | <sup>3</sup> F - <sup>1</sup> S | | | | | | | | | | |
| | | | [1989.6] | 2270 | 52532 | 5 | 1 | E2 | 0.20 | 0.0038 | Е | 1n |
| 6. | | <sup>1</sup> D - <sup>3</sup> P | | | | | | | | | | |
| | | | 101001 | 14099 | 16669 | F | E | M | 0.000 | 1.0 | Ð | |
| | | | [33933] | 14032 | 16978 | 0
5 | 3 | M1 | 0.098 | 0.39 | E | 1 |
| | | | [00000] | * | | 5 | 3 | E2 | 1.8(6) | 0.14 | Ē | 1 |
| | | | [31250] | 14032 | 17231 | 5 | 1 | E 2 | 2.4(-6) | 0.043 | Е | 1 |
| 7. | | <sup>1</sup> D - <sup>1</sup> G | | | | | | | | | | |
| | | | [11014] | 14032 | 2310 9 | 5 | 9 | E2 | 6.2(4) | 0.54 | Е | 1 |

Ni III: Forbidden transitions

| F | 4 | 3 |
|---|---|---|
|---|---|---|

Ni III: Forbidden transitions - Continued

| No. | Transition
Array | Multiplet | λ
(Å) | E_i (cm <sup>-1</sup>) | $\frac{E_k}{(\mathrm{cm}^{-1})}$ | g i | ₿k | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|---------------------|---------------------------------|----------------------|---------------------------|----------------------------------|------------|--------|-----------------------|---------------------------------------|----------------|---------------|------------|
| | | | | | | | | | | | | |
| 8. | | $^{1}D - ^{1}S$ | | | | | | | | 1 | | |
| | | | [2596.6] | 14032 | 52532 | 5 | 1 | E2 | 10 | 0.72 | Е | 1 n |
| 9. | | <sup>3</sup> P – <sup>3</sup> P | | | | | | | | | | |
| | | | [316170] | 16662 | 16978 | 5 | 3 | M1 | 5.9(-4) | 2.1 | C+ | 1 |
| | | | [395310] | 16978 | 17231 | 3 | 1 | M 1 | 8.6(-4) | 2.0 | C+ | 1 |
| 10. | | <sup>3</sup> P - <sup>1</sup> G | | | | | | | | | | |
| | | | [15507] | 16662 | 23109 | 5 | 9 | E 2 | 2.7(-5) | 0.13 | Е | 1 |
| 11. | | <sup>3</sup> P - <sup>1</sup> S | | | | | | | | | | |
| | | | [2787.0]
[2811.8] | 16662
16978 | 52532
52532 | 5
3 | 1
1 | E2
M1 | 1.9
2.9 | 0.19
0.0024 | E
E | 1n
1n |

"The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

Niıv

Mn Isoelectronic Sequence

÷314

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21**223**

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Ground State: $1s^22s^22p^63s^23p^63d^{74}F_{9/2}$

Ionization Energy: $54.9 \text{ eV} = 443000 \text{ cm}^{-1}$

Forbidden Transitions

List of tabulated lines

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|
| 1470.8 | 8 | 2366.3 | 7 | 3987.6 | 12 | 5321.6 | 20 |
| 1497.0 | 8 | 2390.7 | 7 | 3990.3 | 6 | 5363.3 | 3 |
| 1511.3 | 8 | 2415.0 | 7 | 4071.8 | 29 | 5517.7 | 2 |
| 1516.4 | 8 | 2424.2 | 7 | 4084.0 | 12 | 5809.1 | 23 |
| 1529.8 | 8 | 2444.6 | 27 | 4084.6 | 6 | 5820.1 | 2 |
| 1531.0 | 8 | 2449.3 | 7 | 4142.8 | 29 | 5905.4 | 2 |
| 1544.7 | 8 | 2479.9 | 24 | 4160.5 | 16 | 5910.0 | 2 |
| 2004.5 | 13 | 2482.9 | 27 | 4179.0 | 29 | 5964.2 | 26 |
| 2014.5 | 13 | 2549.5 | 27 | 4234.7 | 16 | 6117.9 | 26 |
| 2030.2 | 13 | 2591.1 | 27 | 4253.9 | 29 | 6119.3 | 2 |
| 2038.9 | 13 | 3612.0 | 5 | 4363.5 | 16 | 6124.1 | 2 |
| 2040.4 | 13 | 3623.7 | 6 | 4421.8 | 4 | 6178.4 | 23 |
| 2065.4 | 13 | 3689.5 | 6 | 4445.2 | 16 | 6218.7 | 2 |
| 2075.7 | 17 | 3739.3 | 6 | 4451.3 | 4 | 6343.5 | 23 |
| 2125.1 | 17 | 3751.4 | 5 | 4537.9 | 4 | 6349.2 | 2 |
| 2153.9 | 17 | 3774.2 | 5 | 4627.0 | 4 | 6450.9 | 2 |
| 2254.6 | 21 | 3822.0 | 6 | 4754.3 | 4 | 6629.1 | 26 |
| 2279.4 | 7 | 3858.9 | 6 | 4772.5 | 3 | 6819.5 | 26 |
| 2287.0 | 21 | 3883.9 | 12 | 4946.7 | 20 | 9379.1 | 11 |
| 2301.4 | 7 | 3899.8 | 5 | 5041.6 | 3 | 9602.7 | 11 |
| 2306.7 | 21 | 3921.7 | 12 | 5052.0 | 20 | 10181 | 11 |
| 2340.7 | 21 | 3926.7 | 5 | 5059.9 | 3 | 11135 | 11 |
| 2342 9 | 7 | 3948.5 | 12 | 5288.1 | 3 | 11452 | 11 |

List of tabulated lines - Continued

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|--|
| 12739 | 15 | 18927 | 10 | 84032 | 1 | 168990 | 9 | |
| 14660 | 15 | 19492 | 19 | 89421 | 14 | 172780 | 1 | |
| 14855 | 15 | 21314 | 10 | 97202 | 22 | 237410 | 28 | |
| 15908 | 10 | 24228 | 19 | 99723 | 18 | 402790 | 9 | |
| 17561 | 10 | 28998 | 19 | 117230 | 1 | | | |
| 18077 | 10 | 59465 | 25 | 158740 | 30 | | | |

For this spectrum, we have chosen the work of Hansen *et al.*,<sup>1</sup> who calculated M1 and E2 transition probabilities for transitions within the $3d^7$ ground configuration. These authors used a single configuration approximation, which should be fairly reliable, since the ground configuration is well separated from other configurations of the same parity. Also, the authors determined eigenvector components by a parametric fitting of theoretical energy expressions to observed energy levels.

Finally, Hartree-Fock calculations were used to determine s_q , the radial electric quadrupole integral, which is needed in the calculation of E2 transition probabilities.

Reference

<sup>1</sup>J. E. Hansen, A. J. J. Raassen, and P. H. M. Uylings, Astrophys. J. 277, 435 (1984).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i (cm <sup>-1</sup>) | E_{k} (cm <sup>-1</sup>) | g i | g, | Type of
transition | $\begin{array}{c} \boldsymbol{A_{ki}} \\ (\mathbf{s}^{-1}) \end{array}$ | S
(at. u.) | Accu-
racy | Source |
|-----|-------------------------------|-----------|----------------------------------|---------------------------|-----------------------------|--------------|--------------|-----------------------|---|--|---------------|-------------|
| 1. | $3d^{\gamma}$ - $3d^{\gamma}$ | 4F - 4F | | | | | | | | | | |
| | | | [84032]
[117230] | 0.0
1189.7 | 1189.7
2042.5 | 10
8 | 86 | M1
M1 | 0.057
0.036 | 10
13 | C+
C+ | 1 |
| 2. | | ⁴F - ⁴P | [172780] | 2042.5 | 2621.1 | 6 | 4 | M1 | 0.013 | 9.9 | C+ | 1 |
| | | | [5517.7]
[5820.1] | 0.0
1189.7 | 18119
18367 | 10
8 | 6
4 | E2
E2 | 0.068
0.035 | 1.2
0.56 | E
E | 1
1 |
| | | | [5910.0]
[5905.4] | 2042.5
1189.7 | 18958
18119 | 6
8
8 | 2
6
6 | E2
M1
E2 | 0.026
0.0053
0.015 | 0.22
2.4(-4) <sup>a</sup>
0.38 | E
E
E | 1
1
1 |
| | | | [6124.1]
[6119.3] | 2042.5 | 18367
18958 | 6
6
4 | 4
4
2 | M1
E2
E2 | 0.0018
0.020
0.033 | $ \begin{array}{c c} 6.1(-5) \\ 0.41 \\ 0.34 \end{array} $ | E
E
E | 1
1
1 |
| | | | [6218.7]
[6349.2] | 2042.5 | 18119
18367 | 6
6
4 | 6
6
4 | M1
E2
M1 | 0.0020
0.0027
3.3(-4) | $ \begin{array}{c c} 1.1(-4) \\ 0.090 \\ 1.3(-5) \end{array} $ | E
E
E | 1
1
1 |
| | | | [6450.9] | 2621.1 | 18119 | 4
4
4 | 4
6
6 | E2
M1
E2 | 0.0054
6.9(-4)
2.5(-4) | 0.13
4.1(-5)
0.010 | E
E
E | 1
1
1 |
| 3. | | ⁴F - ²G | | | | | | | (-) | 0.010 | 2 | - |
| | | | [5041.6] | 0.0 | 19830 | 10
10 | 10
10 | M1
E2 | 0.91
1.3(-4) | 0.043
0.0025 | E
E | 1 |
| | | | [5059.9]
[4772.5]
[5363.3] | 0.0
1189.7 | 20948
20948
19830 | 8
10
8 | 8
8
10 | M1
M1
M1 | 0.35
0.034
0.28 | 0.013
0.0011
0.016 | E
E
E | 1
1
1 |
| | | | [5288.1] | 2042.5 | 20948 | 6 | 8 | M 1 | 0.25 | 0.011 | Е | 1 |

Ni IV: Forbidden transitions

| F | 4 | 5 |
|---|---|---|
|---|---|---|

Ni IV: Forbidden transitions - Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | gi | g. | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|---------------------|------------------------|----------------------|------------------------------|---------------------------|--------|--------|-----------------------|---------------------------------------|--------------------|---------------|--------|
| 4. | | ⁴F – ²P | | | | | | | | | | |
| | | | | | | | | | | | - | |
| | | | [4451.3]
[4421 8] | 1189.7
2042.5 | 23649
24651 | 8 | 4 | E2
E2 | 0.0099 | 0.041 | E | 1 |
| | | | [4627.0] | 2042.5 | 23649 | 6 | 4 | M1 | 0.17 | 0.0025 | Ē | 1 |
| | | | | | • | 6 | 4 | E2 | 0.0043 | 0.022 | E | 1 |
| | | | [4537.9] | 2621.1 | 24651 | 4 | | MI
E2 | 0.0039 | 2.7(-5)
0.0055 | E | 1 |
| | | | [4754.3] | 2621.1 | 23649 | 4 | 4
4 | M1
E2 | 0.12
0.0011 | 0.0019
0.0064 | Ē
E | 1 |
| 5. | | ⁴F − ² H | | | | | | | | | | |
| | | | [3926.7] | 1189.7 | 26649 | 8 | 12 | E 2 | 1.7(-5) | 1.1(-4) | Е | 1 |
| | | | [3899.8] | 2042.5 | 27678 | 6 | 10 | E2 | 1.6(-5) | 8.6(-5) | E | 1 |
| | | | [3751.4] | 0.0 | 26649 | 10 | 12 | M1
E2 | 0.0016
2.5(-4) | 3.8(-5) | E | |
| | | | [3774.2] | 1189.7 | 27678 | 8 | 10 | M1 | 0.0065 | 1.3(-4) | Ē | 1 |
| | | | | • | | 8 | 10 | E2 | 6.9(-5) | 3.1(-4) | E | 1 |
| | | | [3612.0] | , 0.0
, " | 2/6/8 | 10 | 10 | M1
E2 | 0.013
3.7(-5) | 2.3(-4)
1.4(-4) | E | |
| 6. | | ⁴F - 2D2 | | | | | | | | | | |
| | | | [3689 5] | 0.0 | 27097 | 10 | 6 | E2 | 0.0011 | 0.0027 | Е | 1 |
| | | | [3623.7] | 1189.7 | 28778 | 8 | 4 | E2 | 0.0013 | 0.0019 | Ē | 1 |
| | | | [3858.9] | 1189.7 | 27097 | 8 | 6 | M1 | 1.7 | 0.022 | E | 1 |
| | | | [3739 3] | 2042.5 | 28778 | 8 | 6 | E2
M1 | 4.0(-4) | 0.0012 | E | 1 |
| | | | [0100.0]
* | , | 20110 | 6 | 4 | E2 | 8.4(-4) | 0.0015 | Ē | 1 |
| | | | [3990.3] | 2042.5 | 27097 | 6 | 6 | M1 | 0.18 | 0.0025 | E | 1 |
| | | | [3822.0] | 2621.1 | 28778 | 6 | 6 | E2
M1 | 2.3(5) | 8.3(-5)
0.0070 | E | 1 |
| | | | , | , | | 4 | 4 | E2 | 4.0(-5) | 7.8(-5) | E | 1 |
| | | | [4084.6] | 2621.1
″ | 27097 | 4
4 | 6
6 | M1
E2 | 0.081
3.1(-6) | 0.0012
1.3(-5) | E
E | 1 |
| 7. | | ⁴F - <sup>2</sup> F | | | | | | | | | | |
| | | | [2301.4] | 0.0 | 43438 | 10 | 6 | E 2 | 0.0010 | 2.3(-4) | E | 1 |
| | | | [2279.4] | 0.0 | 43859 | 10 | 8 | M1
F2 | 0.28 | 9.8(-4) | D
E | 1 |
| | | | [2366.3] | 1189.7 | 43438 | 8 | 6 | M1 | 0.072 | 2.1(-4) | D | i |
| | | | *
* | 1100 5 | 40050 | 8 | 6 | E2 | 9.9(-4) | 2.6(-4) | E | 1 |
| | | | [2342.9] | 1189.7 | 43859 | 8 | 8 | E2 | 7.5(-4) | 2.1(-4)
2.5(-4) | E | 1 |
| | | | [2415.0] | 2042.5 | 43438 | 6 | 6 | M1 | 0.055 | 1.7(-4) | D | 1 |
| | | | 10900 71 | 0040 5 | 49050 | 6 | 6 | E2 | 0.0013 | 3.8(-4) | E | 1 |
| | | | [2390.7] | 2042.5 | 43899 | 6 | 8 | E2 | 0.0022 | 4.5(-4)
8.2(-4) | E | 1 |
| | | | [2449.3] | 2621.1 | 43438 | 4 | 6 | M 1 | 0.28 | 9.2(-4) | D | 1 |
| | | | r0494 91 | 9691 1 | 43950 | 4 | 6
8 | E2
E2 | 0.0049 | 0.0015
2.0(-4) | E | |
| | | | [2424.2] | 2021.1 | 40007 | 1 | 0 | 201 | 4.5(-4) | 2.0(-4) | | 1 |

Ni IV: Forbidden transitions - Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i (cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | Bi | ₿ĸ | Type of
transition | A <sub>ki</sub>
(s <sup>−1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|---------------------|----------------------------------|----------------------|---------------------------|---------------------------|-------------|-------------|-----------------------|---------------------------------------|--|---------------|--------|
| 8. | | ⁴ F - 2D1 | | | | : | | | | | | |
| | | | [1470.9] | | 67000 | 10 | c | E9 | 0.074 | 0.0019 | E | |
| | | | [1470.8] | 1189.7 | 67360 | 8 | 4 | E2
E2 | 0.074 | 2.6(-4) | E | 1 |
| | | | [1497.0] | 1189.7 | 67990 | 8 | 6 | M 1 | 0.26 | 1.9(-4) | E | 1 |
| | | | [1531.0] | 2042.5 | 67360 | 8
6
6 | 6
4 | E2
M1
E2 | 0.0055
0.29 | 1.5(-4)
1.5(-4) | E | 1 |
| | | | [1516.4] | 2042.5 | 67990 | 6 | 4
6
6 | E2
M1 | 3.4(-5)
0.040 | 6.8(-7)
3.1(-5) | E | 1 |
| | | | [1544.7] | 2621.1 | 67360 | | 4 | E2
M1
E9 | 0.0039 | 1.1(-4)
1.1(-4) | E | 1 |
| | | | [1529.8] | 2621.1 | 67990 | 4
4
4 | 4
6
6 | E2
M1
E2 | 0.0026
0.019
0.0016 | $ \begin{array}{c c} 5.4(-5) \\ 1.5(-5) \\ 4.8(-5) \end{array} $ | E
E
E | 1 1 1 |
| 9. | | 4P - 4P | | | | | | | | | | |
| | | | [402790]
[168990] | 18119
18367 | 18367
18958 | 6
4 | 4
2 | M1
M1 | 3.4(-4)
0.0089 | 3.3
3.2 | C+
C+ | 1
1 |
| 10. | | <sup>4</sup> P - <sup>2</sup> P | | | | | | | | | | |
| | | | [18077] | 18119 | 23649 | 6 | 4 | M 1 | 0.33 | 0.29 | D | 1 |
| | | | [15908] | 18367 | 24651 | 4 | 2 | M1 | 6.4(-4) | 1.9(-4) | D | 1 |
| | | | [17561] | 18958 | 23649 | 4 | 42 | M1
M1 | 0.17 | 0.17 | מ | 1 |
| | | | [21314] | 18958 | 23649 | 2 | 4 | M 1 | 0.064 | 0.092 | D | 1 |
| 11. | | <sup>4</sup> P - <sup>2</sup> D2 | | | | | | | | | | |
| | | | [11135] | 18119 | 27097 | 6 | 6 | M 1 | 0.10 | 0.031 | Е | 1 |
| | | | [9602.7] | 18367 | 28778 | 4 | 4 | M1 | 0.022 | 0.0029 | Е | 1 |
| | | | [9379.1] | 18119 | 28778 | 6 | 4 | M1
M1 | 0.0090 | 0.0011 | E | 1 |
| | | | [10181] | 18958 | 28778 | 2 | 4 | M1
M1 | 0.085 | 0.022 | E | 1 |
| 12. | | ⁴P - <sup>2</sup> F | | | | | | | | | | |
| | | | [3921.7] | 18367 | 43859 | 4 | 8 | E2 | 0.0037 | 0.016 | Е | 1 |
| | | | [4084.0] | 18958 | 43438 | 2 | 6 | E2 | 0.0010 | 0.0041 | Е | 1 |
| | | | [3883.9] | 18119 | 43859 | 6 | 8 | M1
F2 | 6.0(-4) | 1.0(-5) | E | |
| | | | [3987.6] | 18367 | 43438 | 4 | 6 | M1 | 1.3(-4) | 1.8(-6) | E | 1 |
| | | | [3948.5] | 18119 | 43438 | 4
6 | 6
6 | E2
M1 | 0.0020 | 0.0072
6.8(-5) | E | 1 |
| 13 | | 4P - 2D1 | | | | D | 0 | EZ | 6.8(-5) | 2.3(4) | Е | |
| 10. | | 1 01 | | | | | | | | | | |
| | | | [2004.5] | 18119 | 67990 | 6 | 6 | M1 | 1.9 | 0.0034 | E | 1 |
| | | | [2040.4] | 18367 | 67360 | 4 | 4 | E2
M1 | 0.0015 | 1.7(-4)
9.1(-4) | E | 1 |
| | | | [2030.2] | 18119 | 67360 | 6 | 4 | M1 | 0.13 | 3.4(-4) | E | 1 |
| | | | [2014.5] | 18367 | 67990 | 4 | 4
6
6 | M1
F2 | 2.9(-4)
0.30 | 2.4(-5)
5.5(-4) | E | 1 |
| | | | [2065.4] | 18958 | 67360 | 2 | 4 | M1 | 0.19 | 2.5(-4) | E | 1 |
| | | | [2038.9] | 18958 | 67990 | 2 | 4
6 | E2
E2 | 0.063 | 0.0056 | E | 1 |

Ni IV: Forbidden transitions - Continued

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|-----|---------------------|----------------------------------|-------------------------------|----------------------------------|--|-------------|-------------|-----------------------|---------------------------------------|-------------------------|---------------|-------------|
| No. | Transition
Array | Multiplet | λ
(Å) | $\frac{E_i}{(\mathrm{cm}^{-1})}$ | <i>E</i> <sup><i>k</i></sup> (cm <sup>-1</sup>) | g i | g⊾ | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
| 14. | | <sup>2</sup> G - <sup>2</sup> G | | | | | | | | | | |
| | | | [89421] | 19830 | 20948 | 10 | 8 | M1 | 0.020 | 4.2 | C+ | 1 |
| 15 | | 2G - 2H | (00 12-) | | | | | | | | | |
| 10. | | | [14660] | 19830 | 26649 | 10 | 12 | M 1 | 0.094 | 0.13 | Е | 1 |
| | | | [14855]
[12739] | 20948
19830 | 27678
27678 | 8
10 | 10
10 | M1
M1 | 0.089
0.31 | 0.11
0.24 | E
E | 1 |
| 16. | | <sup>2</sup> G - <sup>2</sup> F | | | | | | | | | | |
| 1 | | | [4234.7] | 19830 | 43438 | 10 | 6 | E2 | 0.037 | 0.18 | Е | 1 |
| | | | [4160.5] | 19830 | 43859 | 10
10 | 8
8 | M1
E2 | 0.22
0.093 | 0.0047 | E | 1
1 |
| | | | [4445.2] | 20948 | 43438 | 8 | 6
6 | M1
E2 | 0.18
0.078 | 0.0035 | E | 1 |
| | | | [4363 .5] | 20948 | 43859 | 8
8 | 8
8 | M1
E2 | 0.33
0.0075 | 0.0081
0.057 | E
E | 1
1 |
| 17. | | ²G - ²D1 | | | | | | | | | | |
| | | | [2075.7] | 19830 | 67990
67360 | 10 | 6 | E2 | 8.5 | 1.2 | E | 1 |
| | | | [2135.5] | 20948 | 67990 | 8 | 6 | M1
E2 | 0.0045
0.60 | 9.6(-6)
0.093 | E
E | 1 |
| 18. | | <sup>2</sup> P - <sup>2</sup> P | | | | | | | | | | |
| | | | [99723] | 23649 | 24651 | 4 | 2 | M 1 | 0.017 | 1.3 | C+ | 1 |
| 19. | | <sup>2</sup> P - <sup>2</sup> D2 | | | | | | | | | | |
| | | | [28998]
[24228]
[19492] | 23649
24651
23649 | 27097
28778
28778 | 4
2
4 | 6
4
4 | M1
M1
M1 | 0.037
0.064
0.37 | 0.20
0.13
0.41 | E
E
E | 1
1
1 |
| 20. | | <sup>2</sup> P – <sup>2</sup> F | | | | | | | | | | |
| | | | [4946.7] | 23649 | 43859 | 4 | 8 | E2 | 0.011 | 0.16 | E | 1 |
| | | | [5321.6]
[5052.0] | 24651
23649 | 43438
43438 | 244 | 6
6
6 | E2
M1
E2 | 0.010
0.0035
0.018 | 0.15
1.0(-4)
0.21 | E
E
E | 1 1 1 |
| 21. | | ²P - ²D1 | | | | | | | | | | |
| | | | [2306.7] | 24651 | 67990 | 2 | 6 | E2 | 0.60 | 0.14 | Е | 1 |
| | | | [2254.6] | 23649 | 67990 | 4 | 6 | M1
E2 | 0.19
2.1 | 4.8(-4)
0.44 | E | 1 |
| | | | [2340.7] | 24651 | 67360
• | 22 | 4 | M1
E2 | 0.0055
1.2 | 1.0(-5)
0.20 | E
E | 1
1 |
| | | | [2287.0] | 23649 | 67360
, | 4 | 4 | M1
E2 | 0.052
0.66 | 9.2(5)
0.098 | E
E | 1
1 |
| 22. | | ²H - ²H | | | | | | | | | | |
| | | | [97202] | 26649 | 27678 | 12 | 10 | M 1 | 0.016 | 5.4 | C+ | 1 |

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| N1 IV: Forbidden transitions — C | ontinued |
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|----------------------------------|----------|

| No. | Transition
Array | Multiplet | λ
(Å) | E_i (cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | gı | Type of
transition | $egin{array}{c} A_{ki} \ (\mathbf{s}^{-1}) \end{array}$ | <i>S</i>
(at. u.) | Accu-
racy | Source |
|-----|---------------------|-----------------------------------|----------------------|---------------------------|---------------------------|------------|--------|-----------------------|---|----------------------|---------------|--------|
| | | 2 LI 2 F | | | | | | | | | | |
| 20. | | H -F | 15000 11 | 90040 | 18050 | 10 | | 50 | 0.050 | | _ | |
| | | | [5809.1]
[6343.5] | 26649
27678 | 43859
43438 | 12 | 8
6 | E2
E2 | 0.059
0.036 | 1.9
1.3 | E
E | 1 |
| | | | [6178.4] | 27678 | 43859 | 10
10 | 8
8 | M1
E2 | 0.0016
0.0044 | 1.1(-4)
0.19 | E
E | 1 |
| 24. | | <sup>2</sup> H – <sup>2</sup> D1 | | | | | | | | | | |
| | | | [2479.9] | 27678 | 67990 | 10 | 6 | E2 | 0.15 | 0.050 | Е | 1 |
| 25. | | <sup>2</sup> D2 - <sup>2</sup> D2 | | | | | | | | | | |
| | | | [59465] | 27097 | 28778 | 6 | 4 | M 1 | 0.070 | 2.2 | C+ | 1 |
| 26. | | <sup>2</sup> D2 - <sup>2</sup> F | | | | | | | | | | |
| | | | [6629.1] | 28778 | 43859 | 4 | 8 | E2 | 0.0038 | 0.23 | Е | 1 |
| | | | [5964.2]
* | 27097 | 43859 | 6
6 | 8 | M1
E2 | 0.022
0.024 | 0.0014 0.86 | E | 1
1 |
| | | | [6819.5] | 28778 | 43438 | 4 | 6
6 | M1
E2 | 0.012 | 8.5(-4)
0.47 | E | 1 |
| | | | [6117.9] | 27097 | 43438
<i>"</i> | 6
6 | 6
6 | M1
E2 | 0.045
0.0047 | 0.0023 | E | 1 |
| 27. | | <sup>2</sup> D2 - <sup>2</sup> D1 | | | | | | | | | | |
| | | | [2444.6] | 27097 | 67990 | 6 | 6 | M 1 | 0.0099 | 3.2(-5) | D | 1 |
| | | | -
[2591.1] | -
28778 | 67360 | 6
4 | 6
4 | E2
M1 | 0.54
0.0012 | 0.17
3.1(-6) | E
D | 1
1 |
| | | | ,
[2482.9] | 27097 | 67360 | 4 | 4 | E2
M1 | 0.75
1.2 | 0.21 | E | 1 |
| | | | [2549.5] | 28778 | 67990 | 6 | 4 | E2
M1 | 0.14 | 0.031 | E | 1 |
| | | | [2010.0] | 20110 | | 4 | 6 | E2 | 0.0036 | 0.0014 | Ē | 1 |
| 28. | | <sup>2</sup> F - <sup>2</sup> F | | | | | | | | | | |
| | | | [237410] | 43438 | 43859 | 6 | 8 | M 1 | 8.6(-4) | 3.4 | C+ | 1 |
| 29. | | <sup>2</sup> F – <sup>2</sup> D1 | | | | | | | | | | |
| | | | [4253.9]
[4142.8] | 43859
43859 | 67360
67990 | 8 | 4 | E2
M1 | 0.051 | 0.17 | E | 1 |
| | | | [4179.0] | 43438 | 67360 | 8 | 6 | E2
M1 | 0.42 | 1.8 | E | 1 |
| | | | [4071 9] | 19490
* | 67990 | 6 | 4 | E2 | 0.45 | 1.2 | E | 1 |
| | | | [4071.8] | 40400 | 01990 | 6 | 6 | E2 | 0.065 | 0.013 | E | 1 |
| 30. | | <sup>2</sup> D1 – <sup>2</sup> D1 | | | | | | | | | | |
| | | | [158740] | 67360 | 67990 | 4 | 6 | M 1 | 0.0027 | 2.4 | C+ | 1 |

"The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

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Cr Isoelectronic Sequence

Ground State: $1s^2 2s^2 2p^6 3s^2 3p^6 3d^6 {}^5D_4$

Ionization Energy: $76.06 \text{ eV} = 613500 \text{ cm}^{-1}$

Forbidden Transitions

| List | of | tabulated | lines |
|------|----|-----------|-------|
|------|----|-----------|-------|

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|
| 2384.8 | 5 | 2904.7 | 4 | 3485.6 | 3 | 3706.9 | 2 |
| 2436.5 | 5 | 2935.0 | 4 | 3519.0 | 3 | 3726.7 | 1 |
| 2454.0 | 5 | 2981.8 | 4 | 3540.8 | 3 | 3752.7 | 1 |
| 2472.6 | 5 | 3006.1 | 4 | 3560.1 | 3 | 3957.2 | 1 |
| 2486.1 | 5 | 3013.7 | 4 | 3566.9 | 3 | 4053.5 | 1 |
| 2490.7 | 5 | 3036.2 | 4 | 3588.5 | 2 | 4117.2 | 1 |
| 2509.9 | 5 | 3380.7 | 3 | 3600.2 | 1 | | |
| 2514.6 | 5 | 3432.6 | 3 | 3625.0 | 2 | | |
| 2521.7 | 5 | 3446.2 | 3 | 3674.4 | 1 | | |

For this spectrum, we have chosen the work of Raassen *et al.*,<sup>1</sup> who calculated M1 transition probabilities for transitions within the $3d^6$ ground configuration. These authors used a single configuration approximation in intermediate coupling. They determined eigenvector components by a parametric fitting of theoretical energy expressions to observed energy levels.

Reference

<sup>1</sup>A. J. J. Raassen, Th. A. M. van Kleef, and B. C. Metsch, Physica 84C, 133 (1976).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | gi | g. | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|----------------------------------|----------------------------------|--|---|---|---------------------------------|---------------------------------|--|---|---|---------------------------------|---------------------------------|
| 1. | 3d <sup>6</sup> -3d <sup>6</sup> | <sup>5</sup> D - <sup>3</sup> P2 | | | | | | | | | | |
| | | | [3957.2]
[3674.4]
[3600.2]
[4053.5]
[3726.7]
[4117.2]
[3752.7] | 889.7
1489.9
1871.5
1489.9
1871.5
1871.5
2057.6 | 26153
28698
29640
26153
28698
26153
28698 | 7
5
3
5
3
3
1 | 5
3
1
5
3
5
3 | M1
M1
M1
M1
M1
M1
M1 | 2.3
2.9
3.8
7(-4) <sup>a</sup>
0.0063
0.24
0.54 | $\begin{array}{c} 0.026\\ 0.016\\ 0.0066\\ 9(-6)\\ 3.6(-5)\\ 0.0031\\ 0.0032\\ \end{array}$ | E
E
E
E
E
E
E | 1
1
1
1
1
1
1 |
| 2. | | <sup>5</sup> D <sup>3</sup> H | [3625.0]
[3706.9]
[3588.5] | 0.0
889.7
0.0 | 27578
27859
27859 | 9
7
9 | 11
9
9 | M1
M1
M1 | 1.4(-4)
0.029
0.17 | 2.7(-6)
4.9(-4)
0.0026 | E
E
E | 1
1
1 |

Ni v: Forbidden transitions

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| No. | Transition
Array | Multiplet | λ
(Å) | $\frac{E_i}{(\mathrm{cm}^{-1})}$ | E_k (cm <sup>-1</sup>) | g i | g. | Type of
transition | $egin{array}{c} egin{array}{c} <i>S</i>
(at. u.) | Accu-
racy | Source | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 3. | | <sup>5</sup> D - <sup>3</sup> F2 | | | | | | | | | | |
| | | | [3432.6]
[3485.6]
[3519.0]
[3380.7]
[3446.2]
[3540.8]
[3560.1] | 0.0
889.7
1489.9
0.0
889.7
889.7
1489.9 | 29124
29571
29899
29571
29899
29124
29571
29571 | 9
7
5
9
7
7
5 | 9
7
5
7
5
9
7 | M1
M1
M1
M1
M1
M1
M1 | 2.3
1.3
0.53
0.23
0.15
0.41
0.44 | 0.031
0.014
0.0043
0.0023
0.0011
0.0061
0.0052 | EEEEEE | 1
1
1
1
1
1
1 |
| 4. | | ⁵D - ³G | [3566.9] | 1871.5 | 29899 | 3 | 5 | M 1 | 0.25 | 0.0021 | E | 1 |
| | | | [3006.1]
[3013.7]
[3036.2]
[2935.0]
[2981.8]
[2904.7] | 0.0
889.7
1489.9
0.0
889.7
0.0 | 33257
34062
34416
34062
34416
34416 | 9
7
5
9
7
9 | 11
9
7
9
7
7
7 | M1
M1
M1
M1
M1
M1 | 0.0030
0.025
0.018
0.10
0.046
0.0070 | $\begin{array}{c} 3.3(-5) \\ 2.3(-4) \\ 1.3(-4) \\ 8.4(-4) \\ 3.2(-4) \\ 4.5(-5) \end{array}$ | E
E
E
E
E | 1
1
1
1
1
1 |
| 5. | | <sup>5</sup> D – <sup>3</sup> D | [2384.8]
[2454.0]
[2486.1]
[2436.5]
[2490.7]
[2509.9]
[2472.6]
[2514.6]
[2521.7] | 0.0
889.7
1489.9
889.7
1489.9
1871.5
1489.9
1871.5
2057.6 | 41920
41627
41701
41920
41627
41701
41920
41627
41701 | 9
7
5
7
5
3
5
3
1 | 7
5
3
7
5
3
7
5
3
7
5
3 | M1
M1
M1
M1
M1
M1
M1
M1
M1
M1 | $1.2 \\ 0.12 \\ 0.018 \\ 0.34 \\ 0.57 \\ 0.76 \\ 0.22 \\ 0.44 \\ 0.62$ | $\begin{array}{c} 0.0042\\ 3.3(-4)\\ 3.1(-5)\\ 0.0013\\ 0.0016\\ 0.0013\\ 8.6(-4)\\ 0.0013\\ 0.0011\\ \end{array}$ | D
D
D
D
D
D
D
D
D
D
D
D | 1
1
1
1
1
1
1
1
1 |

Ni v: Forbidden transitions - Continued

"The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

Ni vii

Ti Isoelectronic Sequence

Ground State: 1s<sup>2</sup>2s<sup>2</sup>2p<sup>6</sup>3s<sup>2</sup>3p<sup>6</sup>3d<sup>4</sup> <sup>5</sup>D<sub>0</sub>

Ionization Energy: $133 \text{ eV} = 1070000 \text{ cm}^{-1}$

Forbidden Transitions

List of tabulated lines

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|
| 2676.2 | 4 | 2916.6 | 1 | 3026.2 | 1 | 3168.0 | 1 |
| 2685.5 | 4 | 2943.1 | 3 | 3048.2 | 3 | 3221.6 | 1 |
| 2712.5 | 4 | 2962.0 | 1 | 3054.7 | 3 | 3315.6 | 2 |
| 2728.5 | 4 | 2983.0 | 3 | 3106.2 | 3 | 3344.2 | 2 |
| 2749.9 | 4 | 2989.3 | 3 | 3131.4 | 3 | 3355.0 | 1 |
| 2795.0 | 4 | 3024.3 | 3 | 3140.2 | 1 | 3414.3 | 2 |

For this spectrum, we selected the work of Henrichs,<sup>1</sup> who calculated magnetic dipole transition probabilities for 24 lines within the $3d^4$ configuration. The calculations were performed in intermediate coupling, and the eigenvector components were determined by a least-squares fitting of theoretically derived energies to observed energy levels.

Reference

<sup>1</sup>H. F. Henrichs, Astron. Astrophys. 44, 41 (1975).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | gi | g⊧ | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|----------------------------------|--|--|---|--|--------------------------------------|--------------------------------------|--|--|--|--------------------------------------|--------------------------------------|
| 1. | 3d <sup>4</sup> -3d <sup>4</sup> | <sup>5</sup> D - <sup>3</sup> P2
(1F) | | | | | | | | | | |
| | | | [3026.2]
[3221.6]
[3355.0]
[2962.0]
[3168.0]
[2916.6] | 1520
804
279
804
279
279 | 34555
31836
30077
34555
31836
34555 | 7
5
3
5
3
3 | 5
3
1
5
3
5 | M1
M1
M1
M1
M1
M1 | 3.1
4.7
6.1
0.005
8(4)
0.11 | $\begin{array}{c} 0.016 \\ 0.017 \\ 0.0085 \\ 2(-5)^{a} \\ 1(-6) \\ 5.1(-4) \end{array}$ | E
E
E
E
E | 1
1
1
1
1 |
| 2. | | <sup>5</sup> D - <sup>3</sup> H
(2F) | [3140.2] | 0 | 31836 | 1 | 3 | M1 | 0.51 | 0.0018 | E | 1 |
| | | | [3344.2]
[3315.6]
[3414.3] | 2392
1520
2392 | 32286
31672
31672 | 9
7
9 | 11
9
9 | M1
M1
M1 | 2(-4)
0.01
0.05 | 3(-6)
1(-4)
7(-4) | E
E
E | 1
1
1 |
| 3. | | <sup>5</sup> D - <sup>3</sup> F2
(3F) | | | | | | | | | | |
| | | | [3106.2]
[3048.2]
[2989.3]
[3131.4]
[3054.7]
[3024.3]
[2983.0]
[2943.1] | 2392
1520
804
2392
1520
1520
804
279 | 34576
34317
34247
34317
34247
34576
34317
34247 | 9
7
5
9
7
7
5
3 | 9
7
5
7
5
9
7
5 | M1
M1
M1
M1
M1
M1
M1
M1 | 3.2
1.9
0.87
0.26
0.15
0.70
0.75
0.48 | 0.032
0.014
0.0043
0.0021
7.9(-4)
0.0065
0.0052
0.0023 | E
E
E
E
E
E
E
E | 1
1
1
1
1
1
1
1 |
| 4. | | <sup>5</sup> D - <sup>3</sup> G | | | | | | | | | | |
| 1 | | | [2712.5]
[2685.5]
[2676.2]
[2749.9]
[2728.5]
[2795.0] | 2392
1520
804
2392
1520
2392 | 39247
38746
38160
38746
38160
38160 | 9
7
5
9
7
9 | 11
9
7
9
7
7 | M1
M1
M1
M1
M1
M1 | 0.004
0.06
0.07
0.20
0.16
0.02 | $\begin{array}{c} 3(-5) \\ 4(-4) \\ 3(-4) \\ 0.0014 \\ 8.4(-4) \\ 1(-4) \end{array}$ | E
E
E
E
E | 1
1
1
1
1
1 |

Ni vII: Forbidden transitions

"The number in parentheses following the tabulated value indicates the power of ten by which the value has to be multiplied.

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Ni IX

F-52

Ca Isoelectronic Sequence

Ground State: 1s<sup>2</sup>2s<sup>2</sup>2p<sup>6</sup>3s<sup>2</sup>3p<sup>6</sup>3d<sup>2</sup> <sup>3</sup>F<sub>2</sub>

Ionization Energy: $193 \text{ eV} = 1560000 \text{ cm}^{-1}$

Allowed Transitions

For this spectrum, we have chosen the data of Fawcett, Ridgeley, and Ekberg.<sup>1</sup> These authors experimentally observed and classified sixteen Ni IX lines in the $3p^63d^2-3p^53d^3$ transition array. For fifteen of these lines, Fawcett *et al.* calculated oscillator strengths by the Hartree-XR method (self-consistent-field calculations with exchange, configuration interaction, and relativistic effects). We estimate these data to be accurate within fifty percent.

Reference

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<sup>1</sup>B. C. Fawcett, A. Ridgeley, and J. O. Ekberg, Phys. Scr. 21, 155 (1980).

| Ni | IX: | Allowed | transitions |
|----|-----|---------|-------------|
| | | | |

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | Bi | g. | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|--|----------------------------------|---|--------------------------------|--|-----------------------|-----------------------|--|--|------------------------------------|--|-----------------------|-----------------------|
| 1. | 3p <sup>6</sup> 3d <sup>2</sup> -
3p <sup>5</sup> (<sup>2</sup> P*)3d <sup>3</sup> (<sup>2</sup> H) | ³F − ³G° | | | | | | | | | | | |
| | | | 165.436
166.079
166.306 | 4070
1880
0 | 608530
604000
601300 | 9
7
5 | 11
9
7 | 970
870
430 | 0.49
0.46
0.25 | 2.4
1.8
0.69 | 0.64
0.51
0.10 | D
D
D | 1
1
1 |
| 2. | | <sup>1</sup> G - <sup>1</sup> G* | 147.013 | | | 9 | 9 | 4100 | 1.3 | 5 .8 | 1.08 | D | 1 |
| 3. | 3p <sup>6</sup> 3d <sup>2</sup> -
3p <sup>5</sup> (<sup>2</sup> P°)3d <sup>3</sup> (<sup>2</sup> G) | <sup>1</sup> G - <sup>1</sup> H° | 165.436 | | | 9 | 11 | 730 | 0.37 | 1.8 | 0.52 | D | 1 |
| 4. | 3p <sup>6</sup> 3d <sup>2</sup> -
3p <sup>5</sup> (<sup>2</sup> P°)3d <sup>3</sup> (<sup>4</sup> F) | <sup>3</sup> F - <sup>3</sup> F° | | | | | | | | | | | |
| | | | 150.836
151.022
151.281
150.32
150.574 | 4070
1880
0
1880
0 | 667080
664080
661050
667080
664080 | 9
7
5
7
5 | 9
7
5
9
7 | 2800
2200
2300
180
180 | 0.95
0.75
0.80
0.077
0.083 | 4.2
2.6
2.0
0.27
0.21 | 0.93
0.72
0.60
-0.27
-0.38 | D
D
D
D
D | 1
1
1
1
1 |
| 5. | | <sup>3</sup> F - <sup>3</sup> D° | | | | | | | | | | | |
| | | | 141.356
140.917
141.002
140.917
140.542 | 4070
1880
0
1880
0 | 711510
711520
709210
711510
711520 | 9
7
5
7
5 | 7
5
3
7
5 | 2600
2600
1900
120
230 | 0.61
0.56
0.33
0.034
0.068 | 2.6
1.8
0.77
0.11
0.16 | $0.74 \\ 0.59 \\ 0.22 \\ -0.62 \\ -0.47$ | D
D
D
D
D | 1
1
1
1
1 |

Ni IX

Forbidden Transitions

For this ion, we selected the work of Warner and Kirkpatrick,<sup>1</sup> who used a single-configuration approximation and calculated radial integrals with scaled Thomas-Fermi wavefunctions. We have tabulated M1 and E2 transition probabilities for 5 lines within the $3d^2$ configuration. Warner and Kirkpatrick also calculated electric quadrupole *A*-values for transitions within the $3d^2-3d4s$ transition array. We have omitted these lines, however, since accurate experimental energy levels within the $3d^2 \cdot 3f$ term, we have recalculated

Warner and Kirkpatrick's *A*-values by using observed energy-level data instead of theoretically derived values. Due to the lack of reliable observational material, we did not provide energy level values for the <sup>1</sup>D, <sup>3</sup>P, and <sup>1</sup>G terms.

Reference

<sup>1</sup>B. Warner and R. C. Kirkpatrick, Mon. Not. R. Astron. Soc. 144, 397 (1969).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | $\frac{E_k}{(\mathrm{cm}^{-1})}$ | g i | 8k | Type of
transition | $egin{array}{c} egin{array}{c} S
(at. u.) | Accu-
racy | Source | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1. | $3d^2 - 3d^2$ | <sup>3</sup> F - <sup>3</sup> F | | | | | | | | | | |
| | | | [45650]
[53180] | 1880
0 | 4070
1880 | 7
5 | 9
7 | M1
M1 | 0.21
0.17 | 6.7
6.6 | с
с | 1n
1n |
| 2. | | <sup>1</sup> D - <sup>3</sup> P | | | | | | | | | | |
| | | | [19010] | | | 5 | 5 | M 1 | 0.51 | 0.65 | Е | 1 |
| 3. | | <sup>1</sup> D - <sup>1</sup> G | [7141.9] | | | 5 | 9 | E2 | 8.1(-4) <sup>a</sup> | 0.081 | Е | 1 |
| 4. | | <sup>3</sup> P - <sup>1</sup> G | | | | | | | | | | |
| | | | [11440] | | | 5 | 9 | E 2 | 1.9(-5) | 0.020 | Е | 1 |

Ni IX: Forbidden transitions

"The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

Ni xı

Ar Isoelectronic Sequence

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44-4

Ground State: $1s^22s^22p^63s^23p^6 {}^{1}S_0$

Ionization Energy: $321.0 \text{ eV} = 2589000 \text{ cm}^{-1}$

Allowed Transitions

Line strengths for the $3p^{6}-3p^{5}3d$ resonance transitions of this argon-like ion were taken from the superpositionof-configurations (SOC) calculations of Weiss,<sup>1</sup> which are expected to be fairly accurate. The remainder of the oscillator strengths were interpolated from the Dirac-Hartree-Fock data of Lin *et al.*,<sup>2</sup> who included correlation only in the lower state.

References

| No. | Transition
Array | Multiplet | λ
(Å) | E_i (cm <sup>-1</sup>) | $\frac{E_k}{(\mathrm{cm}^{-1})}$ | gi | g. | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|--|---|----------|---------------------------|----------------------------------|----|----|--|----------------------|---------------|--------|---------------|---------|
| 1. | 3p <sup>6</sup> -3p <sup>5</sup> 3d | <sup>1</sup> S – <sup>3</sup> P° | | | | | | | | | | | |
| | | | 211.428 | 0 | 472974 | 1 | 3 | 0.14 | 2.9(-4) <sup>a</sup> | 2.0(-4) | -3.54 | Е | 1 |
| 2. | | <sup>1</sup> S - <sup>3</sup> D° | | | | | | | | | | | |
| | | | 186.976 | 0 | 534828 | 1 | 3 | 4.3 | 0.0068 | 0.0042 | -2.17 | Е | 1 |
| 3. | | <sup>1</sup> S - <sup>1</sup> P° | 148.374 | 0 | 673973 | 1 | 3 | 2340 | 2.31 | 1.13 | 0.364 | C+ | 1 |
| 4. | 3p <sup>6</sup> -
3p <sup>5</sup> (<sup>2</sup> P <sub>3/2</sub>)4s | ${}^{1}S - ({}^{3}\!/_{2}, {}^{1}\!/_{2})^{\circ}$ | | | | | | | | | | | |
| | | | 78.744 | 0 | 1269900 | 1 | 3 | 610 | 0.17 | 0.044 | -0.77 | D | interp. |
| 5. | 3p <sup>6</sup> -
3p <sup>5</sup> (<sup>2</sup> P <sub>1/2</sub>)4s | <sup>1</sup> S - (<sup>1</sup> / <sub>2</sub> , <sup>1</sup> / <sub>2</sub>)° | | | | | | | | | | | |
| | | | 77.393 | 0 | 1292100 | 1 | 3 | 850 | 0.23 | 0.059 | -0.64 | D | interp. |
| 6. | 3p <sup>6</sup> –
3p <sup>5</sup> (<sup>2</sup> P <sub>3/2</sub>)4d | <sup>1</sup> S - <sup>2</sup> [<sup>3</sup> / <sub>2</sub>]° | | | | | | | | | | | |
| | | | 63.641 | 0 | 1571300 | 1 | 3 | 2500 | 0.45 | 0.094 | -0.35 | D | interp. |
| 7. | $3p^{6}-3p^{5}(^{2}P_{1/2}^{\circ})4d$ | <sup>1</sup> S – <sup>2</sup> [<sup>3</sup> / <sub>2</sub>]° | | | | | | | | | | | |
| | | | 62.730 | 0 | 1594100 | 1 | 3 | 1200 | 0.22 | 0.045 | -0.66 | D | interp. |

Ni XI: Allowed transitions

"The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

Ni xıı

Cl Isoelectronic Sequence

Ground State: $1s^2 2s^2 2p^6 3s^2 3p^5 {}^{2}P_{3/2}^{\circ}$

Ionization Energy: $352 \text{ eV} = 2840000 \text{ cm}^{-1}$

Allowed Transitions

Line strengths for transitions of the arrays $3s^23p^5$ - $3s^3p^6$ and $3p^5-3p^43d$ are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Huang *et al.*<sup>1</sup> These relativistic calculations include a perturbative treatment of the Breit interaction and the Lamb shift. Configuration mixing was limited to some configurations within the n=3 complex. Those configurations which were assumed to lie far above $3p^5$ or $3p^43d$ in energy were excluded, as were all configurations outside the complex.

According to the semi-empirical HX (Hartree-Fock with statistical allowance for exchange) calculations of

Bromage et al.<sup>2</sup> for Fe x, some levels of the $3p^43d$ configuration are strongly mixed in the LS basis, and in a few cases the LS designations given in Ref. 2 differed from those of Huang et al. The level designations used in this compilation are in accord with the theoretical results of Refs. 1 and 2 for Fe x. Percentage compositions published by Bromage<sup>3</sup> for the levels of the $3p^43d$ configuration in V vII and Ni XII indicate that the designations for the iron ion are appropriate for the neighboring ions of the chlorine isoelectronic sequence. Transitions involving highly mixed levels have been excluded, as have the very weak transitions. The calculated wavelengths of Huang *et al.* differ appreciably from the observed ones found in the literature. Thus the available experimentally determined wavelengths were used in making the conversion from line strengths to f- and A-values. (Otherwise, the calculated wavelengths of Huang *et al.* were used, but they provide only a rough idea of the spectral-line positions.) Bromage *et al.* indicate that it was necessary to scale down some configuration-interaction parameters by a greater amount than usual in order to fit their calculated energy levels for Fe x to the experimental data. This could be an

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indication that neglecting to take configuration interaction into account on a larger scale yields significant errors in the energy levels and/or f-values.

References

- <sup>1</sup>K.-N. Huang, Y.-K. Kim, K. T. Cheng, and J. P. Desclaux, At. Data Nucl. Data Tables 28, 355 (1983).
- <sup>2</sup>G. E. Bromage, R. D. Cowan, and B. C. Fawcett, Phys. Scr. 15, 177 (1977).
- <sup>3</sup>G. E. Bromage, Astron. Astrophys., Suppl. Ser. 41, 79 (1980).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | $egin{array}{c} E_k \ (\mathrm{cm}^{-1}) \end{array}$ | g i | ₿Ł | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fix | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|--|----------------------------------|--------------------|------------------------------|---|------------|--------|--|----------------------|-------------------|----------------|---------------|--------|
| | | | | | | | | | | | | | |
| 1. | 3s <sup>2</sup> 3p <sup>5</sup> -3s3p <sup>6</sup> | <sup>2</sup> P° – <sup>2</sup> S | 302.35 | 7877 | 338615 | 6 | 2 | 73 | 0.0332 | 0.198 | 0.70 | C | 1 |
| | | | 295.321 | 0 | 338615 | 4 | 2 | 52 | 0.0337 | 0.131 | -0.87 | C- | 1 |
| | | | 317.475 | 23630 | 338015 | Z | 2 | 21 | 0.032 | 0.007 | -1.19 | 0- | 1 |
| 2. | 3p <sup>5</sup> -3p <sup>4</sup> (<sup>3</sup> P)3d | <sup>2</sup> P° – <sup>4</sup> F | | | | | | | | | | | |
| | | | [193] | | | 4 | 6 | 0.66 | 5.5(-4) <sup>a</sup> | 0.0014 | -2.66 | Е | 1 |
| 3. | | <sup>2</sup> P° – <sup>4</sup> P | | | | | | | | | | | |
| | | | [189] | | 8 | 4 | 4 | 0.49 | 2.6(-4) | 6.5(-4) | -2.98 | E | 1 |
| | | | [201]
[192] | | | 2
4 | 2
2 | 1.2
5.3 | 7.2(-4)
0.0015 | 9.5(-4)
0.0037 | -2.84
-2.23 | E | 1 |
| 4. | | 2P° - 2F | | | | | | | | | | | |
| | | | [182] | | | 4 | 6 | 0.27 | 2.0(-4) | 4.8(-4) | -3.10 | E | 1 |
| 5. | | ²₽° - ²D | 152.20 | 7877 | 66 48 9 0 | 6 | 10 | 2070 | 1.20 | 3.61 | 0.86 | C– | 1 |
| | | | 152.153 | 0 | 657233 | 4 | 6 | 2080 | 1.08 | 2.17 | 0.64 | C | 1 |
| | | | 153.174
147.847 | 23630
0 | 676375 | 24 | 4 | 1990
41 | 1.40
0.013 | 1.41
0.026 | 0.447 | D | |
| 6. | 3p <sup>5</sup> -3p <sup>4</sup> (<sup>1</sup> D)3d | ²₽° − ²F | | | | | | | | | | | |
| | | | [172] | | | 4 | 6 | 2.6 | 0.0017 | 0.0039 | -2.16 | Е | 1 |
| 7. | | ²₽° − ²S | 1 62.6 1 | 7877 | 622843 | 6 | 2 | 1900 | 0.25 | 0.79 | 0.17 | С- | 1 |
| | | | 160.554
166.88 | 0
23630 | 622843
622843 | 4
2 | 2
2 | 1400
453 | 0.27
0.189 | 0.58
0.208 | 0.04
-0.422 | C-
C- | 1
1 |
| 8. | $3p^{5}-3p^{4}(^{1}S)3d$ | ²₽° – ²D | | | | | | | | | | | |
| | | | [167]
[161] | | | 2
4 | 4 | 14
5.7 | 0.012
0.0022 | 0.013
0.0047 | -1.63 - 2.05 | D
E | 1
1 |

Ni XII: Allowed transitions

"The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

Ni xu

Forbidden Transitions

Line strengths for the magnetic dipole and electric quadrupole contributions to the transition between the two levels of the $3p^5$ configuration are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Huang *et al.*<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for mixing among odd-parity configurations was limited to the set $3s^23p^5$, $3s3p^53d$, $3p^53d^2$, and $3s^23p^33d^2$. The strength of the electric

quadrupole transition as defined in Ref. 1 was multiplied by the factor 2/3 which is needed to bring this value into conformance with the definition of quadrupole strengths used in the NBS tables.

Reference

<sup>1</sup>K.-N. Huang, Y.-K. Kim, K. T. Cheng, and J. P. Desclaux, At. Data Nucl. Data Tables 28, 355 (1983).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i (cm <sup>-1</sup>) | $\frac{E_k}{(\mathbf{cm}^{-1})}$ | g i | 8 k | Type of
transition | $egin{array}{c} egin{array}{c} S
(at. u.) | Accu-
racy | Source | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1. | 3p <sup>5</sup> -3p <sup>5</sup> | ²₽° – ²₽° | 4231.4 | ,0
," | 23630
, | 4 | 2
2 | M1
E2 | 237
0.080 | 1.33
0.13 | B
D- | 1 1 |

Ni XII: Forbidden transitions

Ni xui

S Isoelectronic Sequence

Ground State: $1s^22s^22p^63s^23p^{4}{}^{3}P_2$

Ionization Energy: $384 \text{ eV} = 3100000 \text{ cm}^{-1}$

Allowed Transitions

Oscillator strengths are tabulated for a few transitions of the arrays $3s^23p^4-3s^3p^5$ and $3p^4-3p^33d$. These are the results of the Hartree-XR (Hartree-Fock with relativistic effects and statistical allowance for exchange) calculations of Bromage.<sup>1</sup> The percentage compositions are in good agreement with those of Bromage *et al.*<sup>2</sup> for Fe XI. The term designations used here are in accord with the results of these two sources. Transitions involving levels of low purity in LS coupling are omitted, as are very weak transitions.

References

<sup>1</sup>G. E. Bromage, Astron. Astrophys., Suppl. Ser. 41, 79 (1980).

<sup>2</sup>G. E. Bromage, R. D. Cowan, and B. C. Fawcett, Phys. Scr. 15, 177

(1977).

| Ni XIII: | All | owed | transitions |
|----------|-----|------|-------------|
|----------|-----|------|-------------|

| No. | Transition
Array | Multiplet | λ
(Å) | E_i (cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | ₿k | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fa | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|---|---|-------------------------------|---------------------------|---------------------------|-------------|-------------|--|----------------------|---------------------|------------------------|---------------|-------------|
| 1. | $3s^23p^4-3s^3p^5$ | <sup>3</sup> P - <sup>3</sup> P° | | | | | | | | | | | |
| | | | 302.844 | 0 | 330203 | 5 | 5 | 29 | 0.040 | 0.20 | -0.70 | D | 1 |
| 2. | | <sup>1</sup> D - <sup>1</sup> P ° | 267.468 | 47033 | 420910 | 5 | 3 | 100 | 0.066 | 0.29 | -0.48 | D | 1 |
| 3. | $3p^{4}-3p^{3}(^{2}D^{\circ})3d$ | <sup>3</sup> P - <sup>3</sup> P° | | | | | | | | | | | |
| | | | 164.15
[165.2]
[169.59] | 0
19542 | 609200
609200 | 5
3
3 | 5
1
5 | 1300
1700
210 | 0.52
0.23
0.15 | 1.4
0.38
0.25 | 0.41
-0.16
-0.35 | D
D
D | 1
1
1 |
| 4. | | <sup>3</sup> P - <sup>1</sup> D° | | | | | | | | | | | |
| | | | [154.69] | 19542 | 666000 | 3 | 5 | 150 | 0.087 | 0.13 | -0.58 | D | 1 |
| 5. | | <sup>1</sup> D – <sup>1</sup> D ° | 161.56 | 47033 | 666000 | 5 | 5 | 1400 | 0.54 | 1.4 | 0.43 | с | 1 |
| 6. | 1 | <sup>1</sup> D − <sup>1</sup> F° | 157.55 | 47033 | 681750 | 5 | 7 | 1920 | 1.00 | 2.59 | 0.70 | с | 1 |
| 7. | 3p <sup>4</sup> -3p <sup>3</sup> (<sup>2</sup> P°)3d | <sup>3</sup> P - <sup>3</sup> P° | | | | | | | | | | | |
| | | | [174.0] | | | 5 | 5 | 88 | 0.040 | 0.11 | -0.70 | D | 1 |
| 8. | | <sup>1</sup> S - <sup>1</sup> P° | 161.78 | 97836 | 715960 | 1 | 3 | 1640 | 1.93 | 1.03 | 0.286 | с | 1 |

Ni XIII

Forbidden Transitions

Transition probabilities for magnetic dipole and electric quadrupole lines within the $3p^4$ configuration are the results of the scaled Thomas-Fermi calculations of Mendoza and Zeippen.<sup>1</sup> They included a number of correlation configurations in their basis set and introduced Breit-Pauli relativistic corrections as a perturbation to the nonrelativistic Hamiltonian.

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Reference

<sup>1</sup>C. Mendoza and C. J. Zeippen, Mon. Not. R. Astron. Soc. 202, 981 (1983).

λ (Å) $egin{array}{c} A_{ki} \ (\mathbf{s}^{-1}) \end{array}$ \boldsymbol{s} No. Transition Multiplet Type of Accu-Source E_i E_k g_i ₿k (cm<sup>-1</sup>) (cm^{-1}) transition (at. u.) Array racy ${}^{3}P - {}^{3}P$ $3p^{4}-3p^{4}$ 1. 157 2.34 C+ 19542 3 1 5116.03 0 5 M1 . . 5 3 **E**2 0.019 0.12 D-1 20040 1.9 [201000] 19542 3 M1 0.0063 $\mathbf{D}+$ 1 1 20040 0.036 0.066 Е [4988.6] 0 5 1 $\mathbf{E}2$ 1 ${}^{3}P - {}^{1}D$ 2. Е 2125.50 47033 5 5 M1 260 0.46 1 0 . 0.053 . 5 5 $\mathbf{E2}$ 0.41 Е 1 [3636.5] 19542 47033 3 5 **M**1 18 0.16 Е 1 0.0044 3 E20.0083 Е $\mathbf{5}$ 1 [3703.6] 20040 47033 1 5 E20.0034 0.0071 Е 1 3. ${}^{3}P - {}^{1}S$ [1022.1] 97836 0.0021 0 $\mathbf{5}$ 1 E23.1 Е 1 1277.23 19542 97836 3 1 M1 2500 0.19 Е 1

Ni XIII: Forbidden transitions

Ni xıv

97836

5 1

E2

12

0.21

D- 1

P Isoelectronic Sequence

4.

Ground State: 1s<sup>2</sup>2s<sup>2</sup>2p<sup>6</sup>3s<sup>2</sup>3p<sup>3</sup> <sup>4</sup>S<sup>\*</sup><sub>3/2</sub>

Ionization Energy: $430 \text{ eV} = 3470000 \text{ cm}^{-1}$

 ${}^{1}D - {}^{1}S$

[1968.4]

47033

Allowed Transitions

List of tabulated lines

| | Wavelength (A) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|------|---|--|----------------|------|--|--|
| 16 | 170 16 | 15 | 101 | 14 | 900 200 | |
| 10 | 172.10 | 15 | 191 | 14 | 292.399 | 3 |
| 13 | 172.80 | 15 | 192 | 5,12 | 295.55 | 3 |
| 16 | 177.28 | 18 | 196 | 12 | 297 | 1 |
| 10 🍴 | 178 | 17 | 198 | 12 | 302.264 | 1 |
| 18 | 181 | 17 | 213 | 8 | 316.113 | 1 |
| 6 | 182.14 | 9 | 216 | 8 | 324 | 4 |
| 6 | 185.96 | 9 | 225 | 7 | 332 | 4 |
| 15 | 186.66 | 9 | 239 | 11 | 336 | 4 |
| 15 | 188.69 | 9 | 285.88 | 3 | 369.58 | 2 |
| 6 | 189 | 5 | 288.894 | 3 | | - |
| | 6
3
6
0
8
6
6
5
5
5
6 | 6 172.16 3 172.80 6 177.28 0 178 8 181 6 182.14 6 185.96 5 186.66 5 188.69 6 189 | | | $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ |

(a)
Line strengths for transitions of the arrays $3s^23p^3$ - $3s^3p^4$ and $3p^3-3p^23d$ are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Huang.<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing was limited to configurations within the n=3 complex having no more than two electrons in the 3d subshell.

Huang published neither an energy-level diagram nor percentage compositions for levels of the $3s^23p^3$, $3s^3p^4$, and $3s^23p^23d$ configurations in Ni XIV. We have used the percentages given by Bromage *et al.*<sup>2</sup> for Fe XII, and by Bromage<sup>3</sup> for V IX and Ni XIV, as a guide to naming the levels; their values resulted from Hartree-Fock calculations with relativistic effects and statistical allowance for exchange (HXR), and incorporated correlation effects due to a few configurations within the n = 3 complex.

in a

Whenever a term designation of a level in Fe XII, as given in Ref. 1, is different from that indicated in Ref. 2, all transitions involving the corresponding level in Ni XIV are omitted from this compilation.

Transitions involving levels which are indicated to be of low purity in LS coupling are omitted here. Lines which are characterized by very small f-values are assigned lower accuracy ratings; the weakest lines have been excluded.

References

<sup>1</sup>K.-N. Huang, At. Data Nucl. Data Tables 30, 313 (1984).

<sup>2</sup>G. E. Bromage, R. D. Cowan, and B. C. Fawcett, Mon. Not. R. Astron. Soc. 183, 19 (1978).

<sup>3</sup>G. E. Bromage, Astron. Astrophys., Suppl. Ser. 41, 79 (1980).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | ₿k | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | <i>fi</i> h | <i>S</i>
(at. u.) | log gf | Accu-
racy | Source |
|-----|--|----------------------------------|------------------|------------------------------|---------------------------|------------|--------|--|---------------|----------------------|--------|---------------|--------|
| 1 | 3e <sup>2</sup> 3p <sup>3</sup> -3e3p <sup>4</sup> | 4S° _ 4P | 308 | | | 4 | 12 | 21 | 0.091 | 0.37 | 0.44 | D | 1 |
| 1. | 03 0p 08 0p | · · | 000 | | | - | | | | | | _ | |
| | | | 316.113 | 0 | 316343 | 4 | 6 | 20 | 0.046 | 0.19 | -0.74 | D | 1 |
| | | | 302.264
[297] | U | 330837 | 4 | 4
2 | 24 | 0.030 | 0.12 | -1.19 | D | 1 |
| 2. | | ²D° - ⁴P | | | | | | | | | | | |
| | | | [369.58] | 45769 | 316343 | 4 | 6 | 0.34 | 0.0010 | 0.0051 | -2.38 | Е | 1 |
| 3. | | <sup>2</sup> D° – <sup>2</sup> D | 290.99 | 5044 9 | 39 4107 | 10 | 10 | 40 | 0.051 | 0.49 | -0.29 | D- | 1 |
| | | | 292.399 | 53569 | 395567 | 6 | 6 | 36 | 0.047 | 0.27 | -0.55 | D | 1 |
| | | | 288.894 | 45769 | 391917 | 4 | 4 | 46 | 0.058 | 0.22 | -0.64 | D | 1 |
| | | | [295.55] | 53569 | 391917 | 6 | 4 | 0.16 | $1.4(-4)^{a}$ | 8.3(-4) | -3.07 | E | 1 |
| | | | [285.88] | 45769 | 395567 | 4 | 6 | 0.11 | 2.0(-4) | 7.7(-4) | 3.09 | E | 1 |
| 4. | | <sup>2</sup> P° - <sup>2</sup> D | 330 | | | 6 | 10 | 6.2 | 0.017 | 0.11 | 0.99 | E | 1 |
| | | | [332] | | | 4 | 6 | 7.8 | 0.019 | 0.084 | -1.11 | D | 1 |
| | | | [324] | | | 2 | 4 | 3.7 | 0.012 | 0.025 | -1.63 | D | 1 |
| | | | [336] | | | 4 | 4 | 0.44 | 7.5(-4) | 0.0033 | -2.53 | E | 1 |
| 5. | 3p <sup>3</sup> -3p <sup>2</sup> (<sup>3</sup> P)3d | 4S° – 4D | | | | | | | | | | | |
| | | | [189] | | | 4 | 6 | 6.0 | 0.0048 | 0.012 | -1.71 | Е | 1 |
| | | 1 | [192] | | | 4 | 4 | 5.4 | 0.0030 | 0.0075 | -1.93 | Е | 1 |
| 6. | | ⁴S° - ⁴P | 170.26 | 0 | 587 3 40 | 4 | 12 | 960 | 1.2 | 2.8 | 0.70 | D | 1 |
| | | | 171.37 | 0 | 583530 | 4 | 6 | 940 | 0.62 | 1.4 | 0.39 | D | 1 |
| | | | 169.69 | 0 | 589310 | 4 | 4 | 980 | 0.43 | 0.95 | 0.23 | D | 1 |
| | | | 168.12 | 0 | 594810 | 4 | 2 | 850 | 0.18 | 0.40 | -0.14 | D | 1 |
| 7. | | ²D° - 4F | | | | | | | | | | | |
| | | | [225] | | | 4 | 4 | 3.2 | 0.0025 | 0.0073 | -2.01 | Е | 1 |

Ni xIV: Allowed transitions

Ni XIV: Allowed transitions - Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | g, | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | <i>S</i>
(at. u.) | log gf | Accu-
racy | Source |
|-----|--|----------------------------------|--|----------------------------------|--------------------------------------|------------------|------------------|--|------------------------------------|----------------------------------|------------------------------------|------------------|------------------|
| 8. | | ²D° – 4D | | | | | | | | | | | |
| | | | [213]
[216]
[213] | | | 6
6
4 | 6
4
2 | 1.9
6.5
8.1 | 0.0013
0.0030
0.0027 | 0.0055
0.013
0.0077 | -2.11
-1.74
-1.96 | E
E
E | 1
1
1 |
| 9. | | <sup>2</sup> D° – <sup>4</sup> P | | | | | | | | | | | |
| | | | [188.69]
[186.66]
[182.14]
[185.96] | 53569
53569
45769
45769 | 583530
589310
594810
583530 | 6
6
4
4 | 6
4
2
6 | 19
9.3 •
150
10 | 0.010
0.0033
0.037
0.0078 | 0.038
0.012
0.089
0.019 | $-1.21 \\ -1.71 \\ -0.83 \\ -1.51$ | E
E
E | 1
1
1
1 |
| 10. | | <sup>2</sup> D° - <sup>2</sup> F | | | | | | | | | | | |
| | | | 164.13 | 53569 | 662840 | 6 | 8 | 1200 | 0.65 | 2.1 | 0.59 | Е | 1 |
| 11. | | <sup>2</sup> P° – <sup>4</sup> D | | | | | | | | | | | |
| | | | [239] | | | 4 | 2 | 4.7 | 0.0020 | 0.0064 | -2.09 | Е | 1 |
| 12. | | <sup>2</sup> P° – <sup>4</sup> P | | | | | | | | | | | |
| | | | [198]
[192]
[196] | | | 4
2
4 | 4
2
2 | 4.0
29
38 | 0.0023
0.016
0.011 | 0.0061
0.020
0.028 | -2.03
-1.50
-1.36 | E
E
E | 1
1
1 |
| 13. | 3p <sup>3</sup> -3p <sup>2</sup> (<sup>1</sup> D)3d | ⁴S° - ²D | | | | | | | | | | | |
| | | | [157. 62] | 0 | 634430 | 4 | 6 | 2.3 | 0.0013 | 0.0027 | -2.28 | Е | 1 |
| 14. | | ²D° - ²G | | | | | | | | | | | |
| | | | [191] | | | 6 | 8 | 5.1 | 0.0037 | 0.014 | -1.65 | Е | 1 |
| 15. | | <sup>2</sup> D° – <sup>2</sup> D | 171.49 | 50449 | 633570 | 10 | 10 | 640 | 0.28 | 1.6 | 0.45 | D | 1 |
| | | | 172.16
170.50
[172.80]
[169.88] | 53569
45769
53569
45769 | 634430
632280
632280
634430 | 6
4
6
4 | 6
4
4
6 | 470
710
140
17 | 0.21
0.31
0.041
0.011 | 0.71
0.69
0.14
0.025 | $0.10 \\ 0.09 \\ -0.61 \\ -1.35$ | D
D
D
D | 1
1
1
1 |
| 16. | | <sup>2</sup> D° – <sup>2</sup> P | | | | | | - | | | | | |
| | | | [159]
[157] | | | 6
4 | 4
4 | 8.4
22 | 0.0021
0.0082 | 0.0067
0.017 | $-1.89 \\ -1.48$ | E
E | 1 |
| 17. | | <sup>2</sup> P• - <sup>2</sup> D | 180 | | | 6 | 10 | 83 | 0.068 | 0.24 | -0.39 | Е | 1 |
| | | | [181]
[178]
[181] | | | 4
2
4 | 6
4
4 | 74
89
7.4 | 0.055
0.084
0.0037 | 0.13
0.099
0.0087 | $-0.66 \\ -0.77 \\ -1.84$ | D
D
E | 1
1
1 |
| 18. | | <sup>2</sup> P* – <sup>2</sup> P | | | | | | | | | | | |
| | | | 177.28
[168] | | | 4
2 | 4
4 | 560
240 | 0.27
0.20 | 0.62
0.22 | 0.03
0.40 | E
E | 1 |

Ni xiv

Forbidden Transitions

Line strengths for magnetic dipole and electric quadrupole transitions within the $3p^3$ configuration are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Huang.1 These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing was limited to configurations within the n=3 complex having no more than two electrons in the 3d subshell. Strengths of electric quadrupole transitions as defined in Ref. 1 were multiplied by the factor $\frac{2}{3}$ which is needed to bring these values into conformance with the definition of quadrupole strengths used in the NBS tables. We have excluded from this compilation the electric quadrupole contributions to the ${}^{4}S_{3/2}^{\circ} - {}^{2}P_{3/2}^{\circ}$ and ${}^{4}S_{3/2}^{\circ} - {}^{2}P_{1/2}^{\circ}$ transitions, since their strengths are very small and thus subject to considerable uncertainty.

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<u>کیت</u>

Data for these same transitions calculated by Mendoza and Zeippen<sup>2</sup> with the scaled Thomas-Fermi approach with allowance for correlation are generally in very good agreement with the results of Ref. 1. These latter calculations treated relativistic effects by introducing Breit-Pauli corrections as a perturbation to the nonrelativistic Hamiltonian.

References

<sup>1</sup>K.-N. Huang, At. Data Nucl. Data Tables **30**, 313 (1984).
 <sup>2</sup>C. Mendoza and C. J. Zeippen, Mon. Not. R. Astron. Soc. **198**, 127 (1982).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i (cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | g i | gx | Type of
transition | $egin{array}{c} egin{array}{c} <i>S</i>
(at. u.) | Accu-
racy | Source | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1. | 3p <sup>3</sup> -3p <sup>3</sup> | ⁴S° ~ 2D° | | | | | | | | | | |
| | | | 1866.75
2184.20 | .0
.0 | 53569
45769 | 4
4
4
4 | 6
6
4
4 | M1
E2
M1
E2 | 7.6
0.23
160
0.077 | 0.011
0.019
0.25
0. 009 1 | D
E
C
E | 1
1
1
1 |
| 2. | | ⁴S° –²P° | | | | | | | | | | |
| | | | [1030]
[1180] | | | 4
4 | 4
2 | M1
M1 | 740
460 | 0.12
0.056 | C
D | 1
1 |
| 3. | | <sup>2</sup> D° – <sup>2</sup> D° | | | | | | | | | | |
| | | | [12817] | 45769
, | 53569
″ | 4
4 | 6
6 | M1
E2 | 4.27
5.3(-5) <sup>a</sup> | 2.00
0.066 | C+
E | 1
1 |
| 4. | | <sup>2</sup> D° - <sup>2</sup> P° | | | | | | | | | | |
| | | | [3170]
[2320]
[2540]
[1960] | | | 6
6
4
4
4 | 2
4
2
2
4
4 | E2
M1
E2
M1
E2
M1
E2 | 0.34
210
2.3
160
1.4
600
1.3 | 0.13
0.39
0.37
0.19
0.17
0.67
0.087 | D-
C
D-
C
D-
C
E | 1
1
1
1
1
1
1 |
| 5. | | <sup>2</sup> P° – <sup>2</sup> P° | | | | | | | | | | |
| | | | [8620] | | | 2
2 | 4
4 | M1
E2 | 11.4
2.6(-4) | 1.08
0.029 | C+
E | 1
1 |

Ni XIV: Forbidden transitions

Ni xv

Si Isoelectronic Sequence

Ground State: $1s^22s^22p^63s^23p^2 {}^{3}P_0$

Ionization Energy: $464 \text{ eV} = 3740000 \text{ cm}^{-1}$

Allowed Transitions

List of tabulated lines

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|
| 50.249 | 14 | 179.28 | 7 | 258 | 2 | 311.756 | 1 |
| 60.890 | 15 | 181 | 13 | 268 | 2 | 312.03 | 1 |
| 64.635 | 16 | 191.45 | 11 | 269 | 2 | 319.063 | 1 |
| 149 | 9 | 206 | 5 | 269.05 | 2 | 324.35 | 1 |
| 163.64 | 8 | 208 | 5 | 278 | 2 | 324.65 | 1 |
| 173.73 | 12 | 212 | 5 | 278.386 | 2 | 359.78 | 3 |
| 175 | 6 | 231 | 10 | 298.15 | 1 | 367 | 4 |

Line strengths for transitions of the arrays $3s^23p^2$ - $3s^3p^3$ and $3p^2-3p^3d$ are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Huang.<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing included all configurations within the n = 3 complex.

Huang published neither an energy-level diagram nor percentage compositions for levels of the $3s^23p^2$, $3s3p^3$, and $3s^23p3d$ configurations in Ni xv. We have used the percentages given by Bromage *et al.*<sup>2</sup> for Fe XIII, and by Bromage<sup>3</sup> for V x and Ni xv, as a guide to naming the levels; their values resulted from Hartree-Fock calculations with relativistic effects and statistical allowance for exchange (HXR), and incorporated correlation effects due to a partial set of configurations within the n=3complex. Whenever the term designation of a level in Fe XIII, as given in Ref. 1, is different from that indicated in Ref. 2, all transitions involving the corresponding level in Ni xv are omitted from this compilation. A few *f*-values for transitions to configurations in which one electron occupies the n=4 shell were interpolated from the results of Kastner *et al.*<sup>4</sup> for Fe XIII and Zn XVII, which were computed by a multiconfiguration scaled Thomas-Fermi approach.

Transitions involving levels which are indicated to be of low purity in LS coupling are omitted here. Lines which are characterized by very small f-values are assigned lower accuracy ratings; the weakest lines have been excluded.

References

- <sup>1</sup>K.-N. Huang, At. Data Nucl. Data Tables 32, 503 (1985).
- <sup>2</sup>G. E. Bromage, R. D. Cowan, and B. C. Fawcett, Mon. Not. R. Astron. Soc. 183, 19 (1978).
- <sup>3</sup>G. E. Bromage, Astron. Astrophys., Suppl. Ser. 41, 79 (1980).
- <sup>4</sup>S. O. Kastner, M. Swartz, A. K. Bhatia, and J. Lapides, J. Opt. Soc. Am. 68, 1558 (1978).

| _ | No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_{k} (cm <sup>-1</sup>) | g i | ₿ŧ | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|---|-----|---|----------------------------------|--|--|--|-----------------------|----------------------------|--|--|--|---|-------------------|------------------|
| | 1. | 3s <sup>2</sup> 3p <sup>2</sup> –3s 3p <sup>3</sup> | <sup>3</sup> P - <sup>3</sup> D• | 314.63 | 20181 | 338010 | 9 | 15 | 18 | 0.044 | 0.41 | -0.40 | Е | 1 |
| | | | | 319.063
311.756
298.15
[324.35]
[312.03]
[324.65] | 27376
14917
0
27376
14917
27376 | 340794
335681
335400
335681
335400
235400 | 5
3
1
5
3 | 7
5
3
5
3
3 | 15
20
19
0.21
3.3
0.20 | $\begin{array}{c} 0.032 \\ 0.049 \\ 0.074 \\ 3.4(-4)^{a} \\ 0.0049 \\ 1.9(-4) \end{array}$ | 0.17
0.15
0.073
0.0018
0.015 | -0.79
-0.84
-1.13
-2.77
-1.84 | D
D
E
D- | 1
1
1
1 |
| | | | | [324.65] | 21316 | 335400 | Э | 3 | 0.20 | 1.9(-4) | 0.0010 | -3.03 | Е | 1 |

Ni xv: Allowed transitions

| F-(| 63 |
|-----|----|
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Ni xv: Allowed transitions - Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | <i>E</i> <sub>i</sub>
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | gi | gr | $\begin{array}{c} A_{ki} \\ (10^8 \ \mathrm{s}^{-1}) \end{array}$ | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|---|-----------------------|---|---|--|------------------------------|----------------------------|----------------------------|---|--|---|--|--------------------------|-----------------------|
| 2. | | <sup>3</sup> P – <sup>3</sup> P° | 272 | -
-
- | | 9 | 9 | 50 | 0.056 | 0.45 | -0.30 | D | 1 |
| generative and the second second second second second second second second second second second second second s | | | 278.386
[268]
[278]
[269]
[269.05]
[258] | 27376
14917 | 386589
386589 | 5
3
5
3
3
1 | 5
3
3
1
5
3 | 43
28
9.4
53
3.7
16 | 0.050
0.030
0.0066
0.019
0.0068
0.047 | 0.23
0.079
0.030
0.051
0.018
0.040 | -0.60
-1.05
-1.48
-1.24
-1.69
-1.33 | D
D
D-
C-
D- | 1
1
1
1
1 |
| 3. | | <sup>1</sup> D – <sup>3</sup> D ° | [200] | | | | | 10 | 0.041 | 0.040 | -1.00 | | * |
| | | | [359.78] | 62849 | 340794 | 5 | 7 | 1.7 | 0.0047 | 0.028 | -1.63 | Е | 1 |
| 4. | | <sup>1</sup> S - <sup>3</sup> P° | | | | | | | | | | | |
| | | | [367] | | | 1 | 3 | 0.41 | 0.0025 | 0.0030 | -2.61 | Е | 1 |
| 5. | 3p <sup>2</sup> -3p3d | <sup>3</sup> P - <sup>3</sup> F° | | | | | | | | | | | |
| | | | [208]
[206]
[212] | | | 5
3
5 | 7
5
5 | 6.1
2.0
3.1 | 0.0055
0.0022
0.0021 | 0.019
0.0044
0.0074 | -1.56
-2.19
-1.97 | E
E
E | 1
1
1 |
| 6. | | <sup>3</sup> P - <sup>3</sup> P° | | | | | | | | | | | |
| | | | [175] | | , | 3 | 1 | 570 | 0.087 | 0.15 | -0.58 | D | 1 |
| 7. | | <sup>3</sup> P ~ <sup>3</sup> D° | | | -
- | | | | | | | | |
| | | | 179.28 | 27376 | 585170 | 5 | 7 | 750 | 0.51 | 1.5 | 0.41 | D | 1 |
| 8. | | <sup>3</sup> P - <sup>1</sup> F <sup>•</sup> | | | | | | | | | | _ | |
| 0 | | 3n 1nº | [163.64] | 27376 | 638460 | 5 | 7 | 56 | 0.032 | 0.085 | -0.80 | Е | |
| 9. | | r-r | [149] | | | 1 | 3 | 7.1 | 0.0071 | 0.0035 | -2.15 | Е | 1 |
| 10. | | <sup>1</sup> D - <sup>3</sup> F° | [1:0] | | | | | | | 0.0000 | | - | - |
| | | | [231] | | 1 | 5 | 5 | 5.9 | 0.0047 | 0.018 | -1.63 | Е | 1 |
| 11. | | <sup>1</sup> D - <sup>3</sup> D* | | | | | | | | | | | |
| | | | [191.45] | 62849 | 585170 | 5 | 7 | 41 | 0.032 | 0.10 | -0.80 | Е | 1 |
| 12. | | <sup>1</sup> D - <sup>1</sup> F° | 173.73 | 62849 | 638460 | 5 | 7 | 760 | 0.479 | 1.37 | 0.379 | с | 1 |
| 13. | | <sup>1</sup> S - <sup>1</sup> P° | [181] | | | 1 | 3 | 680 | 1.0 | 0.60 | 0.00 | D | 1 |
| 14. | 3p <sup>2</sup> –3p4d | <sup>1</sup> D - <sup>1</sup> F* | 50.249 | 62849 | 2052900 | 5 | 7 | 6800 | 0.36 | 0.30 | 0.26 | D | interp. |
| 15. | 3p3d-3p4f | <sup>3</sup> F° - <sup>3</sup> G | | | | | | | | | | | |
| | | | 60.890 | | | 9 | 11 | 1.0(+4) <sup>a</sup> | 0.71 | 1.3 | 0.81 | D | interp. |
| 16. | | <sup>1</sup> F ° - <sup>1</sup> G | 64.635 | 638460 | 2185600 | 7 | 9 | 9600 | 0.77 | 1.1 | 0.73 | E | interp. |

Ni xv

Forbidden Transitions

List of tabulated lines

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|--|
| 335.94 | 12 | 720 | 6 | 1954 | 8 | 2818.2 | 2 | |
| 401 | 10 | 730 | 6 | 1964.3 | 8 | 3651.8 | 1 | |
| 409.20 | 11 | 1030 | 3 | 2000 | 8 | 6701.7 | 1 | |
| 530 | 9 | 1100 | 5 | 2040 | 4 | 8024.1 | 1 | |
| 550 | 9 | 1190 | 3 | 2085.61 | 2 | 18500 | 7 | |
| 580 | 9 | 1200 | 5 | 2183.0 | 8 | 19550 | 7 | |
| 620 | 9 | 1900 | 8 | 2200 | 8 | 360000 | 7 | |

Line strengths for magnetic dipole and electric quadrupole transitions are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Huang.<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration interaction encompassed all configurations within the n=3 complex. Huang calculated line strengths for transitions within the $3p^2$ configuration, as well as for transitions between pairs of odd-parity levels whose lower level is one of the four lowest-lying odd-parity levels in the n=3 complex. Transitions involving odd-parity levels which are indicated by Bromage *et al.*<sup>2</sup> (for Fe XIII) or Bromage<sup>3</sup> (for V x and Ni xv) to be of low purity in *LS* coupling in

Fe-group species are omitted here, as are lines whose strengths are very small. Strengths of electric quadrupole transitions as reported in Ref. 1 were multiplied by the factor $^{2}/_{3}$ which is needed to bring these values into conformance with the definition of quadrupole strengths used in the NBS tables.

References

<sup>1</sup>K.-N. Huang, At. Data Nucl. Data Tables 32, 503 (1985).

<sup>2</sup>G. E. Bromage, R. D. Cowan, and B. C. Fawcett, Mon. Not. R. Astron. Soc. 183, 19 (1978).

<sup>3</sup>G. E. Bromage, Astron. Astrophys., Suppl. Ser. 41, 79 (1980).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | gi | g. | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|---------------------|---------------------------------|-----------------------------------|------------------------------|------------------------------|------------------|------------------|-----------------------|---|--------------------------------|--------------------|------------------|
| 1. | $3p^2 - 3p^2$ | <sup>3</sup> P - <sup>3</sup> P | | | | * | | | | | | |
| | | | 8024.1
,
6701.7
[3651.8] | 14917
″
0
0 | 27376
14917
27376 | 3
3
1
1 | 5
5
3
5 | M1
E2
M1
E2 | 22.7
9.9(-4) <sup>a</sup>
56.5
0.030 | 2.17
0.098
1.89
0.058 | C+
E
C+
E | 1
1
1
1 |
| 2. | | <sup>3</sup> P - <sup>1</sup> D | | | | | | | | | | |
| | | | [2818.2]
2085.61 | 27376
 | 62849
"
62849 | 5
5
3
3 | 5
5
5
5 | M1
E2
M1
E2 | 200
0.17
200
0.12 | 0.85
0.091
0.33
0.014 | E
E
E
E | 1
1
1
1 |
| 3. | | <sup>3</sup> P ~ <sup>1</sup> S | | | | | | | | | | |
| | | | [1190]
[1030] | | | 5
3 | 1
1 | E2
M1 | 9.2
2500 | 0.013
0.10 | E
E | 1
1 |
| 4. | | <sup>1</sup> D - <sup>1</sup> S | [2040] | | | 5 | 1 | E2 | 9.0 | 0.19 | D- | 1 |

Ni xv: Forbidden transitions

| F- | - 6 | 5 |
|----|-----|---|
| _ | _ | _ |

Ni xv: Forbidden transitions - Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | g i | g. | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|---|-----------------------------------|---------------------|------------------------------|------------------------------|-------------|--------|-----------------------|---------------------------------------|-----------------|---------------|--------|
| 5. | 3s 3p <sup>3</sup> -3s 3p <sup>3</sup> | <sup>5</sup> S° – <sup>3</sup> D° | | | | | | | | | | |
| | | | [1100] | - | · | 5 | 7 | M1
F2 | 6.4 | 0.0022 | E | 1 |
| | | | [1200] | | | 5 | 5 | M1
F2 | 130 | 0.043 | E | 1 |
| | | | [1200] | * | | 5
5
5 | 3 | M1
E2 | 43
0.27 | 0.0048 | E
E
E | 1 |
| 6. | | <sup>5</sup> S° – <sup>3</sup> P° | | | | | | | | | | |
| | | | [720]
[730] | | | 5
5 | 5
3 | M1
M1 | 1400
830 | 0.097
0.036 | E
E | 1
1 |
| 7. | | <sup>3</sup> D° – <sup>3</sup> D° | | | | | | | | | | |
| | | | [19550] | 335681
* | 340794 | 5 | 7 | M1
E2 | 2.20
3.4(-6) | 4.27 | C-
E | 1 |
| | | | [360000]
[18500] | 335400
335400 | 335681
340794 | 3 | 5
7 | M1
E2 | 5.0(-4)
1.3(-6) | 4.3
0.012 | Ē | 1
1 |
| 8. | | <sup>3</sup> D° – <sup>3</sup> P° | | | | | | | | | | |
| | | | [2200]
[2000] | | | 75 | 3 | E2
E2 | 2.2
6.8 | 0.20 | D-
D- | 1 |
| | | | [2183.0] | 340794 | 386589
″ | 777 | 55 | M1
E2 | 190
2.3 | 0.37 | E
D- | 1 |
| | | | [2000]
[2000] | | | 5
3 | 3
1 | E2
M1 | 0.54
330 | 0.031 0.099 | E
E | 1 |
| | | | [1964.3] | 335681
″ | 386589
″ | 5
5 | 5
5 | M1
E2 | 180
2.1 | 0.25
0.18 | E
D- | 1
1 |
| | | | [1900]
″ | | - | 3 | 3
3 | M1
E2 | 380
3.6 | 0.29
0.16 | E
D- | 1
1 |
| | | | [1954] | 335400
* | 386589
* | 3
3 | 5
5 | M1
E2 | 51
0.86 | 0.070
0.073 | E
E | 1
1 |
| 9. | 3s3p <sup>3</sup> -3s <sup>2</sup> 3p3d | <sup>3</sup> D° – <sup>3</sup> F° | | | | | | | | | | |
| | | | [530]
[580] | | | 5
3 | 9
7 | E2
E2 | 23
8.4 | 0.0051 0.0023 | E
E | 1 |
| | | | [550]
[620] | | | 7
5 | 9
5 | M1
M1 | 1100
45 | 0.059
0.0020 | E
E | 1
1 |
| 10. | | <sup>3</sup> D° – <sup>3</sup> P° | | | | | | | | | | |
| | | | [401] | | | 5 | 1 | E2 | 440 | 0.0027 | Е | 1 |
| 11. | | <sup>3</sup> D° - <sup>3</sup> D° | | | | | | | | | | |
| | | | [409.20] | 340794 | 585170 | 7 | 7 | M 1 | 84 | 0.0015 | E | 1 |
| 12. | | <sup>3</sup> D° − <sup>1</sup> F° | | | | _ | _ | | 100 | 0.0010 | | |
| | | | [335.94] | 340794 | 638460 | 7 | 7 | M1 | 130 | 0.0013 | E | 1 |

Ni xvi

Al Isoelectronic Sequence

Ground State: $1s^22s^22p^63s^23p^{-2}P_{1/2}^{\circ}$

Ionization Energy: $499 \text{ eV} = 4020000 \text{ cm}^{-1}$

Allowed Transitions

List of tabulated lines

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-------------|----------------|-------------------|----------------|----------|----------------|---------|
| 152
160 | 25,34
37 | 194
194.04 | 22,31,41,42
20 | 228
231 | 27
19 | 266
288.165 | 16
2 |
| 161 | 37 | 195.27 | 20 | 232.475 | 4 | 297 | 11 |
| 162 | 36,37 | 196 | 41 | 233 | 18,19 | 299 | 9,15 |
| 163 | 36 | 197 | 29,42 | 235 | 18,19 | 300 | 8 |
| 166 | 35 | 198 | 29,41 | 236 | 18 | 302 | 32 |
| 167 | 35 | 199 | 31 | 237.875 | 4 | 304 | 8 |
| 168 | 35 | 200 | 22 | 238 | 6,18 | 309.179 | 2 |
| 170 | 24 | 204 | 7,40 | 239.550 | 3 | 313.22 | 2 |
| 171 | 30 | 206 | 33 | 245 | 6,17 | 317 | 15 |
| 172 | 24 | 209 | 7 | 246 | 10 | 320 | 15 |
| 175 | 30 | 210 | 33 | 247 | 17 | 328 | 13 |
| 180 | 39 | 212 | 33 | 249 | 10,17 | 335 | 13 |
| 182 | 39 | 215 | 7,21 | 250 | 10 | 338 | 13 |
| 183 | 22,38 | 216 | 28 | 254 | 6,16 | 346 | 13 |
| 185.23 | 20 | 217 | 21,33 | 255 | 5 | 382 | 1 |
| 187 | 22,23 | 218 | 21 | 256.62 | 3 | 385 | 1 |
| 188 | 23 | 218.391 | 4 | 257 | 26 | 407 | 14 |
| 190 | 29 | 219 | 28 | 259 | 26 | 428 | 12 |
| 192 | 23 | 221 | 21 | 262 | 26 | 447 | 12 |
| 193 | 23,42 | 223.119 | 4 | 263 | 16 | | |

Line strengths for transitions of the arrays $3s^23p - 3s^2p^2$, $3s^2p^2 - 3s^2p^2$, $3s^2p^2 - 3p^3$, $3s^23d - 3s^2p^2 - 3s^2d$, and $3s^2p^2 - 3s^2p^2 s^2 - 3s$

Huang published neither an energy-level diagram nor percentage compositions for levels of the $3s^23p$, $3s^2p$, $3s^23d$, $3p^3$, and $3s^3p^3d$ configurations in Ni xvi. We have used the percentages given by Fawcett<sup>2</sup> as a guide to naming the levels; the latter's values resulted from Hartree-Fock calculations with relativistic effects and statistical allowance for exchange (HXR), and incorporated correlation effects due to all configurations within the n = 3 complex. Transitions involving levels which are indicated to be of low purity in LS coupling are omitted here. Lines which are characterized by very small *f*-values are assigned lower accuracy ratings; the weakest lines have been excluded. A few wavelengths computed by Huang differ significantly from those which resulted from the fitting and scaling procedure applied by Fawcett<sup>2</sup>; lines for which the wavelengths are in serious disagreement have been omitted.

References

- <sup>1</sup>K.-N. Huang, At. Data Nucl. Data Tables 34, 1 (1986) and private communication.
- <sup>2</sup>B. C. Fawcett, At. Data Nucl. Data Tables 28, 557 (1983).

| F | 6 | 7 |
|---|---|---|
|---|---|---|

Ni XVI: Allowed transitions

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | g i | g k | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|-------------------------------------|----------------------------------|--|------------------------------|--------------------------------------|------------------|------------------|--|--|-------------------------------|---|--------------------|------------------|
| 1. | 3s²3p-3s3p² | ²P° - <sup>4</sup> P | | | | | | | | | | | |
| | | | [385]
[382] | | | 4
2 | 6
2 | 0.57
0.58 | 0.0019
0.0013 | 0.0097
0.0032 | $-2.12 \\ -2.59$ | E
E | 1
1 |
| 2. | | <sup>2</sup> P° – <sup>2</sup> D | 302.10 | 18507 | 349528 | 6 | 10 | 26 | 0.059 | 0.35 | -0.45 | Е | 1 |
| | | | 309.179
288.165
[313.22] | 27761
0
27761 | 351198
347023
347023 | 4
2
4 | 6
4
4 | 23
32
0.43 | 0.049
0.079
6.3(-4) <sup>a</sup> | 0.20
0.15
0.0026 | -0.71
-0.80
-2.60 | D
D
E | 1
1
1 |
| 3. | | <sup>2</sup> P° – <sup>2</sup> S | 250.66 | 18507 | 417449 | 6 | 2 | 230 | 0.073 | 0.36 | -0.36 | Е | 1 |
| | | | [256.62]
239.550 | 27761
0 | 417449
417449 | 4
2 | 2
2 | 3.8
260 | 0.0019
0.22 | 0.0064
0.35 | $-2.12 \\ -0.35$ | E
E | 1
1 |
| 4. | | <sup>2</sup> P° - <sup>2</sup> P | 229.28 | 18507 | 454660 | 6 | 6 | 480 | 0.38 | 1.7 | 0.35 | Е | 1 |
| | | | 232.475
223.119
237.875
218.391 | 27761
0
27761
0 | 457894
448191
448191
457894 | 4
2
4
2 | 4
2
2
4 | 407
130
260
95 | 0.330
0.095
0.11
0.136 | 1.01
0.14
0.35
0.195 | $\begin{array}{r} 0.120 \\ -0.72 \\ -0.35 \\ -0.57 \end{array}$ | C-
E
E
C- | 1
1
1
1 |
| 5. | 3s 3p <sup>2</sup> -3p <sup>3</sup> | 4P - 2D° | | | | | | | | | | | |
| | 3
 | | [255] | | | 6 | 6 | 1.9 | 0.0019 | 0.0094 | -1.95 | Е | 1 |
| 6. | | 4P - 4S° | 248 | | | 12 | 4 | 400 | 0.12 | 1.2 | 0.17 | D | 1 |
| | | | [254]
[245]
[238] | | | 6
4
2 | 4
4
4 | 180
140
75 | 0.12
0.13
0.13 | 0.59
0.41
0.20 | -0.15
-0.29
-0.59 | D
D
D | 1
1
1 |
| 7. | | <sup>4</sup> P - <sup>2</sup> P° | | | | | | | | | | } | |
| | | | [215]
[209]
[204] | | | 6
4
2 | 4
4
4 | 3.0
8.3
4.2 | 0.0014
0.0055
0.0053 | 0.0059
0.015
0.0071 | $-2.08 \\ -1.66 \\ -1.98$ | E
E
E | 1
1
1 |
| 8. | | <sup>2</sup> D - <sup>2</sup> D° | | | | s : | | | | | | | |
| | | | [304]
[300] | | | 6
4 | 6
6 | 40
4.5 | 0.055
0.0091 | 0.33
0.036 | $-0.48 \\ -1.44$ | E
E | 1
1 |
| 9. | | <sup>2</sup> D – <sup>4</sup> S° | | | | | | | | | 5 | | - |
| | | | [299] | | | 4 | 4 | 2.7 | 0.0036 | 0.014 | -1.85 | Е | 1 |
| 10. | | <sup>2</sup> D – <sup>2</sup> P° | 249 | | | 10 | 6 | 150 | 0.083 | 0.68 | -0.08 | D | 1 |
| | | - | [249]
[250]
[246] | | | 6
4
4 | 4
2
4 | 120
160
15 | 0.077
0.076
0.014 | 0.38
0.25
0.045 | $-0.33 \\ -0.52 \\ -1.26$ | D
D
D | 1
1
1 |
| 11. | | <sup>2</sup> S - <sup>2</sup> P* | [297] | | | 2 | 4 | 25 | 0.066 | 0.13 | -0.88 | Е | 1 |
| 12. | | <sup>2</sup> P - 4 S° | [=0.] | | | | | | | | | - | - |
| | | | [447]
[428] | | | 4
2 | 4 | 1.2
0.34 | 0.0037
0.0019 | 0.022
0.0053 | -1.83
-2.42 | E
E | 1
1 |

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Ni XVI: Allowed transitions - Continued

| | | | | | | | | · | | | | | |
|-----|--|----------------------------------|----------------|---------------------------|------------------------------|------------|----|--|--------|---------------|----------------|---------------|--------|
| No. | Transition
Array | Multiplet | λ
(Å) | E_i (cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | g i | ₿k | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
| 10 | | 20 200 | | | | 0 | | 40 | 0.074 | 0.40 | 0.05 | | |
| 13. | | <sup>2</sup> P - <sup>2</sup> P | 331 | | | 6 | 6 | 43 | 0.074 | 0.49 | -0.35 | E | 1 |
| | | | [338] | | | 4 | 4 | 37 | 0.063 | 0.28 | -0.60 | D | 1 |
| | | | [335] | | | | 2 | 46 | 0.077 | 0.17 | -0.81
-1.53 | E | 1 |
| | | | [328] | | | 2 | 4 | 0.46 | 0.0015 | 0.0032 | -2.53 | Ē | 1 |
| 14. | 3s <sup>2</sup> 3d−
3s3p(³P°)3d | <sup>2</sup> D – <sup>4</sup> P° | | | | | | | | | | | |
| | | | [407] | | | 6 | 6 | 0.50 | 0.0012 | 0.010 | -2.13 | Е | 1 |
| 15. | | <sup>2</sup> D – <sup>2</sup> F° | 307 | | | 10 | 14 | 26 | 0.050 | 0.51 | -0.30 | Е | 1 |
| | | | [299] | | | 6 | 8 | 27 | 0.049 | 0.29 | -0.53 | Е | 1 |
| | | | [317] | | | 4 | 6 | 17 | 0.038 | 0.16 | -0.81 | E | 1 |
| | | | [320] | | | 6 | 6 | 5.7 | 0.0087 | 0.055 | -1.28 | Е | 1 |
| 16. | | <sup>2</sup> D – <sup>2</sup> P° | 262 | | | 10 | 6 | 13 | 0.0082 | 0.071 | - 1.08 | Е | 1 |
| | | | [266] | | | 6 | 4 | 7.0 | 0.0049 | 0.026 | -1.53 | E | 1 |
| | | | [254] | | | 4 | | 3.3
11 | 0.0016 | 0.0054 | -2.19
-1.34 | E | 1 |
| 17. | $\frac{3s^23d}{3s3p}(^1P^\circ)3d$ | <sup>2</sup> D - <sup>2</sup> F° | 247 | | | 10 | 14 | 330 | 0.42 | 3.4 | 0.62 | Е | 1 |
| | | | [249] | | | 6 | 8 | 330 | 0.41 | 20 | 0.39 | E | 1 |
| | | | [245] | | | 4 | 6 | 320 | 0.43 | 1.4 | 0.24 | Ē | 1 |
| | | | [247] | | | 6 | 6 | 9.2 | 0.0084 | 0.041 | -1.30 | Е | 1 |
| 18. | | <sup>2</sup> D – <sup>2</sup> D* | 235 | | | 10 | 10 | 250 | 0.21 | 1.6 | 0.32 | Е | 1 |
| | | | [235] | | | 6 | 6 | 250 | 0.21 | 0.96 | 0.09 | E | 1 |
| | | | [236]
[238] | | | 4 | 4 | 120 | 0.10 | 0.31 | -0.40
-0.35 | E | 1 |
| | | | [233] | | | 4 | 6 | 1.7 | 0.0020 | 0.0062 | -2.09 | Ē | 1 |
| 19. | | <sup>2</sup> D - <sup>2</sup> P° | 234 | | | 10 | 6 | 400 | 0.19 | 1.5 | 0.29 | D | 1 |
| | | | [233] | | | 6 | 4 | 240 | 0.13 | 0.60 | -0.11 | D | 1 |
| | | | [235] | | | 4 | 2 | 380 | 0.16 | 0.49 | -0.20 | D | 1 |
| | | | [201] | | | 4 | 4 | 100 | 0.13 | 0.39 | -0.29 | | |
| 20. | 3 p -3d | $^{2}P^{\circ} - ^{2}D$ | 191.09 | 18507 | 541820 | 6 | 10 | 490 | 0.45 | 1.7 | 0.43 | D | 1 |
| | | | [194.04] | 27761 | 543120 | 4 | 6 | 460 | 0.39 | 0.99 | 0.19 | D | 1 |
| | | | 185.23 | 0
27761 | 539870 | | 4 | 420 | 0.43 | 0.53 | -0.06 | D | 1 |
| 21. | $3s 3p^2 -$
$3s 3p (^3\mathbf{P}^\circ) 3d$ | 4P - 4F° | [100.21] | 21101 | 565610 | 1 | - | 50 | 0.034 | 0.14 | -0.00 | | 1 |
| | | | | | | - | | | | | | | |
| | | | [217] | | | 6 | 8 | 5.2 | 0.0049 | 0.021 | -1.53 | E | 1 |
| | | | [221] | | | 6 | 6 | 1.6 | 0.0012 | 0.0052 | -2.15 | Ē | 1 |
| | | | [218] | | | 4 | 4 | 1.7 | 0.0012 | 0.0035 | -2.31 | E | 1 |

Ni xvi: Allowed transitions - Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | $egin{array}{c} E_i \ (\mathbf{cm}^{-1}) \end{array}$ | <i>E</i> <sup><i>k</i></sup> (cm <sup>-1</sup>) | g i | g. | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | f ik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|---------------------|----------------------------------|---|---|--|-----------------------|------------------|--|--|--|---|------------------|-----------------------|
| 22. | | 4P - 4P° | | | | | | | | | | | |
| | | | [200]
[183]
[187]
[194] | | | 6
2
4
4 | 6
2
2
6 | 32
0.31
330
280 | 0.019
1.6(-4)
0.085
0.24 | 0.076
1.9(-4)
0.21
0.61 | -0.94
-3.50
-0.47
-0.02 | E
D
E | 1
1
1
1 |
| 23. | | 4P - 4D° | | | | | | | | | | | |
| | | | [192]
[187]
[192]
[188]
[193] | | | 6
4
6
2
4 | 8
6
2
2 | 454
120
310
470
9.3 | 0.335
0.097
0.17
0.25
0.0026 | 1.27
0.24
0.64
0.31
0.0066 | $\begin{array}{r} 0.303 \\ -0.41 \\ 0.01 \\ -0.30 \\ -1.98 \end{array}$ | C
D
D
E | 1
1
1
1
1 |
| 24. | | 4P - 2F° | | | | | | | | | | | |
| | | | [170]
[172] | | | 6
4 | 8
6 | 8.2
1.5 | 0.0048
0.0010 | 0.016
0.0023 | -1.54
-2.39 | E
E | 1
1 |
| 25. | | <sup>4</sup> P - <sup>2</sup> P° | | | | | | | | | | | |
| | | | [152] | | | 2 | 4 | 5.6 | 0.0039 | 0.0039 | -2.11 | E | 1 |
| 26. | | <sup>2</sup> D – <sup>4</sup> F° | | | | | | | | | | | |
| | | | [257]
[259]
[262] | | | 6
4
6 | 6
4
4 | 1.4
2.0
1.6 | 0.0014
0.0021
0.0011 | 0.0072
0.0070
0.0056 | -2.07
-2.09
-2.19 | E
E
E | 1
1
1 |
| 27. | | ²D − ⁴P° | | | | | | | | | | | |
| | | | [228] | | | 6 | 6 | 14 | 0.011 | 0.050 | -1.18 | Е | 1 |
| 28. | | ²D – ⁴D° | | | | | | | | | | | |
| | | | [219]
[216] | | | 6
4 | 8
6 | 6.8
1.8 | 0.0065
0.0019 | 0.028
0.0054 | $-1.41 \\ -2.12$ | E
E | 1
1 |
| 29. | | ²D − ²F° | 1 93 | | | 10 | 14 | 190 | 0.15 | 0.96 | 0.18 | Е | 1 |
| | | | [190]
[197]
[198] | | | 6
4
6 | 8
6
6 | 200
150
44 | 0.14
0.13
0.026 | 0.53
0.33
0.10 | -0.07
-0.29
-0.81 | E
E
E | 1
1
1 |
| 30. | | <sup>2</sup> D – <sup>2</sup> P° | | | | | | - | | | | | |
| | | | [171]
[175] | | | 4
4 | 2
4 | 2.2
0.45 | 4.9(-4)
2.1(-4) | 0.0011
4.8(-4) | -2.71
-3.08 | E
E | 1
1 |
| 31. | | <sup>2</sup> S – <sup>2</sup> P° | 197 | | | 2 | 6 | 370 | 0.65 | 0.84 | 0.11 | Е | 1 |
| | | | [199]
[194] | | | 2
2 | 4
2 | 490
110 | 0.58
0.063 | 0.76
0.080 | 0.06
-0.90 | E
E | 1
1 |
| 32. | | <sup>2</sup> P - <sup>4</sup> P° | | | | | | | | | | | |
| | | | [302] | | | 4 | 6 | 0.51 | 0.0011 | 0.0042 | -2.37 | Е | 1 |

Ni XVI: Allowed transitions - Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | ₿Ł | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fa | S
(at. u.) | log gf | Accu-
racy | Source |
|-------------|---|----------------------------------|----------------------------------|------------------------------|---------------------------|------------------|------------------|--|----------------------------------|---------------------------------|------------------------------|------------------|------------------|
| | | | | | | | | | | | | | |
| 33. | | ²P - ²P° | 213 | 1 | | 6 | 6 | 210 | 0.14 | 0.5 9 | -0.07 | Е | 1 |
| | | | [217]
[206]
[210]
[212] | | | 4
2
4
2 | 4
2
2
4 | 110
370
49
1.1 | 0.077
0.24
0.016
0.0014 | 0.22
0.32
0.045
0.0020 | 0.51
0.33
1.19
2.54 | D
E
D
E | 1
1
1
1 |
| 34. | 3s 3p <sup>2</sup>
3s 3p(<sup>1</sup> P°)3d | <sup>4</sup> P - <sup>2</sup> F° | | | | | | | | | | | |
| | | | [152] | | | 6 | 8 | 6.6 | 0.0030 | 0.0091 | -1.74 | Е | 1 |
| 35. | | <sup>2</sup> D - <sup>2</sup> F° | 167 | | | 10 | 14 | 310 | 0.18 | 1.0 | 0.26 | Е | 1 |
| | | | [168]
[166]
[167] | | | 6
4
6 | 8
6
6 | 320
310
15 | 0.18
0.19
0.0064 | 0.59
0.42
0.021 | $0.03 \\ -0.11 \\ -1.42$ | E
E
E | 1
1
1 |
| 36. | | <sup>2</sup> D - <sup>2</sup> D° | | | | | | | | | | | |
| | | | [162]
[163] | | | 4
6 | 4
4 | 2.1
2.5 | 8.4(-4)
6.5(-4) | 0.0018
0.0021 | -2.47
-2.41 | E
E | 1
1 |
| 37. | | <sup>2</sup> D - <sup>2</sup> P° | 161 | | | 10 | 6 | 6.1 | 0.0014 | 0.0075 | -1.85 | Е | 1 |
| | | | [161]
[162]
[160] | | | 6
4
4 | 4
2
4 | 4.0
1.2
4.6 | 0.0010
2.3(-4)
0.0018 | 0.0033
4.9(-4)
0.0037 | $-2.21 \\ -3.04 \\ -2.15$ | E
E
E | 1
1
1 |
| 38. | | <sup>2</sup> S - <sup>2</sup> D° | | | | | | | | | | | |
| | | | [183] | | | 2 | 4 | 21 | 0.021 | 0.025 | -1.38 | Е | 1 |
| 39 . | | <sup>2</sup> S - <sup>2</sup> P° | 181 | | | 2 | 6 | 130 | 0.19 | 0.23 | -0.41 | Е | 1 |
| | | | [180]
[182] | | | 2
2 | 4
2 | 71
250 | 0.069
0.13 | 0.082
0.15 | -0.86
-0.60 | E
E | 1
1 |
| 40. | | <sup>2</sup> P - <sup>2</sup> F° | | | | | | | | | | | |
| | | | [204] | | | 4 | 6 | 8.0 | 0.0074 | 0.020 | -1.53 | Е | 1 |
| 41. | | <sup>2</sup> P – <sup>2</sup> D° | 195 | | | 6 | 10 | 660 | 0.62 | 2.4 | 0.57 | Е | 1 |
| | | | [196]
[194]
[198] | | | 4
2
4 | 6
4
4 | 670
550
52 | 0.58
0.62
0.031 | 1.5
0.79
0.080 | $0.37 \\ 0.09 \\ -0.91$ | E
E
E | 1
1
1 |
| 42. | | <sup>2</sup> P - <sup>2</sup> P° | | | | | | | | | | | |
| | | | [194]
[193]
[197] | | | 4
2
4 | 4
2
2 | 350
55
120 | 0.20
0.031
0.035 | 0.51
0.039
0.090 | $-0.10 \\ -1.21 \\ -0.86$ | D
E
C- | 1
1
1 |

Ni xvı

Forbidden Transitions

Line strengths for magnetic dipole and electric quadrupole transitions within the $3s^23p$ <sup>2</sup>P° and $3s^23p^4P$ terms are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Huang.<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing included all configurations within the n=3 complex. Strengths of electric quadrupole transi-

tions as reported in Ref. 1 were multiplied by the factor $^{2}/_{3}$ which is needed to bring these values into conformance with the definition of quadrupole strengths used in the NBS tables.

Reference

<sup>1</sup>K.-N. Huang, At. Data Nucl. Data Tables 34, 1 (1986).

| Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_{k} (cm <sup>-1</sup>) | gi | ₿⊧ | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|--|--|--|---|---|---|---|---|---|---|--|--|
| 3р-3р | ²₽° - ²₽° | | | | | | | | | | |
| | | 3601.1 | 0 | 27761 | 2 | 4 | M1
F9 | 192 | 1.33 | | 1 |
| | | " | | | Ž | 4 | EZ | 0.067 | 0.096 | E | 1 |
| 3s 3p <sup>2</sup> -3s 3p <sup>2</sup> | 4P - 4P | | | | | | | | | | |
| | | [7320] | | | 4 | 6 | M1 | 40.3 | 3.52 | С | 1 |
| | | | | | 4 | 6 | E2 | 0.0019 | 0.14 | D | 1 |
| | | [8500] | | | 2 | 4 | M 1 | 35.8 | 3.26 | С | 1 |
| | | - | | | 2 | 4 | E2 | 1.1(-4)* | 0.012 | Е | 1 |
| | | [3930] | | | 2 | 6 | E2 | 0.033 | 0.11 | D | 1 |
| | Transition
Array
3p-3p
3s3p <sup>2</sup> -3s3p <sup>2</sup> | Transition
ArrayMultiplet $3p-3p$ $^2P^\circ - ^2P^\circ$ $3s3p^2-3s3p^2$ $^4P - ^4P$ | Transition
ArrayMultiplet λ
(Å) $3p-3p$ $^2P^{\circ} - ^2P^{\circ}$ 3601.1 $3s 3p^2 - 3s 3p^2$ $^4P - ^4P$ [7320]
[8500]
[3930] | Transition
ArrayMultiplet λ
(Å) E_i
(cm^{-1}) $3p-3p$ $^2P^{\circ} - ^2P^{\circ}$ 3601.10 $3s 3p^2 - 3s 3p^2$ $^4P - ^4P$ [7320]
[8500]
[3930][3930] | Transition
Array Multiplet λ
(Å) E_i
(cm <sup>-1</sup>) E_i
(cm <sup>-1</sup>) $3p-3p$ $^2P^{\circ} - ^2P^{\circ}$ 3601.1 0 27761 $3s 3p^2 - 3s 3p^2$ $^4P - ^4P$ [7320] 10 10 [8500] [3930] [3930] 10 10 | Transition
Array Multiplet λ
(Å) E_i
(cm <sup>-1</sup>) E_k
(cm <sup>-1</sup>) g_i $3p-3p$ $^2P^{\circ} - ^2P^{\circ}$ 3601.1 0 27761 2 $3s 3p^2 - 3s 3p^2$ $^4P - ^4P$ [7320] 4 4 4 [8500] 2 [900] | Transition
Array Multiplet λ
(Å) E_i
(cm <sup>-1</sup>) E_k
(cm <sup>-1</sup>) g_i g_k $3p-3p$ $2P^* - ^2P^*$ 3601.1 0 27761 2 4 $3s 3p^2 - 3s 3p^2$ $^4P - ^4P$ [7320] 4 6 [8500] [8500] 2 4 2 [9330] [9330] [930] 2 6 | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ |

Ni XVI: Forbidden transitions

Ni xvii

Mg Isoelectronic Sequence

Ground State: $1s^22s^22p^63s^2$ $^{1}S_0$

Jonization Energy: $571.08 \text{ eV} = 4606000 \text{ cm}^{-1}$

| Allowed | Transitions | |
|---------|-------------|--|
|---------|-------------|--|

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-------|----------------|------|----------------|-----|
| 30.919 | 16 | 207 | 5 | 269.0 | 19 | 294 | 10 |
| 42.855 | 15 | 207.50 | 17 | 269.39 | 3 | 296 | 10 |
| 54.451 | 26 | 208.66 | 17 | 270.4 | 19 | 323 | 9 |
| 55.361 | 27 | 209.5 | 17 | 272 | 4 | 339 | 9 |
| 57.348 | 28 | 214 | 21 | 277 | 11 | 343 | 9 |
| 169 | 18 | 215.89 | 20 | 278 | 11 | 355 | 9 |
| 173 | 24 | 216 | 22,25 | 279 | 11 | 358 | 9 |
| 175 | 18 | 217 | 21 | 280 | 10 | 362 | 9 |
| 197.39 | 17 | 226 | 21 | 281.50 | 3 | 366.7 | 1 |
| 199.87 | 17 | 227 | 23 | 282 | 8,10 | 372.7 | 6 |
| 200.53 | 17 | 249.180 | 2 | 284 | 14 | 412.2 | 6 |
| 204 | 22 | 251.97 | 3 | 285.59 | 3 | 419 | 7 |
| 205 | 22 | 263.55 | 3 | 289 | 4 | 441.3 | 6 |
| 206 | 21 | 266.06 | 3 | 292 | 13 | 465 | 12 |

Oscillator strengths for the three transitions $3s^{2}$ S_0 – 3snp <sup>1</sup>P<sub>1</sub>° (n = 3-5) are the results of the relativistic random phase approximation (RRPA) calculations of Shorer et al.,<sup>1</sup> who allowed for correlation within the context of a frozen core. Oscillator strength data of Fawcett<sup>2</sup> guoted for most transitions of the arrays 3s 3p - $3p^2$, $3s^3d - 3p^3d$, $3s^3p - 3s^3d$, and $3p^2 - 3p^3d$, were derived by means of Hartree-Fock calculations which included relativistic effects and statistical allowance for exchange (HXR); he incorporated correlation effects due to all configurations in the n = 3 complex. A-values for all intercombination lines tabulated here were determined by Bhatia and Kastner<sup>3</sup> using a scaled Thomas-Fermi (STF) approach with allowance for configuration mixing; these data are included here, but the A-values were first converted to line strengths and then reconverted to oscillator strengths and transition probabilities which incorporate more accurate wavelength values.

Kastner *et al.*<sup>4</sup> calculated A-values for a number of lines of the array 3p 3d - 3p 4f in Fe xv and Zn xix by

application of a multiconfiguration STF approach. These transition probabilities were converted to oscillator strengths, from which f-values for a few transitions of this array in Ni XVII were interpolated.

Transitions involving levels which are indicated in Ref. 2 to be of low purity in *LS* coupling in Ni XVII, or in Ref. 4 to be of low purity in neighboring Mg-like ions, are omitted here. Lines which are characterized by very small *f*-values are assigned lower accuracy ratings.

References

- <sup>1</sup>P. Shorer, C. D. Lin, and W. R. Johnson, Phys. Rev. A 16, 1109 (1977).
- <sup>2</sup>B. C. Fawcett, At. Data Nucl. Data Tables 28, 579 (1983).
- <sup>3</sup>A. K. Bhatia and S. O. Kastner, J. Quant. Spectrosc. Radiat. Transfer 24, 53 (1980).
- <sup>4</sup>S. O. Kastner, M. Swartz, A. K. Bhatia, and J. Lapides, J. Opt. Soc. Am. 68, 1558 (1978).

Ni XVII: Allowed transitions

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | gi | 8× | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|---------------------|----------------------------------|--|--|--|----------------------------|----------------------------|--|--|--|---|----------------------------|--------------------------------------|
| 1. | 3s²-3s3p | <sup>1</sup> S - <sup>3</sup> P° | | | | | | | | | | | |
| | | | 366.7 | 0 | 272700 | 1 | 3 | 0.58 | 0.0035 | 0.0042 | -2.46 | Е | 3 |
| 2. | | <sup>1</sup> S - <sup>1</sup> P° | 249.180 | 0 | 401316 | 1 | 3 | 275 | 0.767 | 0.629 | -0.115 | в | 1 |
| 3. | 3s3p-3p2 | <sup>3</sup> P° – <sup>3</sup> P | 268.2 | 283500 | 656400 | 9 | 9 | 210 | 0.23 | 1.8 | 0.31 | D | 2 |
| | | | 266.06
269.39
285.59
281.50
251.97
263.55 | 293700
272700
293700
272700
272700
264500 | 669600
643900
643900
627900
669600
643900 | 5
3
5
3
3
1 | 5
3
3
1
5
3 | 140
58
85
210
50
86 | 0.15
0.063
0.062
0.083
0.080
0.27 | 0.66
0.17
0.29
0.23
0.20
0.23 | $-0.12 \\ -0.72 \\ -0.51 \\ -0.60 \\ -0.62 \\ -0.57$ | D
C
C
C
D
C | 2
2
2
2
2
2
2
2 |
| 4. | | <sup>3</sup> P° – <sup>1</sup> D | | | | | | | | - | | | |
| | | | [289]
[272] | | r. | 5
3 | 5
5 | 27
15 | 0.034
0.028 | 0.16
0.076 | $-0.77 \\ -1.07$ | E
E | 3
3 |
| 5. | | <sup>3</sup> P° – <sup>1</sup> S | | | | | | | | | | | |
| | | | [207] | | | 3 | 1 | 3.2 | 6.8(-4) <sup>a</sup> | 0.0014 | -2.69 | Е | 3 |
| 6. | | <sup>1</sup> P° – <sup>3</sup> P | | | | | | | | | | | |
| | | | [372.7]
[412.2]
[441.3] | 401316
401316
401316 | 669600
643900
627900 | 3
3
3 | 5
3
1 | 5.9
0.14
1.4 | 0.020
3.4(4)
0.0014 | 0.075
0.0014
0.0059 | -1.21
-2.99
-2.39 | E
E
E | 3
3
3 |
| 7. | | <sup>1</sup> P° - <sup>1</sup> D | [419] | | | 3 | 5 | 18 | 0.080 | 0.33 | -0.62 | Е | 2 |
| 8. | | <sup>1</sup> P° - <sup>1</sup> S | [282] | | | 3 | 1 | 240 | 0.097 | 0.27 | -0.54 | С | 2 |
| 9. | 3s 3d –3p 3d | <sup>3</sup> D - <sup>3</sup> F° | 336 | | | 15 | 21 | 64 | 0.15 | 2.5 | 0.35 | D | 2 |
| | | | [323]
[339]
[355]
[343]
[358]
[362] | | | 7
5
3
7
5
7 | 9
7
5
7
5
5 | 75
50
38
13
10
0.10 | $\begin{array}{c} 0.150\\ 0.12\\ 0.12\\ 0.023\\ 0.020\\ 1.4(-4) \end{array}$ | 1.12
0.67
0.42
0.18
0.12
0.0012 | $\begin{array}{r} 0.021 \\ -0.22 \\ -0.44 \\ -0.79 \\ -1.00 \\ -3.01 \end{array}$ | C
C
D
C
D
E | 2
2
2
2
2
2
2 |
| 10. | | <sup>3</sup> D - <sup>3</sup> D* | | | | | | | | | | | |
| | | | [282]
[294]
[296]
[280] | | | 7
3
5
5 | 7
3
3
7 | 84
25
74
26 | 0.10
0.032
0.058
0.042 | 0.65
0.093
0.28
0.19 | -0.15
-1.02
-0.54
-0.68 | C
E
E
C | 2
2
2
2 |
| 11. | | <sup>3</sup> D - <sup>3</sup> P° | | | | | | | | | | | |
| | | | [279]
[278]
[277] | | | 5
3
3 | 3
1
3 | 37
130
96 | 0.026
0.050
0.11 | 0.12
0.14
0.30 | -0.89
-0.82
-0.48 | E
C
E | 2
2
2 |
| 12. | | <sup>1</sup> D - <sup>1</sup> D° | [465] | | | 5 | 5 | 8.6 | 0.028 | 0.21 | -0.85 | D | 2 |
| 13. | | <sup>1</sup> D - <sup>1</sup> F° | [292] | | | 5 | 7 | 220 | 0.40 | 1.9 | 0.30 | D | 2 |
| 14. | | <sup>1</sup> D - <sup>1</sup> P° | [284] | | | 5 | 3 | 150 | 0.11 | 0.51 | -0.26 | D | 2 |

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Ni xvii: Allowed transitions -- Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i (cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | ₿k | $A_{ki} \ (10^8 \ { m s}^{-1})$ | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|-----------------------|--|---|--|--|----------------------------|----------------------------|---------------------------------------|---|--|---|----------------------------|--------------------------------------|
| | | | | | | | | | | | | | |
| 15. | $3s^2 - 3s 4p$ | <sup>1</sup> S - <sup>1</sup> P° | 42.855 | 0 | 2333500 | 1 | 3 | 4750 | 0.392 | 0.055 | -0.407 | с | 1 |
| 16. | 3s <sup>2</sup> -3s5p | ${}^{1}S - {}^{1}P^{\circ}$ | 30.919 | 0 | 3234300 | 1 | 3 | 2770 | 0.119 | 0.0121 | -0.92 | с | 1 |
| 17. | 3s 3p – 3s 3d | <sup>3</sup> P° – <sup>3</sup> D | 204.0 | 283500 | 773800 | 9 | 15 | 263 | 0.273 | 1.65 | 0.390 | с | 2 |
| | | | 207.50
199.87
197.39
208.66
200.53
[209.5] | 293700
272700
264500
293700
272700
293700 | 775600
773000
771100
773000
771100
771100 | 5
3
1
5
3
5 | 7
5
3
5
3
3 | 250
210
160
61
120
6.6 | 0.226
0.21
0.28
0.040
0.070
0.0026 | 0.77
0.41
0.18
0.14
0.14
0.0090 | $\begin{array}{r} 0.053 \\ -0.20 \\ -0.55 \\ -0.70 \\ -0.68 \\ -1.89 \end{array}$ | C
C
C
C
C
D | 2
2
2
2
2
2
2
2 |
| 18. | | <sup>3</sup> P° – <sup>1</sup> D | | | | | | | | | | | |
| | | | [175]
[169] | 293700
272700 | 864520
864520 | 5
3 | 5
5 | 0.28
5.1 | 1.3(-4)
0.0037 | 3.7(-4)
0.0061 | -3.19
-1.96 | E
E | 3
3 |
| 19. | | <sup>1</sup> P° - <sup>3</sup> D | | | | | | | | | | | |
| | | | [269.0]
[270.4] | 401316
401316 | 773000
771100 | 3
3 | 5
3 | 0.20
0.41 | 3.7(-4)
4.5(-4) | 9.7(-4)
0.0012 | -2.96
-2.87 | E
E | 3
3 |
| 20. | | <sup>1</sup> P° – <sup>1</sup> D | 215.89 | 401316 | 864520 | 3 | 5 | 480 | 0.56 | 1.2 | 0.23 | D | 2 |
| 21. | 3p²–3p3d | <sup>3</sup> P - <sup>3</sup> D° | | | | | | | | | | | |
| | | | [217]
[206]
[214]
[226] | | | 5
1
3
5 | 7
3
3
3 | 240
300
48
2.6 | 0.24
0.57
0.033
0.0012 | 0.86
0.39
0.070
0.0045 | 0.08
-0.24
-1.00
-2.22 | D
E
E
E | 2
2
2
2 |
| 22. | | <sup>3</sup> P - <sup>3</sup> P° | | | | | | 1 | | | | | |
| | | | [204]
[216]
[205] | | | 3
5
3 | 3
3
1 | 180
71
240 | 0.11
0.030
0.050 | 0.22
0.11
0.10 | -0.48
-0.82
-0.82 | E
E
C | 2
2
2 |
| 23. | | <sup>1</sup> D - <sup>1</sup> D° | [227] | | | 5 | 5 | 160 | 0.12 | 0.45 | -0.22 | Е | 2 |
| 24. | | <sup>1</sup> D - <sup>1</sup> P° | [173] | | | 5 | 3 | 4.8 | 0.0013 | 0.0037 | -2.19 | Е | 2 |
| 25. | | <sup>1</sup> S - <sup>1</sup> P° | [216] | | | 1 | 3 | 270 | 0.57 | 0.41 | -0.24 | с | 2 |
| 26. | 3p3d-3p4f | ³F° - ³G | | | | | | | | | | | |
| | | | 54.451 | | | 9 | 11 | 1.5(+4) | 0.81 | 1.3 | 0.86 | с | interp. |
| 27. | | <sup>3</sup> P° - <sup>3</sup> D | | | | | | | | | | | |
| | | | 55.361 | | | 1 | 3 | 6700 | 0.93 | 0.17 | -0.03 | с | interp. |
| 28. | | <sup>1</sup> F ° - <sup>1</sup> G | 57.348 | | | 7 | 9 | 1.4(+4) | 0.90 | 1.2 | 0.80 | C | interp. |

Ni xvii

Forbidden Transitions

| List of | tabulated | lines |
|---------|-----------|-------|
|---------|-----------|-------|

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|
| 115.67 | 9 | 861 | 6 | 2400 | 3 | 6250 | 3 |
| 149.3 | 10 | 888 | 4 | 3330 | 5 | 12000 | 1 |
| 156 | 11 | 912 | 7 | 3420 | 1 | 27700 | 5 |
| 731.0 | 2 | 929.4 | 2 | 3890 | 3 | 38000 | 8 |
| 777.6 | 2 | 1160 | 4 | 4760 | 1 | 53000 | 8 |

Transition probabilities for forbidden lines involving pairs of levels belonging to the set of configurations $3s^2$, 3s 3p, $3p^2$, and 3s 3d were computed by Bhatia and Kastner<sup>1</sup> using a scaled Thomas-Fermi approach with allowance for configuration mixing. These data are quoted here, but we first converted the transition probabilities to line strengths, which we then reconverted to A-values in order to incorporate more accurate wavelength values. The weakest lines were excluded from this compilation.

Reference

<sup>1</sup>A. K. Bhatia and S. O. Kastner, J. Quant. Spectrosc. Radiat. Transfer 24, 53 (1980).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | g⊧ | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | <i>S</i>
(at. u.) | Accu-
racy | Source |
|-----|----------------------------------|-----------------------------------|-------------------------------|------------------------------|----------------------------|-------------|-------------|-----------------------|---------------------------------------|-------------------------|---------------|-------------|
| 1. | 3s3p-3s3p | <sup>3</sup> P° – <sup>3</sup> P° | | | | | | | | | | |
| | | | [4760]
[12000]
[3420] | 272700
264500
264500 | 293700
272700
293700 | 3
1
1 | 5
3
5 | M1
M1
E2 | 125
10
0.037 | 2.49
2.0
0.051 | C+
D+
E | 1
1
1 |
| 2. | | <sup>3</sup> P° – <sup>1</sup> P° | | | | | | | | | | |
| | | | [929.4]
[777.6]
[731.0] | 293700
272700
264500 | 401316
401316
401316 | 5
3
1 | 3
3
3 | M1
M1
M1 | 210
210
350 | 0.019
0.011
0.015 | E
E
E | 1
1
1 |
| 3. | 3p <sup>2</sup> -3p <sup>2</sup> | <sup>3</sup> P - <sup>3</sup> P | | | | | | | | | | |
| | | | [3890]
[6250]
[2400] | 643900
627900
627900 | 669600
643900
669600 | 3
1
1 | 5
3
5 | M1
M1
E2 | 190
70
0.13 | 2.1
1.91
0.031 | D
C
E | 1
1
1 |
| 4. | | ${}^{3}P - {}^{1}S$ | | | | | | | | | | |
| | | | [1160]
[888] | | | 5
3 | 1
1 | E2
M1 | 26
2500 | 0.032
0.066 | E
E | 1
1 |

Ni xvII: Forbidden transitions

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | ₿k | Type of
transition | $egin{array}{c} A_{ki} \ (\mathbf{s}^{-1}) \end{array}$ | <i>S</i>
(at. u.) | Accu-
racy | Source |
|-----|---------------------|---------------------------------|--------------------|------------------------------|---------------------------|------------|--------|-----------------------|---|----------------------|---------------|--------|
| 5. | | <sup>1</sup> D - <sup>3</sup> P | | | | | | | | | | |
| | | | [3330]
[27700] | | | 5
5 | 5
3 | M1
M1 | 150
0.17 | 1.0
0.41 | E
E | 1
1 |
| 6. | | <sup>1</sup> D - <sup>1</sup> S | [861] | | | 5 | 1 | E2 | 340 | 0.097 | Е | 1 |
| 7. | 3p²-3s3d | <sup>1</sup> S - <sup>1</sup> D | [912] | | | 1 | 5 | E2 | 37 | 0.070 | Е | 1 |
| 8. | 3s 3d -3s 3d | <sup>3</sup> D – <sup>3</sup> D | | | | | | | | | | |
| | | | [38000]
[53000] | 773000
771100 | 775600
773000 | 5
3 | 7
5 | M1
M1 | 0.30
0.16 | 4.3
4.5 | D+
D | 1 1 |
| 9. | 3s²-3s3d | <sup>1</sup> S - <sup>1</sup> D | [115.67] | 0 | 864520 | 1 | 5 | E2 | $2.1(+6)^{a}$ | 0.13 | D- | 1 |
| 10. | $3s^2 - 3p^2$ | <sup>1</sup> S - <sup>3</sup> P | | | | | | | | | | |
| | | | [149.3] | 0 | 669600 | 1 | 5 | E2 | 6.3(+4) | 0.014 | Е | 1 |
| 11. | | <sup>1</sup> S - <sup>1</sup> D | [156] | | | 1 | 5 | E2 | 2.1(+5) | 0.059 | Е | 1 |

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Ni XVII: Forbidden transitions - Continued

Ni xviii

Na Isoelectronic Sequence

Ground State: $1s^22s^22p^63s^2S_{1/2}$

Ionization Energy: $607.06 \text{ eV} = 4896200 \text{ cm}^{-1}$

Allowed Transitions

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|
| 24.881 | 17 | 38.573 | 20 | 67.092 | 53 | 130.3 | 51 |
| 25.070 | 17 | 38.643 | 20 | 67.132 | 53 | 130.9 | 43 |
| 25.071 | 17 | 38.658 | 20 | 67.16 | 53 | 131.3 | 43 |
| 26.02 | 15 | 41.015 | 2 | 68.526 | 37 | 131.9 | 43 |
| 26.020 | 4 | 41.218 | 2 | 69.075 | 37 | 136.0 | 70 |
| 26.046 | 4 | 43.814 | 9 | 69.094 | 37 | 136.1 | 70 |
| 26.218 | 15 | 44.365 | 9 | 76.254 | 46 | 136.2 | 70 |
| 26.23 | 15 | 44.405 | 9 | 76.359 | 46 | 145.4 | 74 |
| 27.98 | 27 | 52.502 | 41 | 76.377 | 46 | 145.5 | 74 |
| 27.982 | 13 | 52.615 | 19 | 80.077 | 45 | 146 | 74 |
| 28.01 | 27 | 52.720 | 19 | 80.212 | 45 | 187.5 | 61 |
| 28.018 | 27 | 52.745 | 19 | 80.321 | 45 | 189.4 | 61 |
| 28.220 | 13 | 52.829 | 41 | 81.974 | 52 | 189.5 | 61 |
| 28.223 | 13 | 52.835 | 41 | 82.001 | 52 | 211.8 | 68 |
| 29.383 | 25 | 57.27 | 50 | 82.034 | 52 | 212.1 | 68 |
| 29.422 | 25 | 57.37 | 50 | 94.661 | 29 | 212.2 | 68 |
| 29.424 | 25 | 57.376 | 50 | 95.175 | 29 | 220.43 | 7 |
| 29.779 | 3 | 57.84 | 39 | 99.275 | 35 | 233.75 | 7 |
| 29.829 | 3 | 58.197 | 39 | 100.4 | 35 | 236.31 | 7 |
| 31.845 | 23 | 58.24 | 39 | 100.5 | 35 | 239.8 | 73 |
| 31.890 | 23 | 59.780 | 18 | 102.2 | 65 | 240.0 | 73 |
| 31.893 | 23 | 59.950 | 18 | 102.8 | 65 | 244.2 | 67 |
| 32.034 | 11 | 60.056 | 54 | 110 | 72 | 244.7 | 67 |
| 32.340 | 11 | 60.064 | 54 | 110.5 | 72 | 246.5 | 67 |
| 32.350 | 11 | 60.089 | 54 | 114.46 | 44 | 291.983 | 1 |
| 32.493 | 22 | 60.212 | 18 | 114.6 | 44 | 320.56 | 1 |
| 32.533 | 22 | 63.512 | 48 | 114.74 | 44 | 595.2 | 33 |
| 32.543 | 22 | 63.589 | 48 | 116.0 | 75 | 632.5 | 33 |
| 36.990 | 21 | 63.597 | 48 | 125 | 63 | 641.0 | 33 |
| 37.049 | 21 | 64.872 | 30 | 125.2 | 63 | 731.5 | 28 |
| 37.055 | 21 | 65.032 | 30 | 130.1 | 51 | 801.9 | 28 |
| | | 11 | 1 | | | | |

List of tabulated lines

Strengths of the lines of the 3s-3p and 3p-3d transitions were taken from Edlen's interpolation formulae.<sup>1</sup> These were based on the results of Weiss' Hartree-Fock calculations,<sup>2</sup> in which ratios of relativistic Dirac to nonrelativistic line strengths in hydrogenic ions were applied as scaling factors to the nonrelativistic Hartree-Fock line strengths in the corresponding sodiumlike species. Oscillator strengths for the 4p-4d transitions were derived by Gruzdev and Sherstyuk<sup>3</sup> using the relativistic variant of their effective orbital quantum number method, which utilizes a Coulomb potential in conjunction with a semiempirical orbital quantum number which is determined from experimental energy levels. Strengths of the lines of the 3s-4p and 3p-4d transitions, as well as f-values of the 3d-4f transitions, were interpolated from the results of the relativistic single-configuration Hartree-Fock calculations of Kim and Cheng<sup>4</sup> for Fe xv1 and, depending on the transition, either Kr xxv1 or Mo xxx11.

The lifetimes of the $3p_{1/2,3/2}$ and $3d_{5/2}$ levels were measured by Pegg *et al.*<sup>5</sup> using the beam-foil technique. They used a multiexponential fitting procedure to analyze their results, but did not incorporate a simulation of repopulation from higher levels, so that their method of cascade analysis is not so sophisticated as that reported elsewhere<sup>6,7</sup> for the lifetimes of the corresponding levels in Fe XVI. Nevertheless, the reciprocals of the lifetimes determined by Pegg *et al.* agree, to within their error

estimates, with the theoretical *A*-values derived from Edlen's interpolation formulae, with our uncertainty estimates of the theoretical results taken into account.

Multiplet f-values calculated by Tull et al.<sup>8</sup> using the frozen-core Hartree-Fock approach are quoted for numerous transitions nl-n'l' ($3 \le n \le 5$; $4 \le n' \le 8$; l, l'=s,p,d,f). Data for additional transitions (namely, those for which $n,n' \leq 10$, where n,n' are the principal quantum numbers of the lower and upper states, respectively) can be found in Ref. 8. Whenever wavelengths of individual lines within a multiplet either were available directly or could be determined from the energy levels, the multiplet strength was distributed among the lines according to LS-coupling rules, except in the case of the 5f-8d transition, where the wavelengths for all the lines in the multiplet are identical. The strength of the $3p^{2}P^{\circ}$ -4s<sup>2</sup>S multiplet was not distributed between the two lines in the multiplet, however, since the calculations of Kim and Cheng indicate that in the corresponding transition in neighboring sodiumlike ions (Fe xvi and

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Mo XXXII) the ratio of the two line strengths deviates somewhat from the value that would be obtained in the case of pure *LS* coupling.

Transitions with small *f*-values were generally assigned lower accuracy ratings.

References

- <sup>1</sup>B. Edlen, Phys. Scr. 17, 565 (1978).
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 <sup>3</sup>P. F. Gruzdev and A. I. Sherstyuk, Opt. Spectrosc. (USSR) 46, 353 (1979).
- <sup>4</sup>Y.-K. Kim and K.-T. Cheng, J. Opt. Soc. Am. 68, 836 (1978).
- <sup>5</sup>D. J. Pegg, P. M. Griffin, B. M. Johnson, K. W. Jones, and T. H. Kruse, Astrophys. J. 224, 1056 (1978).
- <sup>6</sup>J. P. Buchet, M. C. Buchet-Poulizac, A. Denis, J. Desesquelles, and M. Druetta, Phys. Rev. A 22, 2061 (1980).
- <sup>7</sup>E. Träbert, K. W. Jones, B. M. Johnson, D. C. Gregory, and T. H. Kruse, Phys. Lett. A **87**, 336 (1982).
- <sup>8</sup>C. E. Tull, R. P. McEachran, and M. Cohen, At. Data 3, 169 (1971).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | g i | g. | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | <i>S</i>
(at. u.) | log gf | Accu-
racy | Source |
|-----|---------------------|----------------------------------|----------|------------------------------|------------------------------|------------|----|--|--------|----------------------|--------|---------------|---------|
| | | | | | | | | | | | | | |
| 1. | 3s-3p | <sup>2</sup> S – <sup>2</sup> P° | 300.92 | 0 | 332310 | 2 | 6 | 90.1 | 0.367 | 0.727 | -0.134 | В | 1 |
| | | | 291.983 | 0 | 342486 | 2 | 4 | 99.1 | 0.253 | 0.487 | -0.295 | в | 1 |
| | | | 320.56 | 0 | 311950 | 2 | 2 | 73.8 | 0.114 | 0.240 | -0.643 | В | 1 |
| 2. | 3s-4p | <sup>2</sup> S - <sup>2</sup> P° | 41.078 | 0 | 2434400 | 2 | 6 | 3100 | 0.23 | 0.063 | -0.33 | С | interp. |
| | | | 41.015 | 0 | 2438400 | 2 | 4 | 2970 | 0.150 | 0.0405 | -0.52 | С | interp. |
| | | | 41.218 | 0 | 2426400 | 2 | 2 | 3200 | 0.0814 | 0.0221 | -0.788 | C+ | interp. |
| 3. | 3s~5p | <sup>2</sup> S - <sup>2</sup> P* | 29.796 | 0 | 3356200 | 2 | 6 | 1900 | 0.074 | 0.015 | -0.83 | с | 8 |
| | | | 29.779 | 0 | 3358100 | 2 | 4 | 1900 | 0.051 | 0.010 | -0.99 | с | ls |
| | | | 29.829 | 0 | 3352400 | 2 | 2 | 1900 | 0.025 | 0.0050 | 1.29 | С | ls |
| 4. | 3s-6p | <sup>2</sup> S - <sup>2</sup> P° | 26.029 | 0 | 3841900 | 2 | 6 | 1100 | 0.0334 | 0.0057 | -1.175 | С | 8 |
| | | | 26.020 | 0 | 3843200 | 2 | 4 | 1100 | 0.022 | 0.0038 | -1.35 | c | ls |
| | | | 26.046 | 0 | 3839400 | 2 | 2 | 1100 | 0.011 | 0.0019 | -1.65 | С | ls |
| 5. | 3s-7p | <sup>2</sup> S - <sup>2</sup> P° | | | | 2 | 6 | | 0.0183 | | -1.437 | с | 8 |
| 6. | 3s-8p | <sup>2</sup> S - <sup>2</sup> P° | | | | 2 | 6 | | 0.0113 | | -1.65 | с | 8 |
| 7. | 3p-3d | <sup>2</sup> P° – <sup>2</sup> D | 229.30 | 332310 | 768420 | 6 | 10 | 195 | 0.256 | 1.16 | 0.187 | в | 1 |
| | | | 233.75 | 342486 | 770300 | 4 | 6 | 183 | 0.225 | 0.694 | -0.045 | В | 1 |
| | | | 220.43 | 311950 | 765610 | 2 | 4 | 183 | 0.266 | 0.386 | -0.274 | B | 1 |
| | | | 200.01 | 342400 | 105010 | 4 | 4 | 23.4 | 0.0240 | 0.0700 | -1.007 | В | 1 |
| 8. | 3p-4s | <sup>2</sup> P° - <sup>2</sup> S | 50.777 | 332310 | 2301700 | 6 | 2 | 4600 | 0.059 | 0.059 | -0.45 | C- | 8 |
| 9. | 3p-4d | <sup>2</sup> P° – <sup>2</sup> D | 44.181 | <i>332310</i> | 2595700 | 6 | 10 | 6800 | 0.330 | 0.288 | 0.297 | С | interp. |
| | | | 44.365 | 342486 | 2596500 | 4 | 6 | 6800 | 0.301 | 0.176 | 0.081 | С | interp. |
| | | | 43.814 | 311950
342486 | 2594400
2594400 | | 4 | 5500
1140 | 0.32 | 0.092 | -0.20 | C | interp. |
| | | | 11.100 | 012100 | 2004400 | 1 | | 1110 | 0.0001 | 0.0107 | -0.01 | | interp. |

Ni xviii: Allowed transitions

Ni XVIII: Allowed transitions - Continued

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | <i>E</i> *
(cm <sup>-1</sup>) | gi | gı | $\begin{array}{c} A_{ki} \\ (10^8 \ \mathrm{s}^{-1}) \end{array}$ | fia | <i>S</i>
(at. u.) | log gf | Accu-
racy | Source |
|-----|---------------------|--|--------------------|------------------------------|-----------------------------------|--------|----|---|----------------|----------------------|-----------------|---------------|----------|
| 10 | 3n-5c | 2 D° – 2 G | | | | 6 | 9 | | 0.0119 | | _1 146 | C | 8 |
| 10. | 5p-08 | 1-5 | | | | | | 1000 | 0.0115 | | -1.140 | 0 | |
| 11. | 3p-5d | <sup>2</sup> P <sup>o</sup> - <sup>2</sup> D | 32.238 | 332310 | 3434200 | 6 | 10 | 4000 | 0.104 | 0.066 | 0.205 | C | 8 |
| | | | 32.340
32.034 | 342486
311950 | 3434600
3433700 | 4 | 6 | 4000 | 0.094 | 0.040 | -0.43 | C | ls |
| | | | [32.350] | 342486 | 3433700 | 4 | 4 | 660 | 0.010 | 0.0044 | -1.38 | D | Ls |
| 12. | 3 <i>p-6s</i> | <sup>2</sup> P° - <sup>2</sup> S | | | | 6 | 2 | | 0.0047 | | -1.55 | D | 8 |
| 13. | 3p-6d | <sup>2</sup> P° – <sup>2</sup> D | 28.14 0 | 332310 | 3885900 | 6 | 10 | 2360 | 0.0466 | 0.0259 | -0.55 | с | 8 |
| | | | 28.220 | 342486 | 3886100 | 4 | 6 | 2330 | 0.0417 | 0.0155 | -0.78 | с | ls |
| | | | 27.982 | 311950 | 3885700 | 2 | 4 | 2000 | 0.047 | 0.0086 | -1.03 | C | ls |
| | | | [28.223] | 342480 | 3003100 | 4 | 4 | 300 | 0.0040 | 0.0017 | -1.14 | | 48 |
| 14. | 3p-7s | <sup>2</sup> P° – <sup>2</sup> S | | | | 6 | 2 | | 0.0024 | | -1.84 | D | 8 |
| 15. | 3p-7d | <sup>2</sup> P° – <sup>2</sup> D | 26.15 | 332310 | 4156000 | 6 | 10 | 1490 | 0.0254 | 0.0131 | -0.82 | C | 8 |
| | | | 26.218 | 342486 | 4156700 | 4 | 6 | 1500 | 0.023 | 0.0079 | -1.04 | C | ls |
| | | | [26.02] | 311950 | 4155000 | | 4 | 240 | 0.0255 | $8.7(-4)^{\circ}$ | -1.292
-2.00 | D | 18
18 |
| 16. | 3p-8s | <sup>2</sup> P° - <sup>2</sup> S | | | | 6 | 2 | | 0.0014 | | -2.08 | D | 8 |
| 17. | 3p-8d | <sup>2</sup> P° - <sup>2</sup> D | 25.007 | 332310 | 4331200 | 6 | 10 | 1000 | 0.0156 | 0.0077 | -1.029 | c | 8 |
| | | | 95.070 | 349486 | 4991900 | | 6 | 990 | 0.014 | 0.0046 | _1 25 | C | 1. |
| | | | 23.010 | 311950 | 4331300 | 2 | 4 | 860 | 0.014 | 0.0026 | -1.50 | c | ls |
| | | | [25.071] | 342486 | 4331100 | 4 | 4 | 160 | 0.0015 | 5.1(-4) | -2.21 | D | ls |
| 18. | 3d-4p | <sup>2</sup> D - <sup>2</sup> P° | 60.024 | 768420 | 2434400 | 10 | 6 | 1080 | 0.0349 | 0.069 | -0.457 | C | 8 |
| | | | 59.950 | 770300 | 2438400 | 6 | 4 | 960 | 0.035 | 0.041 | -0.68 | C- | ls |
| | | | 60.212 | 765610 | 2426400 | 4 | 2 | 1100 | 0.029 | 0.023 | -0.94 | C- | ls |
| | | | [59.780] | 765610 | 2438400 | 4 | 4 | 110 | 0.0058 | 0.0046 | -1.63 | ם | 45 |
| 19. | 3d-4f | $^{2}D - ^{2}F^{\circ}$ | 52.679 | 768420 | 2666700 | 10 | 14 | 1.60(+4) | 0.93 | 1.62 | 0.97 | С | interp. |
| | | | 52.720 | 770300 | 2667100 | 6 | 8 | 1.6(+4) | 0.89 | 0.93 | 0.73 | C | interp. |
| | | | 52.615
[52.745] | 765610 | 2666200
2666200 | 4
6 | 6 | 1.5(+4)
1060 | 0.93
0.0444 | 0.64
0.0463 | -0.57 | C | interp. |
| 20. | 3 <i>d</i> -5p | <sup>2</sup> D - <sup>2</sup> P° | 38.643 | 768420 | 3356200 | 10 | 6 | 420 | 0.0057 | 0.0073 | -1.24 | D | 8 |
| | | | [38.643] | 770300 | 3358100 | 6 | 4 | 390 | 0.0058 | 0.0044 | -1.46 | D | ls |
| | | | [38.658] | 765610 | 3352400 | 4 | 2 | 420 | 0.0047 | 0.0024 | -1.72 | D | ls |
| | | | [38.573] | 765610 | 3358100 | 4 | 4 | 43 | 9.6(-4) | 4.9(-4) | -2.41 | E | ls |
| 21. | 3d-5f | $^{2}D - ^{2}F^{\circ}$ | 37.026 | 768420 | 3469200 | 10 | 14 | 5900 | 0.170 | 0.207 | 0.230 | С | 8 |
| | | | 37.049 | 770300 | 3469400 | 6 | 8 | 5900 | 0.161 | 0.118 | -0.014 | C | ls |
| | | | 36.990
[37.0551 | 765610 | 3469000
3469000 | 4
6 | 6 | 390 | 0.17 | 0.083 | -0.17
-1.32 | D | ls
Ls |
| 22. | 3d-6p | <sup>2</sup> D - <sup>2</sup> P° | 32.536 | 768420 | 3841900 | 10 | 6 | 220 | 0.0021 | 0.0022 | -1.68 | D | 8 |
| | | | 100 5 403 | 770000 | 0040000 | | | 100 | 0.0000 | 0.0019 | 1.09 | D | 10 |
| | | | [32.543] | 765610 | 3839400 | 4 | 42 | 210 | 0.0020 | 7.3(-4) | -1.92
-2.17 | D | ls |
| | | | [32.493] | 765610 | 3843200 | 4 | 4 | 22 | 3.5(-4) | 1.5(-4) | -2.85 | Е | Ls |
| | | | | | | 1 | 1 | | | | | | 1 |

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Ni xviii: Allowed transitions - Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | g, | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|---------------------|----------------------------------|----------------------------------|-------------------------------|-------------------------------|-------------|-------------|--|----------------------------|-----------------------------|---|---------------|----------------|
| 23. | 3d-6f | <sup>2</sup> D – <sup>2</sup> F° | 31.871 | 768420 | 3906000 | 10 | 14 | 3000 | 0.063 | 0.066 | -0.20 | с | 8 |
| | | | 31.890
31.845
[31.893] | 770300
765610
770300 | 3906100
3905800
3905800 | 6
4
6 | 8
6
6 | 3000
2700
200 | 0.060
0.062
0.0030 | 0.038
0.026
0.0019 | -0.44
-0.61
-1.74 | C
C
D | ls
ls
ls |
| 24. | 3d-7p | <sup>2</sup> D - <sup>2</sup> P° | | | | 10 | 6 | | 0.0010 | | -2.00 | D | 8 |
| 25. | 3d-7f | <sup>2</sup> D - <sup>2</sup> F° | 29.407 | 7 6 8420 | 4169000 | 10 | 14 | 1700 | 0.0308 | 0.0298 | -0.51 | с | 8 |
| | | | 29.422
29.383
[29.424] | 770300
765610
770300 | 4169100
4168900
4168900 | 6
4
6 | 8
6
6 | 1690
1580
110 | 0.0293
0.0308
0.0015 | 0.0170
0.0119
8.5(-4) | -0.76
-0.91
-2.06 | C
C
D | ls
ls
ls |
| 26. | 3d-8p | <sup>2</sup> D - <sup>2</sup> P° | | | | 10 | 6 | | 5.8(-4) | | -2.24 | Е | 8 |
| 27. | 3d-8f | <sup>2</sup> D - <sup>2</sup> F° | 28.00 | 768420 | 4339000 | 10 | 14 | 1080 | 0.0177 | 0.0163 | -0.75 | с | 8 |
| | | | 28.018
27.98
[28.01] | 770300
765610
770300 | 4339400
4340000
4340000 | 6
4
6 | 8
6
6 | 1100
1000
72 | 0.017
0.018
8.5(-4) | 0.0093
0.0065
4.7(-4) | $-1.00 \\ -1.15 \\ -2.29$ | C
C
E | ls
ls
ls |
| 28. | 4s-4p | <sup>2</sup> S - <sup>2</sup> P° | 753. 6 | 2301700 | 2434400 | 2 | 6 | 19.4 | 0.496 | 2.46 | -0.003 | с | 8 |
| | | | [731.5]
[801.9] | 2301700
2301700 | 2438400
2426400 | 2
2 | 4
2 | 21.2
16 | 0.341
0.16 | 1.64
0.82 | -0.167
-0.51 | C
C | ls
ls |
| 29. | 4s-5p | <sup>2</sup> S – <sup>2</sup> P° | <i>94.832</i> | 2301700 | 3356200 | 2 | 6 | 660 | 0.265 | 0.165 | -0.276 | c | 8 |
| | | | [94.661]
[95.175] | 2301700
2301700 | 3358100
3352400 | 2
2 | 4
2 | 660
650 | 0.176
0.088 | 0.110
0.055 | -0.452
-0.76 | C
C | ls
ls |
| 30. | 4s-6p | <sup>2</sup> S - <sup>2</sup> P° | 64.927 | 2301700 | 3841900 | 2 | 6 | 430 | 0.081 | 0.035 | -0.79 | с | 8 |
| | | | [64.872]
[65.032] | 2301700
2301700 | 3843200
3839400 | 2
2 | 4
2 | 430
440 | 0.054
0.028 | 0.023
0.012 | -0.97
-1.25 | C
C | ls
Ls |
| 31. | 4s-7p | <sup>2</sup> S – <sup>2</sup> P° | | | | 2 | 6 | | 0.0376 | | -1.124 | c | 8 |
| 32. | 4s-8p | <sup>2</sup> S - <sup>2</sup> P° | | | | 2 | 6 | | 0.0210 | | -1.377 | С | 8 |
| 33. | 4p-4d | <sup>2</sup> P° - <sup>2</sup> D | 620.0 | 2434400 | 2595700 | 6 | 10 | 38 | 0.37 | 4.5 | 0.34 | C | 3 |
| | | | [632.5]
[595.2]
[641.0] | 2438400
2426400
2438400 | 2596500
2594400
2594400 | 4
2
4 | 6
4
4 | 37
37
5.8 | 0.33
0.39
0.036 | 2.7
1.5
0.30 | $\begin{array}{c c} 0.12 \\ -0.11 \\ -0.84 \end{array}$ | C
C
C | 3
3
3 |
| 34. | 4p-5s | ²P° - ²S | | | | 6 | 2 | | 0.101 | | -0.218 | с | 8 |
| 35. | 4p-5d | <sup>2</sup> P° – <sup>2</sup> D | 100.0 | 2434400 | 3434200 | 6 | 10 | 1200 | 0.301 | 0.59 | 0.257 | С | 8 |
| | | | [100.4]
[99.275]
[100.5] | 2438400
2426400
2438400 | 3434600
3433700
3433700 | 4
2
4 | 6
4
4 | 1200
1000
190 | 0.26
0.31
0.029 | 0.35
0.20
0.039 | $0.02 \\ -0.21 \\ -0.93$ | C
C
D | ls
ls
ls |
| 36. | 4 <i>p</i> -6s | <sup>2</sup> P° – <sup>2</sup> S | | | | 6 | 2 | | 0.0203 | | -0.91 | с | 8 |
| 37. | 4p-6d | <sup>2</sup> P° - <sup>2</sup> D | 68.894 | 2434400 | 3885900 | 6 | 10 | 830 | 0.098 | 0.13 | -0.23 | с | 8 |
| | | | [69.075]
[68.526]
[69.094] | 2438400
2426400
2438400 | 3886100
3885700
3885700 | 4
2
4 | 6
4
4 | 800
680
130 | 0.086
0.095
0.0096 | 0.078
0.043
0.0087 | -0.46
-0.72
-1.42 | C
C
D | ls
ls
ls |

Ni XVIII: Allowed transitions -- Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | $egin{array}{c} E_i \ ({f cm}^{-1}) \end{array}$ | E_k (cm <sup>-1</sup>) | g i | ₿k | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|------------------------|----------------------------------|----------------------|--|---------------------------|------------|--------|--|---------------|---------------|--|---------------|----------|
| | | | | | | | | | | | | | |
| 38. | 4p-7s | <sup>2</sup> P° – <sup>2</sup> S | | | | 6 | 2 | | 0.0080 | | -1.32 | D | 8 |
| 39. | 4p-7d | <sup>2</sup> P° - <sup>2</sup> D | 58.07 | 2434400 | 4156000 | 6 | 10 | 550 | 0.0460 | 0.053 | -0.56 | С | 8 |
| | | | [58.197] | 2438400 | 4156700 | 4 | 6 | 550 | 0.042 | 0.032 | -0.78 | C | ls |
| | | | [57.84]
[58.24] | 2426400
2438400 | 4155000
4155000 | 2
4 | 4
4 | 470
90 | 0.047 | 0.018 | -1.02
-1.74 | D | ls
ls |
| 40. | 4 <i>p</i> -8s | <sup>2</sup> P° - <sup>2</sup> S | | | | 6 | 2 | | 0.0041 | | -1.61 | D | 8 |
| 41. | 4 <i>p</i> -8 <i>d</i> | <sup>2</sup> P° – <sup>2</sup> D | 52.720 | 2434400 | 4331200 | 6 | 10 | 373 | 0.0259 | 0.0270 | -0.81 | с | 8 |
| | | | [52.829] | 2438400 | 4331300 | 4 | 6 | 371 | 0.0233 | 0.0162 | -1.031 | с | ls |
| | | | [52.502]
[52.835] | 2426400
2438400 | 4331100
4331100 | 24 | 4 | 320
62 | 0.026 | 0.0090 | -1.28
-1.99 | CD | ls
ls |
| 49 | Ad-Af | 2D - 2F° | [02:000] | | | 10 | 14 | | 0 102 | | 0.009 | C | 8 |
| 40 | | 20 200 | 1915 | 2525700 | 995,0900 | 10 | | 510 | 0.102 | 0.95 | 0.000 | | |
| 43. | 4 <i>d</i> −5 <i>p</i> | -D - P | 131.5 | 2595700 | 3356200 | 10 | 0 | 510 | 0.080 | 0.35 | -0.10 | C | 8 |
| | | | [131.3] | 2596500 | 3358100
3352400 | 6 | 4 | 470 | 0.081 | 0.21 | -0.31 | C | ls |
| | | | [130.9] | 2594400 | 3358100 | 4 | 4 | 52 | 0.003 | 0.023 | -1.27 | D | ls |
| 44. | 4 <i>d</i> -5 <i>f</i> | <sup>2</sup> D – <sup>2</sup> F° | 114.5 | 2595700 | 3469200 | 10 | 14 | 2700 | 0.74 | 2.8 | 0.87 | с | 8 |
| | | | 114.74 | 2596500 | 3469400 | 6 | 8 | 2700 | 0.71 | 1.6 | 0.63 | c | ls |
| | | | 114.46
[114.6] | 2594400
2596500 | 3469000
3469000 | 4
6 | 6
6 | 2500
180 | 0.73
0.035 | 1.1
0.080 | $\begin{array}{c} 0.47 \\ -0.67 \end{array}$ | C
D | ls
ls |
| 45. | 4 <i>d</i> -6 <i>p</i> | <sup>2</sup> D - <sup>2</sup> P° | 80.244 | 2595700 | 3841900 | 10 | 6 | 240 | 0.0139 | 0.0367 | -0.86 | с | 8 |
| | | | [80.212] | 2596500 | 3843200 | 6 | 4 | 216 | 0.0139 | 0.0220 | -1.079 | c | ls |
| | | | [80.321] | 2594400 | 3839400 | 4 | 2 | 239 | 0.0115 | 0.0122 | -1.336 | C | ls |
| 46 | AJ EF | 270 2150 | 76 919 | 2034100 | 2006000 | 10 | 14 | 1470 | 0.180 | 0.452 | 0.955 | C | 8 |
| 40. | 40-0/ | -D-F | 70.310 | 2555700 | 3300000 | 10 | 14 | 1410 | 0.100 | 0.402 | 0.200 | | |
| | | | [76.359]
[76.254] | 2596500
2594400 | 3906100
3905800 | 6 | 8 | 1470 | 0.171 | 0.258 | 0.011
-0.142 | C | ls |
| | | | [76.377] | 2596500 | 3905800 | 6 | 6 | 99 | 0.0086 | 0.013 | -1.29 | D | Ls . |
| 47. | 4 <i>d</i> -7 <i>p</i> | <sup>2</sup> D - <sup>2</sup> P° | | | | 10 | 6 | | 0.0052 | | -1.28 | D | 8 |
| 48. | 4 <i>d</i> -7 <i>f</i> | $^{2}D - ^{2}F^{\circ}$ | 63.561 | 2595700 | 4169000 | 10 | 14 | 870 | 0.074 | 0.15 | -0.13 | С | 8 |
| | | | [63.589] | 2596500 | 4169100 | 6 | 8 | 850 | 0.068 | 0.086 | -0.39 | с | ls |
| | | | [63.512] | 2594400
2596500 | 4168900 | 4 | 6 | 790
56 | 0.072 | 0.060 | -0.54
-1.69 | CD | ls
Is |
| 49. | 4d-8p | <sup>2</sup> D - <sup>2</sup> P° | [00.001] | 200000 | 4100000 | 10 | 6 | | 0.0026 | 0.0040 | -1.59 | D | 8 |
| 50. | 4d-8f | <sup>2</sup> D - <sup>2</sup> F° | 57.37 | 2595700 | 4339000 | 10 | 14 | 560 | 0.0389 | 0.073 | -0.410 | с | 8 |
| | , | | [57 976] | 2596500 | 1339400 | 6 | 8 | 560 | 0.037 | 0.042 | -0.65 | C | 10 |
| | | | [57.27] | 2594400 | 4340000 | 4 | 6 | 520 | 0.038 | 0.029 | -0.81 | č | ls |
| | | | [57.37] | 2596500 | 4340000 | 6 | 6 | 38 | 0.0019 | 0.0021 | -1.95 | D | ls |
| 51. | 4f-5d | <sup>2</sup> F° – <sup>2</sup> D | 130.3 | 2666700 | 3434200 | 14 | 10 | 100 | 0.0181 | 0.109 | -0.60 | С | 8 |
| | | | [130.3] | 2667100 | 3434600 | 8 | 6 | 95
100 | 0.018 | 0.062 | -0.84 | C | ls
Is |
| | | | [130.3] | 2666200 | 3434600 | 6 | 6 | 4.8 | 0.0103 | 0.0031 | -2.14 | D | ls |
| | | | | | | | | | | | | | |

Ni XVIII: Allowed transitions - Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | gi | g, | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | <i>S</i>
(at. u.) | log gf | Accu-
racy | Source |
|--------------|---------------------|---|----------------------|------------------------------|------------------------------|----|--------|--|--|----------------------|-----------------|---------------|----------|
| | | | | | | | | | | | | | |
| 52. | 4f-6d | ${}^{2}\mathbf{F}^{\circ} - {}^{2}\mathbf{D}$ | 82.021 | 2666700 | 3885900 | 14 | 10 | 42 | 0.0030 | 0.011 | -1.38 | D | 8 |
| | | | [82.034] | 2667100 | 3886100 | 8 | 6 | 39 | 0.0029 | 0.0063 | -1.63 | D | ls |
| | | | [82.001]
[81.974] | 2666200 | 3885700 | 6 | 4
6 | 1.9 | 0.0027 | 3.1(-4) | -2.94 | E | ls
ls |
| 53. | 4f-7d | ${}^{2}\mathbf{F}^{\circ} - {}^{2}\mathbf{D}$ | 67.16 | 2666700 | 4156000 | 14 | 10 | 23 | 0.0011 | 0.0034 | 1.81 | D | 8 |
| | | | [67.132] | 2667100 | 4156700 | 8 | 6 | 21 | 0.0011 | 0.0019 | -2.07 | D | ls |
| | | | [67.16]
[67.092] | 2666200
2666200 | 4155000
4156700 | 6 | 4
6 | 23 | 0.0011
7.3(-5) | 0.0014
9.7(-5) | -2.20
-3.36 | D
E | ls
ls |
| 54. | 4f-8d | <sup>2</sup> F° – <sup>2</sup> D | 60.078 | 2666700 | 4331200 | 14 | 10 | 13 | 5.1(-4) | 0.0014 | -2.15 | E | 8 |
| | , | | 160 0001 | 9667100 | 4991900 | | c | 10 | 51(4) | 000 1) | 9.90 | F | 1. |
| | | | [60.089] | 2666200 | 4331300 | 6 | 4 | 12 | $\begin{vmatrix} 3.1(-4) \\ 4.7(-4) \end{vmatrix}$ | 5.6(-4) | -2.55 | E | ls |
| | | | [60.056] | 2666200 | 4331300 | 6 | 6 | 0.62 | 3.4(-5) | 4.0(-5) | -3.69 | Е | ls |
| 55. | 5s-5p | <sup>2</sup> S - <sup>2</sup> P° | | | | 2 | 6 | | 0.64 | | 0.11 | с | 8 |
| 56. | 5s-6p | <sup>2</sup> S - <sup>2</sup> P° | | | | 2 | 6 | | 0.287 | | -0.241 | с | 8 |
| 57. | 5s-7p | <sup>2</sup> S – <sup>2</sup> P° | | | | 2 | 6 | | 0.089 | | -0.75 | С | 8 |
| 58. | 5s-8p | <sup>2</sup> S – <sup>2</sup> P° | | | | 2 | 6 | | 0.0415 | | -1.081 | c | 8 |
| 59. | 5p-5d | <sup>2</sup> P° - <sup>2</sup> D | | | | 6 | 10 | | 0.53 | | 0.50 | с | 8 |
| 60. | 5p-6s | <sup>2</sup> P° - <sup>2</sup> S | | | | 6 | 2 | | 0.143 | | -0.067 | с | 8 |
| 61. | 5p-6d | $^{2}P^{\circ} - ^{2}D$ | 188.8 | 3356200 | 3885900 | 6 | 10 | 321 | 0.286 | 1.07 | 0.235 | с | 8 |
| | | | [189.4] | 3358100 | 3886100 | 4 | 6 | 320 | 0.26 | 0.64 | 0.01 | C | ls |
| | | | [187.5]
[189.5] | 3352400
3358100 | 3885700
3885700 | 4 | 4 | 274
53 | 0.289 | 0.357 | -0.238
-0.94 | D | ls
ls |
| 62. | 5p-7s | <sup>2</sup> P° - <sup>2</sup> S | | | | 6 | 2 | | 0.0288 | | -0.76 | с | 8 |
| 63. | 5p-7d | <sup>2</sup> P° - <sup>2</sup> D | 125 | 3356200 | 4156000 | 6 | 10 | 250 | 0.096 | 0.24 | -0.24 | с | 8 |
| | | | [125.2] | 3358100 | 4156700 | 4 | 6 | 240 | 0.085 | 0.14 | -0.47 | C | ls |
| | | | [125] | 3352400
3358100 | 4155000
4155000 | 24 | 4 | 210
41 | 0.097 | 0.080 | -0.71
-1.41 | D | ls
ls |
| 64. | 5p-8s | <sup>2</sup> P° ~ <sup>2</sup> S | | | | 6 | 2 | | 0.0114 | | -1.165 | с | 8 |
| 65. | 5p-8d | <sup>2</sup> P° – <sup>2</sup> D | 102.6 | 3356200 | 4331200 | 6 | 10 | 175 | 0.0459 | 0.093 | -0.56 | с | 8 |
| | | | [102.8] | 3358100 | 4331300 | 4 | . 6 | 170 | 0.041 | 0.056 | -0.78 | с | ls |
| | | | [102.2] | 3352400 | 4331100 | 2 | 4 | 150 | 0.046 | 0.031 | -1.04 | C | ls |
| | | | [102.8] | 3338100 | 4331100 | 4 | 4 | 29 | 0.0046 | 0.0062 | -1.74 | D | LS . |
| 6 6 . | 5d-5f | <sup>2</sup> D - <sup>2</sup> F° | | | | 10 | 14 | | 0.181 | | 0.258 | С | 8 |
| 67. | 5 d -6p | <sup>2</sup> D – <sup>2</sup> P* | 245.3 | 3434200 | 3841900 | 10 | 6 | 238 | 0.129 | 1.04 | 0.111 | С | 8 |
| | | | [244.7]
[246 5] | 3434600
3433700 | 3843200
3839400 | 6 | 4 | 210
235 | 0.13 | 0.62 | -0.11 | C
C | ls
In |
| | | | [244.2] | 3433700 | 3843200 | 4 | 4 | 24 | 0.021 | 0.069 | -1.07 | D | Ls
Ls |
| 1 | | | | | | | | | | | | | |

| F - | 8 | 3 |
|-----|---|---|
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Ni XVIII: Allowed transitions - Continued

| No. | Transition
Array | Multiplet | λ
(Å) | E_i (cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | gi | ₿ŧ | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | f ik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|---------------------|----------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------|-------------|--|----------------------------|--------------------------|---------------------------|---------------|----------------|
| 68. | 5d-6f | ²D - ²F° | 212.0 | 3434200 | 3906000 | 10 | 14 | 700 | 0.66 | 4.6 | 0.82 | с | 8 |
| | | | [212.1]
[211.8]
[212.2] | 3434600
3433700
3434600 | 3906100
3905800
3905800 | 6
4
6 | 8
6
6 | 690
640
46 | 0.62
0.65
0.031 | 2.6
1.8
0.13 | 0.57
0.41
0.73 | C
C
D | ls
ls
ls |
| 69. | 5d-7p | <sup>2</sup> D - <sup>2</sup> P° | | | | 10 | 6 | | 0.0232 | | 0.63 | с | 8 |
| 70. | 5d-7f | ² D − ² F ° | 136.1 | 3434200 | 4169000 | 10 | 14 | 458 | 0.178 | 0.80 | 0.250 | с | 8 |
| | | | [136.1]
[136.0]
[136.2] | 3434600
3433700
3434600 | 4169100
4168900
4168900 | 6
4
6 | 8
6
6 | 460
430
31 | 0.17
0.18
0.0085 | 0.46
0.32
0.023 | 0.01
-0.15
-1.29 | C
C
D | ls
Is
Is |
| 71. | 5d-8p | <sup>2</sup> D - <sup>2</sup> P° | | | | 10 | 6 | | 0.0087 | | -1.06 | D | 8 |
| 72. | 5d-8f | $^{2}D - ^{2}F^{\circ}$ | 110 | 3434200 | 4339000 | 10 | 14 | 310 | 0.078 | 0.28 | -0.11 | с | 8 |
| | | | [110.5]
[110]
[110] | 3434600
3433700
3434600 | 4339400
4340000
4340000 | 6
4
6 | 8
6
6 | 300
280
20 | 0.073
0.076
0.0037 | 0.16
0.11
0.0080 | $-0.36 \\ -0.52 \\ -1.66$ | C
C
D | ls
ls
ls |
| 73. | 5f-6d | <sup>2</sup> F° − <sup>2</sup> D | 240.0 | 3469200 | 3885900 | 14 | 10 | 72 | 0.0444 | 0.491 | -0.206 | с | 8 |
| | | | [240.0]
[240.0]
[239.8] | 3469400
3469000
3469000 | 3886100
3885700
3886100 | 8
6
6 | 6
4
6 | 69
72
3.4 | 0.0445
0.0413
0.0030 | 0.281
0.196
0.014 | -0.449
-0.61
-1.75 | C
C
D | ls
Is
Is |
| 74. | 5f-7d | <sup>2</sup> F° - <sup>2</sup> D | 146 | 3469200 | 4156000 | 14 | 10 | 35 | 0.0079 | 0.053 | -0.96 | D | 8 |
| | | | [145.5]
[146]
[145.4] | 3469400
3469000
3469000 | 4156700
4155000
4156700 | 8
6
6 | 6
4
6 | 33
34
1.6 | 0.0078
0.0073
5.2(4) | 0.030
0.021
0.0015 | $-1.20 \\ -1.36 \\ -2.50$ | D
D
E | ls
ls
ls |
| 75. | 5f-8d | <sup>2</sup> F° - <sup>2</sup> D | [116.0] | 3469200 | 4331200 | 14 | 10 | 20 | 0.0029 | 0.016 | -1.39 | D | 8 |

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Forbidden Transitions

| List | of | tabulated | lines |
|------|----|-----------|-------|
|------|----|-----------|-------|

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|
| 29.115 | 28 | 77.567 | 9 | 142.8 | 18 | 303.5 | 49 |
| 31.981 | 30 | 80.671 | 12 | 142.9 | 18 | 306.8 | 49 |
| 38.513 | 27 | 80.710 | 12 | 143.0 | 18 | 307.0 | 49 |
| 38.545 | 27 | 85.027 | 42 | 144.5 | 41 | 339.2 | 32 |
| 42.477 | 29 | 88.269 | 33 | 144.7 | 41 | 341.6 | 32 |
| 43.018 | 29 | 88.339 | 33 | 145.7 | 41 | 369.0 | 20 |
| 43.035 | 29 | 95.914 | 37 | 180.7 | 44 | 369.5 | 20 |
| 47.028 | 4 | 96.993 | 37 | 182.5 | 44 | 372 | 20 |
| 47.712 | 4 | 97.031 | 37 | 182.6 | 44 | 379.8 | 22 |
| 47.987 | 4 | 101 | 46 | 200 | 50 | 380.1 | 22 |
| 52.604 | 40 | 101.9 | 46 | 201 | 50 | 380.2 | 22 |
| 53.908 | 35 | 102 | 46 | 201.5 | 50 | 380.5 | 22 |
| 53.97 | 35 | 107.3 | 6 | 203.7 | 13 | 417.0 | 36 |
| 54.618 | 5 | 108.7 | 6 | 206.1 | 13 | 437.3 | 36 |
| 54.681 | 5 | 109.4 | 6 | 207.8 | 13 | 439.0 | 36 |
| 54.759 | 5 | 111.4 | 16 | 221.0 | 14 | 568 | 24 |
| 54.822 | 5 | 111.5 | 16 | 221.2 | 14 | 572.7 | 24 |
| 57.389 | 39 | 114.9 | 19 | 221.5 | 14 | 573.4 | 24 |
| 57.780 | 39 | 115 | 19 | 221.7 | 14 | 585 | 25 |
| 63.115 | 34 | 119.0 | 8 | 224.4 | 21 | 586.5 | 25 |
| 63.131 | 34 | 119.1 | 8 | 224.5 | 21 | 587.2 | 25 |
| 64.094 | 10 | 119.3 | 8 | 224.6 | 21 | 857.6 | 43 |
| 65.100 | 31 | 119.4 | 8 | 224.7 | 21 | 898.5 | 43 |
| 65.300 | 31 | 122.5 | 45 | 228.8 | 17 | 901.7 | 43 |
| 67.595 | 38 | 123.3 | 45 | 228.9 | 17 | 1510 | 48 |
| 68.134 | 38 | 124.5 | 11 | 229.0 | 17 | 1590 | 48 |
| 68.148 | 38 | 124.6 | 11 | 229.1 | 17 | 1600 | 48 |
| 70.582 | 7 | 124.7 | 11 | 230 | 23 | 3273 | 1 |
| 71.185 | 7 | 129.82 | 26 | 230.6 | 23 | 8330 | 3 |
| 71.378 | 7 | 130.61 | 26 | 230.8 | 23 | 21300 | 2 |
| 77.417 | 9 | 138.3 | 15 | 267.2 | 47 | | |
| 77.441 | 9 | 138.5 | 15 | 267.5 | 47 | | |
| 77.543 | 9 | 139 | 15 | 270.0 | 47 | | |
| | | 11 | | lf | | | |

Electric quadrupole strengths for numerous multiplets in this sodiumlike ion were determined by Tull *et al.*<sup>1</sup> using the frozen-core Hartree-Fock approach with no allowance for configuration mixing. *LS*-coupling rules were applied to obtain strengths of lines within multiplets. The strongest lines for which fairly accurate wavelengths could be derived from experimentally determined energy levels are quoted in this compilation.

The strengths given in Ref. 1 for transitions in which both $\Delta n = 0$ and $\Delta l = 0$ (i.e., transitions between the two levels of a given term) are overstated, and had to be reduced as follows:
$$\begin{split} & S(np\ ^2\mathrm{P}_{1/2}^{\circ} - np\ ^2\mathrm{P}_{3/2}^{\circ}) = \mathrm{S}(\mathrm{Ref.}\ 1) \times (1/3) \\ & S(nd\ ^2\mathrm{D}_{3/2} - nd\ ^2\mathrm{D}_{5/2}) = \mathrm{S}(\mathrm{Ref.}\ 1) \times (3/25) \\ & S(nf\ ^2\mathrm{F}_{5/2}^{\circ} - nf\ ^2\mathrm{F}_{7/2}^{\circ}) = \mathrm{S}(\mathrm{Ref.}\ 1) \times (3/49). \end{split}$$

Reference

<sup>1</sup>C. E. Tull, M. Jackson, R. P. McEachran, and M. Cohen, J. Quant. Spectrosc. Radiat. Transfer 12, 893 (1972).

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| | Ni xvm: | Forbidden | transitions |
|--|---------|-----------|-------------|
|--|---------|-----------|-------------|

| No. | Transition
Array | Multiplet | λ
(Å) | E_i (cm <sup>-1</sup>) | $\frac{E_k}{(\mathrm{cm}^{-1})}$ | g i | ₿⊧ | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Sour |
|-----|------------------------|-----------------------------------|----------------------------------|-------------------------------|----------------------------------|-------------|-------------|-----------------------|---------------------------------------|----------------|---------------|--------------------------------|
| 1. | 30-30 | <sup>2</sup> P° – <sup>2</sup> P° | | | | | | | | | | |
| | -7 -7 | | [3273] | 311950 | 342486 | 2 | 4 | E 2 | 0.11 | 0.094 | D | 1 |
| 2. | 3d-3d | <sup>2</sup> D – <sup>2</sup> D | | | | | | | | | - | |
| | | | [21300] | 7656100 | 770300 | 4 | 6 | E 2 | 1.7(-6) <sup>a</sup> | 0.027 | D- | 1 |
| 3. | 4 <i>p</i> -4 <i>p</i> | ²₽° – ²₽° | | | | | | | | | | |
| | 9- 4- | 2100 2100 | [8330] | 2426400 | 2438400 | 2 | 4 | E 2 | 0.013 | 1.2 | D- | 1 |
| 4. | 3p-4p | r - r | [47 719] | 342486 | 2438400 | 4 | 4 | F2 | 6.6(+7) | 0.039 | п | 1 /2 |
| | | | [47.987]
[47.028] | 342486
311950 | 2426400
2438400 | 42 | 2
4 | E2
E2 | 1.3(+8)
7.1(+7) | 0.039 | D
D | 1,13
1,13
1,13 |
| 5. | 3d-4d | <sup>2</sup> D - <sup>2</sup> D | | | | | | | | | | |
| | | | [54.759]
[54.681] | 770300
765610 | 2596500
2594400 | 6 | 6
4 | E2
E2 | 3.6(+7)
3.2(+7) | 0.063 | DD | 1, <i>ls</i> |
| | | | [54.822]
[54.618] | 770300
765610 | 2594400
2596500 | 6
4 | 4
6 | E2
E2 | 1.4(+7)
9.2(+6) | 0.016
0.016 | E
E | 1, <i>ls</i>
1, <i>ls</i> |
| 6. | 4 <i>p−</i> 5 <i>p</i> | <sup>2</sup> P° - <sup>2</sup> P° | | | | | | | | | | |
| | | | [108.7]
[109.4] | 2438400
2438400 | 3358100
3352400 | 4 | 4
2 | E2
E2 | 1.07(+7)
2.07(+7) | 0.387
0.387 | C
C | 1, <i>ls</i>
1, <i>ls</i> |
| | | ~ ~ | [107.3] | 2426400 | 3358100 | 2 | 4 | E2 | 1.14(+7) | 0.387 | C | 1, <i>ls</i> |
| 7. | 4 <i>p</i> -6 <i>p</i> | ²P° - ²P° | [71 107] | 9499400 | 00.40000 | | | 120 | | 0.020 | n | |
| | | | [71.185]
[71.378]
[70.582] | 2438400
2438400
2426400 | 3839400
3843200 | 4
4
2 | 4
2
4 | E2
E2
E2 | 1.4(+7)
7.2(+6) | 0.030 | D
D
D | 1,4s
1,4s
1,4s |
| 8. | 4 <i>d</i> -5 <i>d</i> | <sup>2</sup> D - <sup>2</sup> D | | | | | | | | | | |
| | | | [119.3]
[119.1] | 2596500
2594400 | 3434600
3433700 | 6 | 6
4 | E2
E2 | 8.1(+6)
7.1(+6) | 0.70
0.406 | C
C | 1, <i>ls</i> |
| | | | [119.4]
[119.0] | 2596500
2594400 | 3433700
3434600 | 6
4 | 4
6 | E2
E2 | 3.01(+6)
2.04(+6) | 0.174
0.174 | C-
C- | 1, ls
1, ls |
| 9. | 4d-6d | <sup>2</sup> D - <sup>2</sup> D | | | | | | | | | | |
| | | | [77.543]
[77.441] | 2596500
2594400 | 3886100
3885700 | 6
4 | 6
4 | E2
E2 | 4.8(+6)
4.2(+6) | 0.048
0.028 | D
D | 1, <i>ls</i>
1, <i>ls</i> |
| | | | [77.567]
[77.417] | 2596500
2594400 | 3885700
3886100 | 6
4 | 4
6 | E2
E2 | 1.8(+6)
1.2(+6) | 0.012
0.012 | E
E | 1, <i>ls</i>
1, <i>ls</i> |
| 10. | 4d-7d | <sup>2</sup> D - <sup>2</sup> D | | | | | | | | | | |
| | | | [64.094] | 2596500 | 4156700 | 6 | 6 | E2 | 3.1(+6) | 0.012 | D | 1, l s |
| 11. | 4 <i>f</i> -5 <i>f</i> | <sup>2</sup> F° – <sup>2</sup> F° | | | | | | | | | | |
| | | | [124.6]
[124.6] | 2667100
2666200 | 3469400
3469000 | 8
6 | 8
6 | E2
E2 | $4.7(+6) \\ 4.48(+6)$ | 0.67 | C | 1, <i>ls</i> |
| | | | [124.7]
[124.5] | 2667100
2666200 | 3469000
3469400 | 8
6 | 6
8 | E2
E2 | 7.4(+5)
5.6(+5) | 0.080 | D
D | 1, <i>ls</i>
 1, <i>ls</i> |

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Ni XVIII: Forbidden transitions -- Continued

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | gi | g. | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|------------------------|---|--|--|--|------------------|------------------|----------------------------|--|----------------------------------|--------------------|--|
| 12. | 4 <i>f–</i> 6 <i>f</i> | <sup>2</sup> F° - <sup>2</sup> F° | | | | | | | | | | |
| | | | [80.710]
[80.671] | 2667100
2666200 | 3906100
3905800 | 8
6 | 8
6 | E2
E2 | 2.3(+6)
2.2(+6) | 0.038
0.027 | D
D | 1, <i>ls</i>
1, <i>ls</i> |
| 13. | 5 <i>p-</i> 6 <i>p</i> | ²P° - ²P° | | | | | | | | | | |
| | | | [206.1]
[207.8]
[203.7] | 3358100
3358100
3352400 | 3843200
3839400
3843200 | 4
4
2 | 4
2
4 | E2
E2
E2 | $2.50(+6) \\ 4.79(+6) \\ 2.65(+6)$ | 2.21
2.21
2.21 | C
C
C | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |
| 14. | 5d-6d | <sup>2</sup> D - <sup>2</sup> D | | | | | | | | | | |
| | | | [221.5]
[221.2]
[221.7]
[221.0] | 3434600
3433700
3434600
3433700 | 3886100
3885700
3885700
3886100 | 6
4
6
4 | 6
4
4
6 | E2
E2
E2
E2 | $2.13(+6) \\ 1.88(+6) \\ 8.0(+5) \\ 5.4(+5)$ | 4.06
2.37
1.02
1.02 | C
C
C-
C- | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |
| 15. | 5d-7d | <sup>2</sup> D - <sup>2</sup> D | | | | | | | | | | |
| | | | [138.5]
[139]
[139]
[138.3] | 3434600
3433700
3434600
3433700 | 4156700
4155000
4155000
4156700 | 6
4
6
4 | 6
4
4
6 | E2
E2
E2
E2
E2 | $\begin{array}{c} 1.46(+6) \\ 1.25(+6) \\ 5.3(+5) \\ 3.7(+5) \end{array}$ | 0.266
0.155
0.066
0.066 | C
C
D
D | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |
| 16. | 5d-8d | <sup>2</sup> D - <sup>2</sup> D | | | | | | | | | | |
| | | | [111.5]
[111.4]
[111.5]
[111.4] | 3434600
3433700
3434600
3433700 | 4331300
4331100
4331100
4331300 | 6
4
6
4 | 6
4
4
6 | E2
E2
E2
E2 | 9.9(+5)8.8(+5)3.7(+5)2.4(+5) | 0.061
0.036
0.015
0.015 | D
D
E
E | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |
| 17. | 5f-6f | <sup>2</sup> F° - <sup>2</sup> F° | | | | | | | | | | |
| | | | [229.0]
[228.9]
[229.1]
[228.8] | 3469400
3469000
3469400
3469000 | 3906100
3905800
3905800
3906100 | 8
6
8
6 | 8
6
6
8 | E2
E2
E2
E2 | $\begin{array}{c} 1.63(+6) \\ 1.57(+6) \\ 2.6(+5) \\ 2.0(+5) \end{array}$ | 4.89
3.52
0.59
0.59 | C
C
C-
C- | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |
| 18. | 5f-7f | <sup>2</sup> F° – <sup>2</sup> F° | | | | | | | | | | |
| | | | [142.9]
[142.9]
[143.0]
[142.8] | 3469400
3469000
3469400
3469000 | 4169100
4168900
4168900
4169100 | 8
6
8
6 | 8
6
6
8 | E2
E2
E2
E2 | $\begin{array}{c c} 1.00(+6) \\ 9.6(+5) \\ 1.6(+5) \\ 1.2(+5) \end{array}$ | 0.284
0.205
0.034
0.034 | C
C
D
D | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |
| 19. | 5f-8f | <sup>2</sup> F <sup>•</sup> - <sup>2</sup> F <sup>•</sup> | | | | | | | | | | |
| | | | [114.9]
[115] | 3469400
3469000 | 4339400
4340000 | 8.
6 | 8
6 | E2
E2 | 6.4(+5)
6.1(+5) | 0.061
0.044 | D
D | 1, <i>ls</i>
1, <i>ls</i> |
| 20. | 6d-7d | <sup>2</sup> D - <sup>2</sup> D | | | | | | | | | | |
| | | | [369.5]
[372]
[372]
[369.0] | 3886100
3885700
3886100
3885700 | 4156700
4155000
4155000
4156700 | 6
4
6
4 | 6
4
4
6 | E2
E2
E2
E2
E2 | 6.8(+5)
5.8(+5)
2.5(+5)
1.72(+5) | 16.8
9.8
4.2
4.21 | C
D+
D
C- | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |

Ni XVIII: Forbidden transitions - Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | gi | g⊾ | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|------------------------|-----------------------------------|--|--|--|------------------|------------------|-----------------------|---|--------------------------------|---------------------|--|
| 21. | 6d-8d | <sup>2</sup> D – <sup>2</sup> D | | | | | | | | | | |
| | | | [224.6]
[224.5]
[224.7]
[224.4] | 3886100
3885700
3886100
3885700 | 4331300
4331100
4331100
4331300 | 6
4
6
4 | 6
4
4
6 | E2
E2
E2
E2 | 5.1(+5)
4.5(+5)
1.93(+5)
1.29(+5) | 1.05
0.61
0.263
0.263 | C
C
C-
C- | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |
| 22. | 6 <i>f</i> -7 <i>f</i> | <sup>2</sup> F° – <sup>2</sup> F° | | | | | | | | | | |
| | | | [380.2]
[380.1]
[380.5]
[379.8] | 3906100
3905800
3906100
3905800 | 4169100
4168900
4168900
4169100 | 8
6
8
6 | 8
6
6
8 | E2
E2
E2
E2 | 5.8(+5)
5.6(+5)
9.2(+4)
7.0(+4) | 21.9
15.8
2.63
2.63 | C
C
C-
C- | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |
| 23. | 6 <i>f</i> -8 <i>f</i> | <sup>2</sup> F° – <sup>2</sup> F° | | | | | | | | | | |
| | | | [230.8]
[230]
[230]
[230.6] | 3906100
3905800
3906100
3905800 | 4339400
4340000
4340000
4339400 | 8
6
8
6 | 8
6
6
8 | E2
E2
E2
E2 | $\begin{array}{c} 4.04(+5) \\ 4.0(+5) \\ 6.5(+4) \\ 4.86(+4) \end{array}$ | 1.26
0.91
0.15
0.151 | C
C-
D+
C- | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |
| 24. | 7d-8d | <sup>2</sup> D ~ <sup>2</sup> D | | | | | | | | | | |
| | | | [572.7]
[568]
[573.4]
[568] | 4156700
4155000
4156700
4155000 | 4331300
4331100
4331100
4331300 | 6
4
6
4 | 6
4
4
6 | E2
E2
E2
E2 | $\begin{array}{c} 2.5(+5) \\ 2.3(+5) \\ 9.4(+4) \\ 6.6(+4) \end{array}$ | 56
32
13.9
14 | C
D
C-
D | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |
| 25. | 7 <i>f-</i> 8f | <sup>2</sup> F° - <sup>2</sup> F° | | | - | | | | | | | |
| | | | [587.2]
[585]
[585]
[586.5] | 4169100
4168900
4169100
4168900 | 4339400
4340000
4340000
4339400 | 8
6
8
6 | 8
6
6
8 | E2
E2
E2
E2 | 2.3(+5) 2.2(+5) 3.7(+4) 2.7(+4) | 75
54
9.0
9.0 | C
D
D
C- | 1,ls
1,ls
1,ls
1,ls |
| 26. | 3s-3d | <sup>2</sup> S - <sup>2</sup> D | | | | | | | | | | |
| | | | [129.82]
[130.61] | 0
0 | 770300
765610 | 2
2 | 6
4 | E2
E2 | 8.4(+5)
8.2(+5) | 0.110
0.074 | C
D | 1, <i>ls</i>
1, <i>ls</i> |
| 27. | 3s-4d | <sup>2</sup> S - <sup>2</sup> D | | | | | | | | | | |
| | | | [38.513]
[38.545] | 0
0 | 2596500
2594400 | 2
2 | 6
4 | E2
E2 | 2.8(+8)
2.9(+8) | 0.086
0.058 | D
D | 1, <i>ls</i>
1, <i>ls</i> |
| 28. | 3s-5d | <sup>2</sup> S – <sup>2</sup> D | | | | | | | | | | |
| | | | [29.115] | 0 | 3434600 | 2 | 6 | E2 | 1.5(+8) | 0.011 | D | 1, ls |
| 29. | 3p-4f | <sup>2</sup> P° - <sup>2</sup> F° | | | | | | | | | | |
| | | | [43.018]
[42.477]
[43.035] | 342486
311950
342486 | 2667100
2666200
2666200 | 4
2
4 | 8
6
6 | E2
E2
E2 | 4.92(+8)
4.07(+8)
1.1(+8) | 0.345
0.201
0.057 | C
C
D | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |
| 30. | 3p-5f | <sup>2</sup> P° – <sup>2</sup> F° | | | | | | | | | | |
| | | | [31.981] | 342486 | 3469400 | 4 | 8 | E2 | 7.5(+7) | 0.012 | D | 1, <i>ls</i> |
| 31. | 3 <i>d</i> -4s | <sup>2</sup> D - <sup>2</sup> S | | | 0001700 | | | D o | 0.7(. 7) | 0.099 | D | 1.2 |
| | | | [65.300]
[65.100] | 770300
765610 | 2301700 2301700 | 4 | 2 | E2
E2 | 1.8(+7) | 0.038 | D | 1, <i>ls</i>
1, <i>ls</i> |

Ni XVIII: Forbidden transitions - Continued

| No. | Transition
Array | Multiplet | λ
(Å) | E_i (cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | ₿ŧ | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | <i>S</i>
(at. u.) | Accu-
racy | Source |
|-------------|------------------------|-----------------------------------|----------------------------------|-------------------------------------|-------------------------------|-------------|-------------|-----------------------|--|-------------------------|---------------|--|
| 32. | 4s-4d | <sup>2</sup> S - <sup>2</sup> D | | | | | | | | | | |
| | | | [339.2]
[341.6] | 2301700
2301700 | 2596500
2594400 | 2
2 | 6
4 | E2
E2 | 1.06(+5)
1.02(+5) | 1.70
1.13 | C
C | 1, <i>ls</i>
1, <i>ls</i> |
| 33. | 4s-5d | <sup>2</sup> S – <sup>2</sup> D | | | | | | 1 | | | | |
| | | | [88.269]
[88.339] | 2301700
2301700 | 3434600
3433700 | 2
2 | 6
4 | E2
E2 | 3.1(+7)
3.07(+7) | 0.59
0.393 | C
C | 1, <i>ls</i>
1, <i>ls</i> |
| 34. | 4s-6d | <sup>2</sup> S – <sup>2</sup> D | | | | | | | | | | |
| | | | [63.115]
[63.131] | 2301700
2301700 | 3886100
3885700 | 2
2 | 6
4 | E2
E2 | $2.1(+7) \\ 2.1(+7)$ | 0.074
0.050 | D
D | 1, <i>ls</i>
1, <i>ls</i> |
| 35. | 4s-7d | <sup>2</sup> S – <sup>2</sup> D | | | | | | | | | | |
| | | | [53.908]
[53.97] | 2301700
2301700 | 4156700
4155000 | 22 | 6
4 | E2
E2 | $ \begin{array}{c c} 1.4(+7) \\ 1.4(+7) \end{array} $ | 0.022
0.015 | D
D | 1, <i>ls</i>
1, <i>ls</i> |
| 36. | 4p-4f | <sup>2</sup> P° – <sup>2</sup> F° | | | | | | | | | | |
| | | | [437.3]
[417.0]
[439.0] | 2438400
2426400
2438400 | 2667100
2666200
2666200 | 4
2
4 | 8
6
6 | E2
E2
E2 | $2.36(+4) \\ 2.33(+4) \\ 5200$ | 1.80
1.05
0.300 | C
C
C- | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |
| 37. | 4 <i>p</i> -5 <i>f</i> | <sup>2</sup> P° – <sup>2</sup> F° | | | | | | | | | | |
| | | | [96.993]
[95.914]
[97.031] | 2438400
2426400
2438400 | 3469400
3469000
3469000 | 4
2
4 | 8
6
6 | E2
E2
E2 | 5.8(+7)
4.76(+7)
1.28(+7) | 2.37
1.38
0.394 | C
C
C- | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |
| 38. | 4 <i>p-6f</i> | <sup>2</sup> P° – <sup>2</sup> F° | | | | | | | | | | |
| | | | [68.134]
[67.595]
[68.148] | 2438400
2426400
2438400 | 3906100
3905800
3905800 | 4
2
4 | 8
6
6 | E2
E2
E2 | $2.33(+7) \\ 1.9(+7) \\ 5.1(+6)$ | 0.163
0.095
0.027 | C
D
E | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |
| 39 . | 4p-7f | <sup>2</sup> P° – <sup>2</sup> F° | | | | | | | | | | |
| | | | [57.780]
[57.389] | 2438400
2426400 | 4169100
4168900 | 4
2 | 8
6 | E2
E2 | 1.0(+7)
8.5(+6) | 0.032
0.019 | D
D | 1, <i>ls</i>
1, <i>ls</i> |
| 40. | 4 p- 8f | <sup>2</sup> P° – <sup>2</sup> F° | | | | | | | | | | |
| | | | [52.604] | 2438400 | 4339400 | 4 | 8 | E2 | 5.2(+6) | 0.010 | D | 1, <i>ls</i> |
| 41. | 4f-5p | <sup>2</sup> F° – <sup>2</sup> P° | | | | | | | | | | |
| | | | [144.7]
[145.7]
[144.5] | $\frac{2667100}{2666200}\\ 2666200$ | 3358100
3352400
3358100 | 8
6
6 | 4
2
4 | E2
E2
E2 | $\begin{array}{c} 1.87(+6) \\ 2.11(+6) \\ 3.1(+5) \end{array}$ | 0.282
0.165
0.047 | C
C
D | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |
| 42. | 4 <i>f</i> -6 <i>p</i> | <sup>2</sup> F° – <sup>2</sup> P° | | | | | | | | | | |
| | | | [85.027] | 2667100 | 3843200 | 8 | 4 | E2 | 1.1(+6) | 0.012 | D | 1, <i>ls</i> |
| 43. | 5p-5f | <sup>2</sup> P° – <sup>2</sup> F° | | | | | | | | | | |
| | | | [898.5]
[857.6]
[901.7] | 3358100
3352400
3358100 | 3469400
3469000
3469000 | 4
2
4 | 8
6
6 | E2
E2
E2 | 6200
6000
1350 | 17.2
10.0
2.87 | C
C
C- | 1, <i>ls</i>
1, <i>ls</i>
1, <i>ls</i> |

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Ni xviii: Forbidden transitions - Continued

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| No. | Transition<br>Array    | Multiplet                         | λ<br>(Å)                      | $E_i$<br>(cm ⁻¹ )  | $E_{k}$ (cm ⁻¹ )   | <b>g</b> i  | gx          | Type of<br>transition | $egin{array}{c} A_{ki} \ (\mathbf{s}^{-1}) \end{array}$ | S<br>(at. u.)           | Accu-<br>racy  | Source                                       |
|-----|------------------------|-----------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------|-------------|-----------------------|---------------------------------------------------------|-------------------------|----------------|----------------------------------------------|
| 44. | 5p-6f                  | ² P° – ² F° |                               |                               |                               |             |             |                       |                                                         |                         |                |                                              |
|     |                        |                                   | [182.5]<br>[180.7]<br>[182.6] | 3358100<br>3352400<br>3358100 | 3906100<br>3905800<br>3905800 | 4<br>2<br>4 | 8<br>6<br>6 | E2<br>E2<br>E2        | $1.06(+7) \\ 8.7(+6) \\ 2.34(+6)$                       | 10.2<br>6.0<br>1.70     | C<br>C<br>C–   | 1, <i>ls</i><br>1, <i>ls</i><br>1, <i>ls</i> |
| 45. | 5p-7f                  | ² P° – ² F° |                               |                               |                               |             |             |                       |                                                         |                         |                |                                              |
|     |                        |                                   | [123.3]<br>[122.5]<br>[123.3] | 3358100<br>3352400<br>3358100 | 4169100<br>4168900<br>4168900 | 4<br>2<br>4 | 8<br>6<br>6 | E2<br>E2<br>E2        | 6.3(+6)<br>5.0(+6)<br>1.39(+6)                          | 0.85<br>0.493<br>0.141  | C<br>C<br>C-   | 1, <i>ls</i><br>1, <i>ls</i><br>1, <i>ls</i> |
| 46. | 5p-8f                  | ² P° – ² F° |                               |                               |                               |             |             |                       |                                                         |                         |                |                                              |
|     |                        |                                   | [101.9]<br>[101]<br>[102]     | 3358100<br>3352400<br>3358100 | 4339400<br>4340000<br>4340000 | 4<br>2<br>4 | 8<br>6<br>6 | E2<br>E2<br>E2        | 3.61(+6)<br>2.93(+6)<br>8.1(+5)                         | 0.189<br>0.110<br>0.032 | C<br>C<br>D    | 1, <i>ls</i><br>1, <i>ls</i><br>1, <i>ls</i> |
| 47. | 5f-6p                  | ² F° – ² P° |                               |                               |                               |             |             |                       |                                                         |                         |                |                                              |
|     |                        |                                   | [267.5]<br>[270.0]<br>[267.2] | 3469400<br>3469000<br>3469000 | 3843200<br>3839400<br>3843200 | 8<br>6<br>6 | 4<br>2<br>4 | E2<br>E2<br>E2        | $9.2(+5) \\ 1.02(+6) \\ 1.54(+5)$                       | 2.99<br>1.75<br>0.499   | C<br>C<br>C-   | 1, <i>ls</i><br>1, <i>ls</i><br>1, <i>ls</i> |
| 48. | 6 <i>p</i> -6 <i>f</i> | ² P° – ² F° |                               |                               |                               |             |             |                       | 1                                                       |                         |                |                                              |
|     |                        |                                   | [1590]<br>[1510]<br>[1600]    | 3843200<br>3839400<br>3843200 | 3906100<br>3905800<br>3905800 | 4<br>2<br>4 | 8<br>6<br>6 | E2<br>E2<br>E2        | 1900<br>1900<br>400                                     | 91<br>53<br>15          | C-<br>C-<br>D+ | 1, <i>ls</i><br>1, <i>ls</i><br>1, <i>ls</i> |
| 49. | 6p-7f                  | ² P° – ² F° |                               |                               |                               |             |             |                       |                                                         |                         |                |                                              |
|     |                        |                                   | [306.8]<br>[303.5]<br>[307.0] | 3843200<br>3839400<br>3843200 | 4169100<br>4168900<br>4168900 | 4<br>2<br>4 | 8<br>6<br>6 | E2<br>E2<br>E2        | 2.63(+6) 2.16(+6) $5.9(+5)$                             | 34.1<br>19.9<br>5.7     | C<br>C<br>C–   | 1, <i>ls</i><br>1, <i>ls</i><br>1, <i>ls</i> |
| 50. | 6p-8f                  | ² P° - ² F° |                               |                               |                               |             |             |                       |                                                         |                         |                |                                              |
|     |                        |                                   | [201.5]<br>[200]<br>[201]     | 3843200<br>3839400<br>3843200 | 4339400<br>4340000<br>4340000 | 4<br>2<br>4 | 8<br>6<br>6 | E2<br>E2<br>E2        | $1.90(+6) \\ 1.54(+6) \\ 4.3(+5)$                       | 3.01<br>1.76<br>0.50    | C<br>C-<br>D+  | 1, <i>ls</i><br>1, <i>ls</i><br>1, <i>ls</i> |

### Ni xix

Ne Isoelectronic Sequence

Ground State:  $1s^22s^22p^{6} S_0$ 

Ionization Energy:  $1541 \text{ eV} = 12430000 \text{ cm}^{-1}$ 

#### Allowed Transitions

| Lì | st | of | tabul | ated | lines |
|----|----|----|-------|------|-------|
|    |    |    |       |      |       |

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|
| 9.140          | 19  | 13 779         | 14  | 45.2           | 33  | 227            | 28  |
| 9.153          | 11  | 14.043         | 13  | 45.3           | 33  | 237            | 28  |
| 9.977          | 22  | 38.8           | 27  | 46.0           | 39  | 242            | 28  |
| 10.110         | 21  | 38.9           | 26  | 46.4           | 34  | 256            | 29  |
| 10.157         | 20  | 39.1           | 26  | 77.32          | 2   | 257            | 30  |
| 10.283         | 19  | 39.3           | 26  | 79.81          | 1   | 258            | 32  |
| 10.433         | 18  | 40.5           | 36  | 80             | 5   | 305            | 24  |
| 11.539         | 10  | 40.7           | 36  | 82             | 6   | 348            | 31  |
| 11.599         | 9   | 41.132         | 37  | 86.36          | 4   | 359            | 23  |
| 12.435         | 17  | 42.3           | 38  | 90             | 7   | 736            | 25  |
| 12.656         | 16  | 42.6           | 35  | 91             | 7,8 |                |     |
| 12.812         | 15  | 43.4           | 40  | 91.02          | 3   |                |     |

A-values for numerous transitions involving an electron jump of the type 2s-np (n=2-4), 2p-ns, 2p-nd, 3s-np, 3p-nd (n=3,4), or 3p-4s were calculated by Loulergue and Nussbaumer¹ using scaled Thomas-Fermi wavefunctions. The following configurations were included in their basis:  $2s^22p^6$ ,  $2s^22p^5nl$ , and  $2s2p^6nl$  (for n=3: l=s, p, d; for n=4: l=s, p, d, f). Their results are quoted here, but, in cases where better wavelength data were available, their transition probabilities were first converted to line strengths, which were then reconverted to f- and A-values by using the more accurate wavelengths. Data for resonance lines were not modified, as the calculated wavelengths of Ref. 1 for these lines are fairly accurate.

Transition probabilities for a few lines for which Loulergue and Nussbaumer did not report results were taken from the work of Pokleba and Safronova,² who used wavefunctions calculated by a charge-expansion perturbation theory approach with allowance for mixing of configurations in which a single 2s or 2p electron is excited to an n = 3 orbital but with no inclusion of configurations in which an electron occupies the n = 4 shell.

Transitions involving levels of the  $2p^{5}3p$  and  $2p^{5}3d$ 

configurations which are indicated by Jupen and Litzen³ to be of low to moderate purity in LS coupling in Fe XVII are excluded here, as are very weak lines. Transitions involving the corresponding levels in the  $2p^54l$  configurations are excluded as well, as no percentage composition data were available for these levels. The pattern of levels within the  $2s2p^63d$  configuration resulting from the calculations of Loulergue and Nussbaumer is entirely different from that determined by Vainshtein and Safronova,⁴ whose energy levels were apparently used by Pokleba and Safronova in their transition probability calculations. We have thus excluded transitions out of these levels from our tabulation.

#### References

- ¹M. Loulergue and H. Nussbaumer, Astron. Astrophys. **45**, 125 (1975). ²A. K. Pokleba and U. I. Safronova, Preprint No. 11, Akad. Nauk
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C. Jupen and C. Enzen, Thys. Set. 30, 112 (1964).

⁴L. A. Vainshtein and U. I. Safronova, Spektroskopicheskie Konstanty Atomov, 5-122 (Ed. V. B. Belyanin, Akad. Nauk SSSR, Ot. Ob. Fiz. Astron., Nauch. Sov. Spektrosk., Moscow, 1977).

## Ni XIX: Allowed transitions

| No. | Transition<br>Array                                                      | Multiplet                                                                       | λ<br>(Å) | $\frac{E_i}{(\mathrm{cm}^{-1})}$ | $E_k$<br>(cm ⁻¹ ) | <b>g</b> i | g. | $A_{ki}$<br>(10 ⁸ s ⁻¹ ) | fik    | S<br>(at. u.) | log gf | Accu-<br>racy | Source |
|-----|--------------------------------------------------------------------------|---------------------------------------------------------------------------------|----------|----------------------------------|------------------------------|------------|----|------------------------------------------------|--------|---------------|--------|---------------|--------|
| 1.  | 2s ² 2p ⁵ ( ² P _{3/2} )3s-     | ( ³ / ₂ , ¹ / ₂ )° - ³ S |          |                                  |                              |            |    |                                                |        |               |        |               |        |
|     | 2s2p ⁶ 3s                                                     |                                                                                 |          |                                  |                              |            |    |                                                |        |               |        |               |        |
|     |                                                                          |                                                                                 | [79.81]  | 7103800                          | 8357000                      | 5          | 3  | 1200                                           | 0.069  | 0.090         | -0.47  | D             | 1      |
| 2.  |                                                                          | ( ³ / ₂ , ¹ / ₂ )° - ¹ S |          |                                  |                              |            |    |                                                | 7      |               |        |               |        |
|     |                                                                          |                                                                                 | 77.32    | 7121000                          | 8415000                      | 3          | 1  | 830                                            | 0.025  | 0.019         | -1.13  | D             | 1      |
| 3.  | $2s^22p^5(^2\mathbf{P}_{1/2}^{\circ})3s - 2s^2p^63s$                     | ( ¹ / ₂ , ¹ / ₂ )° - ³ S |          |                                  |                              |            |    |                                                |        |               |        |               |        |
|     |                                                                          |                                                                                 | 91.02    | 7257400                          | 8357000                      | 3          | 3  | 290                                            | 0.036  | 0.032         | -0.97  | D             | 1      |
| 4.  |                                                                          | ( ¹ / ₂ , ¹ / ₂ )° - ¹ S |          |                                  |                              |            |    |                                                |        |               |        |               |        |
|     |                                                                          |                                                                                 | 86.36    | 7257400                          | 8415000                      | 3          | 1  | 440                                            | 0.016  | 0.014         | -1.31  | D             | 1      |
| 5.  | 2s ² 2p ⁵ 3p -<br>2s2p ⁶ 3p             | ³ S – ³ P°                                                |          |                                  |                              |            |    | -                                              |        |               |        |               |        |
|     |                                                                          |                                                                                 | [80]     |                                  |                              | 3          | 3  | 170                                            | 0.016  | 0.013         | -1.31  | E             | 1      |
|     |                                                                          |                                                                                 | [80]     |                                  |                              | 3          |    | 670                                            | 0.022  | 0.017         | -1.19  | D             |        |
| 6.  |                                                                          | ³ D – ³ P [•]                                    |          |                                  |                              |            |    |                                                |        |               |        | -             |        |
|     |                                                                          |                                                                                 | [82]     |                                  |                              | 7          | 5  | 960                                            | 0.069  | 0.13          | -0.32  | D             |        |
| 7.  | 2s²2p°4p-<br>2s2p ⁶ 4p                                        | °S - °P°                                                                        |          |                                  |                              |            |    |                                                |        |               |        |               |        |
|     |                                                                          |                                                                                 | [90]     |                                  |                              | 3          | 3  | 120                                            | 0.015  | 0.013         | -1.36  | Е             | 1      |
|     |                                                                          | <b>1</b>                                                                        | [91]     |                                  |                              | 3          | 1  | 580                                            | 0.024  | 0.022         | -1.14  | Е             | 1      |
| 8.  |                                                                          | °D - °P°                                                                        |          |                                  |                              |            |    |                                                |        |               |        |               |        |
|     |                                                                          |                                                                                 | [91]     |                                  |                              | 7          | 5  | 620                                            | 0.055  | 0.12          | -0.41  | Е             | 1      |
| 9.  | 2s ² 2p°-2s2p°3p                                              | 'S - 'P'                                                                        |          |                                  |                              |            |    | 2000                                           | 0.000  | 0.0015        | 1.0    |               |        |
|     |                                                                          | 10 100                                                                          | 11.599   | 0                                | 8621400                      |            | 3  | 6300                                           | 0.038  | 0.0015        | -1.42  | E             | 1      |
| 10. |                                                                          | ¹ S - ¹ P [*]                                    | 11.539   | U                                | 8666300                      |            | 3  | 4.8(+4)*                                       | 0.29   | 0.011         |        |               | 1      |
| 11. | 2s ⁻ 2p°-2s2p°4p                                              | -S - "P"                                                                        | 0.159    |                                  | 10020000                     | 1          | 9  | 5900                                           | 0.020  | 59( 1)        | 171    | F             | 1      |
| 10  |                                                                          |                                                                                 | 9.100    | 0                                | 10930000                     |            | 3  | 21(14)                                         | 0.020  | 0.0035        | -0.93  |               | 1      |
| 12. | 0_6                                                                      | -S - P                                                                          | 9.140    |                                  | 10540000                     |            | J  | 0.1(+4)                                        | 0.12   | 0.0000        | -0.50  |               | 1      |
| 13. | $2p^{5}-2p^{5}(^{2}\mathbf{P}_{3/2}^{*})3s$                              | -3 - (72,72)                                                                    |          |                                  |                              |            |    |                                                |        |               |        |               |        |
|     |                                                                          |                                                                                 | 14.043   | 0                                | 7121000                      | 1          | 3  | 1.31(+4)                                       | 0.116  | 0.0054        | -0.93  | C-            | 1      |
| 14. | 2p ⁶ -<br>2p ⁵ ( ² P _{1/2} )3s | ¹ S - ( ¹ / ₂ , ¹ / ₂ )* |          |                                  |                              |            |    |                                                |        |               |        |               |        |
|     |                                                                          |                                                                                 | 13.779   | 0                                | 7257400                      | 1          | 3  | 1.23(+4)                                       | 0.105  | 0.00476       | -0.98  | C-            | 1      |
| 15. | 2p ⁶ -2p ⁵ 3d                                      | ¹ S - ^{\$} P*                                               |          |                                  |                              |            |    |                                                |        |               |        |               |        |
|     |                                                                          |                                                                                 | 12.812   | 0                                | 7805200                      | 1          | 3  | 1100                                           | 0.0081 | 3.4(4)        | -2.09  | Е             | 1      |

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Ni XIX: Allowed transitions - Continued

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|-----|---------------------------------------------------------------|---------------------------------------------------------------------------------|----------------|---------------------------------------------|---------------------------|------------|--------|------------------------------------------------|----------------|---------------|----------------|---------------|--------|
| No. | Transition<br>Array                                           | Multiplet                                                                       | λ<br>(Å)       | <i>E_i</i><br>(cm ⁻¹ ) | $E_k$ (cm ⁻¹ ) | <b>g</b> i | ₿k     | $A_{ki}$<br>(10 ⁸ s ⁻¹ ) | f ik           | S<br>(at. u.) | log gf         | Accu-<br>racy | Source |
|     |                                                               |                                                                                 |                |                                             |                           |            |        |                                                |                | -             |                |               |        |
| 16. |                                                               | ¹ S – ³ D*                                                |                |                                             |                           |            |        |                                                |                |               |                |               |        |
|     |                                                               |                                                                                 | 12.656         | 0                                           | 7901400                   | 1          | 3      | 1.0(+5)                                        | 0.72           | 0.030         | -0.14          | D             | 1      |
| 17. |                                                               | ¹ S - ¹ P°                                                | 12.435         | 0                                           | 8041800                   | 1          | 3      | 3.66(+5)                                       | 2.55           | 0.104         | 0.406          | C–            | 1      |
| 18. | $2p^{6}$<br>$2p^{5}(^{2}\mathbf{P}^{s}_{3/2})4s$              | ¹ S - ( ³ / ₂ , ¹ / ₂ )° |                |                                             |                           |            |        |                                                |                |               |                |               |        |
|     |                                                               |                                                                                 | 10.433         | 0                                           | 9585000                   | 1          | 3      | 5100                                           | 0.025          | 8.6(-4)       | -1.60          | D             | 1      |
| 19. | $2p^{6}-2p^{5}(^{2}\mathbf{P}^{\bullet}_{1/2})4s$             | ¹ S - ( ¹ / ₂ , ¹ / ₂ )° |                |                                             |                           |            |        |                                                |                |               |                |               |        |
|     |                                                               |                                                                                 | 10.283         | 0                                           | 9724800                   | 1          | 3      | 4700                                           | 0.022          | 7.6(-4)       | -1.65          | D             | 1      |
| 20. | $2p^{6}-2p^{5}4d$                                             | ¹ S - ³ P°                                                |                |                                             |                           |            |        |                                                |                |               |                |               |        |
|     |                                                               |                                                                                 | 10.157         | 0                                           | 9845400                   | 1          | 3      | 700                                            | 0.0032         | 1.1(-4)       | -2.49          | Е             | 1      |
| 21. |                                                               | ¹ S - ³ D°                                                |                |                                             |                           |            |        |                                                |                |               |                |               |        |
|     |                                                               |                                                                                 | 10.110         | 0                                           | 9891200                   | 1          | 3      | 9.4(+4)                                        | 0.43           | 0.014         | -0.36          | D             | 1      |
| 22. |                                                               | ¹ S - ¹ P°                                                | 9.977          | 0                                           | 10020000                  | 1          | 3      | 1.1(+5)                                        | 0.49           | 0.016         | -0.31          | D             | 1      |
| 23. | 2p ⁵ (²P _{3/2} )3s−<br>2p ⁵ 3p | ( ³ / ₂ , ¹ / ₂ )° - ³ S |                |                                             |                           |            |        |                                                |                |               |                |               |        |
|     |                                                               |                                                                                 | [359]          |                                             |                           | 5          | 3      | 44                                             | 0.051          | 0.30          | -0.60          | D             | 1      |
| 24. |                                                               | ( ³ / ₂ , ¹ / ₂ )° - ³ D |                |                                             |                           |            |        |                                                |                |               |                |               |        |
|     |                                                               |                                                                                 | [305]          |                                             |                           | 5          | 7      | 80                                             | 0.16           | 0.78          | -0.11          | D             | 1      |
| 25. | $2p^{5}(^{2}\mathbf{P}_{1/2}^{\circ})3s - 2p^{5}3p$           | ( ¹ / ₂ , ¹ / ₂ )° - ³ S |                |                                             |                           |            |        |                                                |                |               |                |               |        |
|     |                                                               |                                                                                 | [736]          |                                             |                           | 1          | 3      | 0.060                                          | 0.0015         | 0.0035        | -2.84          | Е             | 2      |
| 26. | 2s2p ⁶ 3s-<br>2s2p ⁶ 4p                 | ³ S - ³ P°                                                | 39.1           |                                             |                           | 3          | 9      | 3800                                           | 0.26           | 0.10          | -0.11          | D             | 1      |
|     |                                                               |                                                                                 | [39.1]         | 8957000                                     | 10020000                  | 3          | 5      | 3900                                           | 0.15           | 0.058         | -0.35          | D             | 1      |
|     |                                                               |                                                                                 | [39.3]         | 0001000                                     | 10550000                  | 3          | 1      | 4300                                           | 0.033          | 0.013         | -1.00          | D             | 1      |
| 27. |                                                               | ³ S - ¹ P°                                                |                |                                             |                           |            |        |                                                |                |               |                |               |        |
|     |                                                               |                                                                                 | [38.8]         | 8357000                                     | 10940000                  | 3          | 3      | 710                                            | 0.016          | 0.0061        | -1.32          | Е             | 1      |
| 28. | 2p ⁵ 3p-2p ⁵ 3d                         | ³ S – ³ P°                                                | 238            | 4                                           |                           | 3          | 9      | 78                                             | 0.20           | 0.47          | -0.22          | Е             | 1      |
|     |                                                               |                                                                                 | [227]<br>[237] |                                             |                           | 3<br>3     | 5<br>3 | 59<br>110                                      | 0.076<br>0.090 | 0.17<br>0.21  | -0.64<br>-0.57 | E<br>D        | 1      |
|     |                                                               |                                                                                 | [242]          |                                             |                           | 3          | 1      | 130                                            | 0.038          | 0.091         | -0.94          | D             | 1      |
| 29. |                                                               | ³ D - ³ P°                                                |                |                                             |                           |            |        |                                                |                |               |                |               |        |
|     |                                                               |                                                                                 | [256]          |                                             |                           | 7          | 5      | 5.5                                            | 0.0039         | 0.023         | - 1.57         | Е             | 2      |

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| Ni xix: | Allowed | transitions — | Continued |
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| No. | Transition<br>Array                                                        | Multiplet                                                                       | λ<br>(Å)                   | <i>Ei</i><br>(cm ⁻¹ ) | $E_k$<br>(cm ⁻¹ ) | gi          | g⊧          | $A_{ki}$<br>(10 ⁸ s ⁻¹ ) | fu                    | S<br>(at. u.)           | log gf                  | Accu-<br>racy | Source      |
|-----|----------------------------------------------------------------------------|---------------------------------------------------------------------------------|----------------------------|----------------------------------|------------------------------|-------------|-------------|------------------------------------------------|-----------------------|-------------------------|-------------------------|---------------|-------------|
| 30. |                                                                            | ³ D – ³ F°                                                |                            |                                  |                              |             |             |                                                |                       |                         |                         |               |             |
|     |                                                                            |                                                                                 | [257]                      |                                  |                              | 7           | 9           | 120                                            | 0.16                  | 0.93                    | 0.04                    | D             | 1           |
| 31. |                                                                            | ⁸ P – ⁸ P°                                                |                            |                                  |                              |             |             |                                                |                       |                         |                         |               |             |
|     |                                                                            |                                                                                 | [348]                      |                                  |                              | 1           | 3           | 1.3                                            | 0.0071                | 0.0081                  | -2.15                   | Е             | 2           |
| 32. |                                                                            | ⁸ P – ⁸ D°                                                |                            |                                  |                              |             |             |                                                |                       |                         |                         |               |             |
| 33. | 2p ⁵ 3p-                                                        | ³ S - ( ³ / ₂ , ¹ / ₂ )° | [258]                      |                                  |                              | 1           | 3           | 54                                             | 0.16                  | 0.14                    | -0.79                   | D             | 2           |
|     | 2p (~P _{3/2} /4s                                                  |                                                                                 | [45.3]<br>[45.2]           |                                  |                              | 3<br>3      | 5<br>3      | 1000<br>45                                     | 0.051<br>0.0014       | 0.023<br>6.2(-4)        | $-0.81 \\ -2.38$        | D<br>E        | 1           |
| 34. |                                                                            | ³ D - ( ³ / ₂ , ¹ / ₂ )° |                            |                                  |                              |             |             |                                                |                       |                         |                         |               |             |
|     |                                                                            |                                                                                 | [46.4]                     |                                  |                              | 7           | 5           | 2600                                           | 0.060                 | 0.064                   | -0.38                   | D             | 1           |
| 35. | 2p ⁵ 3p-<br>2p ⁵ ( ² P _{1/2} )4s | ³ S - ( ¹ / ₂ , ¹ / ₂ )° |                            |                                  |                              |             |             |                                                |                       |                         |                         |               |             |
|     |                                                                            |                                                                                 | [42.6]<br>[42.6]           |                                  |                              | 3<br>3      | 3<br>1      | 72<br>93                                       | 0.0020<br>8.4(-4)     | 8.2(-4)<br>3.5(-4)      | -2.23<br>-2.60          | E<br>E        | 1<br>1      |
| 36. | 2p ⁵ 3p-2p ⁵ 4d                                      | ³ S - ³ P°                                                | 40.6                       |                                  |                              | 3           | 9           | 4700                                           | 0.35                  | 0.14                    | 0.02                    | Е             | 1           |
|     |                                                                            |                                                                                 | [40.5]<br>[40.7]<br>[40.7] |                                  |                              | 3<br>3<br>3 | 5<br>3<br>1 | 3000<br>6400<br>8400                           | 0.12<br>0.16<br>0.070 | 0.049<br>0.064<br>0.028 | -0.43<br>-0.32<br>-0.68 | E<br>D<br>E   | 1<br>1<br>1 |
| 37. |                                                                            | ³ D − ³ F°                                                |                            |                                  |                              |             |             |                                                |                       |                         |                         |               |             |
|     |                                                                            |                                                                                 | 41.132                     |                                  |                              | 7           | 9           | 9400                                           | 0.31                  | 0.29                    | 0.33                    | D             | 1           |
| 38. |                                                                            | ³ P - ³ D°                                                |                            |                                  |                              |             |             |                                                |                       |                         |                         |               |             |
|     |                                                                            |                                                                                 | [42.3]                     |                                  |                              | 1           | 3           | 3800                                           | 0.31                  | 0.043                   | -0.51                   | D             | 1           |
| 39. |                                                                            | ¹ S – ³ D°                                                |                            |                                  |                              |             |             |                                                |                       |                         |                         | _             |             |
|     |                                                                            |                                                                                 | [46.0]                     |                                  |                              | 1           | 3           | 1100                                           | 0.10                  | 0.016                   | -0.98                   | E             | 1           |
| 40. |                                                                            | 'S - 'P"                                                                        | [43.4]                     |                                  |                              | 1           | 3           | 4000                                           | 0.34                  | 0.048                   | -0.47                   | D             | 1           |

## Ni xix

### Forbidden Transitions

The A-value for the single magnetic-dipole transition tabulated here is the result of the Hartree-Fock-Relativistic (HFR) calculations of Cowan.¹ The wavelength is the result of these same calculations and may be somewhat uncertain, as the energy of the J=0 level has not been determined experimentally. For the magnetic quadrupole resonance transition to the J=2 level of the  $2p^{5}3s$  configuration, we quote the A-value determined by Loulergue and Nussbaumer² using scaled Thomas-Fermi

wavefunctions with fairly extensive allowance for configuration mixing.

#### References

¹R. D. Cowan, Los Alamos Scientific Laboratory Informal Report LA-6679-MS (Jan. 1977).

²M. Loulergue and H. Nussbaumer, Astron. Astrophys. 45, 125 (1975).

| Ni | XIX: | Forbidden | transitions |
|----|------|-----------|-------------|
|    |      |           |             |

| No. | Transition<br>Array                                                                                                                    | Multiplet                                                                                                                       | λ<br>(Å) | $E_i$<br>(cm ⁻¹ ) | <i>E</i> _k<br>(cm ⁻¹ ) | <b>g</b> i | g. | Type of<br>transition | A _{ki}<br>(s ⁻¹ ) | S<br>(at. u.) | Accu-<br>racy | Source |
|-----|----------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------|----------|------------------------------|----------------------------------------------|------------|----|-----------------------|---------------------------------------|---------------|---------------|--------|
| 1.  | 2p ⁵ ( ² P [*] _{3/2} )3s -<br>2p ⁵ ( ² P [*] _{1/2} )3s | ( ³ / ₂ , ¹ / ₂ )* - ( ¹ / ₂ , ¹ / ₂ )* |          |                              |                                              |            |    |                       |                                       |               |               |        |
| 2.  | 2p ⁶ -<br>2p ⁵ ( ² P [*] _{3/2} )3s                                                  | ¹ S - ( ³ / ₂ , ¹ / ₂ )°                                                 | [780]    |                              |                                              | 3          | 1  | <b>M</b> 1            | 4.8(+4)*                              | 0.84          | D+            | 1      |
|     |                                                                                                                                        |                                                                                                                                 | 14.077   | 0                            | 7103800                                      | 1          | 5  | M2                    | 4.2(+5)                               | 0.18          | D+            | 2      |

"The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

### Ni xx

F Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^{5} {}^{2}P_{3/2}^{\circ}$ 

Ionization Energy:  $1648 \text{ eV} = 13290000 \text{ cm}^{-1}$ 

#### Allowed Transitions

Oscillator strengths for lines of the multiplet  $2s^22p^{5}{}^{2}P^{\circ} - 2s^2p^{6}{}^{2}S$  are the results of the Dirac-Fock calculations of Cheng et al.,1 which included a perturbative treatment of the Breit interaction and the Lamb shift.

For lines of the arrays  $2p^5-2p^43s$  and  $2p^5-2p^43d$ , we quote the f-values calculated by Fawcett² using Cowan's Hartree-Fock-Relativistic (HFR) method and incorporating scaling of energy parameters on the basis of a least-squares fit to observed energies. Fawcett's calculations included fairly extensive allowance for configuration mixing in both odd- and even-parity states. Transitions involving levels which are indicated by Fawcett to be of low to moderate purity in LS coupling in neighboring fluorinelike ions are excluded from this compilation, as are lines characterized by very small fvalues.

The ratio of A-values for the two resonance lines out of the  $2s2p^{6} {}^{2}S_{1/2}$  level as given in Ref. 1 is in reasonably good agreement with the result of Stratton et al.³ derived from relative-intensity measurements.

#### References

- ¹K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, At. Data Nucl. Data Tables 24, 111 (1979).
- ²B. C. Fawcett, At. Data Nucl. Data Tables 31, 495 (1984).
- ³B. C. Stratton, H. W. Moos, S. Suckewer, U. Feldman, J. F. Seely, and A. K. Bhatia, Phys. Rev. A 31, 2534 (1985).
| Transition<br>Array                                  | Multiplet                        | λ<br>(Å)                     | $E_i$<br>(cm ⁻¹ ) | $E_{k}$ (cm ⁻¹ )   | gi          | g.          | $\begin{array}{c} A_{ki} \\ (10^8 \ \mathrm{s}^{-1}) \end{array}$ | fih                      | S<br>(at. u.)              | log gf                  | Accu-<br>racy | Source      |
|------------------------------------------------------|----------------------------------|------------------------------|------------------------------|-------------------------------|-------------|-------------|-------------------------------------------------------------------|--------------------------|----------------------------|-------------------------|---------------|-------------|
| 2s ² 2p ⁵ -2s2p ⁶   | ² P° – ² S | 86.66                        | 47990                        | 1202000                       | 6           | 2           | 1450                                                              | 0.0544                   | 0.0932                     | -0.486                  | C+            | 1           |
|                                                      |                                  | 83.17<br>94.49               | 0<br>143960                  | 1202000<br>1202000            | 42          | 2<br>2      | 1100<br>368                                                       | 0.0571<br>0.0493         | 0.0625<br>0.0307           | -0.641<br>-1.006        | C+<br>C+      | 1           |
| 2p ⁵ -2p ⁴ ( ³ P)3s | ² P° – ⁴ P |                              |                              |                               |             |             |                                                                   |                          |                            |                         |               |             |
|                                                      |                                  | 13.309<br>13.135             | 0<br>0                       | 7513700<br>7613200            | 44          | 6<br>2      | 1700<br>6000                                                      | 0.0068<br>0.0078         | 0.0012<br>0.0013           | $-1.57 \\ -1.51$        | E<br>E        | 2<br>2      |
|                                                      | ² P° - ² P |                              |                              |                               |             |             |                                                                   |                          |                            |                         |               |             |
|                                                      |                                  | 13.282<br>13.032             | 143960<br>0                  | 7673400<br>7673400            | 2<br>4      | 2<br>2      | 2.0(+4) ^a<br>1.8(+4)                                   | 0.054<br>0.023           | 0.0047<br>0.0039           | 0.97<br>1.04            | D<br>D        | 2<br>2      |
| 2p ⁵ -2p ⁴ ( ¹ D)3s | ² P° – ² D | 13.003                       | 47990                        | 7738300                       | 6           | 10          | 1.8(+4)                                                           | 0.074                    | 0.019                      | -0.35                   | Е             | 2           |
|                                                      |                                  | 12.927<br>13.161<br>[12.916] | 0<br>143960<br>0             | 7735700<br>7742200<br>7742200 | 4<br>2<br>4 | 6<br>4<br>4 | $1.6(+4) \\ 1.9(+4) \\ 1000$                                      | 0.060<br>0.099<br>0.0025 | 0.010<br>0.0086<br>4.3(-4) | -0.62<br>-0.70<br>-2.00 | D<br>D<br>E   | 2<br>2<br>2 |
| 2p ⁵ -2p ⁴ ( ¹ S)3s | ² P° – ² S | 12.656                       | 47990                        | 7949200                       | 6           | 2           | 2.0(+4)                                                           | 0.016                    | 0.0041                     | -1.01                   | E             | 2           |
|                                                      |                                  | [12 580]                     | 0                            | 7949200                       | 4           | 2           | 2800                                                              | 0.0033                   | 55(-4)                     | _1.88                   | F             | 2           |

2 2

6 2

4 2

2 2

4

6 9600

1.7(+4)

2.6(+5)

2.3(+5)

3.4(+4)

7949200

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8421800

8421800

Ni xx: Allowed transitions

"The number in parentheses following the value indicates the power of ten by which this value has to be multiplied.

143960

47990

143960

0

# Ni xx

#### Forbidden Transitions

Line strengths for the magnetic dipole and electric quadrupole contributions to the transition between the two levels of the  $2p^5$  configuration are the results of the Dirac-Fock calculations of Cheng *et al.*¹ These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. The strength of the electric quadrupole transition as defined in Ref. 1 was multiplied by the factor 2/3 which is needed to bring this

12.812

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11.874

12.079

[11.61]

No.

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2.

3

4.

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6

7.

 $2p^{5}-2p^{4(1)}$ 

 $2p^{5}-2p^{4}(^{1}S)3d$ 

 ${}^{2}P^{\circ} - {}^{2}S$ 

 ${}^{2}P^{\circ} - {}^{2}D$ 

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value into conformance with the definition of quadrupole strengths used in the NBS tables.

0.0035

0.044

0.038

0.0059

0.0044

0.042

0.19

0.24

0.074

0.029

2

2

2

2

2

D

D

D

D

D

-1.08

0.05

-0.02

-0.83

-0.94

#### Reference

¹K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, At. Data Nucl. Data Tables 24, 111 (1979).

| No. | Transition<br>Array              | Multiplet                         | λ<br>(Å)    | $E_i$<br>(cm ⁻¹ ) | $E_{k}$ (cm ⁻¹ ) | <b>g</b> i | g⊾     | Type of<br>transition | A _{ki}<br>(8 ⁻¹ ) | <b>S</b><br>(at. u.) | Accu-<br>racy | Source |
|-----|----------------------------------|-----------------------------------|-------------|------------------------------|-----------------------------|------------|--------|-----------------------|---------------------------------------|----------------------|---------------|--------|
| 1.  | 2p ⁵ -2p ⁵ | ² P° – ² P° |             |                              |                             |            |        |                       |                                       |                      |               |        |
|     |                                  |                                   | 694.64<br>- | . ⁰               | 143960                      | 4<br>4     | 2<br>2 | M1<br>E2              | 5.35(+4)*<br>7.3                      | 1.33<br>0.0014       | B<br>D        | 1<br>1 |

# Ni xxi

O Isoelectronic Sequence

Ground State: 1s²2s²2p⁴ ³P₂

Ionization Energy:  $1756 \text{ eV} = 14160000 \text{ cm}^{-1}$ 

### Allowed Transitions

### List of tabulated lines

| Wavelength (Å) | No.   | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-------|----------------|-----|----------------|-----|----------------|-----|
| 11.13          | 25    | 11.67          | 18  | 12.502         | 14  | 95.85          | 1   |
| 11.23          | 26    | 11.72          | 18  | 12.533         | 13  | 96.79          | 1   |
| 11.239         | 21    | 12.079         | 15  | 12.592         | 10  | 97.13          | 6   |
| 11.28          | 24    | 12.166         | 15  | 12.656         | 10  | 100.23         | 1   |
| 11.318         | 19    | 12.179         | 12  | 12.8           | 9   | 103.40         | 8   |
| 11.48          | 20,27 | 12.208         | 11  | 69.62          | 2   | 109.29         | 1   |
| 11.517         | 23    | 12.209         | 16  | 74.431         | 2   | 109.44         | 3   |
| 11.539         | 18    | 12.245         | 15  | 76.45          | 2   | 120.33         | 3   |
| 11.54          | 18    | 12.345         | 16  | 78.28          | 7   | 139.05         | 5   |
| 11.596         | 22    | 12.370         | 12  | 81.69          | 4   |                |     |
| 11.65          | 17    | 12.454         | 10  | 88.81          | 1   |                |     |
| 11.66          | 17    | 12.472         | 11  | 93.91          | 1   |                |     |

The tabulated oscillator strengths for transitions of the arrays  $2s^22p^4-2s2p^5$  and  $2s2p^5-2p^6$  are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*¹ These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing was limited to the n=2 complex. The results should be quite accurate, except in the case of weak lines.

Transition probabilities for lines of the  $2s^22p^4-2s2p^5$ array were calculated by Froese Fischer and Saha² using the multiconfiguration Hartree-Fock (MCHF) method with Breit-Pauli corrections. Their basis set included many configurations outside the n=2 complex, but relativistic effects were not treated to the same degree as in Ref. 1. Line strengths derived from these two sources are in reasonably good agreement, particularly for the stronger transitions.

A few experimental data are available for this ion. Stratton *et al.*³ measured ratios of transition probabilities for two pairs of transitions, one of these pairs originating from the  $2s2p^{5} {}^{3}P_{2}^{\circ}$  level and the other from the  $2s2p^{5} {}^{3}P_{1}^{\circ}$ level. The former agrees very well with the theoretical data of Cheng et al.; the latter is nearly a factor of two larger than theory.

For lines of the arrays  $2p^4-2p^{3}3s$  and  $2p^4-2p^{3}3d$ , we quote the *f*-values calculated by Fawcett⁴ using Cowan's Hartree-Fock-Relativistic (HFR) method and incorporating scaling of energy parameters on the basis of a least-squares fit to observed energies. Fawcett's calculations included fairly extensive allowance for configuration mixing in both odd- and even-parity states. The weakest lines were not reported, and thus are not tabulated here. Transitions involving levels which are indicated by Fawcett to be of low to moderate purity in *LS* coupling in neighboring fluorinelike ions are excluded from this compilation.

- ¹K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, At. Data Nucl. Data Tables 24, 111 (1979).
- ²C. Froese Fischer and H. P. Saha, J. Phys. B 17, 943 (1984).
- ³B. C. Stratton, H. W. Moos, S. Suckewer, U. Feldman, J. F. Seely, and A. K. Bhatia, Phys. Rev. A **31**, 2534 (1985).
- ⁴B. C. Fawcett, At. Data Nucl. Data Tables 34, 215 (1986).

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Ni XXI: Allowed transitions

| No. | Transition<br>Array                                | Multiplet                                     | λ<br>(Å)       | $E_i$<br>(cm ⁻¹ ) | $E_k$ (cm ⁻¹ ) | <b>g</b> i | g. | $\begin{array}{c} A_{ki} \\ (10^8 \ {\rm s}^{-1}) \end{array}$ | f ik          | <i>S</i><br>(at. u.) | log gf | Accu-<br>racy | Source |
|-----|----------------------------------------------------|-----------------------------------------------|----------------|------------------------------|---------------------------|------------|----|----------------------------------------------------------------|---------------|----------------------|--------|---------------|--------|
|     |                                                    |                                               |                |                              |                           |            |    |                                                                |               |                      |        |               |        |
| 1.  | 2s ² 2p ⁴ -2s2p ⁵ | ³ P – ³ P°              | 96.671         | 53080                        | 1087520                   | 9          | 9  | 640                                                            | 0.089         | 0.256                | -0.095 | С             | 1      |
|     |                                                    |                                               | 95.85          | 0                            | 1043300                   | 5          | 5  | 460                                                            | 0.063         | 0.099                | -0.50  | С             | 1      |
|     |                                                    |                                               | 100.23         | 128290                       | 1126000                   | 3          | 3  | 143                                                            | 0.0215        | 0.0213               | -1.190 | C             | 1      |
|     |                                                    |                                               | 88.81<br>93.91 | 128290                       | 1126000                   | ) D<br>3   | 3  | 419                                                            | 0.0297        | 0.0434               | -0.83  | c             | 1      |
| ſ   |                                                    |                                               | 109.29         | 128290                       | 1043300                   | 3          | 5  | 115                                                            | 0.0344        | 0.0371               | -0.99  | č             | 1      |
|     |                                                    |                                               | 96.79          | 92840                        | 1126000                   | 1          | 3  | 190                                                            | 0.079         | 0.025                | -1.10  | С             | 1      |
| 2.  |                                                    | ³ P - ¹ P°              |                |                              |                           |            |    |                                                                |               |                      |        |               |        |
|     |                                                    |                                               | 69 62          | 0                            | 1436370                   | 5          | 3  | 170                                                            | 0.0076        | 0.0087               | _1 42  | E             | 1      |
|     |                                                    |                                               | 76.45          | 128290                       | 1436370                   | 3          | 3  | 18                                                             | 0.0016        | 0.0012               | -2.32  | E             | 1      |
|     |                                                    |                                               | [74.431]       | 92840                        | 1436370                   | 1          | 3  | 23                                                             | 0.0057        | 0.0014               | -2.24  | Е             | 1      |
|     |                                                    | 10 300                                        |                |                              |                           |            |    |                                                                |               |                      |        |               |        |
| 3.  |                                                    | ·D - °P                                       |                |                              |                           |            |    |                                                                |               |                      |        |               |        |
|     |                                                    |                                               | 120.33         | 212230                       | 1043300                   | 5          | 5  | 32                                                             | 0.0070        | 0.014                | -1.46  | Е             | 1      |
|     |                                                    |                                               | [109.44]       | 212230                       | 1126000                   | 5          | 3  | 1.0                                                            | $1.1(-4)^{a}$ | 2.0(-4)              | -3.26  | Е             | 1      |
| 4.  |                                                    | ¹ D - ¹ P°              | 81.69          | 212230                       | 1436370                   | 5          | 3  | 1700                                                           | 0.102         | 0.137                | -0.292 | с             | 1      |
| 5.  |                                                    | ¹ S – ³ P°              |                |                              |                           |            |    |                                                                |               |                      |        |               |        |
|     |                                                    |                                               | [139.05]       | 406820                       | 1126000                   | 1          | 3  | 11                                                             | 0.0093        | 0.0043               | -2.03  | Е             | 1      |
| 6.  |                                                    | ¹ S – ¹ P°              | 97.13          | 406820                       | 1436370                   | 1          | 3  | 120                                                            | 0.050         | 0.016                | -1.30  | с             | 1      |
| 7.  | $2s2p^{5}-2p^{6}$                                  | ³ P° – ¹ S              |                |                              |                           |            |    |                                                                |               |                      |        |               |        |
|     |                                                    |                                               | 78.28          | 1126000                      | 2403490                   | 3          | 1  | 230                                                            | 0.0070        | 0.0054               | -1.68  | Е             | 1      |
| 8.  |                                                    | ¹ P° – ¹ S              | 103.40         | 1436370                      | 2403490                   | 3          | 1  | 1800                                                           | 0.098         | 0.10                 | -0.53  | с             | 1      |
| 9.  | $2p^4 - 2p^3(4S^\circ)3s$                          | ${}^{3}P - {}^{5}S^{\circ}$                   |                |                              |                           |            |    |                                                                |               |                      |        |               |        |
|     |                                                    |                                               | [12.8]         |                              |                           | 5          | 5  | 2000                                                           | 0.0050        | 0.0011               | -1.60  | Е             | 4      |
| 10. |                                                    | ${}^{3}\mathbf{P} - {}^{3}\mathbf{S}^{\circ}$ | 12.537         | 53080                        | 8029700                   | 9          | 3  | 4.8(+4)                                                        | 0.038         | 0.014                | -0.47  | D             | 4      |
|     |                                                    |                                               | [12.454]       | 0                            | 8029700                   | 5          | 3  | 3.3(+4)                                                        | 0.046         | 0.0094               | -0.64  | D             | 4      |
|     |                                                    |                                               | 12.656         | 128290                       | 8029700                   | 3          | 3  | 6700                                                           | 0.016         | 0.0020               | -1.32  | D             | 4      |
|     |                                                    |                                               | 12.592         | 92840                        | 8029700                   | 1          | 3  | 7400                                                           | 0.053         | 0.0022               | -1.28  | D             | 4      |
| 11. | $2p^4 - 2p^3(^2D^\circ)3s$                         | ${}^{3}P - {}^{3}D^{\circ}$                   |                |                              |                           |            |    |                                                                |               |                      |        |               | 1      |
|     |                                                    |                                               | 10,000         |                              | 0101000                   | -          | -  | 1.414.0                                                        | 0.0149        | 0.0000               | 0.00   |               |        |
|     |                                                    |                                               | 12.208         | 128290                       | 8191300<br>8146300        | ) D<br>3   | 3  | 1.41(+4)<br>1.8(+4)                                            | 0.0442        | 0.0089               | -0.66  | D-            | 4      |
|     |                                                    |                                               | 12.112         | 120200                       | 0110000                   |            |    | 1.0(1.1/                                                       |               | 0.000                |        | -             | -      |
| 12. |                                                    | ${}^{3}P - {}^{1}D^{\circ}$                   |                |                              |                           |            |    |                                                                |               |                      |        |               |        |
|     |                                                    |                                               | [19 170]       | 0                            | 8210900                   | 5          | 5  | 2100                                                           | 0.0046        | 92(-4)               | -164   | Е             | 4      |
|     |                                                    |                                               | 12.370         | 128290                       | 8210900                   | 3          | 5  | 3700                                                           | 0.014         | 0.0017               | -1.34  | E             | 4      |
|     |                                                    |                                               |                |                              |                           |            |    |                                                                |               |                      |        |               |        |
| 13. | $2p^4 - 2p^3(^2D^\circ)3s$                         | ${}^{1}D - {}^{8}D^{\circ}$                   |                |                              |                           |            |    |                                                                |               |                      |        |               |        |
|     |                                                    |                                               | [12.533]       | 212230                       | 8191300                   | 5          | 7  | 1800                                                           | 0.0060        | 0.0012               | -1.52  | Е             | 4      |
|     |                                                    |                                               |                |                              |                           |            |    |                                                                |               |                      |        |               |        |

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Ni XXI: Allowed transitions - Continued

| No. | Transition<br>Array                                    | Multiplet                        | λ<br>(Å)                                | $E_i$<br>(cm ⁻¹ ) | $E_k$ (cm ⁻¹ )     | gi               | ₿k               | $A_{ki}$<br>(10 ⁸ s ⁻¹ ) | f ik                            | <i>S</i><br>(at. u.)                | log gf                                                         | Accu-<br>racy      | Source           |
|-----|--------------------------------------------------------|----------------------------------|-----------------------------------------|------------------------------|-------------------------------|------------------|------------------|------------------------------------------------|---------------------------------|-------------------------------------|----------------------------------------------------------------|--------------------|------------------|
| 15. | 2p ⁴ - 2p ³ ( ² P°)3s | ³ P - ³ P° |                                         |                              |                               |                  |                  |                                                |                                 |                                     |                                                                |                    |                  |
|     |                                                        |                                  | 12.245<br>12.079<br>[12.166]            | 128290<br>128290<br>92840    | 8294900<br>8407100<br>8312600 | 3<br>3<br>1      | 1<br>5<br>3      | 1.5(+4)<br>9100<br>1.0(+4)                     | 0.011<br>0.033<br>0.067         | 0.0013<br>0.0039<br>0.0027          | -1.48<br>-1.00<br>-1.17                                        | C<br>E<br>D-       | 444              |
| 16. |                                                        | ¹ D - ³ P° |                                         |                              |                               |                  |                  |                                                |                                 |                                     |                                                                |                    |                  |
|     |                                                        |                                  | 12.209<br>12.345                        | 212230<br>212230             | 8407100<br>8312600            | 5<br>5           | 5<br>3           | 8900<br>8000                                   | 0.020<br>0.011                  | 0.0040<br>0.0022                    | 1.00<br>1.26                                                   | E<br>E             | 4                |
| 17. | $2p^4 - 2p^3(^2P^\circ)3d$                             | ³P − ⁵D°                         |                                         |                              |                               |                  |                  |                                                |                                 |                                     |                                                                |                    |                  |
|     |                                                        |                                  | [11.66]<br>[11.65]                      |                              |                               | 5<br>5           | 5<br>3           | 5400<br>6700                                   | 0.011<br>0. 0082                | 0.0021<br>0.0016                    | -1.26<br>-1.39                                                 | E<br>E             | 4<br>4           |
| 18. | 2p ⁴ - 2p ^s ( ⁴ S°)3d | ³P − ³D°                         |                                         |                              |                               |                  |                  |                                                |                                 |                                     |                                                                |                    |                  |
|     |                                                        |                                  | 11.539<br>[11.67]<br>[11.72]<br>[11.54] | 0                            | 8666300                       | 5<br>1<br>3<br>5 | 7<br>3<br>3<br>3 | 1.2(+5)8.0(+4)2.3(+4)4200                      | 0.33<br>0.49<br>0.048<br>0.0050 | 0.063<br>0.019<br>0.0056<br>9.5(-4) | $\begin{array}{c} 0.22 \\ -0.31 \\ -0.84 \\ -1.60 \end{array}$ | D–<br>D<br>D<br>D– | 4<br>4<br>4<br>4 |
| 19. | $2p^4 - 2p^3(^2D^\circ)3d$                             | ³ P - ³ D° |                                         |                              |                               |                  |                  |                                                |                                 |                                     |                                                                |                    |                  |
|     |                                                        |                                  | 11.318                                  | 0                            | 8835500                       | 5                | 7                | 2.8(+5)                                        | 0.76                            | 0.14                                | 0.58                                                           | D                  | 4                |
| 20. |                                                        | ³ P - ³ P° |                                         |                              |                               |                  |                  |                                                |                                 |                                     |                                                                |                    |                  |
| 21. | $2p^4 - 2p^3(^2D^*)3d$                                 | ³ P – ¹ F° | [11.48]                                 |                              |                               | 3                | 1                | 1.1(+5)                                        | 0.075                           | 0.0085                              | 0.65                                                           | <b>D</b> -         | 4                |
|     |                                                        |                                  | 11.239                                  | 0                            | 8895000                       | 5                | 7                | 5.7(+4)                                        | 0.15                            | 0.028                               | -0.12                                                          | Е                  | 4                |
| 22. |                                                        | ¹ D - ³ D° |                                         |                              |                               |                  |                  |                                                |                                 |                                     |                                                                |                    |                  |
|     |                                                        |                                  | [11.596]                                | 212230                       | 8835500                       | 5                | 7                | 6400                                           | 0.018                           | 0.0034                              | -1.05                                                          | Е                  | 4                |
| 23. |                                                        | ¹ D - ¹ F" | 11.517                                  | 212230                       | 8895000                       | 5                | 7                | 1.4(+5)                                        | 0.39                            | 0.074                               | 0.29                                                           | D-                 | 4                |
| 24. | 2p* - 2p*(*P*)3a                                       | °P - °P                          | [11 98]                                 |                              |                               |                  | 1                | 9.9(+ 5)                                       | 0.14                            | 0.016                               | 0.99                                                           | D                  |                  |
| 25. | 2p ⁴ - 2p ³ ( ² P*)3d | ³ P - ¹ P° | [11.20]                                 |                              |                               | 0                |                  | 2.2(+3)                                        | 0.14                            | 0.016                               | -0.38                                                          | D-                 | 4                |
|     |                                                        |                                  | [11.13]                                 |                              |                               | 3                | 3                | 1.7(+4)                                        | 0.031                           | 0.0034                              | -1.03                                                          | Е                  | 4                |
| 26. |                                                        | ¹ D - ¹ P° | [11.23]                                 |                              |                               | 5                | 3                | 1.7(+4)                                        | 0.019                           | 0.0035                              | -1.02                                                          | D                  | 4                |
| 27. |                                                        | ¹ S - ¹ P* | [11.48]                                 |                              |                               | 1                | 3                | 4.0(+5)                                        | 2.4                             | 0.091                               | 0.38                                                           | D                  | 4                |

# Ni xxı

## Forbidden Transitions

Line strengths tabulated for magnetic dipole and electric quadrupole transitions within the  $2p^4$  configuration are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*¹ These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing was limited to the n=2 complex. Strengths of electric quadrupole transitions as defined in Ref. 1 were multiplied by the factor 2/3 which is needed to bring these values into conformance with the definition of quadrupole strengths used in the NBS tables.

Transition probabilities for these same lines were calculated by Froese Fischer and Saha² using the multiconfiguration Hartree-Fock (MCHF) method with Breit-Pauli corrections. Their basis included many configurations outside the n=2 complex, but relativistic effects were not treated to the same degree as in Ref. 1. Line strengths derived from these data are in quite good agreement with the data of Cheng *et al.* For this ion of the oxygen isoelectronic sequence, correlation effects due to mixing with configurations outside the complex were found by Froese Fischer and Saha to be rather small, as shown by a comparison of the results of their calculations employing an extensive basis to those derived by the same technique but limited to configurations within the n=2 complex.

The weakest lines are excluded from this compilation, as their transition probabilities are considered to be very uncertain.

#### References

¹K. T. Cheng, Y.-K Kim, and J. P. Desclaux, At. Data Nucl. Data Tables 24, 111 (1979).

²C. Froese Fischer and H. P. Saha, Phys. Rev. A 28, 3169 (1983).

| No. | Transition<br>Array              | Multiplet                       | λ<br>(Å)              | $E_i$<br>(cm ⁻¹ ) | $E_k$<br>(cm ⁻¹ ) | <b>g</b> i  | ₿k          | Type of<br>transition | $egin{array}{c} A_{ki} \ (\mathbf{s}^{-1}) \end{array}$ | <i>S</i><br>(at. u.)   | Accu-<br>racy | Source      |
|-----|----------------------------------|---------------------------------|-----------------------|------------------------------|------------------------------|-------------|-------------|-----------------------|---------------------------------------------------------|------------------------|---------------|-------------|
| 1.  | 2p ⁴ -2p ⁴ | 3b - 3b                         |                       |                              |                              |             |             |                       |                                                         |                        |               |             |
|     |                                  |                                 | 779.5<br>2818.2       | 0<br>,<br>92840              | 128290<br>128290             | 5<br>5<br>1 | 3<br>3<br>3 | M1<br>E2<br>M1        | 4.14(+4) ^a<br>2.5<br>560                     | 2.18<br>0.0013<br>1.4  | C<br>E<br>D   | 1<br>1<br>1 |
| 2.  |                                  | ³ P – ¹ D |                       |                              |                              |             |             |                       |                                                         |                        |               |             |
|     |                                  |                                 | 471.15<br>1191.1      | 0<br>128290                  | 212230<br>-<br>212230        | 5<br>5<br>3 | 5<br>5<br>5 | M1<br>E2<br>M1        | 4.2(+4)<br>16<br>1000                                   | 0.82<br>0.0011<br>0.32 | D<br>E<br>D   | 1<br>1<br>1 |
| 3.  |                                  | ³ P – ¹ S |                       |                              |                              |             |             |                       |                                                         |                        |               |             |
|     |                                  |                                 | [359.03]              | 128290                       | 406820                       | 3           | 1           | · <b>M</b> 1          | 3.3(+5)                                                 | 0.57                   | D             | 1           |
| 4.  |                                  | ¹ D - ¹ S | [513. <del>9</del> 0] | 212230                       | 406820                       | 5           | 1           | <b>E</b> 2            | 98                                                      | 0.0021                 | Е             | 1           |

#### Ni XXI: Forbidden transitions

# Ni xxii

N Isoelectronic Sequence

Ground State: 1s²2s²2p^{3 4}S^o_{3/2}

Ionization Energy:  $1894 \text{ eV} = 15280000 \text{ cm}^{-1}$ 

## Allowed Transitions

List of tabulated lines

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|
|                |     |                |     |                |     |                |     |
| 71.48          | 4   | 85.02          | 2   | 103.31         | 1   | 127.30         | 5   |
| 71.54          | 13  | 85.86          | 14  | 103.43         | 6   | 128.86         | 10  |
| 72.52          | 8   | 88.00          | 12  | 105.88         | 11  | 136.30         | 5   |
| 72.837         | 13  | 91.20          | 12  | 106.04         | 1   | 144.80         | 5   |
| 74.37          | 3   | 95.604         | 6   | 106.16         | 16  | 150.26         | 9   |
| 74.49          | 13  | 95.95          | 11  | 114.45         | 10  | 152.89         | 16  |
| 80.16          | 13  | 98.16          | 6   | 117.91         | 1   | 156.56         | 5   |
| 80.55          | 8   | 98.58          | 14  | 118.21         | 15  | 184.19         | 9   |
| 81.04          | 12  | 100.12         | 12  | 123.38         | 5   | 223.22         | 9   |
| 81.794         | 13  | 100.38         | 15  | 124.31         | 16  |                |     |
| 84.06          | 8   | 100.60         | 6   | 124.48         | 10  |                |     |
| 84.24          | 7   | 101.31         | 14  | 126.32         | 16  |                |     |

The tabulated oscillator strengths for transitions of the arrays  $2s^22p^3-2s2p^4$  and  $2s2p^4-2p^5$  are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*¹ These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. The results should be quite accurate, except in the case of weak lines. (A few very weak lines have been omitted from this tabulation.)

# Reference

¹K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, At. Data Nucl. Data Tables 24, 111 (1979).

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| No. | Transition<br>Array                                | Multiplet | λ<br>(Å)                   | $\frac{E_i}{(\mathrm{cm}^{-1})}$ | $E_k$ (cm ⁻¹ )  | gi          | g.          | $A_{ki}$<br>(10 ⁸ s ⁻¹ ) | fik                        | S<br>(at. u.)            | log gf                   | Accu-<br>racy | Source      |
|-----|----------------------------------------------------|-----------|----------------------------|----------------------------------|----------------------------|-------------|-------------|------------------------------------------------|----------------------------|--------------------------|--------------------------|---------------|-------------|
| 1.  | 2s ² 2p ³ -2s2p ⁴ | 4S° - 4P  | 111.15                     | 0                                | 899720                     | 4           | 12          | 192                                            | 0.107                      | 0.156                    | -0.370                   | с             | 1           |
|     |                                                    |           | 117.91<br>106.04<br>103.31 | 0<br>0<br>0                      | 848100<br>943040<br>967960 | 4<br>4<br>4 | 6<br>4<br>2 | 146<br>236<br>266                              | 0.0458<br>0.0398<br>0.0213 | 0.071<br>0.056<br>0.0290 | -0.74<br>-0.80<br>-1.070 | C<br>C<br>C   | 1<br>1<br>1 |
| 2.  |                                                    | 4S° – 2D  |                            |                                  |                            |             |             |                                                |                            |                          |                          |               |             |
| 3.  |                                                    | 4S° – 2S  | 85.02                      | 0                                | 1176180                    | 4           | 4           | 47                                             | 0.0051                     | 0.0057                   | -1.69                    | Е             | 1           |
|     |                                                    |           | 74.37                      | 0                                | 13 <b>4463</b> 0           | 4           | 2           | 39                                             | 0.0016                     | 0.0016                   | -2.19                    | Е             | 1           |
| 4.  |                                                    | 4S* - 2P  | 71.48                      | 0                                | 13 <b>9894</b> 0           | 4           | 4           | 76                                             | 0.0058                     | 0.0055                   | - 1.63                   | Е             | 1           |

Ni XXII: Allowed transitions

Ni XXII: Allowed transitions - Continued

| No. | Transition<br>Array | Multiplet                        | λ<br>(Å)                                                 | $E_i$<br>(cm ⁻¹ )                   | $E_k$ (cm ⁻¹ )                           | <b>g</b> i            | g.                    | $A_{ki}$<br>(10 ⁸ s ⁻¹ ) | fik                                                                 | S<br>(at. u.)                                    | log gf                                                     | Accu-<br>racy         | Source                |
|-----|---------------------|----------------------------------|----------------------------------------------------------|------------------------------------------------|-----------------------------------------------------|-----------------------|-----------------------|------------------------------------------------|---------------------------------------------------------------------|--------------------------------------------------|------------------------------------------------------------|-----------------------|-----------------------|
| 5.  |                     | ²D° - 4P                         |                                                          |                                                |                                                     |                       |                       |                                                |                                                                     |                                                  |                                                            |                       |                       |
|     |                     |                                  | [156.56]<br>[127.30]<br>[136.30]<br>[123.38]<br>[144.80] | 209380<br>157480<br>209380<br>157480<br>157480 | 848100<br>943040<br>943040<br>967960<br>848100      | 6<br>4<br>6<br>4<br>4 | 6<br>4<br>4<br>2<br>6 | 4.4<br>2.9<br>1.1<br>7.4<br>13                 | 0.0016<br>7.0(-4) ^a<br>2.1(-4)<br>8.4(-4)<br>0.0063      | 0.0049<br>0.0012<br>5.7(-4)<br>0.0014<br>0.012   | -2.02<br>-2.55<br>-2.90<br>-2.47<br>-1.60                  | E<br>E<br>E<br>E      | 1<br>1<br>1<br>1<br>1 |
| 6.  |                     | ² D° - ² D | 99.609                                                   | 188620                                         | 1192550                                             | 10                    | 10                    | 450                                            | 0.067                                                               | 0.22                                             | -0.17                                                      | <b>c</b> –            | 1                     |
|     |                     |                                  | 100.60<br>98.16<br>[103.43]<br>[95.604]                  | 209380<br>157480<br>209380<br>157480           | 1203460<br>1176180<br>1176180<br>1203460            | 6<br>4<br>6<br>4      | 6<br>4<br>4<br>6      | 390<br>520<br>0.48<br>1.2                      | $\begin{array}{c} 0.059 \\ 0.075 \\ 5.1(-5) \\ 2.4(-4) \end{array}$ | 0.12<br>0.097<br>1.0(-4)<br>3.0(-4)              | $-0.45 \\ -0.52 \\ -3.51 \\ -3.02$                         | C<br>C<br>E<br>E      | 1<br>1<br>1<br>1      |
| 7.  |                     | ²D° - ²S                         |                                                          |                                                |                                                     |                       |                       |                                                |                                                                     |                                                  |                                                            |                       |                       |
|     |                     |                                  | 84.24                                                    | 157480                                         | 1344630                                             | 4                     | 2                     | 560                                            | 0.030                                                               | 0.033                                            | 0.92                                                       | Е                     | 1                     |
| 8.  |                     | ²D° - ²P                         | 79.607                                                   | 188620                                         | 1444790                                             | 10                    | 6                     | 1100                                           | 0.061                                                               | 0.16                                             | -0.21                                                      | С                     | 1                     |
|     |                     |                                  | 84.06<br>72.52<br>80.55                                  | 209380<br>157480<br>157480                     | 1398940<br>1536480<br>1398940                       | 6<br>4<br>4           | 4<br>2<br>4           | 1200<br>284<br>124                             | 0.084<br>0.0112<br>0.0121                                           | 0.14<br>0.0107<br>0.0128                         | $ \begin{array}{r} -0.30 \\ -1.349 \\ -1.315 \end{array} $ | C<br>C<br>C           | 1<br>1<br>1           |
| 9.  |                     | ²P° - 'P                         |                                                          |                                                |                                                     |                       |                       |                                                |                                                                     |                                                  |                                                            |                       |                       |
|     |                     |                                  | [223.22]<br>[184.19]<br>[150.26]                         | 400120<br>400120<br>302450                     | 848100<br>943040<br>967960                          | 4<br>4<br>2           | 6<br>4<br>2           | 0.29<br>2.8<br>5.3                             | 3.3(-4)<br>0.0014<br>0.0018                                         | 9.7(-4)<br>0.0034<br>0.0018                      | -2.88<br>-2.25<br>-2.44                                    | E<br>E<br>E           | 1<br>1<br>1           |
| 10. |                     | ² P° - ² D | 121.21                                                   | 367560                                         | 1192550                                             | 6                     | 10                    | 57                                             | 0.0208                                                              | 0.0499                                           | -0.90                                                      | с_                    | 1                     |
|     |                     |                                  | 124.48<br>114.45<br>[128.86]                             | 400120<br>302450<br>400120                     | 1203460<br>1176180<br>1176180                       | 4<br>2<br>4           | 6<br>4<br>4           | 67<br>30.3<br>6.4                              | 0.0233<br>0.0119<br>0.0016                                          | 0.0382<br>0.0090<br>0.0027                       | -1.031<br>-1.62<br>-2.19                                   | C<br>C<br>D           | 1<br>1<br>1           |
| 11. |                     | ²P° - ²S                         | 102.35                                                   | 367560                                         | 1344630                                             | 6                     | 2                     | 390                                            | 0.020                                                               | 0.041                                            | -0.91                                                      | C-                    | 1                     |
|     |                     |                                  | 105.88<br>95.95                                          | 400120<br>302450                               | 1344630<br>1344630                                  | 4<br>2                | 2<br>2                | 14<br>440                                      | 0.0012<br>0.061                                                     | 0.0017<br>0.039                                  | $-2.32 \\ -0.91$                                           | D<br>C                | 1<br>1                |
| 12. |                     | ² P° - ² P | <b>9</b> 2.831                                           | 367560                                         | 1444 <b>79</b> 0                                    | 6                     | 6                     | 500                                            | 0.065                                                               | 0.119                                            | -0.410                                                     | с–                    | 1                     |
|     |                     |                                  | 100.12<br>81.04<br>88.00<br>91.20                        | 400120<br>302450<br>400120<br>302450           | 1398940<br>1536480<br>1536480<br>1398940            | 4<br>2<br>4<br>2      | 4<br>2<br>2<br>4      | 102<br>40<br>1200<br>119                       | 0.0153<br>0.0039<br>0.068<br>0.0297                                 | 0.0202<br>0.0021<br>0.079<br>0.0178              | -1.213<br>-2.11<br>-0.57<br>-1.226                         | C<br>D<br>C<br>C      | 1<br>1<br>1<br>1      |
| 13. | 2s2p⁴−2p⁵           | ⁴ P - ² P° |                                                          |                                                |                                                     |                       |                       |                                                |                                                                     |                                                  |                                                            |                       |                       |
|     |                     |                                  | 74.49<br>71.54<br>80.16<br>[72.837]<br>[81.794]          | 848100<br>943040<br>943040<br>967960<br>967960 | 2190550<br>2340890<br>2190550<br>2340890<br>2190550 | 6<br>4<br>4<br>2<br>2 | 4<br>2<br>4<br>2<br>4 | 52<br>6.0<br>34<br>15<br>11                    | 0.0029<br>2.3(-4)<br>0.0033<br>0.0012<br>0.0023                     | 0.0043<br>2.2(-4)<br>0.0035<br>5.8(-4)<br>0.0012 | -1.76<br>-3.04<br>-1.88<br>-2.62<br>-2.34                  | E<br>E<br>E<br>E<br>E | 1<br>1<br>1<br>1<br>1 |
| 14. |                     | ² D - ² P° | 95.410                                                   | 1192550                                        | 2240660                                             | 10                    | 6                     | 680                                            | 0.056                                                               | 0.176                                            | -0.252                                                     | с                     | 1                     |
|     |                     |                                  | 101.31<br>85.86<br>98.58                                 | 1203460<br>1176180<br>1176180                  | 2190550<br>2340890<br>2190550                       | 6<br>4<br>4           | 4<br>2<br>4           | 483<br>490<br>245                              | 0.0495<br>0.0271<br>0.0357                                          | 0.099<br>0.0306<br>0.0463                        | -0.53<br>-0.96<br>-0.85                                    | C<br>C<br>C           | 1<br>1<br>1           |

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | 8k | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fix | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|---------------------|----------------------------------|----------|------------------------------|---------------------------|------------|----|--|--------|---------------|--------|---------------|--------|
| | | | | | | | | | | | | | |
| 15. | | ${}^{2}S - {}^{2}P^{\circ}$ | 111.60 | 1344630 | 2240660 | 2 | 6 | 99 | 0.056 | 0.0409 | -0.95 | C – | 1 |
| | | | 118.21 | 1344630 | 2190550 | 2 | 4 | 111 | 0.0463 | 0.0360 | -1.033 | c | 1 |
| | | | [100.38] | 1344630 | 2340890 | 2 | 2 | 49 | 0.0074 | 0.0049 | -1.83 | D | 1 |
| 16. | | <sup>2</sup> P - <sup>2</sup> P° | 125.65 | 1444790 | 2240660 | 6 | 6 | 460 | 0.11 | 0.27 | 0.19 | с | 1 |
| - 1 | | | 126.32 | 1398940 | 2190550 | 4 | 4 | 330 | 0.080 | 0.13 | -0.49 | c | 1 |
| | | | 124.31 | 1536480 | 2340890 | 2 | 2 | 370 | 0.085 | 0.070 | -0.77 | С | 1 |
| | | | 106.16 | 1398940 | 2340890 | 4 | 2 | 510 | 0.0435 | 0.061 | -0.76 | С | 1 |
| | | | [152.89] | 1536480 | 2190550 | 2 | 4 | 15.1 | 0.0106 | 0.0107 | -1.67 | С | 1 |

Ni XXII: Allowed transitions - Continued

"The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

Ni xxII

Forbidden Transitions

Line strengths tabulated for magnetic dipole and electric quadrupole transitions within the $2p^3$ configuration are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing was limited to the n=2 complex. Strengths of electric quadrupole transitions as defined in Ref. 1 were multiplied by the factor 2/3 which is needed to bring these values into conformance with the definition of quadrupole strengths used in the NBS tables. The weakest lines are excluded from this compilation, as their strengths are considered to be very uncertain.

A-values for the M1 and E2 components of the single transition within the $2p^5$ configuration were obtained by applying Z-expansion formulas published by Oboladze and Safronova.<sup>2</sup> Their values for the magnetic dipole

contribution to this line are in very good agreement with the results of the scaled Thomas-Fermi calculations of Bhatia *et al.*<sup>3</sup> and Bhatia<sup>4</sup> for nitrogenlike Ti and Mn, respectively. It is not clear whether Oboladze and Safronova incorporated configuration interaction into their calculations. Thus the *A*-value for the E2 contribution should be considered rather uncertain.

- <sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, At. Data Nucl. Data Tables 24, 111 (1979).
- <sup>2</sup>N. S. Oboladze and U. I. Safronova, Opt. Spectrosc. (USSR) 48, 469 (1980).
- <sup>3</sup>A. K. Bhatia, U. Feldman, and G. A. Doschek, J. Appl. Phys. **51**, 1464 (1980).
- <sup>4</sup>A. K. Bhatia, J. Appl. Phys. 53, 59 (1982).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_{k} (cm <sup>-1</sup>) | g i | g. | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|----------------------------------|-----------------------------------|----------------------|------------------------------|-----------------------------|------------|--------|-----------------------|---------------------------------------|---------------|---------------|--------|
| 1. | 2p <sup>3</sup> -2p <sup>3</sup> | ⁴S° - ²D° | | | | | | | | | | |
| | | | 477.6
634.8 | 0
0 | 209380
157480 | 4
4 | 6
4 | M1
M1 | 4500
4.2(+4) <sup>a</sup> | 0.11
1.6 | D
D | 1
1 |
| 2. | | <sup>4</sup> S° – <sup>2</sup> P° | | | | | | | | | | |
| | | | [249.93]
[330.63] | 0
0 | 400120
302450 | 4
4 | 4
2 | M1
M1 | 4.8(+4)
7.8(+4) | 0.11
0.21 | D
D | 1 |
| 3. | | <sup>2</sup> D° – <sup>2</sup> D° | | | | | | | | | | |
| | | | [1927] | 157480 | 209380 | 4 | 6 | M 1 | 1040 | 1.65 | с | 1 |
| 4. | | <sup>2</sup> D° - <sup>2</sup> P° | | | | | | | | | | |
| | | | [1074]
[524.27] | 209380
209380 | 302450
400120 | 6 | 24 | E2
M1 | 0.88
3.0(+4) | 0.0015 | E
D | 1 |
| | | | [689.80] | 157480 | 302450 | 4 | 42 | E2
M1 | 9000 | 0.0035 | E
D | 1 |
| | | | [412.13] | 157480 | 400120 | 4 | 2
4 | E2
M1 | 8.6
1.2(+5) | 0.0016 | ED | 1 |
| 5. | | <sup>2</sup> P° – <sup>2</sup> P° | [] | | | - | | | | | _ | - |
| | | | [1024] | 302450 | 400120 | 2 | 4 | M 1 | 5700 | 0.90 | C- | 1 |
| 6. | 2p <sup>5</sup> -2p <sup>5</sup> | <sup>2</sup> P° – <sup>2</sup> P° | | | | | | | | | | |
| | | | [665.16] | 2190550 | 2340890 | 4
4 | 2
2 | M1
E2 | 6.0(+4)
8.2 | 1.3
0.0013 | C+
E | 2
2 |

Ni XXII: Forbidden transitions

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Ni xxiii

C Isoelectronic Sequence

Ground State: $1s^22s^22p^2 {}^{3}P_0$

Ionization Energy: $2011 \text{ eV} = 16220000 \text{ cm}^{-1}$

Allowed Transitions

List of tabulated lines

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|
| 70.752 | 16 | 92.32 | 17 | 109.06 | 3 | 135.42 | 2 |
| 74.07 | 6 | 92.75 | 3 | 111.23 | 19 | 136.47 | 2 |
| 77.027 | 6 | 99.812 | 20 | 111.78 | 19 | 137.55 | 22 |
| 78.21 | 16 | 100.42 | 15 | 111.86 | 2 | 143.89 | 25 |
| 78.751 | 21 | 100.50 | 3 | 112.55 | 29 | 161.15 | 28 |
| 79.99 | 4 | 102.08 | 10 | 120.51 | 23 | 162.30 | 7 |
| 83.707 | 5 | 102.50 | 20 | 126.54 | 2 | 162.74 | 13 |
| 84.721 | 18 | 103.07 | 17 | 127.14 | 14 | 162.85 | 22 |
| 87.50 | 5 | 103.23 | 3 | 127.21 | 19 | 173.86 | 7 |
| 87.66 | 4 | 103.67 | 17 | 127.46 | 2 | 175.59 | 7 |
| 87.77 | 18 | 104.70 | 3 | 128.22 | 8 | 178.51 | 25 |
| 88.11 | 11 | 106.02 | 3 | 128.30 | 2 | 185.33 | 27 |
| 90.49 | 17 | 107.00 | 19 | 128.87 | 26 | 209.98 | 1 |
| 90.96 | 17 | 108.03 | 9 | 131.60 | 19 | 232.37 | 12 |
| 91.094 | 24 | 108.27 | 17 | 132.69 | 8 | 235.61 | 1 |
| 91.83 | 4 | 108.59 | 19 | 133.54 | 22 | 247.04 | 27 |

The tabulated oscillator strengths for transitions of the arrays $2s^22p^2-2s2p^3$ and $2s2p^3-2p^4$ are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing was limited to the n=2 complex. The results should be quite accurate, except in the case of weak lines. (A few very weak lines have been omitted from this tabulation.)

Line strengths derived from these two sources are in reasonably good agreement, particularly for the stronger transitions.

Stratton *et al.*<sup>3</sup> measured the ratio of *A*-values for two lines out of the $2s2p^{3}$ <sup>3</sup>S<sub>1</sub>° level. Their result agrees very well with the theoretical data of Cheng *et al.*

References

Transition probabilities for lines of the $2s^22p^2-2s^2p^3$ array were calculated by Froese Fischer and Saha<sup>2</sup> using the multiconfiguration Hartree-Fock (MCHF) method with Breit-Pauli corrections. Their basis included many configurations outside the n = 2 complex, but relativistic effects we not treated to the same degree as in Ref. 1.

<sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, At. Data Nucl. Data Tables 24, 111 (1979).

<sup>2</sup>C. Froese Fischer and H. P. Saha, Phys. Scr. 32, 181 (1985).

<sup>3</sup>B. C. Stratton, H. W. Moos, S. Suckewer, U. Feldman, J. F. Seely, and A. K. Bhatia, Phys. Rev. A 31, 2534 (1985).

| Ni XXIII: Allowed trans | itions |
|-------------------------|--------|
|-------------------------|--------|

| No. | Transition
Array | Multiplet | λ
(Å) | <i>E</i> <sub>i</sub>
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | g. | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | f ik | S
(at. u.) | log gf | Асси-
гасу | Source |
|-----|--|-----------|----------------------|--|---------------------------|------------|--------|--|---------------------------------|------------------|----------------|---------------|--------|
| 1. | 2s <sup>2</sup> 2p <sup>2</sup> -2s2p <sup>3</sup> | ³₽ - ⁵S* | [235.61]
[209.98] | 161190
109390 | 585620
585620 | 5
3 | 5
5 | 0.66
0.85 | 5.5(-4) <sup>a</sup>
9.4(-4) | 0.0021
0.0019 | -2.56
-2.55 | E | 1 |

Ni XXIII: Allowed transitions - Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | gi | g. | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|---------------------|---|----------------|------------------------------|---------------------------|-----|----|--|---------|---------------|--------|---------------|--------|
| | | | | | | | | | | | | | |
| 2. | | <sup>3</sup> P - <sup>3</sup> D <sup>•</sup> | 126.32 | 126010 | 917630 | 9 | 15 | 100 | 0.040 | 0.15 | -0.44 | D | 1 |
| 1 | | | 128.30 | 161190 | 940610 | 5 | 7 | 74 | 0.0257 | 0.054 | -0.89 | С | 1 |
| | | | 126.54 | 109390 | 899650 | 3 | 5 | 120 | 0.0482 | 0.060 | -0.84 | С | 1 |
| | | | 111.86 | 0 | 893970 | 1 | 3 | 170 | 0.098 | 0.036 | -1.01 | C | 1 |
| | | | [135.42] | 161190 | 899650 | 5 | 5 | 1.0 | 2.8(-4) | 6.2(-4) | -2.85 | E | 1 |
| | | | 127.46 | 109390 | 893970 | 3 | 3 | 4.9 | 0.0012 | 0.0015 | -2.44 | D | 1 |
| | | | [136.47] | 161190 | 893970 | 5 | 3 | 2.0 | 3.3(-4) | 7.4(-4) | -2.78 | Е | 1 |
| 3. | | <sup>3</sup> P - <sup>3</sup> P° | 103.61 | 126010 | 1091190 | 9 | 9 | 306 | 0.0492 | 0.151 | -0.354 | C | 1 |
| | | | 106.02 | 161190 | 1104380 | 5 | 5 | 287 | 0.0484 | 0.084 | -0.62 | c | 1 |
| | | | 103.23 | 109390 | 1078110 | 3 | 3 | 240 | 0.0384 | 0.0391 | -0.94 | С | 1 |
| | | | 109.06 | 161190 | 1078110 | 5 | 3 | 29 | 0.0031 | 0.0056 | -1.81 | D | 1 |
| | | | 104.70 | 109390 | 1064460 | 3 | 1 | 294 | 0.0161 | 0.0166 | -1.316 | C | 1 |
| | | | [100.50] | 109390 | 1104380 | 3 | 5 | 1.1 | 2.9(-4) | 2.9(-4) | -3.06 | Е | 1 |
| | | | 92.75 | 0 | 1078110 | 1 | 3 | 45.2 | 0.0175 | 0.0053 | -1.76 | С | 1 |
| 4. | | <sup>3</sup> P - <sup>3</sup> S° | 88. 956 | 126010 | 1250160 | 9 | 3 | 1170 | 0.0463 | 0.122 | -0.380 | с | 1 |
| | | 1 | 91.83 | 161190 | 1250160 | 5 | 3 | 750 | 0.057 | 0.086 | _0.55 | C | 1 |
| | | | 87.66 | 109390 | 1250160 | 3 | 3 | 280 | 0.0322 | 0.0279 | -1.015 | č | 1 î |
| | | | 79.99 | 100000 | 1250160 | 1 ĭ | 3 | 107 | 0.0308 | 0.0081 | -1.51 | Ċ | 1 |
| | | | 87.50 | 161190 | 1304040 | 5 | 5 | 120 | 0.014 | 0.020 | -1.15 | Ē | 1 |
| | | | | | | | - | | | | | - | 1 |
| 5. | | ${}^{3}P - {}^{1}D^{\circ}$ | | | | | | | | 1 | | | |
| | | | [83.707] | 109390 | 1304040 | 3 | 5 | 6.9 | 0.0012 | 9.9(-4) | -2.44 | E | 1 |
| | | | | | | | | | | | | | |
| 6. | | ${}^{3}P - {}^{1}P^{\circ}$ | | | | | | | | | |] | |
| | | | | | | | | | | | | | |
| | | | [77.027] | 161190 | 1459440 | 5 | 3 | 5.1 | 2.7(-4) | 3.4(-4) | -2.87 | E | 1 |
| | | | 74.07 | 109390 | 1459440 | 3 | 3 | 72 | 0.0059 | 0.0043 | -1.75 | E | 1 |
| | | | | | | l | | | | | |] | 1 |
| 7. | | $^{1}D - ^{3}D^{\circ}$ | | | | | | | | | 1 | | |
| | | | | | | - | - | | 0.0000 | 0.000 | 1.07 | - | |
| | | | [162.30] | 324460 | 940610 | 5 | 17 | 16 | 0.0086 | 0.023 | -1.37 | E | 1 |
| | | | [173.86] | 324460 | 899650 | 5 | 5 | 0.40 | 1.8(-4) | 5.2(-4) | -3.05 | E | 1 |
| 1 | | | [175.59] | 324460 | 893970 | 5 | 3 | 2.8 | 7.8(-4) | 0.0023 | -2.41 | E | 1 |
| | | 10 300 | | | | | | | | | | | |
| 8. | | ·D - •P | | | | | | | | | | | |
| | | | [198 99] | 324460 | 1104380 | 5 | 5 | 19 | 47(-4) | 99(-1) | -2.63 | F | 1 |
| | | | [132 69] | 324400 | 1078110 | 5 | 3 | 2.5 | 39(-4) | 85(-4) | -2.00 | E | 1 |
| | | | [102.00] | 024400 | 1010110 | ľ | | 2.0 | 0.0(-4) | 0.0(-4) | | - | 1 |
| 9. | | ${}^{1}D - {}^{3}S^{\circ}$ | [108.03] | 324460 | 1250160 | 5 | 3 | 7.0 | 7.3(-4) | 0.0013 | -2.44 | Е | 1 |
| | | | | | | | | | | | | | |
| 10. | | $^{1}D - ^{1}D^{\circ}$ | 102.08 | 324460 | 1304040 | 5 | 5 | 530 | 0.083 | 0.14 | -0.38 | С | 1 |
| 11. | | <sup>1</sup> D - <sup>1</sup> P ° | 88.11 | 324460 | 1459440 | 5 | 3 | 830 | 0.058 | 0.084 | -0.54 | с | 1 |
| | | l | | | | l | | | | | | | |
| 12. | | <sup>1</sup> S – <sup>3</sup> D° | | | | | | | | | | | |
| 1 | | | | | | 1 | | | 1 | | | | |
| | | | [232.37] | 463620 | 893970 | 1 | 3 | 0.66 | 0.0016 | 0.0012 | -2.80 | E | 1 |
| | | | | 1 | | | | | | | | | |
| 13. | | <sup>1</sup> S – <sup>3</sup> P° | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| | | | [162.74] | 463620 | 1078110 | 1 | 3 | 2.4 | 0.0028 | 0.0015 | -2.55 | Е | 1 |
| | | | | | | | | | | | | - | |
| 14. | | <sup>1</sup> S – <sup>3</sup> S° | [127.14] | 463620 | 1250160 | 1 | 3 | 10 | 0.0075 | 0.0031 | -2.12 | E | 1 |
| | | 10 10 | 100.10 | 100000 | 1450.440 | | | 010 | 0.000 | 0.000 | 1.00 | | |
| 15. | | 'S - 'P' | 100.42 | 463620 | 1459440 | | 3 | 210 | 0.096 | 0.032 | -1.02 | U | 1 |
| | | | 1 | 1 | | 1 | | 1 | | | | 1 | |

Ni XXIII: Allowed transitions - Continued

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | g i | ₿k | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|------------------------------------|---|--|--|--|----------------------------|----------------------------|--|--|--|---|--------------------------------------|----------------------------|
| 16. | 2s2p <sup>3</sup> -2p <sup>4</sup> | ⁵S° – ³P | | | | | | | | | | | |
| | | | 78.21
[70.752] | 585620
585620 | 1864230
1999010 | 5
5 | 5
3 | 29
3.8 | 0.0027
1.7(-4) | 0.0035
2.0(-4) | -1.87
-3.07 | E
E | 1 |
| 17. | | <sup>3</sup> D° - <sup>3</sup> P | 99.595 | 917630 | 1921700 | 15 | 9 | 530 | 0.0474 | 0.233 | -0.148 | c | 1 |
| | | | 108.27
90.96
92.32
103.67
90.49
103.07 | 940610
899650
893970
899650
893970
893970 | 1864230
1999010
1977150
1864230
1999010
1864230 | 7
5
3
5
3
3 | 5
3
1
5
3
5 | 332
250
439
178
177
60 | 0.0417
0.0186
0.0187
0.0286
0.0217
0.0158 | 0.104
0.0278
0.0171
0.0488
0.0194
0.0161 | $-0.53 \\ -1.032 \\ -1.251 \\ -0.84 \\ -1.186 \\ -1.324$ | C
C
C
C
C
C
C
C | 1
1
1
1
1 |
| 18. | | <sup>3</sup> D° - <sup>1</sup> D | | | | | | | | | | | |
| | | | 87.77
[84.721] | 940610
899650 | 2079990
2079990 | 7
5 | 5
5 | 90
9.3 | 0.0074
0.0010 | 0.015
0.0014 | $-1.29 \\ -2.30$ | E
E | 1
1 |
| 19. | | <sup>3</sup> P° – <sup>3</sup> P | 120.41 | 1091190 | 1921700 | 9 | 9 | 153 | 0.0334 | 0.119 | -0.52 | C- | 1 |
| | | | 131.60
[108.59]
[111.78]
[111.23]
127.21
[107.00] | 1104380
1078110
1104380
1078110
1078110
1064460 | 1864230
1999010
1999010
1977150
1864230
1999010 | 5
3
5
3
3
1 | 5
3
1
5
3 | 39.7
8.5
219
226
44.0
64 | 0.0103
0.0015
0.0246
0.0140
0.0178
0.0329 | 0.0223
0.0016
0.0453
0.0154
0.0224
0.0116 | $\begin{array}{r} -1.288 \\ -2.35 \\ -0.91 \\ -1.377 \\ -1.272 \\ -1.483 \end{array}$ | C
D
C
C
C
C
C | 1
1
1
1
1
1 |
| 20. | | <sup>3</sup> P° - <sup>1</sup> D | | | | | | | | | - | | |
| | | | 102.50
[99.812] | 1104380
1078110 | 2079990
2079990 | 5
3 | 5
5 | 57
23 | 0.0089
0.0058 | 0.015
0.0057 | $-1.35 \\ -1.76$ | E
E | 1
1 |
| 21. | | <sup>3</sup> P° – <sup>1</sup> S | | | | | | | | | | 6 | |
| | | | [78.751] | 1078110 | 2347930 | 3 | 1 | 74 | 0.0023 | 0.0018 | -2.16 | Е | 1 |
| 22. | | ³S⁺ – ³P | 148.91 | 1250160 | 1921700 | 3 | 9 | 119 | 0.119 | 0.175 | 0.447 | c | 1 |
| | | | [162.85]
133.54
137.55 | 1250160
1250160
1250160 | 1864230
1999010
1977150 | 3
3
3 | 5
3
1 | 72
186
253 | 0.0474
0.0497
0.0239 | 0.076
0.066
0.0325 | $ -0.85 \\ -0.83 \\ -1.144$ | C
C
C | 1
1
1 |
| 23. | | <sup>3</sup> S° – <sup>1</sup> D | [120.51] | 1250160 | 2079990 | 3 | 5 | 0.39 | 1.4(-4) | 1.7(-4) | -3.38 | Е | 1 |
| 24. | | <sup>3</sup> S* – <sup>1</sup> S | [91.094] | 1250160 | 2347930 | 3 | 1 | 70 | 0.0029 | 0.0026 | -2.06 | Е | 1 |
| 25. | | <sup>1</sup> D° - <sup>3</sup> P | | | | | | | | | | | |
| | | | [178.51]
[143.89] | 1304040
1304040 | 1864230
1999010 | 5
5 | • 5
3 | 9.8
8.1 | 0.0047
0.0015 | 0.014
0.0036 | -1.63 -2.12 | E
E | 1
1 |
| 26. | | ${}^{1}D^{\circ} - {}^{1}D$ | 128.87 | 1304040 | 2079990 | 5 | 5 | 402 | 0.100 | 0.212 | -0.301 | с | 1 |
| 27. | | <sup>1</sup> P° – <sup>3</sup> P | | | | | | | | | | | |
| | | | [247.04]
[185.33] | 1459440
1459440 | 1864230
1999010 | 3
3 | 5
3 | 1.2
11 | 0.0018
0.0055 | 0.0044
0.010 | -2. 27
-1.78 | E
E | 1
1 |
| 28. | | <sup>1</sup> P • - <sup>1</sup> D | [161.15] | 1459440 | 2079990 | 3 | 5 | 58 | 0.0378 | 0.060 | -0.95 | с | 1 |
| 29. | | <sup>1</sup> P* - <sup>1</sup> S | 112.55 | 1459440 | 2347930 | 3 | 1 | 1000 | 0.063 | 0.070 | -0.72 | С | 1 |

"The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

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Forbidden Transitions

Line strengths tabulated for magnetic dipole and electric quadrupole transitions within the $2p^2$ configuration are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing was limited to the n=2 complex. Strengths of electric quadrupole transitions as defined in Ref. 1 were multiplied by the factor 2/3 which is needed to bring these values into conformance with the definition of quadrupole strengths used in the NBS tables. The weakest lines are excluded from this compilation, as their strengths are considered to be very uncertain.

Transition probabilities for these same lines were cal-

culated by Froese Fischer and Saha<sup>2</sup> using the multicon-

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figuration Hartree-Fock (MCHF) method with Breit-Pauli corrections. Their basis included many configurations outside the n=2 complex, but relativistic effects were not treated to the same degree as in Ref. 1. Line strengths derived from these data are in good agreement with the data of Cheng *et al*.

References

<sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, At. Data Nucl. Data Tables 24, 111 (1979).

<sup>2</sup>C. Froese Fischer and H. P. Saha, Phys. Scr. 32, 181 (1985).

| No. | Transition
Array | Multiplet | λ
(Å) | $\frac{E_i}{(\mathrm{cm}^{-1})}$ | E_k (cm <sup>-1</sup>) | gi | g. | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Асси-
гасу | Source |
|-----|----------------------------------|---------------------------------|---------------------|----------------------------------|---------------------------|-------------|-------------|-----------------------|---------------------------------------|-----------------------|---------------|-------------|
| 1. | 2p <sup>2</sup> -2p <sup>2</sup> | 3P - 3P | | | | | | | | | | |
| | | | 1915.0
911.0 | 109390
0 | 161190
109390 | 3
1 | 5
3 | M1
M1 | 1320
2.07(+4)ª | 1.72
1.74 | c
c | 1
1 |
| 2. | | <sup>3</sup> P – <sup>1</sup> D | | | | | | | | | | |
| | | | 614.8
,
465.4 | 161190
109390 | 324460
″
324460 | 5
5
3 | 5
5
5 | M1
E2
M1 | 3.7(+4)
7.3
4.1(+4) | 1.6
0.0019
0.77 | C
E
D | 1
1
1 |
| 3. | | <sup>3</sup> P – <sup>1</sup> S | | | | | | | | | | |
| | | | [282.30] | 109390 | 463620 | 3 | 1 | M 1 | 3.0(+5) | 0.25 | D | 1 |
| 4. | | <sup>1</sup> D - <sup>1</sup> S | [718.60] | 324460 | 463620 | 5 | 1 | E2 | 16 | 0.0018 | Е | 1 |

Ni XXIII: Forbidden transitions

Ni xxiv

B Isoelectronic Sequence

Ground State: $1s^22s^22p {}^2P_{1/2}^{\circ}$

Ionization Energy: $2131 \text{ eV} = 17190000 \text{ cm}^{-1}$

Allowed Transitions

List of tabulated lines

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|-----|----------------|-----|----------------|-----|
| 75.083 | 7 | 102.89 | 6 | 134.53 | 16 | 213.15 | 11 |
| 75.580 | 7 | 103.43 | 5 | 134.73 | 9 | 218.35 | 1 |
| 79.185 | 7 | 103.53 | 4 | 135.47 | 9 | 221.06 | 15 |
| 87.50 | 3 | 104.64 | 3 | 137.01 | 13 | 224.02 | 1 |
| 88.54 | 4 | 106.68 | 10 | 138.80 | 2 | 227.82 | 12 |
| 88.977 | 6 | 109.03 | 13 | 143.30 | 9 | 264.98 | 1 |
| 92.138 | 6 | 113.14 | 5 | 153.47 | 16 | 338.62 | 14 |
| 96.070 | 6 | 118.52 | 2 | 156.70 | 13 | 339.66 | 1 |
| 97.17 | 10 | 121.15 | 13 | 159.69 | 12 | 354.74 | 11 |
| 98.39 | 6 | 122.72 | 5 | 172.09 | 8 | | |
| 101.13 | 10 | 126.25 | 3 | 184.92 | 8 | | |
| 102.11 | 3 | 127.78 | 9 | 206.88 | 12 | | |

The tabulated oscillator strengths for transitions of the arrays $2s^22p-2s2p^2$ and $2s2p^2-2p^3$ are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. The results should be quite accurate, except in the case of weak lines. (A few very weak lines have been omitted from this tabulation.)

at about V XIX or Cr XX. We have thus labeled these two levels accordingly, in contrast to their labeling by Cheng. *et al.*, which is consistent with their ordering at the neutral end of the B sequence.

Reference

According to several sources (see, e.g., introduction to Fe XXII), the lower of the two levels $2s 2p^2 {}^2P_{1/2}$ and ${}^2S_{1/2}$ is mostly of ${}^2P$ character, having "crossed" the ${}^2S_{1/2}$ level

<sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, At. Data Nucl. Data Tables 24, 111 (1979).

| No. | Transition
Array | Multiplet | λ
(Å) | $\frac{E_i}{(\mathrm{cm}^{-1})}$ | E_k (cm <sup>-1</sup>) | g i | ₿k | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|---------------------|-----------|----------|----------------------------------|---------------------------|------------|----|--|---------------|---------------|--------|---------------|--------|
| 1. | $2s^22p-2s^2p^2$ | ²P° - 4P | | | | | | | | | • | • | |
| | | | [224.02] | 163570 | 609950 | 4 | 6 | 1.4 | 0.0016 | 0.0047 | -2.19 | Е | 1 |
| | | | [264.98] | 163570 | 540950 | 4 | 4 | 0.13 | $1.4(-4)^{a}$ | 4.9(-4) | -3.25 | Е | 1 |
| | 1 | | [218.35] | 100570 | 457980 | z | Z | 1.7 | 0.0012 | 0.0017 | -2.62 | E | 1 |
| ĺ | | | [339.66] | 163570 | 457980 | 4 | 2 | 0.19 | 1.6(4) | 7.2(-4) | -3.19 | E | 1 |
| 2. | | ²P° - ²D | | | | | | | | | | | |
| | | | 138.80 | 163570 | 884030 | 4 | 6 | 72 | 0.0314 | 0.057 | -0.90 | С | 1 |
| | | | 118.52 | 0 | 843710 | 2 | 4 | 150 | 0.063 | 0.049 | -0.90 | č | 1 |

Ni XXIV: Allowed transitions

Ni xxiv: Allowed transitions - Continued

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | 8+ | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fa | <i>S</i>
(at. u.) | log gf | Accu-
racy | Source |
|-----|---------------------|----------------------------------|-------------------|------------------------------|---------------------------|------------|--------|--|-------------------|----------------------|----------------|---------------|--------|
| _ | | | | | | | | | | | | | |
| 3. | | <sup>2</sup> P° – <sup>2</sup> P | 102.94 | 109050 | 1080490 | 6 | 6 | 530 | 0.084 | 0.17 | -0.30 | C- | 1 |
| | | | 102.11 | 163570 | 1142910 | 4 | 4 | 540 | 0.084 | 0.11 | -0.47 | С | 1 |
| Í | | | 104.64 | 0 | 955660 | 2 | 2 | 470 | 0.077 | 0.053 | -0.81 | C | 1 |
| | | | [126.25]
87.50 | 163570 | 955660
1142910 | 4
2 | 2 | 1.8
67 | 2.2(-4)
0.0153 | 3.7(-4)
0.0088 | -3.06
-1.51 | Е
С | 1 |
| 4. | | <sup>2</sup> P° – <sup>2</sup> S | 97.997 | 109050 | 1129490 | 6 | 2 | 510 | 0.0243 | 0.0471 | -0.84 | с_ | 1 |
| | | | 103.53 | 163570 | 1129490 | 4 | 2 | 417 | 0.0335 | 0.0457 | 0.87 | с | 1 |
| | | | 88.54 | 0 | 1129490 | 2 | 2 | 20 | 0.0024 | 0.0014 | -2.32 | D | 1 |
| 5. | $2s2p^2-2p^3$ | 4P - 4S° | 115.85 | 561620 | 1424810 | 12 | 4 | 500 | 0.0339 | 0.155 | -0.391 | С | 1 |
| | | | 122.72 | 609950 | 1424810 | 6 | 4 | 217 | 0.0326 | 0.079 | -0.71 | c | 1 |
| | | | 113.14 | 540950 | 1424810 | 4 | 4 | 165 | 0.0316 | 0.0471 | -0.90 | C | 1 |
| | | | 103.43 | 457980 | 1424810 | 2 | 4 | 130 | 0.0418 | 0.0285 | -1.078 | C | 1 |
| 6. | | <sup>4</sup> P - <sup>2</sup> D° | | | | | | | | | | | |
| | | | 98.39 | 609950 | 1626280 | 6 | 6 | 37 | 0.0053 | 0.010 | -1.50 | Е | 1 |
| | | | [96.070] | 540950 | 1581860 | 4 | 4 | 49 | 0.0068 | 0.0086 | -1.57 | E | 1 |
| | | | [102.89] | 609950
E40050 | 1581860 | 6 | 4 | 6.6 | 7.0(-4) | 0.0014 | -2.38 | E | 1 |
| | | | [92.138] | 457980 | 1581860 | 2 | 4 | 1.5 | 3.6(-4) | 1.5(-4)
2.1(-4) | -3.13
-3.14 | Ē | 1 |
| 7. | | 4P - 2P° | | | | | | | | | | | |
| | | | [79 185] | 609950 | 1872810 | 6 | 4 | 18 | 1 1(-4) | 17(-4) | _3 18 | E | 1 |
| | | | [75.083] | 540950 | 1872810 | 4 | 4 | 4.1 | 3.5(-4) | 3.5(-4) | -2.85 | Ē | 1 |
| | | | [75.580] | 457980 | 1781090 | 2 | 2 | 3.4 | 2.9(-4) | 1.4(-4) | -3.24 | Е | 1 |
| 8. | | <sup>2</sup> D - <sup>4</sup> S° | | | | | | | | | | | |
| | | | [184.92] | 884030 | 1424810 | 6 | 4 | 0.38 | 1.3(-4) | 4.7(-4) | -3.11 | Е | 1 |
| | | | [172.09] | 843710 | 1424810 | 4 | 4 | 3.4 | 0.0015 | 0.0034 | -2.22 | E | 1 |
| 9. | | <sup>2</sup> D - <sup>2</sup> D° | 135.02 | 867900 | 1608510 | 10 | 10 | 175 | 0.0477 | 0.212 | -0.322 | C | 1 |
| | | | 134.73 | 884030 | 1626280 | 6 | 6 | 144 | 0.0393 | 0.105 | -0.63 | C | 1 |
| | | | 135.47 | 843710 | 1581860 | 4 | 4 | 80 | 0.0221 | 0.0394 | -1.054 | C | 1 |
| | | | 143.30
127.78 | 884030
843710 | 1581860 | 4 | 4
6 | 52 | 0.0124 | 0.0351 | -1.128 | c | 1 |
| 10. | | <sup>2</sup> D - <sup>2</sup> P° | 102.63 | 867900 | 1842240 | 10 | 6 | 270 | 0.026 | 0.088 | -0.58 | C - | 1 |
| | | 1 | 101.13 | 884030 | 1872810 | 6 | 4 | 163 | 0.0167 | 0.0334 | -1.000 | С | 1 |
| | | | 106.68 | 843710 | 1781090 | 4 | 2 | 367 | 0.0313 | 0.0440 | -0.90 | С | 1 |
| | | | 97.17 | 843710 | 1872810 | 4 | 4 | 59 | 0.0084 | 0.011 | -1.47 | D | 1 |
| 11. | | <sup>2</sup> P - <sup>4</sup> S° | | | | | | | | | | | |
| | | | [354.74] | 1142910 | 1424810 | 4 | 4 | 0.42 | 7.9(-4) | 0.0037 | -2.50 | Е | 1 |
| | | | [213.15] | 955660 | 1424810 | 2 | 4 | 3.3 | 0.0045 | 0.0063 | -2.05 | E | 1 |
| 12. | | <sup>2</sup> P - <sup>2</sup> D° | 189.39 | 1080490 | 1608510 | 6 | 10 | 51 | 0.045 | 0.17 | -0.56 | D | 1 |
| | | | [206.88] | 1142910 | 1626280 | 4 | 6 | 37.4 | 0.0360 | 0.098 | -0.84 | С | 1 |
| | | | 159.69 | 955660 | 1581860 | 2 | 4 | 89 | 0.068 | 0.071 | -0.87 | C | 1 |
| | | | [227.82] | 1142910 | 1581860 | 4 | 4 | 0.49 | 3.8(-4) | 0.0011 | -2.82 | E | 1 |

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Ni XXIV: Allowed transitions - Continued

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | gi | ₿k | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fa | S
(at. u.) | log <i>gf</i> | Accu-
racy | Source |
|-----|---------------------|----------------------------------|--|--|--|------------------|------------------|--|-------------------------------------|------------------------------------|------------------------------------|------------------|------------------|
| 13. | | ²₽ - ²₽* | 131.28 | 1080490 | 1842240 | 6 | 6 | 220 | 0.058 | 0.15 | -0.46 | с_ | 1 |
| | | | 137.01
121.15
[156.70]
109.03 | 1142910
955660
1142910
955660 | 1872810
1781090
1781090
1872810 | 4
2
4
2 | 4
2
2
4 | 260
44
21
36.8 | 0.073
0.0097
0.0038
0.0131 | 0.13
0.0077
0.0078
0.0094 | $-0.53 \\ -1.71 \\ -1.82 \\ -1.58$ | C
D
D
C | 1
1
1
1 |
| 14. | | ²S − ⁴S° | [338.62] | 1129490 | 1424810 | 2 | 4 | 0.18 | 6.2(-4) | 0.0014 | -2.91 | Е | 1 |
| 15. | | ²S − ²D° | | | | | | | | | | | |
| | | | [221.06] | 1129490 | 1581860 | 2 | 4 | 6.3 | 0.0093 | 0.014 | -1.73 | D | 1 |
| 16. | | <sup>2</sup> S - <sup>2</sup> P* | 140.30 | 1129490 | 1842240 | 2 | 6 | 72 | 0.064 | 0.059 | -0.89 | С | 1 |
| | | | 134.53
[153.47] | 1129490
1129490 | 1872810
1781090 | 2
2 | 4
2 | 28.4
127 | 0.0154
0.0447 | 0.0136
0.0452 | 1.51
1.049 | C
C | 1
1 |

"The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

Ni xxiv

Forbidden Transitions

The line strengths tabulated for the single magnetic dipole and single electric quadrupole transition within the $2s^22p$ ground state configuration are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations include a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing is limited to the n=2 complex. The strength of the electric quadrupole transition as defined in Ref. 1 was multiplied by the factor 2/3 in order to bring this value into conformance with the definition of the quadrupole strength used in the NBS tables.

Transition probabilities for the same lines were calculated by Froese Fischer and Saha<sup>2</sup> using the multiconfiguration Hartree-Fock (MCHF) method with Breit-Pauli corrections. Their orbital basis includes many configurations outside the n=2 complex, but relativistic effects were not treated to the same degree as in Ref. 1. The line strengths for both the M1 and E2 transitions, derived from these data by interpolation between appropriately spaced ions of the B sequence, are in very good agreement with the data of Cheng *et al.*<sup>1</sup>

References

<sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, At. Data Nucl. Data Tables 24, 111 (1979).

<sup>2</sup>C. Froese Fischer and H. P. Saha, Phys. Rev. A 28, 3169 (1983).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | <i>E</i> <sup>k</sup>
(cm <sup>-1</sup>) | Bi | g⊾ | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Accu-
racy | Source |
|-----|------------------------|-----------------------------------|------------|------------------------------|--|--------|--------|-----------------------|---------------------------------------|------------------|---------------|--------|
| 1. | 2 <i>p</i> -2 <i>p</i> | <sup>2</sup> P° – <sup>2</sup> P° | | | | | | | | | | |
| | | | 609.9
″ | , <sup>0</sup> | 163960 | 2
2 | 4
4 | M1
E2 | 3.95(+4)*
5.1 | 1.33
1.03(-3) | B
C | 1
1 |

Ni xxiv: Forbidden transitions

Ni xxv

Be Isoelectronic Sequence

Ground State: 1s<sup>2</sup>2s<sup>2</sup> <sup>1</sup>S<sub>0</sub>

Ionization Energy: $2295 \text{ eV} = 18510000 \text{ cm}^{-1}$

Allowed Transitions

| List of tabulated lin | nes |
|-----------------------|-----|
|-----------------------|-----|

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|-----|----------------|----------|----------------|-------|----------------|-----|
| 0.10 | 11 | 0.70 | 12 | 0.04 | 26 | 117.01 | |
| 9.19 | 11 | 9.70 | 13 | 9.94 | 20 | 117.91 | 2 |
| 9.27 | 10 | 9.71 | 29 | 9.95 | 19 | 120.47 | 4 |
| 9.30 | 11 | 9.74 | 24 | 9.97 | 25,31 | 126.73 | 3 |
| 9.31 | 10 | 9.75 | 28 | 10.02 | 21 | 128.85 | 3 |
| 9.32 | 10 | 9.76 | 24,27,29 | 10.07 | 21 | 130.99 | 7 |
| 9.34 | 9 | 9.77 | 12 | 10.08 | 21,35 | 135.95 | 3 |
| 9.39 | 8 | 9.78 | 27 | 10.09 | 19,30 | 151.91 | 3 |
| 9.42 | 16 | 9.80 | 28 | 10.17 | 21 | 158.84 | 3 |
| 9.43 | 10 | 9.85 | 33 | 10.20 | 21 | 165.34 | 3 |
| 9.49 | 15 | 9.86 | 27,34 | 10.21 | 22 | 188.15 | 6 |
| 9.56 | 14 | 9.87 | 27 | 10.23 | 21 | 238.82 | 1 |
| 9.60 | 24 | 9.91 | 19,27 | 10.32 | 20 | 278.01 | 5 |
| 9.63 | 24 | 9.92 | 32 | 10.46 | 23 | 326.58 | 5 |
| 9.64 | 24 | 9.93 | 27 | 104.07 | 4 | 499.50 | 5 |

Oscillator strengths for transitions of the arrays $2s^2-2s 2p$ and $2s 2p-2p^2$ are taken from the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations include the configuration interaction most relevant for the states of these configurations, as well as a perturbative treatment of the Breit interaction and the Lamb shift. The results should be quite accurate, except for the weakest intercombination lines. (The ${}^{3}P_{1}^{o} - {}^{1}S_{0}$ transition of the $2s 2p-2p^{2}$ array has been omitted here, since the *f*-value is considerably smaller than those of the other lines of this array.)

A number of sources of reliable data, from other relativistic calculations, are available for the 2s-2p transitions. However, with the exception of some of the weaker lines, they all agree well with the results of Cheng *et al.*<sup>1</sup> The latter are quoted exclusively here since they provide data from a single set of comprehensive calculations, all done at a uniform and reasonably accurate level of approximation, for the valence shell 2s-2ptransitions for all ions of the isoelectronic sequence.

The f-values for the $2s^2-2s 3p$, 2s 2p-2p 3p, 2s 2p-2s 3s, $2p^2-2p 3s$, 2s 2p-2s 3d, and $2p^2-2p 3d$ arrays of transitions are taken from the work of Fawcett,<sup>2</sup> who used Cowan's version of the relativistic Hartree-Fock method with intermediate coupling and configuration interaction. This work provides a comprehensive set of data for the entire

isoelectronic sequence, calculated at a uniform level of approximation. Some of these transitions, for some ions of this sequence, have also been calculated by Bhatia *et* $al.^3$ using the program SUPERSTRUCTURE, which includes configuration interaction and intermediate coupling. Where they overlap, these two sets of calculations agree to within the uncertainties assigned here. Transitions involving the J=1 levels of 2p 3p <sup>3</sup>S and <sup>3</sup>P have been omitted because of erratic behavior of the *f*-values along the sequence.

Oscillator strengths for the transition array $2s^2-2s4p$ are the results of the relativistic random phase approximation (RRPA) calculations of Lin and Johnson.<sup>4</sup>

A few multiplet *f*-values for transitions involving the outer electron alone, 2s3s-2s3p and 2s3p-2s3d, have been interpolated along the isoelectronic sequence and assigned a low accuracy.

- <sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, At. Data Nucl. Data Tables 24, 111 (1979).
- <sup>2</sup>B. C. Fawcett, At. Data Nucl. Data Tables 30, 1 (1984); 33, 479 (1985).
- <sup>3</sup>A. K. Bhatia, U. Feldman, and J. F. Seely, At. Data Nucl. Data Tables 35, 449 (1986).
- 4C. D. Lin and W. R. Johnson, Phys. Rev. A 15, 1046 (1977).

Ni xxv: Allowed transitions

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | 8× | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|---------------------|----------------------------------|--|--|---|----------------------------|-----------------------|--|---|--|---|-----------------------|----------------------------|
| | | | | | | | | | | | | | |
| 1. | 2s²-2s2p | <sup>1</sup> S – <sup>3</sup> P° | | | | | | | | | | | |
| | | | [238.82] | 0 | 418720 | 1 | 3 | 0.82 | 0.0021 | 0.0017 | -2.68 | D | 1 |
| 2. | | <sup>1</sup> S - <sup>1</sup> P* | [117.91] | 0 | 848100 | 1 | 3 | 238 | 0.149 | 0.0578 | -0.827 | в | 1 |
| 3. | $2s2p-2p^{2}$ | <sup>8</sup> P° - <sup>3</sup> P | 145.92 | 486870 | 1172200 | 9 | 9 | 150 | 0.0479 | 0.207 | -0.366 | в | 1 |
| | | | [151.91]
[135.95]
[165.34]
[158.84]
[126.73]
[128.85] | 549500
418720
549500
418720
418720
378190 | 1207800
1154300
1154300
1048300?
1207800
1154300 | 5
3
5
3
3
1 | 5
3
1
5
3 | 76.6
51.2
48.8
138
70.0
83.7 | 0.0265
0.0142
0.0120
0.0174
0.0281
0.0625 | 0.0663
0.0191
0.0327
0.0273
0.0352
0.0265 | $\begin{array}{r} -0.878 \\ -1.371 \\ -1.222 \\ -1.282 \\ -1.074 \\ -1.204 \end{array}$ | B
B
B
B
B | 1
1
1
1
1
1 |
| 4. | | <sup>3</sup> P° – <sup>1</sup> D | | | | | | | | | | | |
| | | | [120.47]
[104.07] | 549500
418720 | 1379600
1379600 | 5
3 | 5
5 | 77
7.4 | 0.0167
0.0020 | 0.0331
0.0021 | -1.078
-2.22 | C
D | 1
1 |
| 5. | | <sup>1</sup> P° - <sup>3</sup> P | | | | | | | | | | | |
| | | | [278.01]
[326.58]
[499.50] | 848100
848100
848100 | 1207800
1154300
1048300? | 3
3
3 | 5
3
1 | 5.7
0.13
0.24 | $\begin{vmatrix} 0.011 \\ 2.1(-4)^{a} \\ 3.0(-4) \end{vmatrix}$ | 0.030
6.8(-4)
0.0015 | $-1.48 \\ -3.20 \\ -3.05$ | D
E
E | 1
1
1 |
| 6. | | <sup>1</sup> P° - <sup>1</sup> D | [188.15] | 848100 | 1379600 | 3 | 5 | 59.1 | 0.0523 | 0.0972 | -0.804 | в | 1 |
| 7. | | <sup>1</sup> P° – <sup>1</sup> S | [130.99] | 848100 | 1611500 | 3 | 1 | 399 | 0.0342 | 0.0442 | -0.989 | в | 1 |
| 8. | 2s²–2s3p | <sup>1</sup> S - <sup>3</sup> P° | | | | | | | | | | | |
| | | | [9.39] | 0 | 10650000 | 1 | 3 | 6.6(+4) | 0.26 | 0.0080 | -0.59 | C - | 2 |
| 9. | | <sup>1</sup> S – <sup>1</sup> P° | [9.34] | 0 | 10707000 | 1 | 3 | 1.1(+5) | 0.45 | 0.014 | -0.35 | C- | 2 |
| 10. | 2s2p-2p3p | <sup>3</sup> P° - <sup>3</sup> D | | | | | | | | | | | |
| | | | [9.31]
[9.32]
[9.27]
[9.43]
[9.31] | 549500
418720
378190
549500
418720 | 11296000
11153000
[11162000]
11153000
[11162000] | 5
3
1
5
3 | 7
5
3
5
3 | 8.2(+4)7.8(+4)2.2(+4)15004.1(+4) | 0.15
0.17
0.084
0.0020
0.053 | 0.023
0.016
0.0026
3.1(-4)
0.0049 | $-0.12 \\ -0.29 \\ -1.08 \\ -2.00 \\ -0.80$ | C–
C–
D
D | 2
2
2
2
2
2 |
| 11. | | <sup>3</sup> P° - <sup>3</sup> P | | | | | | | | | | | |
| | | | [9.30]
[9.30]
[9.19] | 549500
418720
418720 | 11306000
[11173000]
11306000 | 5
3
3 | 5
1
5 | 6.9(+4)
9.3(+4)
1600 | 0.090
0.040
0.0033 | 0.014
0.0037
3.0(-4) | -0.35
-0.92
-2.00 | C
D
D | 2
2
2 |
| 12. | | <sup>1</sup> P° - <sup>1</sup> P | [9.77] | 848100 | [11080000] | 3 | 3 | 1.7(+4) | 0.025 | 0.0024 | -1.12 | D | 2 |
| 13. | | <sup>1</sup> P° – <sup>3</sup> D | | | 1 | | | | | | | | |
| | | | [9.70] | 848100 | [11162000] | 3 | 3 | 1.8(+4) | 0.025 | 0.0024 | -1.12 | D | 2 |
| 14. | | <sup>1</sup> P° - <sup>3</sup> P | | | | | | | | | | | |
| | | | [9.56]
[9.56] | 848100
848100 | 11306000
[11313000] | 3
3 | 5
3 | 3.4(+4)
5.1(+4) | 0.077
0.070 | 0.0073
0.0066 | -0.64
-0.68 | D
C- | 2
2 |

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Ni xxv: Allowed transitions - Continued

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | <i>E</i> <sub>k</sub>
(cm <sup>-1</sup>) | g i | ₿k | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fix | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|-----------------------|----------------------------------|----------|------------------------------|--|------------|----|--|--------|---------------|--------|---------------|--------|
| | | | | | | | | | | | | | |
| 15. | | <sup>1</sup> P° - <sup>1</sup> D | [9.49] | 848100 | [11381000] | 3 | 5 | 8.9(+4) | 0.20 | 0.019 | -0.22 | C | 2 |
| 16. | | <sup>1</sup> P° – <sup>1</sup> S | [9.42] | 848100 | [11460000] | 3 | 1 | 9.0(+4) | 0.040 | 0.0037 | -0.92 | D | 2 |
| 17. | $2s^2 - 2s4p$ | <sup>1</sup> S - <sup>3</sup> P° | | | | | | | | | | | |
| | | | | | | 1 | 3 | | 0.032 | | _149 | р | 4 |
| | | | | | | | | | 0.15 | | 0.00 | | |
| 18. | | ·S - ·P | | 1 | | | 0 | | 0.15 | | -0.82 | | 4 |
| 19. | 2s 2p -2s 3s | <sup>3</sup> P° – <sup>3</sup> S | 10.02 | 486870 | [10465000] | 9 | 3 | 5.2(+4) | 0.026 | 0.0078 | -0.63 | D | 2 |
| | | | [10.09] | 549500 | [10465000] | 5 | 3 | 2.8(+4) | 0.026 | 0.0043 | -0.89 | D | 2 |
| | | | [9.95] | 418720 | [10465000] | 3 | 3 | 1.8(+4) | 0.026 | 0.0026 | -1.11 | D | 2 |
| | | | [9.91] | 378190 | [10465000] | 1 | 3 | 6100 | 0.027 | 8.8(-4) | -1.57 | D | 2 |
| 20. | | <sup>1</sup> P° – <sup>1</sup> S | [10.32] | 848100 | [10536000] | 3 | 1 | 2.1(+4) | 0.011 | 0.0011 | -1.48 | D | 2 |
| 21. | 2p <sup>2</sup> -2p3s | <sup>3</sup> P - <sup>3</sup> P° | 10.11 | 1172200 | [11062000] | 9 | 9 | 3.5(+4) | 0.053 | 0.016 | -0.32 | D | 2 |
| | | | [20.02] | 1207800 | (111900001 | 5 | 5 | $21(\pm 4)$ | 0.032 | 0.0053 | 0.80 | D | 2 |
| | | | [10.03] | 1154300 | [10983000] | 3 | 3 | 6000 | 0.0093 | 9.3(-4) | -1.55 | D | 2 |
| | | | [10.23] | 1207800 | [10983000] | 5 | 3 | 1.6(+4) | 0.015 | 0.0025 | -1.12 | Ď | 2 |
| | | | [10.20] | 1154300 | [10963000] | 3 | 1 | 3.1(+4) | 0.016 | 0.0016 | -1.32 | D | 2 |
| | | | [10.02] | 1154300 | [11130000] | 3 | 5 | 1.5(+4) | 0.037 | 0.0037 | -0.95 | D | 2 |
| | | | [10.07] | 1048300? | [10983000] | 1 | 3 | 1.2(+4) | 0.055 | 0.0018 | -1.26 | D | 2 |
| 22. | | <sup>1</sup> D - <sup>1</sup> P° | [10.21] | 1379600 | [11176000] | 5 | 3 | 2.8(+4) | 0.026 | 0.0044 | -0.89 | D | 2 |
| 23. | | <sup>1</sup> S - <sup>1</sup> P° | [10.46] | 1611500 | [11176000] | 1 | 3 | 1.1(+4) | 0.054 | 0.0019 | -1.27 | D | 2 |
| 24. | 2s2p-2s3d | <sup>3</sup> P° - <sup>3</sup> D | 9.69 | 486870 | 10805000 | 9 | 15 | 3.09(+5) | 0.72 | 0.208 | 0.81 | C– | 2 |
| | | | [9 74] | 549500 | 10813000 | 5 | 7 | 3.0(+5) | 0.60 | 0.096 | 0.48 | C- | 2 |
| | | | [9,63] | 418720 | 10800000 | 3 | 5 | 2.4(+5) | 0.55 | 0.052 | 0.22 | C- | 2 |
| | | | [9.60] | 378190 | 10794000 | 1 | 3 | 1.8(+5) | 0.75 | 0.024 | -0.12 | C- | 2 |
| 1 | | | [9.76] | 549500 | 10800000 | 5 | 5 | 7.7(+4) | 0.11 | 0.018 | -0.26 | C- | 2 |
| | | | [9.64] | 418720 | 10794000 | 3 | 3 | 1.3(+5) | 0.18 | 0.017 | -0.27 | C- | 2 |
| | | | [9.76] | 549500 | 10794000 | 5 | 3 | 8400 | 0.0072 | 0.0012 | -1.44 | C- | 2 |
| 25. | | <sup>1</sup> P° - <sup>1</sup> D | [9.97] | 848100 | 10880000 | 3 | 5 | 2.5(+5) | 0.61 | 0.060 | 0.26 | C- | 2 |
| 26. | $2p^2 - 2p 3d$ | $^{3}P - ^{3}F^{\circ}$ | | | | ļ | | | | 2 | | | |
| | | | [9.94] | 1207800 | 11271000 | 5 | 7 | 1.29(+5) | 0.268 | 0.0438 | 0.127 | C- | 2 |
| 27. | | <sup>3</sup> P - <sup>3</sup> D° | 9.82 | 1172200 | 11357000 | 9 | 15 | 2.84(+5) | 0.68 | 0.199 | 0.79 | C- | 2 |
| 1 | | | [9.78] | 1207800 | 11437000 | 5 | 7 | 2.9(+5) | 0.59 | 0.095 | 0.47 | C- | 2 |
| | | | [9.87] | 1154300 | 11283000 | 3 | 5 | 2.03(+5) | 0.493 | 0.0481 | 0.170 | C- | 2 |
| | | | [9.76] | 1048300? | 11296000 | 1 | 3 | 3.03(+5) | 1.30 | 0.0418 | 0.114 | C- | 2 |
| | | | [9.93] | 1207800 | 11283000 | 5 | 5 | 2.2(+4) | 0.032 | 0.0052 | -0.80 | D | 2 |
| | | | [9.86] | 1154300 | 11296000 | 3 | 3 | 5.7(+4) | 0.083 | 0.0081 | -0.60 | C- | 2 |
| | | | [9.91] | 1207800 | 11296000 | 5 | 3 | 3800 | 0.0034 | 5.5(-4) | -1.77 | D | 2 |
| 28. | | <sup>3</sup> P - <sup>1</sup> D° | | | | | | | | | | | |
| | | | 10 001 | 1007000 | 11/09000 | F | 5 | 4.4(1.4) | 0.064 | 0.010 | _0.49 | C_ | 2 |
| | | | [9.80] | 1154900 | 11408000 | 9 | 5 | 13(15) | 0.30 | 0.029 | _0.45 | D | 2 |
| | | | [9.10] | 1104000 | 11400000 | | ' | 1.0(+0) | 0.00 | 0.020 | 0.00 | | - |

101213

4.48

1.948

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Ni xxv: Allowed transitions - Continued

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | g i | g. | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | f ik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|---------------------|----------------------------------|--|---|--|-----------------------|-----------------------|--|--|--|---|---------------------------|----------------------------|
| 29. | | <sup>3</sup> P – <sup>3</sup> P° | | | | | | | | | | | |
| | | | [9.76]
[9.71]
[9.76]
[9.71]
[9.71] | 1207800
1154300
1207800
1154300
1154300 | 11456000
11456000
11456000
11456000
11456000 | 5
3
5
3
3 | 5
3
3
1
5 | 1.3(+5)1.8(+5)7.5(+4)2.3(+5)2.7(+4) | 0.19
0.25
0.064
0.11
0.063 | 0.031
0.024
0.010
0.011
0.0060 | -0.02
-0.12
-0.49
-0.48
-0.72 | C-
C-
C-
C-
D | 2
2
2
2
2
2 |
| 30. | | ${}^{1}D - {}^{3}F^{\circ}$ | | | | | | | | | | | |
| | | | [10.09] | 1379600 | [11295000] | 5 | 5 | 7900 | 0.012 | 0.0020 | -1.22 | D | 2 |
| 31. | | <sup>1</sup> D - <sup>1</sup> D° | [9.97] | 1379600 | 11408000 | 5 | 5 | 2.8(+4) | 0.042 | 0.0069 | -0.68 | C- | 2 |
| 32. | | <sup>1</sup> D - <sup>3</sup> P° | | | | | | | | | | | |
| | | | [9.92] | 1379600 | 11456000 | 5 | 5 | 1.3(+5) | 0.19 | 0.031 | -0.02 | с- | 2 |
| 33. | | <sup>1</sup> D - <sup>1</sup> P° | [9.85] | 1379600 | [11535000] | 5 | 3 | 1.7(+4) | 0.015 | 0.0024 | -1.12 | D | 2 |
| 34. | | <sup>1</sup> D - <sup>1</sup> F° | [9.86] | 1379600 | 11525000 | 5 | 7 | 4.8(+5) | 0.98 | 0.16 | 0.69 | C- | 2 |
| 35. | | <sup>1</sup> S – <sup>1</sup> P° | [10.08] | 1611500 | [11535000] | 1 | 3 | 2.80(+5) | 1.28 | 0.0425 | 0.107 | C | 2 |
| 36. | 2s3s-2s3p | <sup>3</sup> S - <sup>3</sup> P° | | | | 3 | 9 | | 0.11 | | -0.48 | D | interp. |
| 37. | | <sup>1</sup> S - <sup>1</sup> P* | | | | 1 | 3 | | 0.050 | | -1.30 | Е | interp. |
| 38. | 2s3p-2s3d | <sup>3</sup> P° - <sup>3</sup> D | | | | 9 | 15 | | 0.025 | | -0.65 | Е | interp. |
| 39. | | <sup>1</sup> P* - <sup>1</sup> D | | | | 3 | 5 | | 0.043 | | -0.89 | Е | interp. |

"The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

Ni xxv

Forbidden Transitions

Transition probabilities for magnetic dipole and electric quadrupole transitions within the 2s2p and $2p^2$ configurations were calculated by Feldman *et al.*<sup>1</sup> using scaled Thomas-Fermi wavefunctions with allowance for configuration interaction and relativistic effects. We modified their transition probability data by the application of experimental wavelengths, i.e., we first converted their *A*-values into line strength data utilizing their theoretical transition energies and then reconverted the line strengths into *A*-values with wavelengths derived from experimental data. This approach should normally yield transition probabilities that are more accurate than those based on theoretically determined wavelengths.

The transition probability for the one electric quadrupole transition listed, which is relatively strong compared to other E2 transitions, has been interpolated from the data of Anderson and Anderson<sup>2</sup> and Glass<sup>3,4</sup> for neighboring ions of the Be sequence. This A-value exhibits a smooth nuclear charge dependence.

- <sup>1</sup>U. Feldman, G. A. Doschek, Ch.-Ch. Cheng, and A. K. Bhatia, J. Appl. Phys. **51**, 190 (1980).
- <sup>2</sup>E. K. Anderson and E. M. Anderson, Opt. Spectrosc. (USSR) **52**, 478 (1982).
- <sup>3</sup>R. Glass, Z. Phys. A 320, 545 (1985).
- <sup>4</sup>R. Glass, Astrophys. Space Sci. 92, 307 (1983).

| No. | Transition
Array | Multiplet | λ
(Å) | <i>E<sub>i</sub></i>
(cm <sup>-1</sup>) | $\frac{E_k}{(\mathrm{cm}^{-1})}$ | 8 i | 8 k | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Асси-
гасу | Source |
|-----|---------------------|-----------------------------------|----------------------|---|----------------------------------|------------|--------|-----------------------|---------------------------------------|---------------------------|---------------|---------------------------|
| 1. | 2s2p-2s2p | <sup>3</sup> P° – <sup>3</sup> P° | | | | | | | | | | |
| | | | [764.64]
[2466.6] | 418720
378190 | 549500
418720 | 3
1 | 5
3 | M1
M1 | 2.91(+4) <sup>a</sup>
1160 | 2.41
1.93 | C+
C+ | 1 |
| 2. | | <sup>3</sup> P° – <sup>1</sup> P° | | | | | | | | | | |
| | | | [334.90]
[232.89] | 549500
418720 | 848100
848100 | 533 | 333 | M1
M1
E2 | 2.1(+4) 3.6(+4) 100 6.5(+4) | 0.087
0.050
1.2(-4) | D
D
D- | 1
1
<i>interp</i> . |
| 3. | $2p^2 - 2p^2$ | <sup>3</sup> P – <sup>3</sup> P | [212.81] | 578190 | 848100 | 1 | 5 | IVIII | 0.5(+4) | 0.070 | | 1 |
| | | | [1869.2]
[943.40] | 1154300
1048300 | 1207800
1154300 | 3 | 5
3 | M1
M1 | 1410
1.96(+4) | 1.71
1.83 | с
с | 1
1 |
| 4. | | <sup>3</sup> P - <sup>1</sup> D | | | | | | | | | | |
| | | | [582.07]
[443.85] | 1207800
1154300 | 1379600
1379600 | 5
3 | 5
5 | M1
M1 | 4.4(+4)
4.9(+4) | 1.6
0.79 | C
D+ | 1 |
| 5. | | <sup>3</sup> P - <sup>1</sup> S | | | | | | | | | | |
| | | | [218.72] | 1154300 | 1611500 | 3 | 1 | M 1 | 4.4(+5) | 0.17 | D | 1 |

Ni xxv: Forbidden transitions

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

Ni xxvı

Li Isoelectronic Sequence

Ground State: $1s^22s^2S_{1/2}$

Ionization Energy: $2399.2 \text{ eV} = 19351000 \text{ cm}^{-1}$

Allowed Transitions

Transition probabilities for the strongest inner-shell transitions to doubly excited n = 2 states are taken from the multiconfiguration Dirac-/fock (MCDF) calculations of Hata and Grant.<sup>1</sup> Their results are in good agreement with the Z-expansion perturbation calculations of Vainshtein and Safronova,<sup>2</sup> who included relativistic corrections at the level of the Pauli approximation.

Oscillator strengths for lines of the principal (2s-2p) resonance multiplet are the results of the MCDF calculations of Cheng *et al.*,<sup>3</sup> which include a perturbative treatment of the Breit interaction and the Lamb shift.

The results of the Hartree-XR (Hartree-Fock with statistical exchange and relativistic effects) calculations

of Fawcett *et al.*<sup>4</sup> are tabulated for the 2p-3s and 2p-3d transitions.

The f-value for the 3d-4f transition was taken from a study of systematic trends along isoelectronic sequences by Smith and Wiese.<sup>5</sup> The tabulated data for the remaining transitions were taken from the theoretical analysis of Martin and Wiese,<sup>6</sup> which was based on a generalized study of systematic trends for several spectral series of the lithium isoelectronic sequence.

Results of the relativistic Hartree-Fock calculations of Kim and Desclaux<sup>7</sup> for several ions of the Li sequence were incorporated into the data of Ref. 6 for the 2s-3p transitions. For all other transitions for which the results

of Ref. 6 are quoted here, no relativistic calculations were available. However, the relativistic calculations of Younger and Weiss<sup>8</sup> for the hydrogen isoelectronic sequence provide a means of assessing the magnitude of relativistic corrections, since the Li sequence is very similar in structure to the H sequence. For those transitions for which relativistic effects were estimated to be significant (specifically, whenever the ratio of the weighted relativistic hydrogenic *f*-values gf_{ik} of any two lines within a multiplet was found to deviate from the corresponding *LS*-coupling line strength ratio by more than 5% for the appropriate value of the nuclear charge *Z*), the *f*-values were excluded from the compilation. A more detailed discussion of this comparison is given in Ref. 6.

Transition probability data are available for numerous transitions involving doubly excited states with the spectator electron occupying the n=3 shell, or higher.<sup>9</sup> These have not been tabluated, however, since they be-

long to, or are very close to belonging to, the unresolved satellites of the helium-like ion.

- <sup>1</sup>J. Hata and I. P. Grant, Mon. Not. R. Astron. Soc. 211, 549 (1984).
- <sup>2</sup>L. A. Vainshtein and U. I. Safronova, At. Data Nucl. Data Tables 21, 49 (1978).
- <sup>3</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, At. Data Nucl. Data Tables 24, 111 (1979).
- <sup>4</sup>B. C. Fawcett, A. Ridgeley, and T. P. Hughes, Mon. Not. R. Astron. Soc. **188**, 365 (1979).
- <sup>5</sup>M. W. Smith and W. L. Wiese, Astrophys. J. Suppl. Ser. 23, No. 196, 103 (1971).
- <sup>6</sup>G. A. Martin and W. L. Wiese, J. Phys. Chem. Ref. Data 5, 537 (1976).
- <sup>7</sup>Y.-K. Kim and J. P. Desclaux, Phys. Rev. Lett. 36, 139 (1976) and private communication.
- <sup>8</sup>S. M. Younger and A. W. Weiss, J. Res. Nat. Bur. Stand., Sect. A 79, 629 (1975).
- <sup>9</sup>L. A. Vainshtein and U. I. Safronova, At. Data Nucl. Data Tables 25, 311 (1980).

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | gi | g, | $A_{ki} \ (10^8 \ { m s}^{-1})$ | fik | S
(at. u.) | log <i>gf</i> | Accu-
racy | Source |
|-----|--|---|------------------------------|------------------------------|----------------------------------|-------------|-------------|---------------------------------|-----------------------|-----------------------------|--------------------------|---------------|-------------|
| 1. | 1s <sup>2</sup> 2s-
1s(<sup>2</sup> S)2s2p(<sup>3</sup> P°) | <sup>2</sup> S - <sup>2</sup> P° | | | | | | | | | | | |
| | | | 1.5996 | 0 | 62516000 | 2 | 2 | $2.7(+6)^{a}$ | 0.10 | 0.0011 | 0.68 | с | 1 |
| 2. | $\frac{1s^{2}2s}{1s(^{2}S)2s2p(^{1}P^{\circ})}$ | <sup>2</sup> S - <sup>2</sup> P° | | | | | | | | | | | |
| | | | 1.5935 | 0 | 62755000 | 2 | 2 | 4.0(+6) | 0.15 | 0.0016 | -0.52 | с | 1 |
| 3. | $1s^{2}2p-1s^{2}p^{2}$ | <sup>2</sup> P° – <sup>2</sup> P | | | | | | | | | | | |
| | | | 1.5973
1.5982
[1.6036] | 604520
426990
604520 | 63211000
62997000
62997000 | 4
2
4 | 4
2
2 | 8.1(+6)
7.3(+6)
2.1(+6) | 0.31
0.28
0.040 | 0.0065
0.0029
8.5(-4) | $0.09 \\ -0.25 \\ -0.79$ | C
C
C | 1
1
1 |
| 4. | | ${}^{2}\mathbf{P}^{\circ} - {}^{2}\mathbf{D}$ | | | | | | | | | | | |
| | | | $1.6005 \\ 1.5977$ | 604520
426990 | 63085000
63017000 | 4
2 | 6
4 | 2.7(+6)
4.4(+6) | 0.16
0.34 | 0.0033
0.0035 | $-0.21 \\ -0.17$ | C
C | 1
1 |
| 5. | | <sup>2</sup> P° – <sup>2</sup> S | | | | | | | 1 | | | | |
| | | | 1.5930 | 604520 | 63380000 | 4 | 2 | 3.4(+6) | 0.065 | 0.0014 | -0.59 | c | 1 |
| 6. | 2s-2p | <sup>2</sup> S – <sup>2</sup> P° | 183.37 | 0 | 545340 | 2 | 6 | 42.0 | 0.0635 | 0.0767 | -0.896 | B+ | 3 |
| | | | 165.42?
234.20 | 0
0 | 604520
426990 | 2
2 | 4
2 | 57.5
19.9 | 0.0472
0.0164 | 0.0514
0.0253 | -1.025
-1.484 | B+
B+ | 3
3 |
| 7. | 2s-3p | <sup>2</sup> S – <sup>2</sup> P° | 9.074 | 0 | 11020000 | 2 | 6 | 1.01(+5) | 0.375 | 0.0224 | -0.125 | B+ | 6 |
| | | | 9.061
9.105 | 0
0 | 1104000
10980000 | 2
2 | 4
2 | 9.99(+4)
1.04(+5) | 0.246
0.129 | 0.0147
0.00773 | $-0.308 \\ -0.588$ | B+
B+ | 6
6 |
| 8. | 2s-4p | <sup>2</sup> S - <sup>2</sup> P° | | | | 2 | 6 | | 0.101 | | -0.695 | C+ | 6 |
| 9. | 2s-5p | <sup>2</sup> S - <sup>2</sup> P° | | | | 2 | 6 | | 0.040 | | -1.10 | C+ | 6 |
| | 1 | | | | | 1 | | ł | | 1 | 1 | | |

Ni xxvi: Allowed transitions

Ni xxvi: Allowed transitions -- Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k
(cm <sup>-1</sup>) | B i | 8k | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | f <sub>ik</sub> | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|------------------------|---|------------------------|------------------------------|----------------------------------|-------------|-------------|--|-------------------------|----------------------------|-------------------------|---------------|-------------|
| | | | | | | | | | | | | | |
| 10. | 2s-6p | <sup>2</sup> S – <sup>2</sup> P° | | | | 2 | 6 | | 0.0213 | | -1.371 | C+ | 6 |
| 11. | 2s-7p | <sup>2</sup> S – <sup>2</sup> P° | | | | 2 | 6 | | 0.0125 | | | C+ | 6 |
| 12. | 2p-3s | <sup>2</sup> P° – <sup>2</sup> S | 9.676 | 545340 | 10880000 | 6 | 2 | 3.8(+4) | 0.018 | 0.0034 | -0.97 | с | 4 |
| | | | 9.732
[9.567] | 604520
426990 | 10880000
10880000 | 4
2 | 2
2 | 2.5(+4)
1.3(+4) | 0.018
0.018 | 0.0023
0.0011 | -1.14
-1.44 | с
с | 4
4 |
| 13. | 2p-3d | <sup>2</sup> P° – <sup>2</sup> D | 9.483 | 545340 | 11090000 | 6 | 10 | 3.02(+5) | 0.68 | 0.127 | 0.61 | с | 4 |
| - | | | 9.535
9.390
9.55 | 604520
426990
604520 | 11090000
11080000
11080000 | 4
2
4 | 6
4
4 | 2.96(+5)
2.59(+5)
5.0(+4) | 0.605
0.685
0.068 | 0.0760
0.0424
0.0086 | 0.384
0.137
-0.57 | C+
C+
C | 4
4
4 |
| 14. | 2p-4d | <sup>2</sup> P* - <sup>2</sup> D | | | - | 6 | 10 | | 0.12 | | -0.14 | C+ | 6 |
| 15. | 2p-5d | <sup>2</sup> P° – <sup>2</sup> D | | | | 6 | 10 | | 0.0450 | | -0.569 | C+ | 6 |
| 16. | 2p-6d | <sup>2</sup> P° - <sup>2</sup> D | | | | 6 | 10 | | 0.0220 | | -0.879 | C+ | 6 |
| 17. | 2p-7d | <sup>2</sup> P° – <sup>2</sup> D | | | | 6 | 10 | | 0.0125 | | -1.125 | C+ | 6 |
| 18. | 3s-4p | <sup>2</sup> S - <sup>2</sup> P° | | | | 2 | 6 | | 0.45 | | -0.05 | с | 6 |
| 19. | 3s-5p | <sup>2</sup> S – <sup>2</sup> P° | | | | 2 | 6 | | 0.108 | | -0.67 | с | 6 |
| 20. | 3s-6p | <sup>2</sup> S – <sup>2</sup> P° | | | | 2 | 6 | | 0.048 | | -1.02 | с | 6 |
| 21. | 3s-7p | <sup>2</sup> S – <sup>2</sup> P° | | | | 2 | 6 | | 0.0250 | | -1.301 | с | 6 |
| 22. | 3p-4d | ²P° – ²D | | | | 6 | 10 | | 0.60 | | 0.56 | в | 6 |
| 23. | 3p-5d | <sup>2</sup> P° – <sup>2</sup> D | | | | 6 | 10 | | 0.138 | | -0.082 | C+ | 6 |
| 24. | 3p-6d | <sup>2</sup> P° – <sup>2</sup> D | | | | 6 | 10 | | 0.0558 | | -0.475 | C+ | 6 |
| 25. | 3p-7d | <sup>2</sup> P° - <sup>2</sup> D | | | | 6 | 10 | | 0.0289 | | 0.761 | C+ | 6 |
| 26. | 3 <i>d</i> -4 <i>f</i> | <sup>2</sup> D – <sup>2</sup> F° | | | | 10 | 14 | | 1.00 | | 1.000 | В | 5 |
| 27. | 4s-5p | <sup>2</sup> S – <sup>2</sup> P ° | | | | 2 | 6 | | 0.483 | | -0.015 | с | 6 |
| 28. | 4s-6p | ${}^{2}S - {}^{2}P^{*}$ | | | | 2 | 6 | | 0.129 | | -0.59 | с | 6 |
| 29. | 4s-7p | <sup>2</sup> S – <sup>2</sup> P° | | | | 2 | 6 | | 0.056 | | -0.95 | С | 6 |
| 30. | 4p-5d | $^{2}P^{\circ} - ^{2}D$ | | | | 6 | 10 | | 0.586 | | 0.546 | C+ | 6 |
| 31. | 4p-6d | <sup>2</sup> P° - <sup>2</sup> D | | | | 6 | 10 | | 0.143 | | -0.067 | C+ | 6 |
| 32. | 4p-7d | <sup>2</sup> P° – <sup>2</sup> D | | | | 6 | 10 | | 0.0618 | | -0.431 | C+ | 6 |

Ni xxvi

Forbidden Transitions

The single magnetic dipole transition within the $1s^22p$ configuration has the line strength of 1.33 in the absence of relativistic effects in the wavefunctions.<sup>1</sup> It is estimated that these effects are negligible, since comprehensive relativistic calculations by Cheng *et al.*<sup>2</sup> for the analogous transition in the $1s^22s^22p$ configuration of the boron sequence show that such relativistic corrections are negligible until much more highly charged ions.

The listed transition probability data are also expected to be quite accurate since the energy levels are derived from experimental data.

An electric quadrupole transition at the same wavelength is estimated to be of negligible strength, as calculated by Bhatia<sup>3</sup> for this transition in the case of Mn XXIII. (He obtains a ratio of about 10^{-3} for the ratio of E2 to M1 line strengths).

References

- <sup>1</sup>W. L. Wiese, M. W. Smith, and B. M. Miles, "Atomic Transition Probabilities", Vol. 11, NSRDS-NBS 22, U.S. Govt. Print. Office, Washington, DC 1969.
- <sup>2</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, At. Data Nucl. Data Tables 24, 111 (1979).
- <sup>3</sup>A. K. Bhatia, private communication (1986).

Ni XXVI: Forbidden transitions

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | $\frac{E_k}{(\mathrm{cm}^{-1})}$ | g i | g. | Type of
transition | $egin{array}{c} egin{array}{c} S
(at. u.) | Accu-
racy | Source | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1. | 2p-2p | <sup>2</sup> P° – <sup>2</sup> P° | [563.38] | [427180] | [604680] | 2 | 4 | M 1 | 5.02(+4) <sup>a</sup> | 1.33 | в | interp. |

Ni xxvii

He Isoelectronic Sequence

Ground State: $1s^{2} S_0$

Ionization Energy: $10288.8 \text{ eV} = 82984000 \text{ cm}^{-1}$

Allowed Transitions

| List of tabulated line |
|------------------------|
|------------------------|

| Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. | Wavelength (Å) | No. |
|----------------|------|----------------|-----|----------------|-----|----------------|-----|
| 1.2534 | 19 | 1.543 | 3,9 | 6.4225 | 25 | 25.500 | 46 |
| 1.2537 | 18 | 1.544 | 9 | 6.5224 | 26 | 25.907 | 47 |
| 1.2824 | 17 | 1.546 | 11 | 6.5520 | 33 | 53.879 | 57 |
| 1.2831 | 16 | 1.547 | 11 | 6.6779 | 34 | 54.177 | 58 |
| 1.3500 | 15 | 1.549 | 5 | 8.6080 | 23 | 55.298 | 60 |
| 1.3516 | 14 | 1.550 | 11 | 8.7475 | 24 | 56.016 | 61 |
| 1.531 | 4 | 1.551 | 7 | 8.8772 | 29 | 168.5 | 21 |
| 1.534 | 13 | 1.558 | 8 | 9.0740 | 30 | 228.0 | 20 |
| 1.537 | 6,10 | 1.5883 | 2 | 17.084 | 43 | 315.5 | 22 |
| 1.538 | 3 | 1.5963 | 1 | 17.241 | 44 | 361.9 | 20 |
| 1.539 | 9 | 5.7489 | 27 | 17.356 | 50 | 388.7 | 20 |
| 1.540 | 9 | 5.8352 | 28 | 17.590 | 51 | | |
| 1.541 | 12 | 5.8471 | 37 | 24.819 | 41 | | |
| 1.542 | 3,9 | 5.9524 | 38 | 25.036 | 42 | | |

Oscillator strengths for transitions of the $1s^2-1s2p$ array are taken from the results of Drake,<sup>1</sup> who incorporated accurate nonrelativistic matrix elements and Dirac hydrogenic matrix elements into a Z-expansion technique in order to provide f-values which would accurately reflect correlation effects for low-Z ions and relativistic effects for high-Z ions of the helium isoelectronic sequence. The f-values for the $1s^{2}$ 1S - 1snp $3P^{\circ}$ (n = 3-5) transitions were interpolated from results of the relativistic random phase approximation (RRPA) calculations of Johnson and Lin.<sup>2</sup> For other s-p and p-s transitions, we tabulate the published RRPA data of Lin et al.<sup>3,4</sup>

The charge expansion results of Laughlin<sup>5</sup> are given for various p-d and d-p transitions, as well as transitions between 4d and 4f levels. For those multiplets involving no change in principal quantum number (3p-3d, 4p-4d, 4d-4f) the f-values should be considered rather uncertain, since they are sensitive to energy differences. Oscillator strengths for the 2p-3d transitions, and for 1s3p $^{3}P^{\circ} - 1s3d$ <sup>3</sup>D, were interpolated from the variational calculations of Weiss.<sup>6</sup> Both of these calculations indicatethat, unlike the triplets, the nd <sup>1</sup>D energy levels (n = 3,4) lie below the np <sup>1</sup>P° levels, and the 4f <sup>1</sup>F° lies below the 4d <sup>1</sup>D.

Brown and Cortez<sup>7</sup> have provided f-values for numerous d-f and f-d transitions for the isoelectronic sequence by fitting Z-expansion formulas to the results of variational calculations for the low-Z ions. Their results for transitions between the lower-lying D and F° terms are tabulated here.

Transition probabilities for the stronger transitions involving the doubly excited n=2 states are taken from the comprehensive, charge expansion perturbation theory calculations of Vainshtein and Safronova.<sup>8</sup> Numerous data are also available for transitions involving doubly excited states where the spectator electron has principal quantum number n=3.<sup>9</sup> However, these data are not tabulated here, since most of the transitions are very close to belonging to the unresolved satellites of the H-like ions, if they do not in fact do so.

- <sup>1</sup>G. W. F. Drake, Phys. Rev. A 19, 1387 (1979).
- <sup>2</sup>W. R. Johnson and C. D. Lin, Phys. Rev. A 14, 565 (1976).
- <sup>3</sup>C. D. Lin, W. R. Johnson, and A. Dalgarno, Astrophys. J. 217, 1011 (1977).
- <sup>4</sup>C. D. Lin, W. R. Johnson, and A. Dalgarno, Phys. Rev. A 15, 154 (1977).
- <sup>5</sup>C. J. Laughlin, J. Phys. B 6, 1942 (1973).
- <sup>6</sup>A. W. Weiss, J. Res. Nat. Bur. Stand., Sect. A 71, 163 (1967).
- <sup>7</sup>R. T. Brown and J.-L. M. Cortez, Astrophys. J. 176, 267 (1972).
- <sup>8</sup>L. A. Vainshtein and U. I. Safronova, At. Data Nucl. Data Tables 21, 49 (1978).
- <sup>9</sup>L. A. Vainshtein and U. I. Safronova, At. Data Nucl. Data Tables 25, 311 (1980).

Ni XXVII: Allowed transitions

| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | gi | ₿k | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log <i>gf</i> | Accu-
racy | Source |
|-----|-----------------------|--|--|--|--|----------------------------|----------------------------|---|---|---|--|--|----------------------------|
| 1. | 1s <sup>2</sup> -1s2p | <sup>1</sup> S - <sup>3</sup> P° | | | | | | | | | - | | |
| | | | [1.5963] | 0 | [62644200] | 1 | 3 | 7.70(+5)ª | 0.0883 | 4.64(-4) | -1.054 | в | 1 |
| 2. | | <sup>1</sup> S - <sup>1</sup> P° | [1.5883] | 0 | [62961500] | 1 | 3 | 6.02(+6) | 0.683 | 0.00357 | -0.166 | В | 1 |
| 3. | 1s 2s - 2s 2p | <sup>3</sup> S - <sup>3</sup> P° | 1.540 | [62367900] | [127300000] | 3 | 9 | 3.8(+6) | 0.41 | 0.0062 | 0.09 | с | 8 |
| | | | [1.538]
[1.542]
[1.543] | [62367900]
[62367900]
[62367900] | [127380000]
[127210000]
[127170000] | 3
3
3 | 5
3
1 | 3.9(+6)
3.6(+6)
3.8(+6) | 0.23
0.13
0.045 | 0.0035
0.0020
6.9(-4) | -0.16
-0.41
-0.87 | C
C
C | 8
8
8 |
| 4. | | <sup>3</sup> S - <sup>1</sup> P° | | | | | | | | | | | |
| | | | [1.531] | [62367900] | [127690000] | 3 | 3 | 2.0(+5) | 0.0070 | 1.1(-4) | -1.68 | D | 8 |
| 5. | | <sup>i</sup> S - <sup>3</sup> P° | | | | | | | | | | | |
| | | | [1.549] | [62644500] | [127210000] | 1 | 3 | 2.0(+5) | 0.022 | 1.1(-4) | -1.67 | D | 8 |
| 6. | | <sup>1</sup> S - <sup>1</sup> P° | [1.537] | [62644500] | [127690000] | 1 | 3 | 3.7(+6) | 0.39 | 0.0020 | -0.41 | с | 8 |
| 7. | $1s2p-2s^2$ | <sup>3</sup> P° – <sup>1</sup> S | | | | | | | | | | | |
| | | | [1.551] | [62644200] | [127130000] | 3 | 1 | 8.2(+5) | 0.0099 | 1.5(-4) | -1.53 | D | 8 |
| 8. | | <sup>1</sup> P° - <sup>1</sup> S | [1.558] | [62961500] | [127130000] | 3 | 1 | 6.5(+5) | 0.0079 | 1.2(-4) | -1.63 | D | 8 |
| 9. | $1s2p-2p^{2}$ | <sup>3</sup> P° - <sup>3</sup> P | 1.542 | [62732300] | [127600000] | 9 | 9 | 6.6(+6) | 0.236 | 0.0108 | 0.328 | с | 8 |
| | | | [1.542]
[1.540]
[1.544]
[1.543]
[1.539]
[1.539] | [62806500]
[62644200]
[62806500]
[62644200]
[62644200]
[62625200] | [127640000]
[127590000]
[127590000]
[127460000]
[127640000]
[127590000] | 5
3
5
3
3
1 | 5
3
3
1
5
3 | $3.5(+6) \\ 1.7(+6) \\ 3.2(+6) \\ 6.9(+6) \\ 2.6(+6) \\ 2.6(+6) \\ 2.6(+6)$ | 0.12
0.060
0.069
0.082
0.15
0.28 | 0.0032
9.2(-4)
0.0017
0.0013
0.0023
0.0014 | -0.20
-0.74
-0.46
-0.61
-0.34
-0.56 | C
C
C
C
C
C
C
C
C
C | 8
8
8
8
8
8 |
| 10. | | <sup>3</sup> P° - <sup>1</sup> D | | | | | | | | | | | |
| | | | [1.537] | [62806500] | [127860000] | 5 | 5 | 2.3(+6) | 0.081 | 0.0021 | -0.39 | с | 8 |
| 11. | | <sup>1</sup> P ° – <sup>3</sup> P | | | | | | | | | | | |
| | | | [1.546]
[1.547]
[1.550] | [62961500]
[62961500]
[62961500] | [127640000]
[127590000]
[127460000] | 3
3
3 | 5
3
1 | 1.6(+6)
2.1(+5)
1.2(+5) | 0.096
0.0075
0.0014 | 0.0015
1.2(-4)
2.2(-5) | -0.54
-1.65
-2.36 | C
D
D | 8
8
8 |
| 12. | | $^{1}P^{\circ} - ^{1}D$ | [1.541] | [62961500] | [127860000] | 3 | 5 | 5.5(+6) | 0.33 | 0.0050 | -0.01 | с | 8 |
| 13. | | <sup>1</sup> P° – <sup>1</sup> S | [1.534] | [62961500] | [128140000] | 3 | 1 | 6.9(+6) | 0.081 | 0.0012 | -0.61 | с | 8 |
| 14. | $1s^2 - 1s 3p$ | <sup>1</sup> S - <sup>3</sup> P <sup>o</sup> | | | | | | | | ĺ | | | |
| | | | [1.3516] | 0 | [73985000] | 1 | 3 | 2.4(+5) | 0.020 | 8.9(-5) | - 1.70 | Е | interp. |
| 15. | | <sup>1</sup> S – <sup>1</sup> P° | [1.3500] | 0 | [74076300] | 1 | 3 | 1.63(+6) | 0.134 | 5.96(-4) | -0.873 | в | 3 |
| 16. | $1s^2-1s4p$ | <sup>1</sup> S - <sup>3</sup> P° | | | | | | | | | | | |
| | | | [1.2831] | 0 | [77938200] | 1 | 3 | 1.0(+5) | 0.0074 | 3.1(-5) | -2.13 | Е | interp. |
| 17. | | ${}^{1}S - {}^{1}P^{\circ}$ | [1.2824] | 0 | [77976200] | 1 | 3 | 6.38(+5) | 0.0472 | 1.99(-4) | -1.326 | В | 3 |

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Ni XXVII: Allowed transitions - Continued

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| No. | Transition
Array | Multiplet | λ
(Å) | E_i
(cm <sup>-1</sup>) | $E_{\mathbf{k}}$ (cm <sup>-1</sup>) | g i | ₿¥ | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|-----------------------|---|-------------------------------|--|--|-------------|-------------|--|------------------------------|----------------------------|----------------------------|---------------|-------------|
| 18 | 18 <sup>2</sup> -1850 | <sup>1</sup> S - <sup>3</sup> P* | | | | | | | | | | | |
| 10. | 10 1000 | | [1.2537] | 0 | [79762600] | 1 | 3 | 5.2(+4) | 0.0037 | 1.5(-5) | -2.43 | Е | interp. |
| 19. | | <sup>1</sup> S – <sup>1</sup> P° | [1.2534] | 0 | [79782000] | 1 | 3 | 3.35(+5) | 0.0237 | 9.78(-5) | - 1.625 | в | 3 |
| 20. | 1s2s-1s2p | <sup>3</sup> S - <sup>3</sup> P° | 274.4 | [62367900] | [62732300] | 3 | 9 | 12.0 | 0.0406 | 0.110 | -0.914 | в | 4 |
| | | | [228.0]
[361.9]
[388.7] | [62367900]
[62367900]
[62367900] | [62806500]
[62644200]
[62625200] | 3
3
3 | 5
3
1 | 21.7
4.82
4.35 | 0.0282
0.00946
0.00328 | 0.0635
0.0338
0.0126 | -1.073
-1.547
-2.006 | B
B
B | 4
4
4 |
| 21. | | <sup>3</sup> S - <sup>1</sup> P* | | | | | | | | | | | |
| | | | [168.5] | [62367900] | [62961500] | 3 | 3 | 5.95 | 0.00253 | 0.00421 | -2.119 | в | 4 |
| 22. | | <sup>1</sup> S - <sup>1</sup> P° | [315.5] | [62644500] | [62961500] | 1 | 3 | 7.53 | 0.0337 | 0.0350 | -1.472 | B | 4 |
| 23. | 1s2s-1s3p | <sup>2</sup> S - <sup>3</sup> P° | | | | | | | | | | | |
| | | | [8.6080] | [62367900] | [73985000] | 3 | 3 | 1.07(+5) | 0.119 | 0.0101 | -0.447 | В | 3 |
| 24. | | <sup>i</sup> S – <sup>i</sup> P° | [8.7475] | [62644500] | [74076300] | 1 | 3 | 1.03(+5) | 0.353 | 0.0102 | -0.452 | В | 3 |
| 25. | 1s2s-1s4p | <sup>2</sup> S - <sup>3</sup> P* | | | | | | | | | | | |
| | | | [6.4225] | [62367900] | [77938200] | 3 | 3 | 5.2(+4) | 0.032 | 0.0020 | -1.02 | В | 3 |
| 26. | | <sup>1</sup> S - <sup>1</sup> P° | [6.5224] | [62644500] | [77976200] | 1 | 3 | 4.4(+4) | 0.085 | 0.0018 | -1.07 | B | 3 |
| 27. | 1s2s-1s5p | <sup>3</sup> S - <sup>3</sup> P <sup>•</sup> | | | | | | | | | | | |
| | | | [5.7489] | [62367900] | [79762600] | 3 | 3 | 2.4(+4) | 0.012 | 6.8(-4) | 1.44 | В | 3 |
| 28. | | <sup>1</sup> S – <sup>1</sup> P° | [5.8352] | [62644500] | [79782000] | 1 | 3 | 2.3(+4) | 0.035 | 6.7(-4) | -1.46 | B | 3 |
| 29. | 1s 2p-1s 3s | <sup>3</sup> P° - <sup>3</sup> S | | | | | | | | | | | |
| | | | [8.8772] | [62644200] | [73909000] | 3 | 3 | 1.1(+4) | 0.013 | 0.0011 | -1.41 | B | 3 |
| 30. | | <sup>1</sup> P° – <sup>1</sup> S | [9.0740] | [62961500] | [73982000] | 3 | 1 | 3.4(+4) | 0.014 | 0.0013 | -1.38 | B | 3 |
| 31. | 1s2p-1s3d | <sup>3</sup> P° - <sup>3</sup> D | | | | 9 | 15 | | 0.69 | | 0.79 | C+ | interp. |
| 32. | | ${}^{1}\mathbf{P}^{\circ} - {}^{1}\mathbf{D}$ | | | | 3 | 5 | | 0.70 | | 0.32 | C+ | interp. |
| 33. | 1s2p-1s4s | <sup>3</sup> P° – <sup>3</sup> S | | | | | | | | | | | |
| | | | [6.5520] | [62644200] | [77906600] | 3 | 3 | 4700 | 0.0030 | 1.9(-4) | -2.05 | C | 3 |
| 34. | | <sup>1</sup> P° – <sup>1</sup> S | [6.6779] | [62961500] | [77936200] | 3 | 1 | 1.3(+4) | 0.0030 | 2.0(-4) | -2.05 | C | 3 |
| 35. | 1s2p-1s4d | <sup>3</sup> P° - <sup>3</sup> D | | | | 9 | 15 | | 0.12 | | 0.03 | C | 2 |
| 36. | | <sup>1</sup> P ° – <sup>1</sup> D | | | | 3 | 5 | | 0.12 | | -0.44 | C | 5 |
| 37. | 1s2p-1s5s | <sup>3</sup> P° - <sup>3</sup> S | | | | | | | | | | | |
| | | | [5.8471] | [62644200] | [79746600] | 3 | 3 | 2300 | 0.0012 | 6.9(-5) | -2.44 | C | 3 |
| 38. | | <sup>1</sup> P° – <sup>1</sup> S | [5.9524] | [62961500] | [79761400] | 3 | 1 | 6800 | 0.0012 | 7.1(-5) | -2.44 | С | 3 |

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Ni XXVII: Allowed transitions - Continued

| No. | Transition
Array | Multiplet | λ
(Å) | <i>E</i> <sub>i</sub>
(cm <sup>-1</sup>) | E_k (cm <sup>-1</sup>) | g i | g. | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | f ik | S
(at. u.) | log <i>gf</i> | Accu-
racy | Source |
|----------|---------------------|--|----------|--|---------------------------|------------|----|--|--------|---------------|---------------|---------------|---------|
| | | | | | | | | | | | | | |
| 39. | 1s 3s - 1s 3p | <sup>3</sup> S – <sup>3</sup> P° | | | | | | | | | | | |
| | | | | | | 3 | 3 | | 0.015 | | -1.35 | с | 3 |
| 40. | | <sup>1</sup> S – <sup>1</sup> P° | | | | 1 | 3 | | 0.057 | | - 1.24 | с | 3 |
| 41. | 1s 3s - 1s 4p | <sup>3</sup> S - <sup>3</sup> P° | | | | | | | | | | | |
| | | | [24.819] | [73909000] | [77938200] | 3 | 3 | 1.42(+4) | 0.131 | 0.0321 | -0.406 | В | 3 |
| 42. | | <sup>t</sup> S – <sup>i</sup> P° | [25.036] | [73982000] | [77976200] | 1 | 3 | 1.37(+4) | 0.387 | 0.0319 | -0.412 | В | 3 |
| 43. | 1s 3s - 1s 5p | <sup>3</sup> S - <sup>3</sup> P° | | | | | | | | | | | |
| | | | [17.084] | [73909000] | [79762600] | 3 | 3 | 7500 | 0.033 | 0.0056 | - 1.00 | в | 3 |
| 44. | | <sup>1</sup> S - <sup>1</sup> P° | [17.241] | [73982000] | [79782000] | 1 | 3 | 7400 | 0.099 | 0.0056 | -1.00 | в | 3 |
| 45. | 1s 3p-1s 3d | <sup>3</sup> P° - <sup>3</sup> D | | | | 9 | 15 | | 0.010 | | - 1.05 | D | interp. |
| 46. | 1s 3p - 1s 4s | <sup>3</sup> P° - <sup>3</sup> S | | | | | | | | | | | |
| | | | [25.500] | [73985000] | [77906600] | 3 | 3 | 3200 | 0.031 | 0.0078 | -1.03 | в | 3 |
| 47. | | <sup>1</sup> P° – <sup>1</sup> S | [25.907] | [74076300] | [77936200] | 3 | 1 | 9800 | 0.033 | 0.0084 | -1.00 | в | 3 |
| 48. | 1s3p-1s4d | <sup>3</sup> P° - <sup>3</sup> D | | | | 9 | 15 | | 0.60 | | 0.73 | c | 5 |
| 49. | | 'P° - 'D | | | | 3 | 5 | | 0.62 | | 0.27 | c | 5 |
| 50. | 1s3p-1s5s | <sup>3</sup> P° - <sup>3</sup> S | | | | | | | | | | | |
| | | | [17.356] | [73985000] | [79746600] | 3 | 3 | 1600 | 0.0070 | 0.0012 | -1.68 | c | 3 |
| 51. | | <sup>1</sup> P° – <sup>1</sup> S | [17.590] | [74076300] | [79761400] | 3 | 1 | 4700 | 0.0073 | 0.0013 | -1.66 | с | 3 |
| 52. | 1s 3d - 1s 3p | <sup>1</sup> D - <sup>1</sup> P° | | | | 5 | 3 | | 0.0019 | | -2.02 | Е | 5 |
| 53. | 1s 3d - 1s 4p | <sup>3</sup> D - <sup>3</sup> P° | | | | 15 | 9 | | 0.012 | | -0.74 | с | 5 |
| 54. | | <sup>1</sup> D - <sup>1</sup> P° | | | | 5 | 3 | | 0.011 | | - 1.26 | с | 5 |
| 55. | 1s 4s-1s4 p | <sup>3</sup> S - <sup>3</sup> P° | | | | | | | | | | | |
| | | | | | | 3 | 3 | | 0.026 | | - 1.11 | Е | 3 |
| 56. | | <sup>1</sup> S - <sup>1</sup> P° | | | | 1 | 3 | | 0.062 | | -1.21 | D | 3 |
| 57. | 1 s4s-1 s5p | <sup>3</sup> S - <sup>3</sup> P <sup>•</sup> | | | | | | | | | | | |
| | | | [53.879] | [77906600] | [79762600] | 3 | 3 | 3380 | 0.147 | 0.0782 | -0.356 | в | 3 |
| 58. | | <sup>1</sup> S – <sup>1</sup> P° | [54.177] | [77936200] | [79782000] | 1 | 3 | 3260 | 0.431 | 0.0769 | -0.366 | в | 3 |
| 59. | 1s4p-1s4d | <sup>3</sup> P° – <sup>3</sup> D | | | | 9 | 15 | | 0.018 | | -0.79 | D | 5 |
| 60. | 1s4p-1s5s | <sup>3</sup> P° - <sup>3</sup> S | | | | | | | | | | | |
| | | | [55.298] | [77938200] | [79746600] | 3 | 3 | 1100 | 0.051 | 0.028 | -0.82 | B | 3 |
| 61 | | 'P' - 'S | [56.016] | [77976200] | [79761400] | 3 | 1 | 3400 | 0.053 | 0.029 | -0.02 | Р | 2 |
| . | | | [20:010] | [| [,,,,,,,,,,,] | | • | 2100 | 0.055 | 0.029 | -0.00 | Б | 5 |

| Ni xxvii: Allowed tr | ansitions — Continued |
|----------------------|-----------------------|
|----------------------|-----------------------|

| No. | Transition
Array | Multiplet | λ
(Å) | E_i (cm <sup>-1</sup>) | <i>E</i> <sup>k</sup> (cm <sup>-1</sup>) | gi | gı | A_{ki}
(10 <sup>8</sup> s <sup>-1</sup>) | fik | S
(at. u.) | log gf | Accu-
racy | Source |
|-----|---------------------|---|----------|---------------------------|---|----|----|--|---------|---------------|--------|---------------|--------|
| | | | | | | | | | | | | | |
| 62. | 1s4d-1s4p | ${}^{1}\mathbf{D} - {}^{1}\mathbf{P}^{\circ}$ | | | | 5 | 3 | | 0.0029 | | -1.84 | Е | 5 |
| 63. | 1s4d-1s4f | ${}^{3}D - {}^{3}F^{\circ}$ | | | | 15 | 21 | | 7.3(4) | | - 1.96 | Е | 5 |
| 64. | 1s4d-1s5f | <sup>3</sup> D - <sup>3</sup> F° | | | | 15 | 21 | | 0.89 | | 1.13 | в | 7 |
| 65. | | <sup>1</sup> D - <sup>1</sup> F° | | | | 5 | 7 | | 0.89 | | 0.65 | в | 7 |
| 66. | 1s4f-1s4d | <sup>1</sup> F° - <sup>1</sup> D | | | | 7 | 5 | | 3.9(-4) | | -2.56 | Е | 5 |
| 67. | 1s4f-1s5d | <sup>3</sup> F° - <sup>3</sup> D | | | | 21 | 15 | | 0.0089 | | -0.73 | с | 7 |
| 68. | · | <sup>1</sup> F ° – <sup>1</sup> D | | | | 7 | 5 | | 0.0089 | | -1.21 | с | 7 |
| 69. | 1858-1850 | <sup>3</sup> S – <sup>3</sup> P° | | | | | | | | | | | |
| | 1000 100 | | | | | 1 | 3 | | 0.026 | | _111 | F | 3 |
| | | | | | | ľ | | | 0.020 | | | | |
| 70. | | <sup>1</sup> S - <sup>1</sup> P ° | | | | 1 | 3 | | 0.10 | | -1.00 | E | 3 |

"The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

Ni xxvII

Forbidden Transitions

The results of multi-configuration Dirac-Fock calculations by Hata and Grant<sup>1</sup> have been selected for this tabulation. Their work includes both a very detailed consideration of configuration interaction—with configurational wavefunction sets containing as many as 51 interacting states—as well as a fully relativistic treatment based on the Dirac Hamiltonian. Their calculated wavelengths are in very close agreement with experimental values. For the ions Ti XXI, V XXII and Fe XXV, where accurate experimental lifetime data are available, the agreement between these and the theoretical results of Hata and $Grant^1$ is excellent, with differences not exceeding a few percent (see the comparison table in the introduction to the forbidden lines of Ti XXI).

Reference

<sup>1</sup>J. Hata and I. P. Grant, Mon. Not. R. Astr. Soc. 211, 549 (1984).

| No. | Transition
Array | Multiplet | λ
(Å) | <i>E</i> i
(cm⁻¹) | $\frac{E_k}{(\mathrm{cm}^{-1})}$ | 81 | 8 k | Type of
transition | A <sub>ki</sub>
(s <sup>-1</sup>) | S
(at. u.) | Асси-
гасу | Source |
|----------|----------------------|---|----------|----------------------|----------------------------------|----|------------|-----------------------|---------------------------------------|---------------|---------------|--------|
| 1.
2. | 1s²-1s2s
1s²-1s2p | <sup>1</sup> S - <sup>3</sup> S
<sup>1</sup> S - <sup>3</sup> P° | [1.6036] | 0 | [62358960] | 1 | 3 | M 1 | 4.52(+8)* | 2.07(-4) | в | 1 |
| | | | [1.5923] | 0 | [62801270] | 1 | 5 | M2 | 1.22(+10) | 0.0942 | в | 1 |

Ni xxvII: Forbidden transitions

Ni xxviii

H Isoelectronic Sequence

Ground State: 1s <sup>2</sup>S<sub>1/2</sub>

Ionization Energy: $10775.48 \text{ eV} = 86909400 \text{ cm}^{-1}$

Allowed Transitions

Electric dipole transition probability data for this hydrogen-like ion can be obtained directly, in a non-relativistic approximation, from the data for neutral hydrogen.<sup>1</sup> The oscillator strength is independent of Z along the entire isoelectronic sequence and is therefore identical to the value for the hydrogen atom. Line strengths scale as Z^{-2} and transition probabilities scale as Z^4 , i.e.,

$$S_Z = Z^{-2} S_{\mathrm{H}}, \qquad A_Z = Z^4 A_{\mathrm{H}}.$$

For higher nuclear charges in this sequence, relativistic corrections will cause these values to deviate increasingly from the non-relativistic ones. The first effect of relativity will be to alter the transition energies, or wavelengths, from the non-relativistic, even though the line strength itself is still well approximated by the non-relativistic value. In this case, experimental energies should be used in the standard conversion formulas, given in the general introduction to this volume, to calculate the most accurate values of f and A. It should be noted that the relativistic removal of the *j*-degeneracy introduces dipole transitions which do not occur in the non-relativistic theory, e.g., $2s_{1/2} - 2p_{3/2}$. For very high Z, it is necessary to use the four-component Dirac spinors rather than two-component Schroedinger functions in theoretical calculations, and this introduces relativistic corrections to the line strengths themselves. Several recent systematic studies of the problem<sup>2,3</sup> indicate that these corrections are not large for stages of ionization in the range 20-30. Corrections for Z = 30 are usually no larger than 5-10% and generally substantially less than 5%. If an accuracy greater than this is required, the reader is referred to these papers<sup>2,3</sup> for a more detailed error analysis.

- <sup>1</sup>W. L. Wiese, M. W. Smith, and B. M. Glennon, Atomic Transition Probabilities – Hydrogen through Neon (A Critical Data Compilation), Vol. I, 157 pp., Nat. Stand. Ref. Data Ser., Nat. Bur. Stand. (U.S.), 4 (May 1966).
- <sup>2</sup>S. M. Younger and A. W. Weiss, J. Res. Nat. Bur. Stand., Sect. A 79, 629 (1975).
- <sup>3</sup>S. J. Rose, Rutherford Appleton Laboratory Report RL-82-114 (December 1982).

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